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# Geochemical criteria for reservoir quality variations in chalk from the North Sea

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# Geochemical Criteria for Reservoir Quality Variations in Chalk from The North Sea

# H. Kunzendorf and P. Sørensen

Factor 1 versus factor 3

Components: Al.Na.Mn.V Sr.Eu.Dy.U POR.FCNU.LS.RHGX.DT.IT.SFLU.ILD.SP.GR.RH0B



Risø National Laboratory, DK-4000 Roskilde, Denmark December 1989

# Geochemical Criteria for Reservoir Qaulity Variations in Chalk from The North Sea

H. Kunzendorf and P. Sørensen

**Chemistry Department** 

Risø National Laboratory, DK-4000 Roskilde, Denmark December 1989 **Abstract.** The research project (EFP-86) systematically investigates the influence of chalk geochemistry on petrophysical parameters determining hydrocarbon reservoir quality, i.e. porosity and permeability.

Two wells of the North Sea Tyra gas field were chosen for the present investigation: the central well TWB-8 and eastern marginal well E-lx. Geophysical logging data with interpretations exist for both wells.

Drill core sections of Upper Maastrichtian and Danian chalk were selected for the geochemical investigations. Chemical data on chalk samples were gathered by using both conventional (X-ray fluorescence) and special instrumental analytical techniques (instrumental neutron activation). The geochemical data are compared with the well-logging results.

Geophysical logging suggests that there is reduced porosity in the Danian reservoir units LDP and UDT in both the central and marginal wells.

The chalk drill core samples from the section with reduced porosity also show a lower Ca content. At the same time, a high Si content is observed in these samples and a number of trace elements in chalk show a similar distribution with depth. Silicon diagenesis is therefore regarded as being responsible for reservoir quality variations in Tyra rocks.

A linear dependence is observed between chalk porosity and silicon content of chalk, i.e. reservoir porosity may be estimated from the Si content of chalk. Chalk permeability may also be determined by Si content but the linear dependency is less significant.

Geochemically, depth distributions of elements Al, Fe and Sc show the same trends as that for Si. Therefore, diagenetic changes in chalk also include clay minerals.

Other features of the Tyra gas reservoir are displayed through the chemical data.

The gas zone in TWB-8 is characterized by low contents of Na and Cl, i.e. lower water saturation is indicated.

Low concentrations of rare earths in all chalk samples show a shale-normalized pattern that is characteristic of marine sediments laid down under oxic conditions. Some changes that occur with depth in the Ce anomaly probably indicates a slight change in the depositional environment.

A most pronounced feature of the Tyra chalk is the depth distribution of manganese: the content continuously decreases with depth, i.e. from Danian (about 2000 ppm) to Maastrichtian strata (less than 200 ppm). In this respect, no other chemical element in chalk correlates with Mn. At present, there is no indication as to which mineral or mineral phase one is likely to find the element.

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# Geokemiske kriterier for reservoirkvaliteters variation i Nordsøkalk

# **Dansk Resumé**

Til den foreliggende undersøgelse udvalgtes to af Tyra strukturens borehuller, den centrale boring TWB-8 og den marginale boring E-lx. For begge borehuller eksisterer borehuls-logging data med delvis interpretation. Til geokemiske studier blev der udtaget prøver fra kalk borekernesektioner, som stratigrafisk dækker kalkaflejringer fra det øverste Maastrichtien og det nederste Danien; disse geologiske enheder udgør kulbrintereservoiret i Tyrastrukturen. Mens TWB-8 skærer gennem Tyra gasreservoiret (heie Danien og de øverste Maastrichtien aflejringer), er der kun i de allerøverste Danienafle'ringer pa E-lx konstateret kulbrinter (olie).

EFP-86 projektet sammenligner både de geofysiske (logging) og de geokemiske (kemiske analyser) data.

De geofysiske data fra boring TWB-8 indikerer lavere porøsitet og permeabilitet i den midterste del af Danien (DGU reservoirenheder LDP og UDT), d.v.s. reduceret reservoirkvalitet. En lignende reduktion af begge petrofysiske parametre er ogsa konstateret i den marginale boring E-lx, omend permeabilitetsværdier her er generelt lavere.

Fordelingen af hovedelementet Ca med dybden i borekerneprøver fra begge boringer viser som forventet lavere indhold i de sektioner, som også har lavere porøsitet.

Kalk med reduceret porøsitet er for begge boringers vedkommende karakteriseret ved høje Si indhold (op til 20% Si); en række sporelementer følger Si, d.v.s. viser også forhøjede værdier. Silicium diagenese i form af silificering af kalkskaller, men også i form af flintdannelse fører generelt til en forringelse af porevolumenet.

Ved at benytte middelværdier for Si and porøsitet i de enkelte reservoirenheder er det muligt at beregne en linear afhængighed for begge parametre. Dermed er det muligt indenfor Tyrastrukturen også at estimere porøsiteten udfra Si indholdet i kalken. Selvom der er en lignende trend for Si og kalkpermeabilitet (aftagende permeabilitet ved stigende Si), er det statistisk ikke muligt at angive en linear afhængighed.

Elementer der følger Si fordelingen med dybden inkluderer Al, Fe and sporelementet Sc. Dermed indikeres, at Si diagenesen også involverer/har involveret lermineraler (smektit); disse elementer kan derfor også benyttes ved reservoirkvalitets estimeringer i Nordsøkalk.

Andre sporstoffer i Tyrakalken er indikative for tilstedeværelse af hydrokarboner: gaszonen er indikeret via lave inhold af elementerne Na og Cl. De er samtidig et udtryk for vandmætningen i formationen.

Sjældne jordartselementer forekommer i meget lave koncentrationer og de viser den fordeling, der er kendetegnende for oxiske aflejringsmiljøer på havbunden, nemlig en udpræget negativ Ce anomali, d.v.s. meget lavere Ce indhold end normale mergelforekomster. Variationer af Ce anomalien med dybden afspejler muligvis aflejringsbetingelserne i Kridt/Tertiærtiden. Det sport of, det theet den mest isjnefåldende fordeling med dybden i de to boringer er thangatt. Judho det af Mn i kalken korrelerer ikke med nogen af de andre grundstoffel og heller ikke med de petrofysiske parametre; Mn i kalk falder stott med dybdent omend der forekommer sektioner (aflejringsperioder) med römdre feld, samt enkelte zoner med signifikant stigning i Mn indholdet. Den korakteristiske fordelingsform med dybden i kalken er også blevet konstateret i talrige boringer fra det Danske Subbassin. Via Mn indholdet er det derfor refactivt fet än afgøre, om en kalkprøve stammer fra Kridt (Mn 500 ppm), og inddeling kan endvidere også foretages i reservoirenheder med hver sit karakteristiske Mn indhold. Fordelingen er også karakteristisk for hele det Danske Subbassin. På nuværende tidspunkt er det ikke muligt at give en fyldestgørende forklæring på den med dybden stigende Mn fordeling.

Fordi det både et hevedelementer og sporstoffer, der peger på forskelle i kalk, skønnes det, at multielement geokemiske kort (i 3-D) vil kunne påvise regionale trends med heusyn til uservoirkvalitet. Det er ikke muligt at fremstille disse kort udfra kvat to beginger i strukturen.

Projektet er udført under Unergiministeriets energiforskningsprogram, EFP-86 (EM-Journal nr. 1315/86-5).

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# **1. Introduction**

Oil and gas are natural energy resources connected with the geological environment, confined almost exclusively to sedimentary sequences. The hydrocarbon accumulations obey the same rules of deposition (emplacement of the mineral phase into a geological body) and, e.g., geological alterations as for instance hard mineral deposits. Most of the methods used for identifying hydrocarbon deposits are therefore also related to those applied in normal terrestrial mineral exploration programmes.

Oil and gas frequently accumulating in deep-seated sedimentary sequences are often controlled by tectonic features. The rocks acting as hydrocarbon reservoirs are mainly sandstones and carbonate rocks with appropriate porosity. In the literature, there are relatively few discussions on the inorganic chemistry of carbonate reservoir rocks which influences porosity figures to a considerable extent. Relatively little knowledge also exists on inorganic chemical processes that connect directly with the migration and emplacement of the hydrocarbons in general. This is partly due to the complex processes occurring in sediments both during and after their burial and when reacting with a hydrocarbon phase.

Fig. 1. Tyra gas field top chalk structure map showing gas-oil contact (broken lines) and positions of wells TWB-8 and E-1x (Depth lines in feet).



Just as formation temperatures are important for generating oil and gas from suitable source rocks, there is evidence that both petrophysical (e.g., porosity, permeability) and petrochemical properties (chemical composition, diagenetic features) play a comparable role for the reservoir rocks. Such parameters must then be regarded as important for the quality of hydrocarbon reservoirs, and they are therefore important figures for any exploitation step that is taken.

There are close relationships and interactions between the chemical deposit, i.e. oil and gas, and the surrounding sedimentary sequences during and after emplacement stages. When discussing the geochemistry of the hydrocarbon accumulations, geochemical studies have therefore to include both organic and inorganic components, i.e. hydrocarbon accumulations cannot be discussed on organic geochemical principles alone.

## L1 Basic Knowledge on Carbonate Rock Geochemistry

Major hydrocarbon occurrences in the North Sea Central Graben area are contained in carbonate rocks (chalk). Geochemical discussions on these rocks may be based on previously accumulated knowledge, e.g., *Chilingar* et al., 1967; *Reeder*, 1979; *Bathurst*, 1980; *Leeder*, 1982; *Harris* et al., 1985. A general reference list concerning the present investigation is given at the end of this report. This list also contains a number of publications relevant for the present investigation, which however were not referred to in detail.

According to Chilingar et al. (1967), carbonate rocks which make up about 15% of the continental crust are polygenetic, i.e. they are composed of both chemical, biochemical, and clastic components. They usually occur in the form of rhythmically repeated sequences reflecting, e.g., climatic or tectonic events during geological times. After deposition, diagenetic changes occur which alter the porosity and permeability of the deposits; they involve organic activitity, chemical processes and the imprint of physical processes.

Because of the generally existing difficulties in defining a proper carbonate rock porosity, *Harbaugh* (1967) differentiates between primary and secondary porosity. Primary porosity is defined as that which arises during depositional stages and which is later reduced by compaction and cementation. Secondary porosity is developed during burial.

Leeder (1982) gives a clear chemical description of the carbonate cycle which because of its fundamental importance is repeated here briefly:

Primary inorganic carbonate precipitation takes place through reactions

$$H_2O + CO_2$$

$$\downarrow$$

$$CaCO_3 + H_2CO_3 \iff Ca^{2+} + 2HCO_3^{-}$$

This means that precipitation of CaCO<sub>3</sub> is favoured by the reactions that decrease the amount of CO<sub>2</sub> or lower the partial pressure  $pCO_2$  of the solution. This case occurs either when temperatures are increased or if organic photosynthesis takes place.

The normal buffering components of seawater are  $HCO_3$  and  $H_2CO_3$ . In the case of increase of acidity of seawater, the following reactions are possible:

and

and

$$H^{+} + CO_3^{+-} \rightarrow HCO_1^{+} + H^{-} \rightarrow H_2CO_3^{-}$$

$$CaCO_{3} + H^{+} \leftrightarrow Ca^{2} + HCO_{3}^{-}$$

In the case where alkalinity increases, the following reactions are encountered:

$$HCO_{3}^{-} + OH^{-} \leftrightarrow CO_{3}^{2-} + H_{2}O$$
  
 $Ca^{2+} + HCO_{3}^{-} + OH^{-} \leftrightarrow CaCO_{3} + H_{2}O$ 

These reaction chains explain the excellent buffering system existing for seawater.

In general, Mg<sup>2+</sup> ions present in seawater will supress and often inhibit the growth of the main carbonate mineral calcite.

Leeder (1982) also considers three major diagenetic stages:

- early meteoric diagenesis,
- early marine diagenesis, and
- subsurface diagenesis by formation waters.

The principal reaction zones are shown schematically in Fig. 2.

Early meteoric diagenesis comprises the vadose and phreatic environments and is closely connected with the percolation of meteoric water. During phreatic meteoric diagenesis, the  $Sr^{2+}$  amount may be significantly reduced. The low-Sr content in the transition zone Upper Maastrichtian/Danian in the Tyra drill cores could be an expression of such processes, i.e. indicate a period of regression with subsequent fresh water influx.





<u>Early marine diagenesis</u> produces beach rocks, fenestrae (birdseye limestone), hardgrounds and geopetal cavity fills. Of interest as regards North Sea chalks is the development of hardgrounds which are frequently observed in connection with the Cretaceous/Tertiary transition. Synsedimentary hardgrounds usually indicate extensive non-deposition, and they reflect the presence of interparticle cement.

<u>Subsurface diagenetical changes</u> caused mainly by circulating formation waters are still not fully understood. Formation waters observed in deeply buried carbonate rocks are usually in equilibrium at the prevailing pressures and temperatures.

These waters, along their circulation paths, may alter aragonite that has been left below the meteoric realm into calcite, and they may change highinto low-Mg calcite. Contrary to early marine diagenesis, ferroan ions are available during subsurface diagenesis and therefore ferroan calcite replacements may develop.

After early diagenesis stages, about 20% porosity is left in the carbonate sediments. Most ancient limestones have a porosity of less than 5% and therefore, large-scale CaCO<sub>3</sub> cementation must have occurred during burial stages for these rocks. The frequent occurrence of ancient limestone with preserved high porosity (A > 20%) is probably the result of rigidity enhancement of the rock fabric by calcite precipitation at grain contacts.

Pressure solution is thought to be the dilute source for diagenesis in the deep realm. It has been observed (e.g. Leeder. 1982) that much of the late cement consists of ferroan calcite. Fe<sup>3+</sup> is obtained by the reduction and dissolution of adsorbed ions on clay mineral platelets. Because of the platelet-like form of clay minerals, circulation of pressurized solutions is enhanced yielding large-scale migration of Ca<sup>2+</sup>, Fe<sup>2+</sup>, Mg<sup>2+</sup>, and CO<sub>3</sub><sup>2-</sup>. Additional Fe<sup>2+</sup> is supplied by the conversion of smectite to illite. It is also known that such generated ferroan calcite cements may be further changed into ferroan dolomite or ankerite at depths exceeding 2.5 km.

## **1.2 North Sea Chalk**

In general terms, chalk is an organic limestone where CaCO<sub>3</sub> containing skeletons are the dominant fraction of the sediment. A practical term for the chalk of the North Sea would be micrite which points to the composition of the matrix as micro-crystalline calcite with grain sizes of less than 0.01 mm.

The dictionary of the American Geological Institute (DIC, 1962) defines chalk as: »A very soft, white to light gray, unindurated limestone composed of tests of floating microorganisms and some bottom-dwelling forms (arimonoids and pelecypods) in a matrix of finely crystalline calcite; some chalk may be almost devoid of organic remains.« The definition given by Whitten and Brooks (1976) is more strict and confines chalk to the Upper Cretaceous limestone deposits of Western Europe.

According to Frykman (1983), petrographically the chalk material from North Sea drill cores contains a very high percentage of coccolith material, generally above 60% with a very widely varying allochem component. These coccolithic tests were deposited in relatively shallow waters, perhaps a few hundred meters deep, at rates exceeding 10 cm/ka.

The non-carbonate fraction is generally 5% by weight and consists mainly of clay and silica. Silica is present in the form of flint layers and chert nodules. These stem from dissolved silica which in general is highly mobile during early diagenesis. Chertification takes place predominantly in the mixed zone, i.e. in the zone between phreatic and marine realms. Nodular cherts are generated mainly in shallow-water carbonate facies. They often have a meteoric component.

Marly layers in the chalk are generally regarded as expressing carbonate production variability, but may also be caused by variable terrigeneous deposition. Also discussed are carbonate dissolution variations by *Frykman* (1983).

Coccolithic tests consist of low-Mg calcites. They are often coated by organic or other materials which are believed to be the reason for their relatively low degree of diagenetic alteration.

During deposition, chalk has a very high primary porosity, often exceeding 70%; during burial this porosity is quickly reduced. Often no cementation is observed in chalks, although they have been buried at depths greater than 2 km. For instance, Danian chalk from the Tyra well TWB-8 has porosities in excess of 30%. The most probable reason for this is the presence of pore solutions rich in  $Mg^{2+}$  at burial stages preventing or delaying CaCO<sub>3</sub> cementation.

As regards the chalk as a hydrocarbon reservoir, *Hardman* (1982) pointed out that chalk reservoir quality is defined by the size characteristica (range and distribution) of pore throats. These parameters, however, may be changed during burial involving both chemical and physical changes in the reservoir rocks.

