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Performance of a wet Flue Gas Desulphurisation Pilot Plant under Oxy-fuel Conditions

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Publication date: 2011

Document Version Publisher's PDF, also known as Version of record

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Citation (APA): Hansen, B. B., & Kiil, S. (2011). Performance of a wet Flue Gas Desulphurisation Pilot Plant under Oxy-fuel Conditions [Sound/Visual production (digital)]. IEAGHG workshop, Oxy-fuel combustion : SO2/SO3/Hg/Corrosion Issues in Oxyfuel Combustion Boiler and Flue Gas Processing Units, London, 01/01/2011

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Performance of a wet Flue Gas Desulphurisation Pilot Plant under Oxy-fuel Conditions

IEAGHG workshop, Oxy-fuel combustion, January 25/26, 2011

 $f(x+\Delta x) = \sum_{i=1}^{\infty} \frac{(\Delta x)^{i}}{i!} f^{(i)}$

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<u>Outline</u>

- Introduction
 - Technical University of Denmark
 - Objective
 - Wet FGD and Oxy-fuel combustion
- Experimental investigation
 - Pilot plant outline and methodology
 - Results

Absorber pH Desulphurisation degree Content of residual limestone

Conclusions and future work



Technical University of Denmark (DTU)

- Founded in 1829
 - Hans Christian Ørsted (Danish Physicist)
- Engineering education and research
- About DTU
 - 19 departements (Lyngby)
 - 4500 employes (1050 Ph.D. Students)
 - 6500 bachelor and master students





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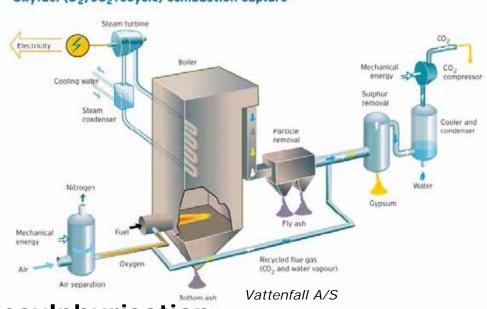


Project objective

Objective

- To investigate the effect of oxy-fuel combustion on wet FGD operation Parameters studied:
 - CO₂ atmosphere
 - Higher flue gas temperature (H_2O content)
 - Higher SO₂ concentration
 - Reduced flue gas flow rate

Oxy-fuel and wet FGD



Oxyfuel (O2/CO2 recycle) combustion capture

Flue gas desulphurisation

- Ensuring a clean CO₂ stream or recycle stream
- Wet FGD widespread, traditional and highly efficient

 $CaCO_{3}(s) + SO_{2}(g) + 2H_{2}O + \frac{1}{2}O_{2} \rightarrow CaSO_{4} \cdot 2H_{2}O(s) + CO_{2}$

Potential process conditions dependent on recycle location



Potential wet FGD process changes

- CO₂ atmosphere
 - CO_2 absorption (absorber) and a decreased limestone dissolution rate $CaCO_3 + 2 H^+ \leftrightarrows Ca^{2+} + CO_2 + H_2O$

Higher saturation temperature

- Wet recycle yields higher gas phase water content
- Decreased SO₂ solubility

• SO₂ concentration/flue gas flow rate

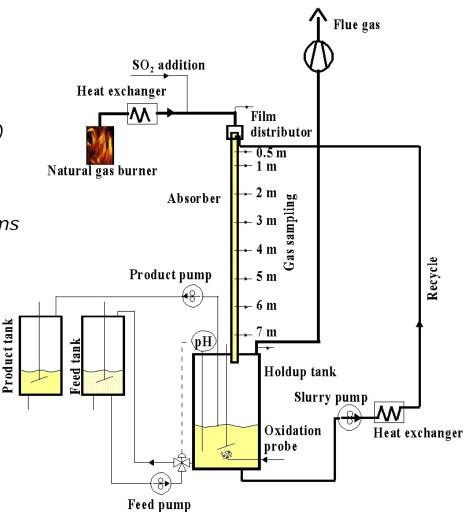
- Recycle location or changing modes of operation (air-firing/oxy-fuel)
- Prolonged gas phase residence time
- Increased importance of liquid phase transport resistance

External oxidation

Pilot plant outline

Overview

- Packed tower absorber
 - Downscaled (single vertical channel)
 - Co-current flow
 - Multiple sampling sites
 - Well controlled gas and liquid streams