## 1.3. Framework of the Present Investigation

Investigations with general validity for carbonate rocks are known (e.g. Chilingur, 1956; Holland et al., 1962; Hirst 1962; Tourtelot, 1964; Berner, 1964; Weber, 1964; Wangershy and Joensuu, 1972; Jorgensen, 1975, 1986a, 1986b). Meanwhile, there has been an ongoing discussion on the geochemistry of source and reservoir rocks in general when interpreting geophysical logging data (e.g. Nyberg et al., 1978; Scott and Smith, 1973; Suau and Spurlin, 1982). These discussions have terminated in the development of a new geochemical well logging device, the GLT Geochemical Logging tool of Schlumberger which uses an array of traditional sondes and a <sup>252</sup>Cf based equipment for neutron activation analysis (Chapman et al., 1987; Herron, 1986; 1987). Elements determined by the logging tool include Si, Fe, Ca, Ti, Gd and Al. In general, such a new logging system reflects the need to characterize the logged sequences by their mineralogical and chemical components so that geophysical log interpretation errors can be minimized.

Contemperaneously to the development of the new geochemical log, inorganic geochemical studies were carried out on the Danish reservoir rocks (Jorgensen, 1975; 1981; Kunzendorf, 1986) leading to a sequence characterization by the contents of minor and trace elements.

The present investigation concerns Danian and Maastrichtian chalk from the Central Graben area of the North Sea. Following earlier investigations on small chalk samples with a modified instrumental neutron activation procedure (*Kunzendorf* et al., 1986a; 1986b), a project was initiated in 1986 combining the application of the new analytical techniques with existing knowledge on two wells from the North Sea Tyra gas field. Boreholes available for detailed investigations within the 3-year EFP-86 project included TWB-8 and E-lx.

The present project aims at a concomittant interpretation of geophysical log data and geochemical data, applied to detail the understanding of the variation in reservoir quality. Investigations based on two wells alone is the absolute minimum. In order to obtain a fair judgement of reservoir quality variations, the wells were chosen from different topographic locations within the structure. The well TWB-8 intersects the central part of the Tyra structure (Fig. 3), while E-lx is located on its eastern margin.

Investigations include the analysis of some two hundred samples from cores in  $L_s$  wer Danian and Upper Maastrichtian strata in the wells. The applied analytical methods were instrumental neutron activation and X-ray fluorescence. By inclusion of wireline logging data from the wells, a geochemical model explaining some of the variations in reservoir quality is proposed.

The work presented here closely relates to a comparable project carried out in 1987 by the University of Copenhagen, named »Bassinanalyse, geokemi og kemostratigrafi i de danske skrivckridt bassiner«. It is intended that both projects will be able to illuminate the significance of inorganic components in the Danish reservoir rocks and also establish a »chemostratigraphic« scheme. The university project will further correlate this scheme with nannofacies studies.

# 2. Geological Setting

# 2.1 Regional Overview

The gas-producing Tyra Field is situated in the Danish Central Graben (Fig. 1) where it occupies an area of about 20 km<sup>2</sup> (top chalk at 6500 feet). A SE-NW cross section of the structure at about 61.75° N and about 60.7° E is shown in Fig. 3 which also outlines the position of the two wells TWB-8 and

Fig. 3. Tyra gas field cross section showing top Danian and Maastrichtian structures and position of TWB-8 and E-1x. Figure made available by Marsk Oil and Gas A/S,



HORIZONTAL DISTANCE IN FEET FROM O POINT ALONG AZIMUTH 80

na ozi osion 12 E-lx from which drill core material was investigated. TWB-8 is positioned on a subtopographical high, where both oil and gas are present; E-lx is located on the easternmost margin of the structure where only a very thin oil zone was observed in the uppermost Danian section.

# 2.2 Tyra Gas Field Chalk Characteristics

A number of stratigraphic and reservoir quality data from the Tyra gas field are available from Marsk Oil & Gas A/S and The Geological Survey of Denmark (DGU). Although there is some debate on the stratigraphic unit nomenclature, the hydrocarbon-bearing chalk sections of the Tyra field may be divided into at least 7 stratigraphic units (Table 1).

For use in the present investigation, a general description of chalk in the Tyra structure was supplied by Marsk Oil & Gas A/S.

Table 1. Proposed stratigraphic units for the Tyra field. Throughout this report DGU reservoir units were used.

Age	Formation	DGU chalk unit	Reservoir unit (DGU)	DUC unit	
Danian	Ekkofisk	6	UDP1	D1	
			UDP2		
			LDP	D2.1	
			UDT	D2.2	
			LDT1	D2.3	
			LDT2	D2.4	
Maastrich- tian	Thor	5+	1M	M1.1	
			2M		
			эм -	M1.2	
			4M	<b>M</b> 2	
			5M		

This description is given briefly below in an abbreviated form.

The lowermost Maastrichtian reservoir unit, <u>3M</u>, which also shows the most well-developed reservoir facies, is a soft-to-moderately hard, beige chalk. Macroscopically, the rock appears as a banded and laminated unit. Not many burrows are found and oil staining is observed along some fractures. In general, the chalk shows few indications of diagenetic alteration. Reservoir quality is excellent with porosities above 40% and permeabilities at 9 mD on

average. A characteristic feature of this chalk section is that it is often intersected by cm-size floatstones representing perhaps an early diagenetic imprint.

Units  $\underline{2M}$  and  $\underline{1M}$  consist of soft to moderately hard, light-yellowish grey chalk with no visible cement. The chalk is characterized by sections with many stylolites. Burrows occur rarely, and few pyrite grains are observed. Ha'rline fractures are numerous. These vary in thicknes on a regional scale in that they are thickest towards the northeast of the Tyra field. Reservoir properties are in general somewhat decreased compared to unit 3M. This decrease is visualized through lower permeabilities (5 to 10 mD) at comparable porosities (30 to 42%).

The top of unit 1.M is a strongly cemented hardground.

The lowermost Danian chalk section, <u>LDT2</u>, usually cannot be found in the central parts of the Tyra structure but where deposited, it is a strongly cemented, beige-to dark grey chalk, characterized by horsetail lamination. Burrows and patterned-chalk structures are very abundant. Pyrite nodules (cm scale) and bands of chert nodules also occur. The rock is rich in clay, and, taking into account that many well-preserved trace fossils occur, it was probably deposited during periodes characterized by low rates of sedimentation. Many other features point to strong diagenetic alterations, and the reservoir parameters are generally poor with porosities declining to about 32% and with markedly lowered permeability values.

Further above, section <u>LDT</u> is moderately hard, partly banded and mottled, and the chalk is white to greyish-beige. The rock appears cemented and shows a number of secondary structures like stylolites, mm-size pyrite nodule clusters, horsetail-structure lamination and patterned-chalk structures. These features are often concentrically arranged and suggest that they have been exposed to strong diagentic overprinting. Most pronounced for the section as regards chemical changes is the abundance of pyrite. The unit has reduced reservoir quality figures, although porosities generally lie between 36 and 40%, but permeabilities are relatively low, ranging between only 0.9 and 3.5 mD. It should be mentioned that reservoir properties are poorest in subsections with pronounced occurrences of patterned-chalk structures.

Unit <u>UDT</u> is a moderately hard, beige chalk which often has a dense horsetail lamination. Layers of foraminiferal mudstone with relatively high content of pyrite (size ! um to 1 mm) occur. Microscopically, cement has been observed, and therefore reservoir quality parameters are reduced (porosities rarely are above 30% and permeabilities well below 1 mD). A whitish-beige chalk layer may be interbedded locally in Unit UDT. This layer has better reservoir quality parameters than unit UDT in general, and this is explained by the lower degree of cementation of this subsection.

The overlying unit <u>LDP</u> is a moderately hard, greyish beige, mottled chalk. A relatively dark patterned-chalk structure is present with some dark spots of pyrite. The rock in general has a high content of foraminifera and pyrite-containing patches. Unit UDT has porosities between 38 and 41%, and permeabilities ranging from 2.9 to 3.6 mD.

The uppermost Danian chalk section, units <u>UDP2</u> and <u>UDP1</u>, are comprised of a moderately hard beige chalk with networks of hairline fractures. The rock contains recrystallized shell fragments and very small chert grains. Reservoir properties are generally better than those of unit LDP (porosities between 43 and 45%, permeabilities between 3.2 and 3.8 mD).

# 3. Sampling and Analytical Techniques

# 3.1 Sampling

Chalk samples were collected from selected intervals of the drill core material stored at Marsk Oil and Gas A/S (TWB-8) and The Geological Survey of Denmark (E-lx). Usually, pieces weighing up to 30 g were taken. After removing the remaining drilling mud, the samples were crushed and finely ground in an agate mortar.

For a number of the TWB-8 samples, a somewhat different sample preparation procedure involving hydrocarbon extraction was employed. However, as there were no significant differences between bulk and hydrocarbon-extracted chalk samples it was soon decided to analyze the bulk rock samples alone. Two further reason for doing this was the difficulty of controlling the extraction processes, and that they always include a possibility of dissolution and/or contamination.

For the analysis, 400-mg sample material was used for both short-lived isotope and normal instrumental neutron activation. Conventional X-ray fluorescence requires at leat a few grams of sample material.

# **3.2 Analytical Procedures**

The present project also aimed at the refinement and use of a rapid instrumental neutron activation (INAA) technique based on the gamma-ray intensities of short-lived radioisotopes. However, because only some ten elements can be determined with this method, other analytical techniques were also applied to increase the geochemical data base. These include normal instrumental neutron activation analysis determining some 20 elements and conventional X-ray fluorescence analysis.

Short-lived instrumental neutron activation analysis has been carried out at 'he delayed-neutron counting facility (uranium analysis) connected with the research reactor DR3 (*Kunzendorf* et al., 1985). In this mode of operation, samples are usually irradiated for 10 s and analyzed for, e.g., Mg, Al, Ca, Ti, and V using counting intervals of 2 and 5 min after termination of appropriate cooling periods. The automatic instrumentation at the irradiation facility allows optimal manipulation of irradiation, cooling and sampling in the minutes range.

Normal INAA analysis was usually carried out on 400-mg samples. After irradiation for 4 hours in the irradiation position 7V2 of the Risø research reactor DR3 (Risø Isotope Laboratory) the samples were cooled for 7 days. Gamma-ray spectrometry was performed with the Mineral Analysis group's Ge(li) detector coupled to a multichannel analyzer (Canberra Series 80). Gamma-ray spectra of the samples were recorded after 1 week (0.5 h counting), 10 days (1 h counting), and 3 weeks (13 h counting) cooling time.

An evaluation of the gamma-ray spectra was carried out by a method based on that reported by *Girardi* et al. (1965) and moderated for use at Risø National Laboratory. While irradiation and gamma-ray spectra recording was conducted at our own laboratory, the final data evaluation was carried out through computer services by the Danish company Tracechem, Copenhagen. Analytical data were generally available within one month, but taking into account the relatively large number of elements analyzed, INAA analysis is a relatively time-consuming operation in the present project.

A number of the chalk samples were also analyzed by conventional X-ray fluorescence analysis (at the Institute of Petrology, University of Copenhagen) to determine standard major, minor, and trace elements in the chalk samples. Silicon values especially were gathered through this method. Furthermore, relatively low uranium values were determined by the delayed-neutron counting facility of the Mineral Analysis Group.

# 4. Results

Work with the project included both analytical work and interpretation of the geochemical data and of geophysical logging data. The logs were delivered by The Geological Survey of Denmark in the form of magnetic tapes.

To interpret the logging data, computer software was developed for the Risø Burroughs B7800 (later A6) computer enabling the direct plotting of the geophysical logging data by using the Risø RIGGS plotting software. Similar software was used later for plotting the geochemical logs.

# 4.1 Drill Core TWB-8

#### 4.1.1 Logging Data from TWB-8

Existing wireline logging data for well TWB-8 include data from electrical, acoustic, and radioactive logging devices. A general description of the welllogging devices and their application is given by, e.g., *Helander* (1983). A problem in well-logging data interpretation is the large number of abbreviations and computer codes which also have been altered considerably during past decades. Selected abbreviations of relevance for the present study are given in Appendix VIII. Logging data in digitized form used in the study are tabulated in Appendices VI and VII.

Unit	Depth	Unit	Porosity	Water	Permea-
	(feet)	thickness (feet)	(%)	saturation (%)	bility (mD)
UDP1	6587	17	46	16	4.5
UDP2	6604	10	46	18	4.9
LDP	6614	17	40	34	2.2
UDT	6631	20	31	5 <del>9</del>	0.6
LDT1	6651	19	38	44	2.1
LDT2	6670	10	37	41	1.9
14.4	6690	10	20	20	25
	0000	12	30	28	3.5
ZM	6692	34	45	24	9.2
3M	6726	41	40	50	5.1
4M	6767	41	40	72	8.3
5M	6808	61	38	92	5.9

Table 2 Average petrophysical and reservoir data for TWB-8.

For TWB-8, the gas-oil-contact (GOC) was set by The Geological Survey of Denmark at 6712 feet (Table 2) with a gas zone of 125 feet, 50% water saturation  $(S_w)$  was at 6726 feet leading to a GOC- 50%  $S_w$  zone of 14 feet, and the oil-water contact (OWC) was determined to lie at 6772 feet with a transition zone (50%  $S_w$ -OWC) of 46 feet.

All the available log data for the well TWB-8 were plotted as evaluation plots (Figures 4 to 6). A short general evaluation of these data is given in the following sections.

Fig. 4. Compensated neutron/litho-density log for TWB-8. Log curves include natural radioactivity (GR) and logs belonging to the CNL and FDC-LDT tools.



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#### 4.1.1.1 Radioactive Logs - CNL and FDC-LDT

Radioactivity logs include natural radioactivity (GR), the Compensated Neutron Log (CNL) andluding Far Detector (FCNL) and Near Detector (NCNL) count rates and their ratios (NRAT), the Formation Density Compensated Log (FDC) and the Litho Density Tool (LDT) including the logging curves WI, LU2, LU, LL, LS, LURH, LSRH, SSI, SS2, SIRH, and LITH (see Appendix VIII).

The neutron ratio NRAT (NCNL divided by FCNL) being inversely propertional to NPHI, the neutron polyosity, divides the TWB-8 well into 2 main units (Fig. 4):

- the section between 6590-6710' with neutron ratio of about 3.1 leading to relatively constant NPHI values of about 0.25 to 0.3.
- the section between 6710-6850' with a neutron ratio of about 4, corresponding to NPHI values of about 0.4-0.45.
- The NPHI plot with depth clearly defines the thickness of the gas reservoir.

The relatively large number of available single log curves existing for the UDC-LDT evaluation log all show the same tendency, expressed here by the LITH log (Fig. 5):

- 1) In the UDP1, UDP2 and LDP sections decreasing cps values are observed, dropping from 180 at the top of unit UDP1 to about 100 cps at the transition to unit UDT.
- 2) For unit UDT, a rather constant value of about 75 cps is found; units LDTl and LDT2 again show higher but constant values (120 cps).

Fig. 5. Evaluation logs for TWB-8 including Lithology Window Count Rate (LITH), Bulk Density (RHOB) and the Borehole-Compensated Sonic Logs (BHC).



- 3) From about 6680' to about 6700' depth, LITH values increase linearly to a value of about 170 cps towards the gas-oil contact and they decline then again to a value of about 100 cps at a depth of 6750' within unit 3M
- 4) LITH values are constant, at about 100 cps, below depths of 6750'.

The LITH log curve is the mirror image of the bulk density curve of TWB-8 (Fig. 5). Density values obtained from cross plots, RHGX (not plotted in the figures) show nearly the same distribution with depth, although some smoother curves appear. In general, density values are higher than the cross plot density values and also, RHGX varies less, holding to about 2.7 g cm<sup>-3</sup> below depths of 6710'.

#### 4.1.1.2 Sonic Logs

The series of sonic logs available for TWB-8 includes AMPL, CBL, DT, SRAT, and IT. Most interesting in this respect is the DT log curve (Fig. 5) which leads to similar divisions into subsections.

#### 4.1.1.3 Electrical Logs

The electrical logs (Fig. 6) include the Spherically-Focused Logs (SFL), the Self-Potential Log (SP) and the Induction Logs. Available were SFLU, SFLA, ILD, ILM and CILD.

Log plots of resistivity and conductivity are similar. The distributions with depth may be divided mainly into 2 subsections displaying clearly the gas zone:

- 1) Down to a depth of 6720' constant values of ILM (10 to 20 ohmm), ILD (10 to 20 ohmm) and CILD (about 125 mmho) are observed
- 2) Values decrease with depth in the rest of the section and stay constant below depths of 6775'.

#### 4.1.2 Geochemical Profiles along Drill Core TWB-8

#### 4.1.2.1 Previous Results

Elemental distributions with depth in drill core TWB-8 based on short-lived instrumental neutron activation analysis were reported previously (*Kunzen-dorf* et al., 1985; 1986). For detailed discussions of these data the reader is referred to these publications. All the previous analytical data are also tabulated in Appendix III.

Briefly, Ca and Al contents of the carbonate rock samples (Danian and Maastrichtian strata) match the trends observed for the core porosity (see Fig. 7). For the Danian section of the drill core, core porosity figures are significantly decreased at higher Al contents. A pronounced feature is the increasing (from bottom to top) Mn content in the carbonate reservoir rocks, reaching over 1000 ppm Mn in the LDP, UDP2, and UDP1 sections.

The differences in chalk geochemistry for the different reservoir units are displayed in the best way by means of Fig. 8 which shows a clear grouping of the data.

As regards the trace elements, there are fewer clear trends, although V seems to follow the Mn distribution more closely than other elements; rare earth elements Eu and Dy correlate with Al. A distinct feature is the relatively low U content in each of the Danian samples, but the lowermost Danian and the uppermost Maastrichtian sections show higher U.



Fig. 6. Electrical logs along section TWB-8.



Fig. 7. Geochemical data and core porosity plotted along the TWB-8 section.

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Fig. 8. Triangular plot of Ca, Mn, and Al data showing grouping according to reservoir units, i.e. geology.

Multivariate statistical evaluation of these data is shown in Figs. 9 and 10. The plots are based on the data given in the Appendix III.

Seven factors are necessary to account for 90% of the variability of the analytical data while 5 account for about 70% variability (Table 3). They indicate that there is a modest integration of the data by multivariate statistics.

The plot of factor 1 versus 2 for all analytical data (Figs. 9 and 10) shows a significant grouping in that all Danian samples plot into the right part of the figure while Maastrichtian samples occupy the left part. Also, on dividing further into subgroups, a clear separation of data according to reservoir unit is observed (right part of the figures).

Factor	Eigenvalue	Percent of trace	Cumulative		
1	3.600	30.00	30.00		
2	1.753	14.61	44.61		
3	1.381	11.51	56.12		
4	1.114	9.28	65.40		
5	0.970	8.08	73.48		
6	0.956	7.97	81.45		
7	0.829	6.91	88.36		

Table 3. R-mode factor analysis of all analytical data from TWB-8.



Fig. 9. R-mode factor analysis of geochemical data of TWB-8. Factors 1 and 2 are plotted.

Fig. 10. R-mode factor analysis plot of geochemical data for TWB-8. Factors 1 and 3 are plotted.



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Fig. 11. R-mode factor analysis of geochemical data including core porosity from TWB-8. Factor I is plotted against 2.

The same grouping is observed when core porosity is added to the data sets (Fig. 11).

Using the data sets to run cluster analysis, 3 elemental groups may be selected:

- 1. Na-Cl-Sr-U
- 2. K-Ca-porosity
- 3. Mg-Al-V-Dy-Mn-Eu

Basically, this means that U is connected with formation waters, porosity is an expression of Ca contents, and V, Mn, and rare earth elements can be ascribed to an Al-rich phase (probably clay) in the samples.

#### 4.1.2.2 Supplementary Data

Sixteen additional samples were analyzed by normal INAA. The results of these measurements are given in Appendix IV. A plot of the data is shown in Figs. 12 and 13.



Fig. 12. Elemental contents in additional drill core samples along TWB-8.

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Fig. 13. Elemental contents in additional drill core samples of TWB-8.

The general observation of the distributions with depth is that a number of elements greatly correlate with Fe and also that the low-porosity section in the Danian part has the highest Fe. Some evidence therefore points to the lowered-porosity section of the Danian TWB-8 section being partly due to the occurrence of clay minerals (high Al, see above) which also have elevated Fe contents (up to 0.4%).

As regards the trace elements, Sc follows Fe closely but also displays the high Al values found in the Danian section. This means that, in principle, Sc could be used as an indicator trace element for clay contents in the chalks. The Br distribution with depth strongly resembles that found for Na and Cl, and because the lowest values of both Cl and Br are found in the hydrocarbon-bearing drill core sections, they express the low formation water content in the pore spaces.

Of special importance for investigations of drill cores is the Ba content, baryte being a major component in drilling fluids used for drilling operations. Where the drilling fluids to invade and penetrate the drill core they would seriously influence the analytical data (contamination). High Ba (above 1000 ppm) is observed in only two samples, so actually no Ba contamination need be taken into consideration.

Selected triangular plots are given in Fig. 14.



Fig. 14. Triangular plots for average Ca, Fe, Na and Sc showing pronounced grouping according to geology. Symbols as in Fig. 8.

Rare earth elements (REE) also correlate with elements Fe, Al and Sc, and they are therefore best ascribed to the clay fraction in the carbonate sediments. As shown in Fig. 13, there is a significant change in the Ce/La ratio, from about 0.6 to about 1.2, at the Maastrichtian-Danian border suggesting that Danian deposition of carbonate sediments probably occurred in more oxidized waters. There is also some fractionation trend with higher La/Yb ratios in the Danian strata, while the ratio Sm/Eu (not plotted) largely remains constant throughout the investigated sections. The latter ratio usually expresses terrestrial input (feldspars) into the sedimentary environment by elevated Eu values.

REE patterns of all samples normalized to North American shale (Fig. 15) show a similar tendency: a more-or-less shale-like pattern (except for Ce) suggesting that REE occurs mainly in the clay fraction of the chalk. The negative Ce anomaly, expressed as very low (< 1) Ce/La ratios are typical for oxic depositional environments. Ce is one of the two REEs that may exist in the tetravalent state in which it is readily precipitated and separated from the other, mainly trivalent, REEs.

A characterization plot based on these rare earth element ratios is shown in Fig. 16; it clearly groups the Danian and Maastrichtian strata.



Fig. 15. North-American shale normalized rare earth element patterns of selected drill core samples along TWB-8.



Fig. 16. REE characterization plot.

#### 4.1.2.3 Average analytical data for TWB-8.

As already mentioned, most of the data from drill core samples TWB-8 were generated during an earlier project (see. Kunzendorf et al., 1985; 1986). Converting the previous data into values for the reservoir units used by The Geological Survey of Denmark (DGU), i.e. calculating average chemical data for the units, some interesting features can be evaluated (Table 4 and Fig. 17).

4	Average isotpes.	Analytica All data	al data in <b>%, ex</b> c	of the cept V, Mr	Danian se h, Sr and	Ction for Eu which	r drill c are given	ore TWB-8 in ppm.	using sh	ort-lived
UDPT	U9 P 2	LDP	UDT	LDTI	1072	1#	211	3n	411	5 m
25:0.42	0.07±0.03	0.10.04	0.12:0.05	0.11 <u>+</u> 0.c	. 13 - 0 - 04	749:192	978+217	1527 <u>+</u> 618	2018-548	1680+57
17:0.97 4		•	•	•	•	5320	2485 <u>+</u> 573 2	2443+629 10	2652 <u>+</u> 1175 13	3325 <u>+</u> 375 2
70 <u>+</u> 3.39 4	0.17 <u>+</u> 0.01 2	0.24 <u>+</u> 0.08 8	0.48 <u>+</u> 0.22 8	0.39 <u>+</u> 0.13 7	0.27 <u>+</u> 0.01 2	1379 <u>+</u> 850 9	75 <b>8.</b> 408 30	676 <u>.</u> 237 30	793 <u>+</u> 220 28	725±65 2
12 <u>+</u> 0.03	0.20.0.00	0.20 <u>+</u> 0.08 7	0.10 <u>+</u> 0.00 8	0,18±0.09 5	0.10.0.01 2	1394-557	2592+823	2332+1213 29	3345+1955	2915 <u>+</u> 148 2
5 5	34.80 <u>1</u> .00 2	36.16 <u>.</u> 2.28 8	27.90 <u>-</u> 2.24 Ø	30.40 <u>+</u> 4.5♥ 7	34.40 <u>+</u> 3.25 2	32.33 <u>1</u> 4.34 9	34.21 <u>+</u> 2.24 27	38.38 <u>+</u> 2.47 29	37.30.1.30	37.30
	5.0	9.5:3.7	0.3 <u>*</u> 3.4 0	7.641.5	8.0 <u>+</u> 1.0 2	6.6 <u>+</u> 1.9 4	4.5.1.1	2.7 <u>+</u> 0.7 17	2.6 <u>+</u> 0,8 19	2.4 <u>+</u> 1.1 2
•• <u>-</u> •32	2	1100 <u>-</u> 534 B	725:08	\$70 <u>+</u> 71 \$	*** <u>*</u> ** 2	431-117	299 • 73	184.20	161 <u>-</u> 24 31	14721
3	892 1	#15 <u>.</u> 351 7	767 <u>-</u> 184 0	849 <u>+</u> 91 6	807-172	749-230	1138-157	1942-128	31	978 <u>-</u> 74 2
, , ,	• •	9.2 T	3.0.0.2	3	9.8 1 1	B.840.2 8	0.40D.) 19	0,320,1 14	0,3 <u>+0</u> ,1 17	0.4 1 1 0.0 1
M. 77		•	•	•	2	•	29	29	31	2
	4 UDP1 25:0.42 17:0.97 4 70:3.39 4 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 12:0.03 10:0.03	4 Average isotpes. upp1 upp2 25-0.42 0.07-0.03 17-0.97 - 4 2 17-0.97 - 4 70-3.39 0.17-0.01 4 2 12-0.03 0.20-0.00 4 1 12-0.00 4 1 10-01	Average         analytic: isotpes. All data           upp1         upp2         LDP           25-0.42         0.07-0.03         0.10-0.04           1*6         2         8           17:0.97         -         -           4         7         -           70-3.39         0.17-0.01         0.24-0.08           4         2         8           12:0.05         0.20-0.00         0.20-0.08           5         2         8	Average         analytical data           isotpes. All data in %, exc           upp1         upp2           upp1         upp2           tope.42         0.07:0.05           0.10:0.42         0.07:0.05           17:0.42         0.07:0.05           17:0.42         0.07:0.05           17:0.42         0.07:0.05           17:0.42         0.07:0.05           17:0.47         -           4         0           17:0.47         -           4         2           4         2           5         2           6         2           7         4           12:0.05         0.20:0.00           12:0.05         0.20:0.00           12:0.05         0.20:0.00           12:0.05         0.20:0.00           12:0.05         0.20:0.00           12:0.05         10:0:0.11:00           12:0:0.1         0.20:0.00           13:0:0:1.00         0.20:0.00           14:0:0:0:0:1         0.20:0.00           15:0:0:1         10:0:0:0:0           10:0:0:0:0:0:0:0:0:0:0:0:0:0:0:0:0:0:0:	4         Average         analytical         data         of         the           upp1         upp2         LDP         upt         LDT         LDT           upp1         upp2         LDP         upt         LDT         LDT           17:0.97         .         .         .         .         .           4         2         .         .         .         .           70:3.39         0.17:0.01         0.24:0.08         0.48:0.22         0.39:0.13           4         2         .         .         .         .           70:3.39         0.17:0.01         0.24:0.08         0.48:0.22         0.39:0.13           4         2         .         .         .         .           70:3.39         0.17:0.01         0.24:0.08         0.48:0.22         0.39:0.13           6         2         .         .         .         .         .           70:4         8         .         .         .         .         .         .           12:0.05         0.20:0.08         0.18:0.08         0.18:0.09         .         .         .	4       Average       analytical data       of the Danian is isotpes. All data       in %, except V, Mn, Sr and         upp1       upp2       LDP       up1       LDT1       LDT2         13:00,42       0.07:0.03       0.10:0.04       0.12:0.05       0.11:0.0       .13:0.04         14:0       2       8       8       4       2         17:0.42       0.07:0.03       0.10:0.04       0.12:0.05       0.11:0.0       .13:0.04         17:0.97       .       .       .       .       .       .         4       2       8       8       7       .       .       .         12:0.07       .	4         Average         Analytical         data         or         The Danian         section         for           upp1         upp2         LDP         up1         LDP         up1         LDP         up1         LDP         up1         LDP         LDP         LDT         LDT <td>4       Average       analytical data       of the Danian section for drill cisotpes. All data       isotpes. All data       isotpes. V, Mn, Sr and Eu which are given         upp1       upp2       LDP       up1       LDT1       LDT2       1R       2R         (250.42       0.07_0.03       0.10_0.04       0.12_0.05       0.11_0.0       .13_0.04       749_192       978_217         17       2       8       8       2       9       29         17_0.97       .       .       .       .3320       2485_5573       1       2         6       2       8       8       .       .      </td> <td>4       Average analytical data of the Danian section for drill core TMB-B isotpes. All data in %, except V, Mn, Sr and Eu which are given in ppm.         upp1       upp2       LDP       up1       LD11       LD12       1N       2N       3N         1320.42       0.07-0.03       0.10-0.04       0.1220.05       0.11+0.4       .1320.04       749-192       978-217       1527-618         104       2       8       4       2       9       29       29         17:0.97       .       .       .       .       .       .       .       .         12:0.03       0.17:0.01       0.24:0.08       0.46:0.22       0.39:0.13       0.27:0.01       1370:059       758:408       67 a 23         12:0.03       0.20:0.08       0.16:0.08       0.18:0.09       0.19:0.01       1394:0557       2592:823       2332:21213         12:0.03       0.20:0.08       0.16:0.08       0.18:0.09       0.19:0.01       1394:0557       2592:823       2332:21213         12:0.05       1.12:0.0       0.16:0.08       0.18:0.09       0.19:0.01       1394:0557       2592:823       2332:21213         12:0.05       1.20:0.0       0.18:0.09       0.19:0.01       1394:0.557       270       29       29     <td>4       Average       Analytical data of the Danian section for drill core fWB-8 using shisotpes. All data in %, except V, Mn, Sr and Eu which are given in ppm.         upp1       upp2       up up1       up1</td></td>	4       Average       analytical data       of the Danian section for drill cisotpes. All data       isotpes. All data       isotpes. V, Mn, Sr and Eu which are given         upp1       upp2       LDP       up1       LDT1       LDT2       1R       2R         (250.42       0.07_0.03       0.10_0.04       0.12_0.05       0.11_0.0       .13_0.04       749_192       978_217         17       2       8       8       2       9       29         17_0.97       .       .       .       .3320       2485_5573       1       2         6       2       8       8       .       .	4       Average analytical data of the Danian section for drill core TMB-B isotpes. All data in %, except V, Mn, Sr and Eu which are given in ppm.         upp1       upp2       LDP       up1       LD11       LD12       1N       2N       3N         1320.42       0.07-0.03       0.10-0.04       0.1220.05       0.11+0.4       .1320.04       749-192       978-217       1527-618         104       2       8       4       2       9       29       29         17:0.97       .       .       .       .       .       .       .       .         12:0.03       0.17:0.01       0.24:0.08       0.46:0.22       0.39:0.13       0.27:0.01       1370:059       758:408       67 a 23         12:0.03       0.20:0.08       0.16:0.08       0.18:0.09       0.19:0.01       1394:0557       2592:823       2332:21213         12:0.03       0.20:0.08       0.16:0.08       0.18:0.09       0.19:0.01       1394:0557       2592:823       2332:21213         12:0.05       1.12:0.0       0.16:0.08       0.18:0.09       0.19:0.01       1394:0557       2592:823       2332:21213         12:0.05       1.20:0.0       0.18:0.09       0.19:0.01       1394:0.557       270       29       29 <td>4       Average       Analytical data of the Danian section for drill core fWB-8 using shisotpes. All data in %, except V, Mn, Sr and Eu which are given in ppm.         upp1       upp2       up up1       up1</td>	4       Average       Analytical data of the Danian section for drill core fWB-8 using shisotpes. All data in %, except V, Mn, Sr and Eu which are given in ppm.         upp1       upp2       up up1       up1

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Fig. 17. Average analytical data distribution along drill core TWB-8.

As already mentioned, Ca is significantly reduced in sections LDP and UDT also, reflecting reduced porosity values at increased Al contents. Water saturation peaks as well in the area of high Al contents. In the gas zone, between 6614' and 6690', therefore, the reservoir quality is significantly reduced.

On comparing average petrophysical data (rho,  $S_w$ , permeability) with average elemental data, some significant grouping of Maastrichtian and Danian strata may be obtained (Fig. 1°)



Fig. 18. Selected X-Y plots for average analytical data of TWB-8.

There is no clear correlation of elemental data with rho, although grouping into Danian and Maastrichtian groups is observed for, e.g., Sr, where Maastrichtian samples generally have higher Sr at comparable rho.

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For water saturation,  $S_w$  (not plotted), there are some positive correlations with the average analytical data. As expected, there is a significant correlation between  $S_w$  and Na involving all chalk units. Also, water saturation divides Maastrichtian and Danian carbonate sediments into groups when plotted against Mn, Sr and Dy. Most interesting is perhaps the plot  $S_w$  vs. Ca where Maastrichtian samples show an increasing tendency while those of the Danian show decreasing  $S_w$  with decreasing Ca.

On comparing the permeability values, there seems to be significant correlation between permeability and average Na, Cl, Ca, and Sr. Permeability vs. average Mn also divides Danian strata (increasing tendency) and Maastrichtian strata (constant average Mn at increasing permeability).