Experimental overview

Air-firing - pH 5.4

• Base-case

Oxy-fuel - pH 5.4

- Oxy-fuel (~ 90 % CO₂)
- Oxy-fuel and 10 mM adipic acid

Oxy-fuel - pH 5.0

- Oxy-fuel
- Oxy-fuel and low gas flow rate
- Oxy-fuel, low flow and T (~ 53 °C)





Experimental methodology

Experimental procedure

- Steady state
 - 5 days desulphurisation
 - 1000 ppm SO_2 flue gas (natural gas burner)
- Oxy-fuel experiments
 - 1000 ppm SO_2 flue gas (gas cylinders)
 - Until a steady limestone consumption rate

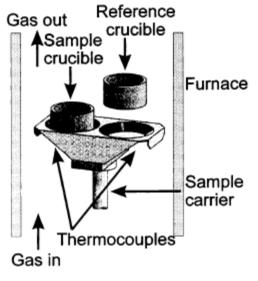




Sampling procedure

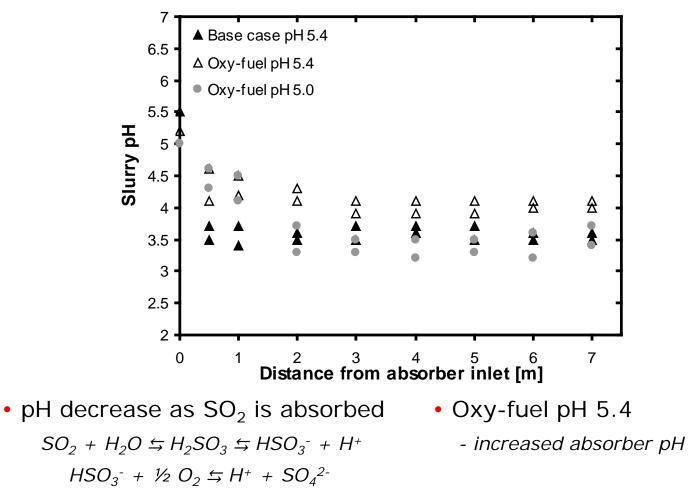
Sampling

- Gas phase composition
 - Absorber profile
 - Overall degree of desulphurisation
- Absorber pH
 - Multiple sampling points
- Residual limestone
 - Thermal analysis in STA