#### 4.1.3 Comparison of Log Data with Element Contents

Logging data are physical measurements of petrophysical properties in sedimentary formations. These properties in turn are closely related to the chemical composition of the rocks. It is therefore worthwhile to compare the chemical core data directly with the log values to establish relationships between chemistry and e.g. rock porosity or permeability. These comparisons should then lead to a better definition of petrophysical parameters via core data.

From the continuous log data we used the log value corresponding to the depth of the core sample taken for chemical analysis. In the correlation analysis, we follow the conventions suggested by Marsk Oil and Gas A/S, i.e. division into Danian units DI and D2, and into Maastrichtian units MI and M2, sometimes choosing further subdivisions according to the Mn distribution with depth. In the X-Y plot examples, however, the division of data is made according to reservoir units.

#### 4.1.3.1 Comparison of Log Data with Ca Core Data from TWB-8

Correlation analysis results using log data and analytical results for Ca are given in Table 5.

Tool	DANIAN	D1	D2	MAAST	M1	M2	All data
GR	- 0.15	0.63	0.20	- 0.28	0.06	- 0.05	- 0.23
SP	0.36	0.35	0.17	~ 0.48	- 0.03	- 0.09	- 0.44
NPHI	0.11	- 0.71	0.00	0.45	- 0.01	- 0.10	0.45
ILM ILD CILD	0.37 0.46 0.52	0.66 0.59 0.26	0.15 - 0.24 - 0.40	- 0.41 - 0.39 0.43	- 0.06 0 22 - 0.23	- 0.24 0.13 - 0.03	- 0.25 - 0.06 0.39
SFLA	0.42	0.56	0.25	- 0.46	0.32	0.57	- 0.28
RHOB	- 0.57	0.75	- 0.45	0.50	0.07	0.24	- 0.01
PET	- 0.05	- 0.83	0.42	0.27			0.20
DT	0.33	0.61	- 0.02	- 0.34	0.09	0.21	0.06
LITH	0.51	0.83	0.36	- 0.47	- 0.07	- 0.30	- 0.03
AMPL	0.00	0.25	- 0,44	0.49			0.48
RHGX	- 0.58	- 0.86	- 0.51	0.51	- 0.10	0.34	0.31

Table 5. Correlation matrix for well-logging and Ca data.

It is usually not sufficient to discuss correlation coefficients without actually plotting the data. The reason for this is that in many cases analytical data (even very large numbers of data) tend to show high correlation in case the range of the data is limited. This means that, although regression analysis gives a high correlation coefficient, there might be no linear dependence at all. X-Y plots in general have the advantage that they flag grouping of data, in the present case with depth in the core.

As seen from the data in Table 5, significant correlations exist for:

- GR and Ca in Dl (r = 0.63),
- NPHI and Ca in MAAST. (0.45),
- ILM and Ca in Dl (0.66),
- ILD and Ca in DANIAN (0.46) and DI (0.59),
- CILD and Ca in MAAST. (0.43),
- SFLA and Ca in DANIAN (0.42), in DI (0.56) and M2 (0.57),
- RHOB and Ca in MAAST. (0.50),
- PEP and Ca in D2 (0.42),
- DT and Ca in Dl (0.61),
- LITH and Ca in DANIAN (0.51) and in D1 (0.83),
- AMPL and Ca in MAAST. (0.49), and
- RHOGX and Ca in MAAST. (0.51).

Here, as mentioned above, DANIAN, DI, and D2 correspond to data from the whole Danian, units DI and D2, respectively, while MAAST., MI and M2 correspond to data from the whole Maastrichtian, units MI and M2, respectively.

On inspecting these correlations in further detail it becomes clear that the correlation GR vs. Ca in Dl is not significant because only a few analytical results are available. The good correlation expressed by a relatively high correlation coefficient therefore is quite misleading.

An interesting grouping is obtained when plotting SP data vs. Ca (Fig. 19). While for Danian samples (UDP1 to LDT2) SP values are relatively constant

Fig. 19. Selected well-log data plotted vs. Ca content in drill core samples.



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at largely varying Ca, most of the Maastrichtian SP data of the lowermost units (3M to 5M) are significantly lower, and by this a clear grouping of data is obtained. Characteristically, the group with Danian data includes also the uppermost Maastrichtian units (IM and 2M).

Plotting NPHI data against Ca, a clear grouping for the Maastrichtian samples is again observed. A distinct feature is that data from unit 2M fit equally into the two groups. As can be seen from the figure, the good correlation coefficient (r = 0.45) we find is an artifact produced by two distinct data groups; and therefore is without meaning.

The induction log data plotted against Ca (not shown in Fig. 19) also suggests grouping of data and in reality no positive correlation, although correlation analysis predicts rather high correlation coefficients. A similar pattern is derived for the SFLA data.

The plots RHOB vs. Ca and LITH vs. Ca (Fig. 19) also show some grouping rather than significant positive correlation, although the groups do overlap.

#### 4.1.3.2 Comparison of Log Data with Al Core Data from TWB-8

Data from the following logs of TWB-8 were compared with Al core data: GR, SP, NPHI, ILM, ILD, CILD, SFLA, RHOB, PEF, DT, LS, LITH, AMPL, and RHGX. Correlation data are given in Table 6.

There are only a few significant element-log correlations (correlation coefficients greater than 0.4). The gamma-ray count rate (in API units) of section D1 correlates well with Al (r = 0.65), while there is no correlation between GR and Al for the whole Danian-Maastrichtian section.

Other significant correlations (correlation coefficient r in parenthesis) between logs and Al are: SP-Al for MI (0.50), CILD-Al for D2 (0.50), RHOB-Al for DAN (0.43), for D2 (0.56) and for M2 (0.40), and RHOGX-Al for D2 (0.52).

Tool	DANIAN	D1	D2	MAAST.	M1	M2	All data
GR	0.15	0.65	- 0.07	0.20			0.09
SP	- 0.08	0.32	- 0.07	0.12	0.50	- 0.36	0.24
NPHI	- 0.27	- 0.33	- 0.22	- 0.41	- 0.53	- 0.06	- 0.37
ILM ILD CILD	- 0.02 - 0.34 0.38	0.10 - 0.54 0.04	- 0.22 - 0.46 0.50	0.27 0.10 - 0.13	0.26 - - 0.35	- 0.35 0.35	0.20 0.10 - 0.23
SFLA	- 0.20	0.24	- 0.30	0.33	0.41	0. <b>93</b>	0.21
RHOB	0.43	0.10	0.56	- 0.18	- 0.25	0.40	0.29
PET	- 0.22	- 0.03	- 0.57	- 0.11			- 0.23
DT	- 0.21	0.06	- 0.14	0.28	0.32	0.08	- 0.26
LITH	- 0.32	- 0.08	- 0.45	0.17	0.23	- 0.31	- 0.18
AMPL	0.07	- 0.20	0.33	- 0.22	··-		- 0.35
RHGX	0.37	- 0.04	0.52	- 0.32	- 0.46	0.23	- 0.11

Table 6. Correlation coefficients of log-data vs Al contents for TWB-8.
On inspecting the relevant data in detail by X-Y plots, it is evident that the correlation GR-Al in the Dl section (not plotted) is an artifact and generated by too few scattered data. Contrary to this, a significant correlation seems to exist for SP-Al in the Ml section alone, but inspecting the data in detail (Fig.20), the characteristical feature is the way the data is grouped.

### Fig. 20. Selected well-logging data plotted against Al content in drill core samples.



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When plotting neutron porosity values (NPHI) against Al, a clear pattern is shown (Fig. 20). Danian and Maastrichtian samples make up three significant groups, but there is no positive correlation, rather a negative one, as should be expected. Al usually connected with the clay mineral fraction should express lower porosity values at higher Al content. It can be seen from the figure that some of 2M (and 1M) samples show high NPHI values, while others (gas-bearing) clearly group within the Danian samples.

Most of the induction logs plotted versus Al show an erratic picture with little or absent grouping of data. Only the plot of CILD-Al data shows 2 main groups, whereas the calculated positive correlation for the D2 section in doubtful.

While correlation analysis predicts a significant positive correlation between RHOB-Al in the Danian section, the grouped data in the plot (Fig. 20) do not confirm this. Also, calculated positive correlations between RHOB and Al for D2 and M2 are rather doubtful. It appears that there is perhaps some further grouping in the Maastrichtian strata. There are too few data for D2 to be sure that the observed positive correlation between RHGX and Al is real, but a grouping of data is observed here as well.

Tool	DANIAN	D1	D2	MAAST.	M1	M2	All data
GR	0.35	- 0.17	0.22	- 0.42	_	-	- 0.29
SP	- 0.25	- 0.45	- 0.23	- 0.47	-		- 0.67
NPHI	- 0.13	0.49	- 0.12	0.47	- 0.32	- 0.10	0.44
ILM ILD CILD	- 0.38 - 0.27 0.38	- 0.10 - 0.26 - 0.44	- 0.15 - 0.27 0.32	- 0.49 - 0.28 0.69	- 0.28 - 0.01 0.34	- 0.47 - 0.36 0.40	- 0.48 - 0.28 0.67
SFLA	- 0.33	0.32	~ 0.41	- 0.61	0.13	- 0.76	- 0.56
RHOB	0.53	0.18	0.50	0.58	- 0.10	0.27	0.48
PEF	0.01	0.40	~ 0.53	0.46	- 0.13	0.10	0.36
DT LITH	- 0,40 - 0,46	0.13 - 0. <b>2</b> 7	- 0.30 - 0.37	- 0.57 - 0.57	0.18	- - 0.33	- 0.41 - 0.47
RHGX	0.53	0.30	0.49	0.58	- 0.41	0.41	0.58

Table 7. Correlation coefficients of log-data vs. Na core data for TWB-8.

#### 4.1.3.3 Comparison of log data with Na core data from TWB-8

Data from the following logs were compared with sodium core data: GR, SP, NPHI, ILM, ILD, CILD, SFLA, RHOB, PEF, DT, LS, LITH, AMPL, and RHGX. Correlation data for this comparison are given in Table 7.

There is no significant correlation of Na with GR data in the whole investigated section. If we introduce a threshold value for significant positive correlation at > 0.4, only RHOB (r = 0.48) and RHGX (0.58) correlate significantly with Na in the drill core section as a whole. A higher correlation (0.69) is obtained for CILD and Na. Good correlation between Na and LITH and AMPL is found for the lower parts of the Maastrichtian section.



Fig. 21. Selected well-logging data plotted vs. Na content in drill core samples.

By plotting the SP and Na data (Fig. 21), two main groups are obtained within which the general trend shows decreasing SP values with depth at increasing Na. In the figure, 1M and 2M data plot within the Danian group. A similar group separation with depth may also be deduced by plotting NPHI vs. Na.

Although the correlation coefficient for the data set CILD-Na is rather high (0.69) by inspecting the data (Fig. 21), it is clear that the apparent correlation may also be interpretated as the presence of two groupings of data.

### 4.1.3.4 Comparison of log data with Mn core data from TWB-8

Characteristic for the comparison of logging data with drill core Mn analyses is the presence of a number of significant and high positive correlations. An overview of the correlations is presented in Fig. 22.

Highest positive correlations (> 0.8) are observed between log data and Mn for

 Dl section:
 SP (0.96), ILM (0.85), SFLA (0.96) and DT (0.97)

 DANIAN section:
 ILD (0.82), LS (0.90), and LITH (0.90)

 MAAST. section:
 SFLA (0.94), DT (0.97), LS (0.85) and LITH (0.85)

These high correlations call for a more detailed investigation.

When all the available Mn data vs. the respective SP data (Fig. 23) are plotted, it becomes evident that one should be sceptical about the high correlation in the Dl section because only few data are available. There is a significant grouping, suggesting at least 4 groups: group 1 includes the data for reservoir units UDP1, UDP2, and LDP; group 2 contains mostly data from UDT, LDT1, LDT2 and partly 1M; group 3 is composed of mainly data from 2M; and group 4 incorporates ail data from 2M to 5M.

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SFLA data plotted against Mn (Fig. 23) suggest a positive and significant correlation for all the Maastrichtian samples (samples from reservoir unit 1M are slightly removed). The Danian samples make up four clear'y separated groups.

On inspecting the curve ILM vs. Mn (Fig. 23), a significant grouping is again seen, the data being split up into 3 main groups. There is a significant positive correlation within the group containing the Maastrichtian data (r = 0.73).

The curve for DT vs. Mn (Fig. 23), although giving very high positive correlation coefficients for some subsections, is most significant for the Maastrichtian data. Three major groups are suggested by the plot: two groups with positive correlation of data and one with negative correlation. The latter group contains both Danian (UDT, LDTI) and Maastrichtian (IM) data.

LITH and RHGX vs. Mn show the same grouping of data, i.e. three distinct data groups (Fig. 23).



Fig. 23. Selected well-logging data plotted against Mn contents in drill core samples.

# 4.1.3.5 Comparison of Log Data with U Core Data from TWB-8

Data for the following logs were compared with U core data: GR, SP, NPHI, ILM, ILD, CILD, SFLA, RHOB, PEF, DT, LS, LITH, AMPL, and RHGX. Correlation data are given in Table 8.

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Table 8. Correlation coefficients of log-data vers. U core data for TWB-8.

Tool	DANIAN	D1	D2	MAAST.	M1	M2	All data
GR	-0.27	-	0.02	0.18	-	-	0.08
SP	0.43	0.40	0.20	0.48	-0.05	0.25	0.31
NPHI	~0.26	0.69	-0.37	-0.1 <del>9</del>	0.12	0.1 <del>9</del>	- 0.01
ILM ILD CILD	0.32 0.36 ~0.45	0.11 - -	-0.18 -0.37 0.45	0.37 0.35 -0.51	0.05 0.17 ~0.14	0.57 0.48 ~0.35	0.38 0.33 -0.33
SFLA	0.57	-	-0.13	0.38	-0.11	0.60	0.28
RHOB	-	-	0.62	-0.58	-0.36	~0.29	0.48
PEF	-	÷	0.26	-0.34	-0.37	0.34	0.22
ЪТ	-	-	-0.14	0.53	-	-	0.50
LITH	-	-	-0.58	0.62	0.44	0.27	0.49
RHGX	-	-	0.51	-0.41	-0.52	-0.54	-0.30

When comparing the data in the table, it may be concluded that Dl shows a significant correlation between SP and U, whereas SP, CILD, RHOB and PEF correlate with U in the section D2. For the Maastrichtian, U correlates positively in the Ml section with LITH only, whereas in the section M2 U correlates with EP, ILM, ILD, SFLA, and LITH.

On comparing the log and geochemical data in the form of X-Y plots (not shown), the general tendency of grouping rather than positive correlation is confirmed.

# 4.2 Drill Core E-1x

# 4.2.1 Log Interpretation Data for E-1x

Average petrophysical and reservoir data for the well E-lx are given in Table 9.

GOC and 50% Sw are not present in E-lx, and the OWC is calculated at 6742'. A zone of > 7 feet comprises the 50%  $S_w$ -OWC, i.e. a very thin oil zone exists in the uppermost Danian.

All available logging data for E-lx were considered. These data were recorded in 1982. The logging equipment differed from that applied when logging TWB-3 (at later times). This means that a number of logging tools were different and generally not as advanced when logging well E-lx. Logs are included for E-lx: SP, IL, GR, DT, CAL1, RHOB, SNP, MLL, MINV, and MNOR.

A number of interpretational plots for E-lx are given in Fig. 24, while porosity and  $s_w$  with depth are plotted in Fig. 25.





Fig. 25. Interpretational porosity and  $s_w$  with depth in hole E-lx.

# 4.2.1.1 Logs Involving Radioactivity Measurements

Natural radioactivity is very low (about 12 GAPI) throughout the well and there is only very little graduation in the GR data (Fig. 24).

The SNP tool giving data in porosity units (PU) points to a porosity degradation in unit UDT (Fig. 24) which shows a constant value of about 20 PU. While SNP values in Danian units UDP1, UDP2, and LDP generally lie at about 35 PU, and they gradually decrease towards the Creataceous-Tertiary boundary; only about 18 PU are observed at the boundary. An increase with depth is then found in units IM and 2M.

Unit	Depth (feet)	Thickness (feet)	Porosity (%)	Sw (%)	Permeabil. (mD)
UDP1	6735	14	35	_	0.9
UDP2	6749	17	35	-	0.9
LDP	6766	46	33	-	0.7
UDT	6812	18	25	-	0.3
LDT1	6830	22	30	-	0.5
LDT2	6852	24	27	-	0.3
1M	6876	20	29	-	0.6
2M	6896	44	32	-	1.2
ЗM	6940	82	31	-	1.2
4M	7022	51	30	-	1.5
5M	7073	75	29	-	1.3

Table 9. Average petrophysical and reservoir data for E-lx.

### 4.2.1.2 Electrical Logs

Results for the microspherically focused log and the microlaterolog, both measuring resistivity near the borehole are shown in Fig. 24.

MLL values are slightly decreasing in unit UDPI towards the transition zone to UDP2 and stay constant within this rock unit. MLL values are slightly higher in unit LDP, while they are significantly increased in unit UDT and are somewhat lower again in units LDT1 and LDT2. The transition to the Maastrichtian strata is marked by high MLL values, decreasing rapidly to a constant level comparable to that for UDT.

Log curves with a behaviour very similar to that of MLL are displayed for MINV, MNOR, LL, IL, and SN. They all show a maximum value in unit UDT.

Very similar data are also recorded by the self-potential tool SP.

#### 4.2.1.3 E-lx Density Logs

The plot of RHOB (Fig. 24) shows values of 2.07 g cm<sup>-3</sup> for Danian units UDP1 and UDP2. Increasing RHOB values are observed for section LDP, increasing to about 2.2 g cm<sup>-3</sup> at the bottom of the LDP section. Section UDP shows the highest RHOB, about 2.35 g cm<sup>-3</sup>, whereas in section LDT1 the value for RHOB drops again to about 2.17 g cm<sup>-3</sup>. Apart from a relatively high-RHOB upper part of section LDT, increasing values are generally observed for this section.

From the C-T boundary onwards, RHOB decreases with depth from a value of about 2.4 g cm<sup>-3</sup> to about 2.2 g cm<sup>-3</sup> in the Upper Maastrichtian section.

#### 4.2.2 Geochemical Profiles along E-lx

Major element contents (Na, Ca, Fe, Al, and Mn) determined by both INAA and XRF are given for all samples in Appendix V, and they are plotted with depth in Figs. 26 to 29.

While Na contents are constant (about 0.2%) throughout the drill core section (Fig. 26), there is a slight decrease of Ca (from about 35% to 30%) in sections UDT, LDT1, and LDT2, i.e. towards the Cretaceous-Tertiary boundary. Ca values are high again in the Maastrichtian samples. The tendency for Ca is somewhat mirrored by Al contents being slightly higher in the lower-most Danian samples. Aluminium contents in general are significantly decreased in the Maastrichtian samples.

Iron content in the samples were determined by both INAA and XRF. The depth profiles for both measurements are compared in Fig. 29. Although there is some difference for both Fe measurements the general tendency is clearly displayed: reduced Fe values are found in the Maastrichtian strata, while in the Danian Fe is relatively constant at about 0.2%. Compared with TWB-8 there is no Fe enrichment observed within the Danian samples.

For manganese the distribution with depth strongly resembles that observed in TWB-8 (Fig. 26). Content continuously decreases from about 4000 ppm (unit UDPI) to the top LDP unit (about 1500 ppm) and then reaches a nearly constant value at about 1000 ppm down to the Cretaceous-Tertiary boundary. Maastrichtian samples then have much lower Mn (less than 500 ppm).



Fig. 26. Na, Ca, Fe, Al, Mn, Ti, Sc, Cr, Co, and As distributions with depth in drill core E-Ix.



Fig. 27. Zn, Br, Rb, Sr, Sb, Cs, Ba, Hf, Th and U distribution with depth in drill core E-lx.

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Fig. 28. Selected rare earth element contents and ratios plotted  $v_s$ . depth in drill core E-1x.



Fig. 29. Fe and U determined by two independent analytical methods plotted vs. depth in drill core E-lx.

As regards Ti, Sc, Cr, Co, and As, the content of each in the chalk samples is very low (Fig. 26); for Ti, Sc and As, there is practically no trend with depth, although Sc values are somewhat higher in the Danian rocks compared with their Maastrichtian counterparts. A clear trend with depth is seen for Cr in that contents in the lowermost chalk units LDT1 and LDT2, but also in 1M and 2M are significantly higher, at generally 10 ppm. Frequently observed fluctuations in the contents of these elements may be explained by the small sample amount analyzed suggesting problems of inhomogeneity.

While Rb contents are very low showing no clear trend with depth (Fig. 27), values for Br, Sr and Sb differ somewhat from each other. There is a slight increase in Sr contents in units LDT1 and LDT2, and for Sb values are slightly higher in the lowermost Danian samples.

Most of the Danian samples show rather constant contents of Cs, Ba, Hf, Th, and U along the drill core (Fig. 27). However, clearly lower values for Cs, Ba, Hf, and Th are observed in the Maastrichtian samples, while U in these samples is significantly higher. Uranium analyses by DNC differ somewhat from those obtained by INAA (Fig. 29), but the distribution with depth is quite similar.

As regards the rare earth elements of which 2 of the 7 analyzed elements are plotted in Fig. 28, they are expectedly low throughout the E-lx drill core section. However, some clear trends are observed. Viewing only La and Ce, these elements are relatively low and constant in Danian sections UDP1 and UDP2 with very low contents at the top of unit LDP. They then increase again towards unit UDT and stay constant throughout the Danian. Maastrichtian strata have generally lower REE content.

Selected rare earth element ratios (Fig. 28) show that Ce/Lz is different in sections UDT, LDTI, and LDT2 (higher) but was significantly reduced in the Maastrichtian strata. This again (see sect. 4.1) would suggest a significant

change in redox conditions at the end of the Maastrichtian. Depositional redox conditions in the carbonates may be viewed through the behaviour of Ce. As they are preferentially removed under oxic depositional conditions, it is concluded that available oxygen was increased in the Danian. There is no clear trend for the other two selected rare earth element ratios (La/Yb, and on Sm/Eu), although the higher Sm/Eu ratios in the Maastrichtian samples could be interpreted to stem from increased terrestrial input.

### 4.2.3 Average Analytical Data for E-1x

Average analytical data for the E-lx drill core section are given in Table 10. Not all of these data were obtained by INAA, i.e. the table also contains XRF data.

The average data are also plotted in Fig. 30 vs. depth. It is clear that there is a significant grouping in element distributions with depth, i.e. for a number of elements similar distributions with depth are observed.

Fig. 30. Average analytical data plotted vs. depth in drill core E-lx. The data are grouped according to depth distributions that are similar to each other.



le- ent	UDP1	UDP2	LDP	UDT	LDT1	LOT2	1M	214
<b>.</b> 0.	)1+0.08 N=5	0.21 <u>+</u> 0.02	0.18+0.04 11	0.20+0.03	0.21+0.04	0.26+0.22	0.11 <u>+</u> 0.03	0.14+0.03
٥.	36+0.30	-	-	-	-	-	-	-
<b>a</b> .	- 10+7-40	34.70 <u>+</u> 1.60	31.20 <u>+6</u> .20	27.60 <u>+</u> 3.80	29.70 <u>+</u> 4.20	26.60+8.20	38.40+0.57	38.60+0.50
<b>o</b> .	65+0.56 5	0.24 <u>+</u> 0.07 5	0.23+0.09 11	0.46+0.36 ē	0.38+0.18 5	0.58+0.62 8	0.09+0.02 5	0.07+0.01 J
ter	nined by	XRF:						
<sup>1</sup> o.	12+0.11	0.21 <u>+</u> 0.10	0.22+0.0 <del>9</del> 11	0.43+0.09	0.38 <u>+</u> 0.23	0.37 <u>+0</u> .19 7	0.0 <b>8</b> +0.03	0.05+0.01 j
<b>ن</b> ۱	74+558 5	105 <u>+</u> 54	110+39 11	197 <u>+</u> 45 6	156+67 5	153+76 7	31+9 5	18+4 3
34	10+611 5	1772+304	1352+204 11	1352+137 6	\$84 <u>+121</u> 5	1104+148 7	47 <b>8+</b> 81 5	313+55 3
0.	42+0.40 5	0.17+0.05 6	0.16+0.04 11	0.25+0.04 6	0.25+0.08 5	0.23+0.11 7	0.06+0.01 5	0.04+0 3
2	.8 <u>+</u> 1.4	2.0 <u>+</u> 0.7	2.3 <u>+</u> 0.8	3.8 <u>+</u> 0.7	3.0 <u>+</u> 0.7	4.2 <u>+</u> ).6	1.5 <u>+</u> 0.4	0.8 <u>+</u> 0.3
10	5 .3 <u>+</u> 8.2	11 5.5+2.2	6 4.7 <u>+1</u> .2	5 6.1 <u>+</u> 2.3	8 11-1 <u>+</u> 3.0	5 14.5 <u>+</u> 8.2	5 10.2+1.6	د 9.9 <u>+</u> 0.9
3	.4±2.9	2.7 <u>+</u> 0.4	6.0 <u>+</u> 3.5	10.4 <u>+</u> 8.0	12.3 <u>+</u> 15.7	12.9 <u>+</u> 11.9	1.3 <u>+</u> 1.4	1.6±1.7
24	⊃ .1 <u>+</u> 8.847	.7 <u>+</u> 28.5	11 23.3 <u>+</u> 13.9	-	-	-	-	3 23±18
4	5 .4 <u>+</u> 3.1	4 1.7 <u>+</u> 0.4	5 2.0 <u>+</u> 0.8	16.4 <u>+</u> 25.6	3.2 <u>+</u> 3.8	6.2 <u>+</u> 8.4	0.9 <u>+</u> 0.6	2
31	4 .0 <u>+</u> 9.330	5 •9±4.3	10 26.0 <u>+</u> 8.9	) 16.3 <u>+</u> 3.3	5 22.8 <u>+</u> 7.6	7 18.2 <u>+</u> 6.5	3 16.0 <u>+</u> 5.0	23.5 <u>+</u> 1.3
	5 .7 <u>+</u> 9.4	5 3,8 <u>+</u> 1.9	11 3.7 <u>+</u> 1.5	6 9.5 <u>+</u> 4.9	5 4.3 <u>+</u> 1.6	8 7.8 <u>+</u> 11.8	5 1.6 <u>+</u> 0.1	) 1.2
10	5 19 <u>+</u> 280	4 1492 <u>+</u> 86	10 1295 <u>+</u> 247	• 1265 <u>+</u> 135	5 1496 <u>+</u> 96	8 1616 <u>+</u> 227	3 1628 <u>+</u> 153	1 1813 <u>+</u> 91
0	5 .1 <u>+</u> 0.1	5 0.1 <u>+</u> 0.1	11 0.2 <u>+</u> 0.2	6 0.5 <u>+</u> 0.2	5 0.4 <u>+</u> 0.2	8 0.7 <u>+</u> 0.8	5 0.1 <u>+</u> 0.1	د 0.1 <u>+</u> 0.1
0	5.4 <u>+</u> 0.5	5 0.2 <u>+</u> 0.1	11 0.2 <u>+</u> 0.1	6 0.2 <u>+</u> 0,1	5 0.2 <u>+</u> 0.1	8 0.3 <u>+</u> 0.5	3 0.1 <u>+</u> 0.0	) 0.1
29	> 5 <u>+</u> 203	2 143 <u>*</u> 11	11 182 <u>+45</u>	8 249 <u>+</u> 57	5 167 <u>+</u> 20	• 183 <u>*</u> 51	, 17 <u>+</u> 11	1 104 <u>+</u> 27
0.	4 <u>+</u> 0.4	0.1 <u>+</u> 0.1	0.2+0.1	0.3+0.1	• 0.2 <u>+</u> 0.1	0.5 <u>+</u> 0.7	3 0.1 <u>+</u> 0.0	0.1
1	3+1.2	0.6+0.2	1.2+0.5	2.3 <u>+</u> 0.4	1.# <u>+</u> 0.4	3.3 <u>+</u> 3.7	0. <u>3+</u> 0. 1	0.2±0.1
0.4	1+0.24	0.23+0.08	0.15+0.04	0,16+0,05	0.15 <u>+</u> 0.05	0.29 <u>+</u> 0.31	0.58 <u>+</u> 0.27	0.62 <u>+</u> 0.14
13.	.8+5.3	11.2+2.8	12.4+J.6	16.J+3.0	17.1 <u>+</u> 3.4	24.4 <u>+</u> 23.9	8.9 <u>+</u> 1.8	7.5 <u>+</u> 1.6
21.	7+9.3 5	15.1+4.4 5	18.6+6.7 11	30.1+4.5 6	26.6 <u>+</u> 6.4 5	39.1+32.7 8	9.7+2.3 5	7.0+1.6 J
12.	6+4.7 5	12.1+2.7	13.5+5.1 11	18.J+1.9 6	17.7 <u>+</u> ].4	29.5 <u>+</u> 28.2 8	8.2 <u>+</u> 1.5 5	8,9+2,0 3
2.	9+0.9 5	2.6+0.4 5	3.6+1.2 11	5.0+1.0 6	4.9+1.0 5	7.2+7.3 8	2.4+0.5 5	1.9+0.6 3
ø.	8+0.2 5	0.5+0.1 5	0,6+0,2 11	0.8+0.2 6	0.8+0.J 5	1.3+1.3 B	0.4+0.1 5	0.3+0.1 3
٥,	4+0.1 5	0.4+0.1 5	0.5+0.1 11	0,6+0,1 6	0.7+0.1 5	1.0+1,0 8	0.3+0.1 5	0.2+0.1 Ĵ
1.	1+0.2 5	1.1+0.3 5	1,1+0.5 11	1.5+0.2	1,5+0.3 5	1,9+1,J 8	1.0+0.2	0.8+0.2 j
ο.	140.1	0,1+0.0	0.2+0.1	0.2+0.0	0.2 <u>+</u> 0.0	0.2+0.2	0.1 <u>+</u> 0.0	0.1 <u>+</u> 0.0

# Table 10. Average analytical data for drill core E-lx.

Group 1 which also contains petrophysical parameters porosity (RHO) and estimated permeability (mD) includes elements Ca and Br; it shows a general decrease of data down to unit UDT. Higher values are found in unit LDTI, decreasing again in LDT2. Maastrichtian units 1M and 2M have generally increased values. The plots also suggest that for E-lx there is a positive correlation between the Ca content in drill core samples and the porosity of the formation.

Group 2 includes elements Fe, Sc, Rb, Sb, rare earth elements, Hf, and Th. The distribution with depth for these elements is approximately the mirrorimage of group 1 distributions. Because of this, group 2 is thought to contain largely elements of the residual fraction incorporating both clays and other residual minerals. The rare earth North American shale normalized distributions are plotted in Fig. 31 showing the increased negative Ce anomaly for Maastrichtian samples.

Group 3 incorporates elements Na, Cs and Cr showing distribution patterns similar to each other. If there are higher elemental contents for unit UDT, this element group could be included into group 2.

Group 4 is made up of elements showing little similarity in their depth distributions. It includes elements Co, Zn, As, Sr, Ba and U. Apparently these elements are resting in some phases clearly differently with respect to those of the other groups. However, some of these elements could also be added to some of the other groups, e.g., Co to group 3.

Fig. 31. Average North-American shale normalized REE patterns in drill core E-lx.



La Ce Pr Nd Pm Sm Eu Gd Th Dy Ho Er Tm Yh Lu

### 4.2.4 Comparison of Selected Analytical Data with Log Data

Because drill core samples from E-lx were analyzed for a large number of chemical elements (normal INAA), comparisons for all of these elements may be carried out. However, only a few of them are selected.

Some results of correlation studies between log data and selected element contents for drill core samples E-lx are given in Fig. 32.

The only positive correlation between Ca and log data is for DT in the Danian section. Inspecting the data of Ca vs. DT (Fig. 32) however, reveals that there is merely a grouping of data, where Danian and the few Maastrichtian data split into 2 groups. Correlation analysis of log data vs. Al shows correlation coefficients close to 0.5, very rarely exceeding 0.55.

Fig. 32. Selected analytical data plotted vs. selected logging data the well E-lx.



A typical example for Al is given in Fig. 32. As was the case in several other examples, a clear grouping is present, but in reality no linear dependence is shown by the plot. It is interesting that UDT and LDT2 show generally higher RHOB values than the rest of the Danian samples.

Among all the possible correlations, the only positive one (r = 0.45) is between Na and SNP for the Maastrichtian samples.

As an example, grouping of data is observed for Na vs. DT (Fig. 32) where the Danian data are split into 2 groups with perhaps further subdivision into two subgroups, the one with the lowest DT clearly being confined to the oldest Danian. A similar tendency is observed for Na vs. RHOB (not plotted).

Correlation analysis of Fe contents vs. log depth for drill hole E-lx data shows that only the combinations with the SN and the IL log give positive correlation coefficients above 0.4 for the Danian. When plotting the data (not shown in Fig. 32) for these two combinations, however, it is obvious that the correlation is an artefact because Fe content varies only little.

Correlation data of Mn vs. log parameters suggest that there is no significant correlation for the Danian samples while the few data for RHOB, SP, SN, IL, LL, MINV, and MNOR all give correlation coefficients with Mn that exceed 0.8.

The selected plots of data (e.g. DT vs. Mn and RHOB vs. Mn, Fig. 32) show the normal trend, namely grouping of data.