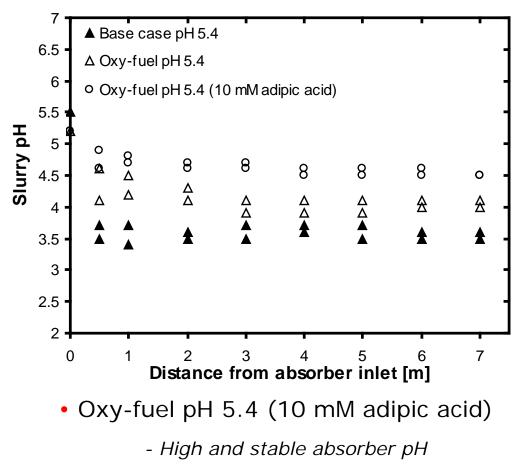


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Absorber pH

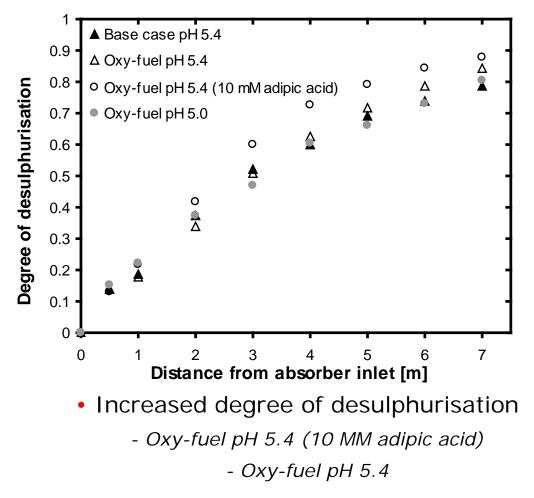


Absorber pH

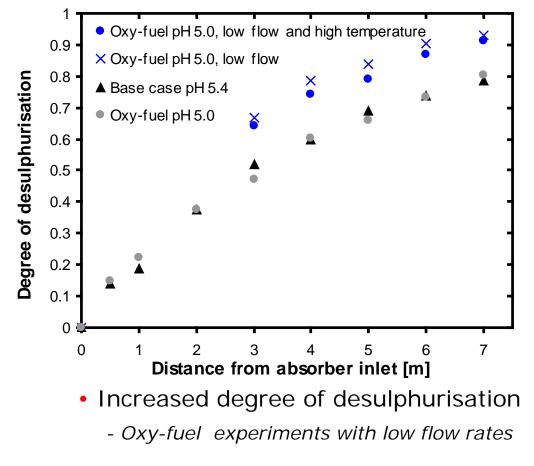




Absorber desulphurisation



Absorber desulphurisation



• Base-case 5.4 and Oxy-fuel pH 5.0 very similar



Total degree of desulphurisation

Experiment	C _{so2} [ppm]	С _{со2} [%]	рН	Т [°С]	η (±1) [%]
Air-firing	1070	7	5.4	46	91
CO ₂ atmosphere (pH 5.4)	1040	90	5.4	44	94
- pH 5.4 (10 mM adipic acid)	1030	90	5.4	44	97
- pH 5.0	1030	91	5.0	43	92
- Reduced flow rate	4940	90	5.0	44	99
- Elevated Temperature	4950	85	5.0	53	99

• CO₂ atmosphere

- Increased desulphurisation degree
- Lower pH counters the effect
- High degree of desulphurisation with 10 mM adipic acid or low Q_{flue}

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Residual limestone

Experiment	C _{so2} [ppm]	C _{CO2} [%]	pН	CaCO₃(±0.6) [g/l]	η (±1) [%]
Air-firing	1070	7	5.4	3.2	91
CO ₂ atmosphere (pH 5.4)	1040	90	5.4	5.0	94
- pH 5.4 (10 mM adipic acid)	1030	90	5.4	5.2	97
- pH 5.0	1030	91	5.0	2.3	92
- Reduced flow rate	4940	90	5.0	1.9	99
- Elevated Temperature	4950	85	5.0	1.7	99

- CO₂ atmosphere
 - Increased residual limestone content
 - Also with 10 mM adipic acid
 - Lower pH counters this effect

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Discussion

Dissolution of limestone

 $CaCO_3 (s) \leftrightarrows Ca^{2+} + CO_3^{2-} \tag{1}$

$$H^+ + CO_3^{2-} \leftrightarrows HCO_3^{-} \tag{2}$$

- $HCO_{3^{-}} + H^{+} \leftrightarrows CO_{2} + H_{2}O \tag{3}$
- $CO_2(aq) \leftrightarrows CO_2(g)$ (4)
- Critical pH changes with CO₂
- Above critical pH (5.2-5.5)
 - Increased HCO₃⁻ concentration
 - Increased CO_3^{2-} at the particle surface
 - Lower Ca²⁺ concentration at the particle surface
 - Drastic reduction in limestone dissolution rate (ΔCa^{2+})
- Verified experimentally by Allers et al. 2003 and Chan et al. 1982

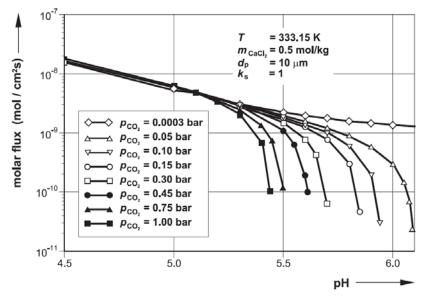


Figure 1. Dissolution rate of limestone particles with a diameter of 10 μ m. Allers et. Al 2003

Conclusions

Desulphurisation of an oxy-fuel flue gas stream

- A higher absorber pH
- An increased content of residual limestone
- An increased degree of desulphurisation
- A minor correction of pH (5.0 vs. 5.4) compensate for the changes
- High degrees of desulphurisation obtained for low flow rates
 - No temperature effect could be distinguished

Publication

- Manuscript "Performance of a wet flue gas desulphurisation pilot plant under oxy-fuel conditions" accepted by Industrial and Engineering Chemistry Research
- Expected publication in spring 2011

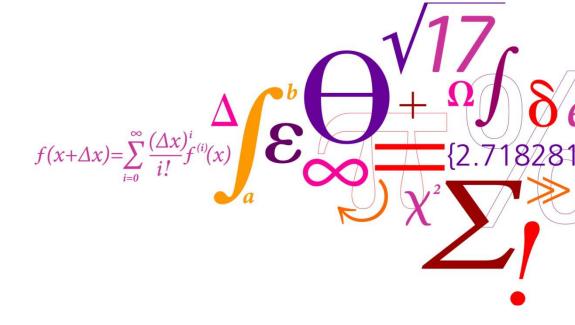


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