### 4.2.5 Multivariate Statistical Analysis

The results of R-mode factor analysis of analytical data for drill core samples from well E-lx are plotted in Fig. 33.

Although only a limited data set is used, it appears that the geochemical drill core data separate the different reservoir rock units and also that the Maastrichtian strata are clearly separated using geochemical data alone. In addition, the thin oil-bearing zone on top of the Danian (unit UDPI) may also be separated through factor analysis of geochemical data.

Fig. 33. Factor score plot of factors 1 and 2 for R-mode factor analysis of data from E-1x.



# 5. Discussions

# **5.1 General Considerations**

General discussions of the data used in the present investigation should comment on their validity and quality before they are used for final interpretational purposes.

The geochemical data were generated from drill cores influenced by chemical and physical processes produced by the drilling operations; these operations were followed by geophysical sensing (well logging) in which measurements are made on rock formations influenced by the drilling.

# 5.1.1 Well Logging Considerations

In the evaluation of oil and gas reservoirs, a number of well-logging techniques are used which are important to be observed. It is not possible, however, to discuss these techniques in more detail within the framework of the present investigation. Only some pertinent observations are presented in the following.

While porosity usually is determined by the sonic log, the formation density log or the neutron log, for estimates of water saturation and hydrocarbon saturation electrical logs are preferred (resistivity logs).

As mentioned above, in interpretating in well logging it is very important to consider the processes involved in the drilling operations. Drilling is carried out using drilling fluids leading to the establishment of distinct influence zones around the drill hole (Fig. 34). All the logging results have to consider some sort of influence spacing within and around the drill hole, into

- 1. Mud cake with hmc thickness
- 2. Flushed zone
- 3. Transition zone
- 4. Undisturbed zone.

Fig. 34. Schematic drill hole representation showing three major zones of influence by the drilling operations.



Generally, the mud cake zone with a thickness often varying between . and about 20 mm has a moderate resistivity, while the flushed zone contains both .nud and oil or gas (if present). In the transition zone, both mud and formation fluids may be present grading into the undisturbed zone which also has, e.g., the true resistivity. It is often the case that formations with high porosities have the lowest invasion depths; mud filtrate, during its penetration into the formation, in unfavourable cases may seal the formation. General figures for an inversion depth (mud cake thickness + flushed zone thickness + transition zone thickness) are less than 1' in formations with high porosity, while for low-porosity formations these depths may increase to up to 10'.

There are some basic equations connected with the different well logging tools; these are not discussed here, however.

A number of standard log interpretational methods are known leading to the determination of the important parameters porosity  $(\emptyset)$ , water saturation  $(S_w)$ , and permeability  $(k_a)$ . Interpretational methods including standard and cross plot techniques have been described in some detail by Helander (1983) and need not be repeated here. Of some importance in this respect, however, are so-called »quick-look« methods combining a number of logs to determine the important parameters.

### 5.1.2 Drill Core Investigations

Other important information about the hydrocarbon reservoir is generally gained by the investigation of drill cores. However, as coring is much more expensive than plain drilling, only a few wells are cored throughout.

There are some problems connected with the collection and evaluation of measurements on drill cores. These have to be considered when discussing analyses of drill cores. Processes that influence the core material are:

- 1. Ahead-flushing of rocks by drilling fluids,
- 2 Pressure alterations of the core, and
- 3. Temperature alterations of the core.

Flushing generally reduces the hydrocarbon content in the core at the same time increasing its water content. Flushing influence is less pronounced, however, in the drill cores because the core usually is removed immediately after it has been cut and protected largely by the coring rods. Pressure and temperature influences may alter values of core porosity, permeability and resistivities in that they often alter the primary structures within the rock by subsequent stress variations in the core. There is little alteration of the geochemistry of the core, but samples for chemical analyses should always be taken within the core and not from its marginal regions because of possible surface contamination by drilling mud.

As regards core analysis, whole-cores, plugs or sidewall cores may be used. Determinations on cores result in data on core porosity, permeability, and residual fluid saturation; these, however, need the removal of residual fluids in the core samples mainly by solvent extraction.

The most important core measurements are those of porosity which include estimates of bulk volume, pore volume, and grain volume. Permeability in terms of vertical and horizontal values may be determined based on the use of liquid or air flows. A number of other measurements are usually carried out on cores.

# 5.2 The Well-Logging Results

As already mentioned, the petrophysical parameters porosity, water saturation, and permeability of the reservoir are usually estimated from the geophysical measurements, i.e. from well logging.

The logging data from both wells alone could be used to evaluate some parameters closely related to chemical properties of the reservoir rocks. There is some problem in comparing the data because logging of the wells was established with different tools at different times and comparison is therefore difficult. However, if we choose some of the physical tools that are comparable, e.g., all the electrical tools, the radioactivity measurements and the sonic results, comparison by multivariate statistics (R-mode factor analysis) including data on both wells may be carried out. Average data are given in Table 11.

Results of this comparison by using all available data (those ascribed to core-sampling depths) for Danian and Maastrichtian units are plotted in Fig. 35.

It appears from the figure that at least for drill hole TWB-8 (left side of Fig. 35) the data is separated according to geology and also to hydrocarbon occurrences but this separation is not evident at drill hole E-1x. Also, the reduction in reservoir quality as seen in units UDT and upper part of LDP (well TWB-8) is, although separated, not clearly displayed through the figure.

Formation	SFLA/ MNOR	GR	ILD/ IL	DT	RHOB	NPHI/ SNP	SP
UDP1 (TWB-8)	7.8	7.1	26.0 <b>*</b>	146	1.75	0.29	236
UDP1 (E-1x)	1.3	12.6	1.1	107	2.13	0.33	11
UDP2 (TWB-8)	4.4	6.9	21.0	127	1.79	0.30	221
UDP2 (E-1x)	0.8	11.7	0.7	108	2.08	0.38	4
LDP (TWB-8)	2.5	7.9	8.0	118	1.93	0.30	200
LDP (E-1x)	1.1	11.5	0.9	103	2.12	0.35	10
UDT (TWB-8)	2.1	9.0	6.0	101	2.17	0.27	199
UDT (E-1x)	2.2	12.8	2.2	83	2.30	0.25	22
LDT1 (TWB-8)	2.5	8.3	9.0	118	1.99	0.28	200
LDT1 (E-1x)	1.7	11.4	1.4	92	2.21	0.31	15
LDT2 (TWB-8)	4.5	8.5	20.0	115	1.99	0.28	222
LDT2 (E-1x)	1.8	12.4	1.5	93	2.25	0.27	20
1M (TWB-8)	5.0	8.4	14.0	132	1.95	0,24	235
1M (E-1x)	2.0	11.1	1.6	87	2.30	0.27	12
2M (TWB-8)	3.9	8.2	27.0 <b>*</b>	139	1.83	0.33	223
2M (E-1x)	1.3	10.5	1.0	93	2.17	0.32	7

Table 11. Average well-logging data for drill holes TWB-8 and E-1x.

\* one value ILD = 2000 (error ?) excluded in average calculations



Fig. 35. R-mode factor analysis of logging data from TWB-8 and E-lx.

It appears from the figure that at least for drill hole TWB-8 (left side of Fig. 35) the data is separated according to geology and also to hydrocarbon occurrences but this separation is not evident at drill hole E-lx. Also, the reduction in reservoir quality as seen in units UDT and upper part of LDP (well TWB-8) is, although separated, not clearly displayed through the figure.

# 5.3 The Geochemistry

The geochemical databases for drill core sections of the two Tyra wells differ because they were constructed from analyses using various analytical strategies. Because a relatively large number of both major and trace elements in the carbonate rocks were determined, these data are sufficient to describe geochemically the different geological units involved.

From the average analytical data of the different rock units for both drill cores, characterization plots can be constructed showing the differing reservoir unit geochemistry (Fig. 36). The average data matrix for TWB-8 (Table 12) was built up from the the additional data (see chapter 4.1.2.3), which unfortunately lacks the analysis for unit LDT2.

Table 12. Average analytical data for drill cores TWB-8 and E-lx.

Formation	Na	Ca	fe	Sc	Cr	Co	Br	Sr	Cs	Ba	Hf	Th	La	Ce	Sm	Eu	YЬ
UDP1 (TW8-8)	0.10	32.4	2170	1.1	6.0	1.7	8.3	983	0.1	171	0.11	0.5	8.8	6.6	1.9	0.34	0.7
UDP1 (E-1x)	0.28	33.4	5375	2.2	6.6	3.3	34.5	1425	0.2	294	0.20	0.8	11.5	17.8	2.5	0.50	1.1
UDP2 (TW8-8)	0.09	33.6	936	1.2	5.7	1.7	8.2	987	0.1	142	0.10	0.4	10.6	8.4	2.4	0 42	07
UDP2 (E-1x)	0.21	34.6	2440	2.0	5.5	2.7	30.9	1492	0.2	143	0.14	0.6	11.2	15.1	2.6	0.50	1.1
LPP (TWB-8)	0.11	32.9	1667	1.9	6.5	3.3	9.9	1042	0.2	158	0 17	0 9	15.0	11.5		0 64	1 0
LDP (E-1x)	0.18	31.2	2309	2.3	4.7	6.0	36.0	1295	0.2	182	0.18	1.2	12.4	18.6	3.6	0.62	1.1
UDT (TNB-8)	0.10	29.6	3260	2.8	8.5	15.7	8.5	1110	0. J	2120	0.27	16	15 4	18.4	36	0 64	1 2
UDT (E-1x)	0.20	27.6	4633	3.8	6.1	10.4	16.3	1265	0.2	249	0.28	2.3	16.3	30.1	5.0	0.82	1.5
LDT1 (TWB-8)	0.16	27.9	4230	3.1	8.4	8.0	12.1	1021	0.3	654	0.31	1.9	19.0	23.2	5.0	0.82	1.2
LDT1 (E-1x)	0.21	29.7	3800	3.0	11.1	12.3	22.8	1496	0.2	167	0.24	1.8	17.1	26.6	4.9	0.84	1.5
LDT2 (TWB-8)	0.00	0.0	0	0.0	0.0	0.0	0.0	0	0.0	0	0.00	0.0	0.0	0.0	0.0	0.00	0.0
LDT2 (E-1x)	0.18	28.7	3757	3.0	11.7	9.9	17.8	1664	0.2	172	0.24	2.0	16.1	28.3	4.6	0.84	1.4
1M (TWB-8)	0.13	20.2	3000	1.9	7.0	3.5	8.1	891	0.1	1370	0.18	1.1	11.3	14.9	3.7	0.55	0.9
1M (E-1x)	0.11	38.5	850	1.5	9.7	1.5	15.7	1673	0.1	90	0.10	0.3	9.0	9.7	2.4	0.38	1.0
2M (TWB-8)	0.16	35.6	785	0.7	3.9	2.9	18.6	1202	0.1	187	0.06	0.2	7.7	5.2	1.7	0.27	0.5
2M (E-1x)	0.14	38.6	700	0.8	9.9	1.6	23.5	1813	0.1	104	0.10	0.2	7.5	7.0	1.9	0.30	0.8

For the average chemical data, there is a relatively clear grouping in Fig. 36 showing that chemical data of comparable reservoir units from the two wells often plot close to each other. For instance, in the Mn-Al-Ca plot, data from TWB-8 (large symbols) plot close to data from E-lx (small symbols). This indicates that the rocks from both drill cores are similar geochemically and that variation generally occurs between the reservoir units. To illustrate the latter observation, we note that the position of the points UDT is quite different than, e.g., that for 2M.

On the other hand, knowing that there is core porosity reduction in unit UDT in the respective core section of TWB-8 (reduction from 40 to less than 20%) but not as clearly developed in core E-lx, the plots in Fig. 36, therefore, give no strong indication of reservoir quality reduction. As a consequence, the reservoir quality variations must be sought merely in the chemical diagenetic changes usually not expressed through the bulk chemistry.

The average data for the two wells (logging and geochemical results) may be combined into a final multivariate statistical analysis to evaluate possible trends within the Tyra structure. The results of R-mode factor analysis are shown in Fig. 37.

The data in Fig. 37 (right plots) show a separation of drill holes. Perhaps subgrouping is also seen showing decreased reservoir quality (mainly units UDT and LDT1).



Fig. 36. Selected characterization plots for drill cores TWB-8 and E-lx.



Fig. 37. Average data for chalk units combined in R-mode factor analysis. Left: logging data alone, right: all data.

# 5.4 Considerations for the Tyra Field Reservoir Quality

# 5.4.1 General Considerations

Reservoir quality measures are tightly coupled to the processes applied to sedimentary basin evolution. For chalk, diagenetic considerations have been discussed in greater detail by, e.g., Sippel and Glover, 1964, Neugebauer, 1973; 1974, Håkansson et al., 1974, Mapstone, 1975, Scholle, 1977, and Hardman, 1982, and some of the features of chalk diagenesis have been discussed in general terms in chapter 1.

Of these, the comprehended work of *Scholle* (1977) may provide a good background to discuss the chemical data generated during the present investigation. He mentions that chalk diagenesis may be divided into early diagenesis and burial diagenesis.

The early stages of diagenesis consist of relatively simple processes in which dewatering of the calcareous sediment through compactional features is mainly dominant. In reality however, early processes may be much more complex involving chemical graduation of the calcareous shells as well; the most important of these processes is the enforcement of shell structures leading to an improvement in rigidity of the sediment. Common features generated during early diagenesis are carbonate cements and replacement glauconites and phosphates. A distinct product of near-surface cementation are hardgrounds (connected with erosional surfaces) having considerably reduced porosities (O < 20%) and occurring within otherwise porous chalks with porosities exceeding 30%.

A significant feature of chalk is its low initial permeability. This prevents the penetration of meteoric water into chalk. As a result, meteoric water can migrate only along bedding planes or created chalk surfaces such as undulating surfaces. According to Scholle (1977), the only way to alter porosity in chalks is by burial. This view, however, is oversimplified and does not explain local porosity variations within chalk reservoirs. As a consequence, Scholle (1977) suggests pressure solution processes that progress with depth, the solutions being preferably transferred via thin clay seams. Such processes lead to carbonate cementation, i.e. porosity deterioration. That these processes were active in chalk is confirmed by the occurrence of solution seams visible on a macro scale, predominantly connected with chalk layers showing increased clay content.

Most of the previously reported geochemical work on chalk is based on stable isotopes and includes only a few major and minor elements. Generally the work is based on relatively few chemical analyses despite generally large size of the sedimentary basins on which conclusions were made. A significant observation is  $\delta O18$  values decrease with depth in chalk, i.e. with porosity. For North Sea chalk it is reported that the deepest chalks have the highest Sr and Mg but most chalk samples from the Deep Sea Drilling Project showed a decrease of Sr with depth of burial.

For the hydrocarbon deposits of the North Sea, where the reservoirs are located at depths of 2 to 3 thousand meters, chalk porosities are often above 30%, although burial diagenesis predicts lower values. *Scholle* (1977) reports porosities for oil-producing Danian and Maastrichtian chalks to be on average between 20 and 30%, but locally significantly higher values are observed. Permeability is very rarely higher than 3 mD. These contradictory features (e.g. high porosity at large burial depth) are at present explained by overpressurizing, both in the sealing rocks (Tertiary shales) and in the reservoir chalks themselves. However, there is also some evidence that oil migration into the chalks occurred during relatively early burial stages, thereby preventing porosity deterioration at later burial.

Basin evolution studies were recently also applied to sandstone diagenesis and porosity modifications by *Bjørlykke* et al. (1989). It is worthwhile to review their findings briefly because, in general, they apply also to carbonate rocks.

Referring to earlier geochemical and isotopic investigations on circulating water in the reservoirs, the authors point to the importance of water stratification merely than to upward flow; meteoric water is thought to penetrate the reservoir on a horizontal more than a vertical scale. Flow rates of meteoric water are estimated to be higher than compactional water flow and therefore the reservoir is generally more heavily influenced by meteoric water. Mixing processes (meteoric/seawater) especially lead to enhanced corrosion of carbonate minerals.

- Curbonate cement development in siliclastic sedimentary rocks has been studied by stable isotopes. Accordingly, early carbonate cements in sandstone reservoirs were found to have  $\delta^{13}C$  values close to zero but cements that precipitate under the influence of meteoric water (early diagenesis) are characterized by negative  $\delta^{13}C$  values.
- Silica cements in these rocks, on the other hand, are generally confined to the deeper burial stages (pressure solutions, stylolitization). Another possibility for silica diagenesis is probably convective pore water flow but few investigations exist on this topic.
- Clay minerals may be converted into other species during burial. The authors suggest that clay diagenesis may continue after hydrocarbon emplacement.

Bjørlykke et al. (1989) also discuss secondary porosity and its change with depth of burial in a sedimentary basin, in general. Porosity alteration is thought to be obtained by slightly acid pore fluids and such processes are best described under the heading chemical diagenesis. Important in this respect is the generally valid observation that porosity in siliclastic sedimentary rocks decreases with depth of burial. At the same time, as the temperature increases chemical processes are also enhanced with depth of burial. After burial and during the course of subsiding, sediment porosity is altered by mainly three processes:

- mechanical compaction: fragile mineral grains due to pressure may be re-orientated or destructed leading to reduced porosity;
- chemical compaction: mineral grain dissolution at grain contacts are usually dominant at burial depths exceeding 2 km (pressure solutions);
- cementation: precipitation of authigenic minerals principally related to chemical compaction;

Regarding carbonate cements, oxygen isotope measurements of samples from arkosic sandstones show that the earliest carbonate cement is a dolomite usually forming at temperatures of 30 to 40° C (*Boles and Ramseyer*), while calcite cement formation is observed at 50-60 and also at 70-80° C, the latter is caused mainly by plagioclase replacement. Also, a (Fe + Mn)/Mg ratio of ca. 3 is characteristic for the calcite cements; most importantly, Mn is very high in nonmarine sections with calcites. Porosity enhancement in the reservoir is obtained by the dissolution of plagioclase leading to Al enrichment. In general, these authors point to the importance of cement growth in single reservoirs.

### 5.4.2 Tyra Field Reservoir Quality and Chemistry

Based on the geophysical and geochemical results of the present study, a number of observations can be deduced. These observations explain in part why there are local reservoir quality variations and also why the reservoir quality in the marginal parts of the structure are generally poorer, although the results from no more than two drill holes are not ideally suited for making general evaluations on the structure.

For comparison, the petrophysical parameters porosity (POR), bulk density (RHOB), permeability (PERM) and neutron porosity (NPHI) are plotted in Fig. 40.



Fig. 38. Average petrophysical parameters plotted against each other. (For symbols see Fig. 37)

# 5.4.2.1 The Bulk Chemistry

The bulk chemistry of chalk from the central part of the Tyra structure (TWB-8) has already been shown through the multivariate statistical attempts (see Chapter 5.3) to differ only slightly from the easternmost margin (E-lx). There is therefore only a weak indication through the bulk chemical data that chemistry is producing large-scale reservoir quality variations. A systematic chemical analysis of Tyra reservoir chalk samples including such a large number of major, minor, and trace elements is however new and has no counterpart in the recent literature. Therefore, chemical variations with depth and on a regional scale (central to marginal parts of a chalk structure) are at present unique findings.

Fig. 39. Average Ca content plotted vs. porosity.



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### 5.4.2.1.1 Major Elements

By systematic evaluation of the chemical data it becomes clear that there are some chemical graduations of the reservoir chalk. For chalk composed of more than 80% of calcitic material only one major element has to be considered, namely Ca. Two observations are apparent through our data. Firstly, there is a significantly lower Ca content in the middle part of the of the central Danian TWB-8 section (reservoir units UDT and LDTI). This is unobserved in E-lx lying in the marginal part. Secondly, Ca contents in general are higher in the Maastrichtian strata. The Ca reduction in the middle part of the Danian TWB-8 section is closely related to Si and this is discussed in the section on Si diagenesis.

Although there are some outliers, it is apparent in the plot of average porosity values against Ca (Fig. 39) that porosity in the Tyra rocks generally increases with increasing Ca content, i.e. all high-porosity reservoir rocks of TWB-8 have high Ca content. In contrast, E-lx reservoir units are characterized by significantly lower Ca.

### 5.4.2.1.2 Minor Elements

Of the minor elements, Al contents are generally lower in Maastrichtian drill core material from both wells. Such graduations must be ascribed mainly to occurrences of clay minerals, although bulk Al contents still are low, on average below 1000 ppm. As a unique feature of TWB-8, Ca reduction goes along with an increase of Al (and other elements) at the Danian section, leading to an Al content of more than 8000 ppm in the lowest sample of section UDT. Such increases in Al in carbonate rocks are usually interpreted as clay supply during quieter depositional stages.

The plot of average Al vs. prorosity (Fig. 40) shows no clear trend and therefore clay is regarded to be of minor importance in porosity reduction in the Tyra chalks.

Fig. 40. Average Al and Fe contents plotted vs. porosity.



Sodium contents in the chalks can be interpreted as an expression of the presence of marine waters in the pore spaces; they precipitate in the form of NaCl after the samples are dried. Although it is very difficult to interpret Na on a more regional scale, the general observation is that due to the presence of hydrocarbons, sodium content is significantly lower (about 1000 ppm) in the respective TWB-8 section when compared to the hydrocarbon-free E-lx section (about 2000 ppm). Because Na significantly decreases above the OWC for TWB-8, the distribution with depth (see Fig. 7) clearly marks both the oil-water contact (OWC) and the gas-oil contact (GOC) (further reduction in Na to a plateau value).

Strontium is the minor element that has been studied most intensively in carbonate rocks. The reasons for this are primarily its geochemical affinity to Ca and its occurrence, usually at the 1000 ppm level in ancient carbonate rocks, thereby being more readily determined. During dissolution of Ca minerals or Ca mineral phases Sr may be fractionated, generally entering the solute phase and being transported to precipitation centers, even at large distances. The Sr distribution trends with depth for both wells are similar, the highest Sr content being found in the Maastrichtian rocks. There is therefore little evidence of reservoir quality changes by chemical processes involving Sr diagenesis.

Iron is an important minor element in carbonate rocks and found mainly when carbonate dissolution locally leads to pH reduction. In such cases, pyrite precipitation may occur in the course of carbonate diagenesis, as for example when the chalk of the Tyra field becomes evident because of macroscopically visible pyrite grains within otherwise homogeneous chalk occur and the Fe content in chalk samples increase (see Figs. 12 and 26). Comparing average Fe data with porosity values for the two wells (Fig. 40), it becomes obvious that reduced porosity goes along with elevated Fe contents.

Manganese and silicon are discussed separately.

### 5.4.2.1.3 Trace Elements

Of the trace elements, more than 20 different ones have been determined in the chalk samples. The trace element distributions with depth not only support some observations for major and minor elements, but they also add significantly to the general geochemical information on carbonate reservoir rocks. We have divided them into groups of trace elements with some geochemical similarity and discuss obvious features in their distribution with depth within the different groups.

### Sc, Br, Rb, Ba, and Hf.

Scandium is usually confined to the clay fraction, and in this respect it should follow Al closely. When the depth distributions of the element for both drill cores are compared (Figs. 12 and Fig. 26), it becomes clear that the Sc distribution in core TWB-8 does indeed follow that of Al (Fig. 7). For this drill core also, there is an increase in Sc values from section LDT to 1M. It is important to mention that, as was the case for Al, scandium values are generally higher in drill core E-lx; we therefore also point out that there is more clay in the carbonate sections. The comparison of average Sc data with porosity values (Fig. 41) indicate that chalks from the Tyra structure with relatively low porosity all show Sc contents greater than 2 ppm.

Bromine is a standard trace element determined by INAA. It is closely related to chlorine in the carbonates, i.e. to the content of formation waters. It therefore also follows the distribution trend of Na already discussed, showing



Fig. 41. Average Sc content plotted vs. porosity.

a general increase with depth in drill core TWB-8. While Br values in this core are usually at 10 ppm and exceed 20 ppm only in the Maastrichtian section, in drill core E-lx, Br values throughout are higher than 20 ppm with a slight tendency to decrease with depth. This behaviour is an indication of the absence of hydrocarbon in the marginal well E-lx.

The content of Rb, which often is associated with K thereby expressing the amount of feldspar in the rock samples, is very low, generally at or below 10 ppm. It is therefore not an important trace element in the Tyra carbonate rocks.

Barium content is important when studying drill core sections from the Tyra gas field. Firstly, Ba is often connected with marine phases (baryte, phosphates). Secondly, high Ba contents in core samples from hydrocarbon exploration wells are usually identified with the contamination of core samples by drilling fluids which often contain additives in the form of baryte. After comparing all the available data, we find perhaps a slight Ba contamination in two additional samples from drill core TWB-8 (Fig. 12) but the Ba values are generally low and at an expected level.

Hafnium which geochemically is closely related to Zr can be taken as an expression of the residual (clay) fraction in chalk. The element often follows Sc, and similar trends are therefore also valid for Hf.

# Cr, Co, Zn, As, and Sb

Of these five trace metals, Cr is expected to be entirely connected with the residual fraction in the chalks. If there were heavy mineral horizons in the carbonates they would evident, among others, through high Cr contents. However, Cr values in general are very low (< 10 ppm), and even the high-Al section of TWB-8 is found to be only 10 ppm. Comparing the depth distribution of Cr in E-lx, there is a significant increase in Cr in samples below chalk unit UDT (jump from 5 to 10 ppm Cr, Fig. 26).

Cobalt - which in the marine environment may be connected with both a biogenic phase or phases directly precipitated from seawater - is often connected with Fe. Therefore, the depth distribution for Co in both investigated drill cores closely follows that of Fe. The same tendency is seen for zinc, but because of the generally very low Zn content, other analytical tools probably have to be applied to determine it.

Arsenic and antimony are of little importance in carbonate sediments. They are geochemically connected with hydrothermal processes and because or one very low content in the chalk samples such influences are regarded as hypothetical.

# Radioactive elements

Of the radioactive elements, uranium is often involved in diagenetic changes in sedimentary rocks, while thorium is generally connected with the residual phases. It is quite clear from Figs. 7, 13 and 27 that the Danian strata of both drill cores have the lowest U content, usually not exceeding 0.2 ppm. Uranium content is higher in the uppermost Maastrichtian chalks; values being generally above 0.5 ppm U are found in samples from both drill cores. In this respect, the U distribution with depth clearly defines the transition of Maastrichtian to Danian strata. In contrast to U, thorium normally connected with the residual phase shows a similar distribution patterns with depth as, e.g., Al.

The plot of average data for the two wells vs. porosity (Fig. 42) shows that at reduced porosity Th values are elevated, while there is no linear dependency between U and porosity.

# Fig. 42. Average U and Th contents plotted vs. porosity.



### Rare earth elements

On comparing the REE distributions of the two drill cores with depth, no clear change in content of REE with depth seems to be present. When the Ce/La ratios of the chalks of both wells are compared it appears, however, that Danian strata have generally higher ratios. On the other hand, on a regional basis (central to marginal part) there is no graduation between values for TWB-8 and E-lx.

If we take the Ce/La ratio as an expression for the depositional environment (fractionation of Ce in an oxidizing environment), it could be argued that deposition during Danian times took place in a more oxidized milieu (higher Ce/La ratios) compared with the Upper Maastrichtian. The ratio also suggests that the depositional environment at the end of the Cretaceous was altered.

According to Jarvis (1984) who investigated Late Cretaceous chalks from northern France, the REE in the chalks are mainly confined to carbonate fluorapatite and sometimes to iron phases. The highest REE contents are generally found in hardgrounds. The process favoured for REE accumulation from seawater is via settling of ferric hydroxide coatings and sinks. This would explain the similar depth distribution trends for Fe and the REE in the Tyra field samples.

#### 5.4.2.2 Si Diagenesis

The sample descriptions for TWB-8 (Appendix I) document the presence of flint layers and hardened chalk horizons in chalk unit LDP grading into obviously silicified chalk (units LDTI and LDT2) sections. This variation is expressed logically by the petrophysical parameters and by the variation of reservoir quality.

The diagenesis of silica in marine sediments has been described in general terms by *Calvert* (1974). Accordingly, most profiles of dissolved silicon in marine sediments show a concentration gradient towards the sediment-seawater interface suggesting a flux of dissolved silicon into the overlying water column. The reason for this is that biogeneous silica in marine sediments usually is not stable even at low temperatures. One consequence is the formation of chert and porcellanites in marine sediments. Most investigations suggest a relatively slow conversion process of biogeneous debris via some transitional products finally into quartz. Submarine hydrothermal activity may add to the silica supply mechanism on the ocean floor.

Early investigations by Lovering and Patten (1962) including simple experiments showed that cold neutral solutions supersaturated with silica were able to move over long distances in carbonate rocks. At contact with them they generate  $CO_2$  or Na; silica would precipitate in turn.

It is also known that dissolved silica in surface sediments reacts with poorly crystalline Fe-Mn oxyhydroxides generating both the mineral todorokite and Fe-rich smecite. Such a process could also be invoked to explain the Si-enrichment which, in the Tyra reservoir rocks, often is coupled to Al and Fe.

After analysing selected samples from TWB-8 for Si, we founds especially high Si values in chalk sections UDT and LDT1 (Fig. 43). These Si values are 3 to 4 times higher than in the other hydrocarbon-bearing chalk units. They correlate closely with Al (Fig. 8) and Fe (Fig. 12) suggesting that dissolved silica was precipitated from silica-bearing solutions at clay horizons, thereby further reducing core porosity.

A similar pattern for Si is also observed in drill core E-lx (not plotted).



Fig. 43. Si distribution along drill core TWB-8 showing elevated contents in Danian strata.

Average Si data for the reservoir units of wells TWB-8 and E-1x are plotted vs. porosity and permeability in Fig. 44. It appears from the figure that most of the high-porosity reservoir units are characterized by Si contents below about 6% (about 13% SiO<sub>2</sub>). If we exclude the E-1x Maastrichtian data, we deduce the following empirical equation:

 $rosity(\%) = -1.35 \times Si (weight \%) + 44.2$ 

i.e. a Si content of 1% in the Tyra chalk decreases porosity by a relative amount of about 3%.

While porosity and Si values consider the uppermost 2 reservoir units of E-lx as of good reservoir quality, permeability figures are significant lower than the comparable ones of TWB-8; generally, permeability values of E-lx are low, even at widely varying Si. This suggests that reservoir quality is influenced not only by the altitude of some geochemical indicators (e.g. Si, Al, Fe), but also by physical parameters (e.g. texture).

### 5.4.2.3 Mn Diagenesis

The most pronounced geochemical feature of the Tyra structure (and the Upper Cretaceous and Lower Paleocene chalk deposits in general) is the distribution of manganese. The distributions with depths in drill cores TWB-8 and E-lx are quite similar (Figs. 7 and 26) although the analytical results for both cores were obtained by two different analytical methods.



Fig. 44. Average Si data plotted vs. porosity and permeability.

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Fig. 45. Average Mn contents plotted vs. porosity.

A number of possible mechanisms explaining the Mn behaviour in the chalk samples has been discussed by *Kunzendorf* et al. (1985). However, as this behaviour is unique for Upper Cretaceous and Danian chalk, it is very likely that Mn occurrences in the chalk deposits are an important expression for the paleoenvironment. Because there is little correlation of Mn content with reservoir quality parameters, e.g. porosity (Fig. 45), Mn behaviour with depth is discussed only briefly within the present investigation.

Plots of detailed and smoothed data in Fig. 46 from drill core TWB-8 show the following trend:

- reservoir units 5M, 4M and 3M are characterized by relatively low Mn (< 200 ppm);</li>
- from the lowermost portion of 2M onwards, Mn values increase linearly to about 400 ppm at the transition to 1M; there is no further Mn increase in 1M;
- Dania chalks all have higher Mn contents than the Maastrichtian strata;
- from the bottom of unit LDT2 there is an upwards increase of Mn contents (from about 600 to 750 ppm) until unit LDP;
- in unit LDP, Mn contents increase from about 750 to about 1500 ppm;
- There is a further linear upwards increase of Mn contents through the uppermost Danian chalks.

The upwards increase of Mn contents has also been found mainly in drilling muds and some drill core material from other wells (e.g., *Jørgensen*, 1986). Besides the possibility of paleoenvironmental influences, such features in general could also be an expression of hydrocarbon invasion and hence be important for the development and retention of reservoir pressure. Because the behaviour of Mn is unique for Danian-Maastrichtian strata of the entire Danish Subbasin, more detailed studies are required to explain, on a fine scale, the geochemical observation.


Fig. 46. Manganese distribution with depth in TWB-8. Left part of the figure shows raw data while the right part gives 5-point averages.

### 5.4.2.4 Regional Geochemical Interpolations

The geochemical data for both drill core may be used in geochemical contouring within the Tyra structure. The most appropriate software to use is the UNIRAS system. The chemical data for the two drill cores were used in the computer manipulations. Because of the relatively large extension between the two drill holes (about 7 km), such efforts are not very meaningful, especially in the absence of any limiting constraint. They are shown here, however, to draw attention to the possibilities of 3-D geochemical mapping.

By introducing fault lines such as, e.g., unit boundaries Top Danian I, Top Maastrichtian 1 and Top Maastrichtian 2, Fig. 47 shows 2-D plots for elements Ca, Al, Na and Mn. Including another well between TWB-8 and E-1x in the investigations, interpolations of geochemical data sets would be more meaningful. SECTION 1

Profile: TWB8 E1- along azimuth 80









Fig. 47. UNIRAS contouring of geochemical data for Ca, Al, Na and Mn of the two wells using stratigraphical borders as contouring fault lines.

I.

# 6. Conclusions

Detailed analytical investigations on drill core samples from two wells of the gas-producing Tyra structure, combined with evaluation of geophysical data in the form of well-logs leads us to conclude the following in connection with reservoir quality variations.

Well logging predicts high porosity chalks for both the central (TWB-8) and marginal parts (E-lx) of the Tyra structure. Permeability values are significantly reduced in the marginal well. The Danian section of TWB-8, in its middle part (units LDP and UDT), shows core porosity reduction down to less than 20% but increases again in the Maastrichtian strata. A similar reduction (start at unit UDT) is observed in the respective section of E-lx, but high porosity is not achieved again in the uppermost Maastrichtian section (1M and 2M). Such features are registered by the geophysical tools but difficult to explain by logging data alone.

The distribution of the major element Ca with depth in both drill cores is similar: contents are generally between 30 and 35%, the higher figures being generally connected with the Maastrichtian strata. The reduced-porosity section of core TWB-8 accordingly shows reduced Ca content.

Important for outlining reservoir quality variations regionally and on a local scale are chemical changes (diagensis) in the chalk induced by minor elements Si, Al, Na and Mn.

Silicon diagenesis is the most important chemical alteration process of the Tyra field reservoir rocks. Visible on a macro scale by chert formation (nodules and layers), it is also observed to act on a smaller scale. In the form of coatings and impregnations, Si diagensis initiates pore space reduction (porosity loss) and permeability is also altered due to different flow characteristics of Si-coated grains.

The Danian Tyra reservoir chalks from the central part of the structure (TWB-8) through the analytical data (up to 16% Si) show that silicification in units LDP and UDT must be responsible for a reduction of core porosity. Other chemical data also suggest that this diagenetical stage goes along with Al and Fe enrichment in the chalks, probably through the emplacement of smectite. Chalk reservoir degradation caused by Si diagenesis can therefore also be monitored through Al and to some extent also through Fe distributions. Locally, secondary Fe may also be generated by carbonate mineral diagenesis leading to pyrite formation.

Sodium and chlorine contents in the reservoir chalks are generally connected with formation waters and could be an indication of water saturation figures. In this respect, oil-bearing drill core sections are outlined through their lowered Na and Cl contents. However, care has to be taken in the interpretation because of possible contamination through drill fluids.

The most significant geochemical feature of the Tyra reservoir rocks is the distribution of Mn with depth overprinting all other observed chemical distributions, i.e. Mn is not connected with any of the other major, minor or trace elements in the chalks. The phenomenon is unique, and viewing the Mn analyses on a relatively large scale (tens of cm) leads to a steadily upwards increasing Mn distribution for both investigated drill core sections. In this respect, the Mn distribution could be related to the paleoenvironment or to a large-scale diagenetic feature, but other, yet unknown explanations could be introduced. Detailed studies are necessar, to outline the behaviour of Mn in the Tyra chalks and the chalks of the Danish subbasin.

Trace elements in chalk can be clearly coupled to appropriate major and minor elements, minerals, or mineral phases. In this respect, some of the trace element distributions could be used instead of major and minor elements to outline changes in the reservoir rocks. For instance, the trace element Sc usually follows closely the distribution observed for Si and Al. For carbonate rocks some of the traces indicate that environmental changes have taken place such as metals connected with residual minerals (heavy mineral horizons).

A special group to be investigated in chalk samples are the rare earth elements, which through their distribution pattern and distribution with depth may outline changes in redox conditions within the sediments (e.g. through the ratio Ce/La) and/or fractionation trends during their precipitation from seawater (ratio of light to heavy REE).

A detailed outline of the inorganic geochemistry and the establishment of 3-D geochemical maps of the Tyra structure requires a more detailed sampling and analysis program from more than only two wells. By taking into account the recent availability of quick analytical methods, this could be facilitated within a reasonable time span.

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# **APPENDIX I**

### **Brief Description of Samples from TWB-8**

6653' LOTZ Silicified chalk showing significant bedding on a 40-cm scale;

Depth	Unit	Remorks	Depth	Uni t	Reserves
6592'2'' 6594'	UD#1 UD#1	No comments Very parous: 6			remaining accurrances support badding on a 3 to 5 cm scale. relatively fee pattern-chait structures, essentially only in one 10 cm thick band; the whole core section shows a crenulated mermistratich lamination.
6597 6599 -	UOPI	No visible structures; porous. Similar to above	6655 6 6657 10	LOT2	Core bas contains gray chert layers. The top of the core bas contains homogeneous chalk with bedding
6601	U071	Top section of the core shows dense anastomosed, healed small fractures which in almost all cases are vertical to the murl			characteristics as described above; below this are there strong track (40 cm long) that crusses three silicified merly bands
6602	U <b>0</b> P1	ianinae. sample is relatively homogeneous with shama of pattern chalk structures. Relatively homogeneous pattern chaik structure sample;	5650°5''	1072	pattern-cholk structures which partly occur close to a vertical Mard, silicified (dissiminated) chelk with pattern-chalk structure; weak 20-ge badding with very low marl content.
6609'9''	10001	Coarse, homogeneous matrix with few healed small fractures; soft chalk (gas?). Relatively homonomous sample (uncleastern?), simple	6663 7 **	1072	<ul> <li>Game beau with 3 silica-rich marly layers (50 to 40 cm distance between layers); Very strong pattern-chalk structure, especially in the between of the case, here, there is a crew slate chert.</li> </ul>
	0471	stylofic: for battern chails structures; just above the sample, dense system of anastomised and crossing healed			layer (B) which cuts the pattern-chain structure, the sample was collected from a section battern the merly layers.
6613	UD#2	fractures Pure coccolith micrite otherwise similar to above some	6665' <b>8</b> ''	LDT2	Core shows a gradual transition from warl (bluish-grey, with 3-mm <u>compress</u> ) to whitish patched pattern-chalk structured. Fromb-like light rock
		Targe crushed echinides.	6667	LOTZ	Similar sections finally, whittish-spotted pattern-chalk struc- ture rock (10-cm layering) in a more orless marly-looking rock.
6617'10' 6619'	1.0P	Sample contains meri laminae and micro-stylolites; some healed microfractures. Sample from an area with prominent alide/"criss cross" healed	6673'8'' 6676'5''	L012 L012	Bluish core with some faw white spats; <u>zoephycos</u> Hend silicified chelk with occurrences of dissiminated pyrite; m-Z
		fractures: from this depth, the rocks are more layers./laminated with oriented open patterm-chelk structures, just dowe one finit layer is a hand and downe chelk	6680 <sup>°</sup>	2M	White pattern-chalk structure which appears open and relatively open with few 0.5 to 1 cm thick layers. Meak pattern-chalk
6623,521,		with microsstylalites, at a depth of \$523 accurrence of thick flint layer with inclusions of soft chelk. Elist semile	5580° 6. '	110	structure. Chert sample.
6624	LOP	Print sample Beneath the flint; chalk is dense, relatively humogeneous and hard with humogeneously occuring pattern-chalk structures in several generations, the pattern-chalk structure is partly con- centrated around bright vertical tracks and some (white) removies			
6527'	LDP	Mard. single unit with graduations (pattern graduation) showing <u>behinichnus</u> corone and some central tracks; the			
6630	104	pactormician scould is relatively nonspendous. Section with pattern chelk structure, relatively homogeneous, but with leyered orientation; relatively soft rock.			
6631.6.,	1011	Dark, silic-fied chalk (derk grey), presumably marly with very dark, pattern-chalk, structures, numerous trace fossils,			
6634161	L071	preferentially <u>2000rtycos</u> . Strongly still:fied section which may be divided into several 10 on thick units some about 3 on thick marks bends occur			
56.7	LDT1	Dispersed chert; core box appears generally derker with more well-defined layering; dark, silicified bands, one visible			
6641'3''	1071	plety-cmert pand. Very pronounced pattern-chalk structures in several grey			
6643-44'	1071	warieties, 5 to 10 cm bedding, top of the core box similar above. At least 40 units with isometrical 1 to 2 cm pattern-chalk struc- tures with some isolated light points; it looks as if the laminated pattern-chalk structure rocks above wes produced by			
6645 <sup>°</sup> 6' 6648 <sup>°</sup> 4'	L011 L011	compaction, Silicified, dark and weak pattern-chalk structure, Few <u>foodhycos</u> occurrences; relatively sharp layering on a 40-cm			
5650'10'	LOTI	scale which in general shows weak pattern-chalk structure. Similar as above but really weakly visible structures.			

# **APPENDIX II**

## **Brief Sampling Section Description of E-lx.**

Depth (feet)	Uhit	Description
6732 - 6735	UDP:	Chelk with light and greenish meri occurring at a death
		of about 6733 , some small glauconite concretions, white
		chalk-like intraclasts
735 - 6737 5	0001	Chelk with some marly horizons; thin glauconitic spar;
		chelk percentage is increasing with depth; pyrite occurs
		In the form of dissignations and concretions, styloli'es
718 . 6740	Long 1	The true rome of lumps
740 - 67.1	UDPT	Little samle enterial autilable from the core. being
		neous laminated chelk, micro-stylolites occur
743 - 6746	UD#1	Little sample material left in core box; chalk is white
		and homogeneous; micro-stylolites occur.
746 - 5748	0071	Write chelk with some brownish herizons
748 - 5751	UDP2	Homogeneous chalk with hurizontal shear zones, petterned
		chalk
751 - 5752	UDIPZ	Patterned chelk.
752 - 5755	UD#2	- Homogeneous chalk with mesizerand micro-stylolites.
		blursh appearance, micro Chondrite
755 - 6758	2092	White to blursh chelk, micro Chondrite
758 - 6751	00/2	Slightly blu sh chalk, micro Chondrite, Heeled fractures.
763 6764	00002	Singencial and the second second state and the second second second second second second second second second s
1/63 - 6/1049	uurz	Homogeneous charte.
766 - 6758	1 D#	Homegeneous chells with micro-stylalites.
758 - 5771	1.0P	Greyish-to brownish challs with some chort horizons
771 - 6774	LDP	Hard havegeneous chalk, healed fractures occur.
774 - 6775	LDP	Monogeneous white chulk; stylolite hurizon at 6774'.
//5 - 5/50		Tunogeneous white chain
/80 - 9/83		fractures write chain with micro-stylelites, realed
783 - 57.86	1.00	Rostly homeneous white chelk: Hicro-stylolites and
		hea.ed fractures; light-colored chert
785 6733	LD#	Very little core Material available, some chert
793 6794	LDP	Slightly brownish white chalk
794 - 6797	LDP	Dense white chalk with skeletal remains
797 - 6799	LOP	Weekly whittish-spatted chelk, light chert hurizon
1/99 - 6802	LDP	white chaik with whittish chert in the upper section.
MC2 - 5804		Ro change.
1007 - 0807	1.00	No change
MBC9 - 5811	LDP .	Dense chalk.
	101	Chulk with some clasts
ALA - SALE	LED T	Chelk with some serie berizon in the lower part
816 - 5019	UDT	No change
819 - 6821	1001	Occurrences of dissimineret spar
821 - 5824	007	No change
1074 - 6026	100	No change.
826 5829	UOT	Ro change
829 - 5831	נסינ	No change
831 - 5834	1011	Challs with some greenish mart horizons
A34 · 5836	LOTI	Gark chalk with light specks, bluish flint
936 5938	LOTI	Whittish-spotted chalk with a generally bluish
		appearance That's with more burning descript and his
09J0 - 984(	CD:1	<ul> <li>Unaria with some provintsh mangins process(y caused by probably oil_ateletas</li> </ul>
A	1071	- promoty unitstationing - Monte chalt with room becentich stations (a)[7] in the
AD-1 (AD-1	10/1	under parts
843 - 5845	(01)	Chalk with flint laver showing oil-staining, core box
		contains Many losse pieces

Depth	(feet)	Unit.	Description
5848	5850	1071	Fint with thick whitlish Margins Chaik with greenish intraclast at the battum (glauconite")
5850 -	5853	1012	Chaik with greenish nodular clasts
5851	6855	1.072	Chalk with creen: sh intraclasts
5.155	6858	1072	memoneneous chain with sheletal intraciasts
5854	5840	1012	nard white chain
6860 ·	5863	1072	Similar
5863 -	5865	1072	<ul> <li>Enails with pyrite, both as concretions and dissiminated, healed fractures</li> </ul>
6865 -	6868	: 072	Similar
6868	587C	1072	Similar
5870 -	6472	1072	No change
5872 -	5875	1972	No change
5875	6878	11	Greyish, relatively hard chalk, vertical stylolites
5878 -	5881	1 M	Chalk with some microfossils, healed fratures
5883 -	6444	18	Greyish chalk with horizontal stylolites
5864 -	5866	19	Chaix with numy herizontel parallel stylolites
5866 -	5889	10	No change
5889 -	5891	1.00	No change
5 <b>3</b> 91 -	61194	1.	Challs with many stylolites, maximum, stylolite hight is 10 mm.
6 <b>8</b> 94 -	6897	214	Greyish Hard chalk with still relatively high stylolite bands
5987 -	5900	214	Mud-coloured chalk, strongly fragmented
6900	6902	Z₩	Ro change

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# **APPENDIX III**

Analytical Results from Short-Lived INAA of Samples from TWB-8. Depth Is in Feet and All Analytical Data Are in ppm, Except Ca (in %) and U (in ppb). If Depth Is Greater than 4 Digits, Then the Last Digit(s) Refer to Inchcs.

Depth	Na	Ng	A1	C1	C.	٧	Min	Sr	Eu	Dy	U	Depth	Ha	Mg	Al	C1	Ca	٧	Min	Sr	Eu	Dy	U
												6695	865		632	2300	39 70	36	377	947	04	: 2	973
65922	11200	25400	86200	655	-	222	186	361	21	6.2	2080	5696	1160	-	1350	2900	31 50	5.2	375	893	0.4	17	396
6594	1390	10800	3010	1030	33.90	23.4	1880			3.0	- 984	6697	736	-	66	1590	33,40	4.9	448	1170	0.3	1.8	467
6597	711	5760	2930	807	34.60	11.1	1690	-	-	2.5	325	6698	933	2280	1710	2130	34.30	6.5	375	995	0.3	1.4	448
65996	839	-	4470	1020	35.00	10.0	1710	1140	-	2.8	396	6699	916	-	857	2740	32.50	3.8	378	1170-	. <del>.</del>	1.0	619
660 I	768	-	2040	1880	34.80	4.6	1640	-	•	2.8	163	6700	1128	-	827	2420	38.10	-	366	1100	0.3	1.5	830
6602	819	4990	2600	1820	33.90	8.7	1690	1750	-	-	230	6701	941	-	1420	2770	34.70	5.5	334	1170	0.4	1.5	725
												67015	1380	-	1440	4440	35.90	-	347	1200	0.4	1.7	859
UD#2:												6702	853	-	1270	2300	33.60	-	340	1160	0.4	1.5	600
66099	733	-	1760	2000	35.80		1530	<b>89</b> 2	-		178	6704	454	-	113	2700	31.90	-	327	1050	0.4	1.4	499
B073	632	-	1000	1960	33.80	5.0	1200	-	-	1.5	132	6/045	/16	-	434	2500	31.20	-	364	1050	0.3	1.9	447
												6/055	82	•	423	2020	31.20	-	305	1150	-	1.4	44/
EE1717			2410	1 880	11 60		1440	1060	_		361	6710	/34	-	647	2230	31.00	,,	28/	12/0	-	1.0	222
6614	947		3550	1000	33.30	- 0.7	1420	1030	-	3.0	285	6711	652	-	276	1630	35.20	4.7	267	1110	-	1.0	511
66207	11		3010	2220	36 20	15.6	1760	-	-	24	314	6713	725		386	1750	36 20	2	766	1110		0.6	490
65213	571		2000	707	30 30	13 5	1210	<b>54</b> 1	-	1.5	183	6714		-	331	-	35 50		-	-	-		466
6624	783	-	1560		35.80	10.2	1260	1010	-	1.9	226	6715	870	-	878	2110	-		259	1210	0.3	1.2	614
6627	1250	-	1750	2870	35.20	8.1	835	567	-	2.3	123	6716	1240	-	730	3436	33.20		216	1440	0.5	1.9	1090
6630	850	-	22 50	1500	36.90	7.0	864	717	-	1.5	187	6717	994	-	876	2620	-	-	228	1330		0.9	438
												6 ' <b>18</b>	1230	-	900	2950	-	-	202	1310	0.5	1.6	95 <b>8</b>
UDT:												6719	680	•	674	1610	36.70	•	235	1290	0.3	1.2	712
66313	1410	-	4780	2840	27.50	8.1	720	853	-	2.2	251	67195	1240	-	499	2420	35.50	-	229	1300	0.3	1.2	467
66346	1200	-	2520	1970	28.80	5.3	674	117		1.5	117	6/20	1430	-	475	3690	35.20	-	210	1320	0.3	1.1	481
963/	1260	-	5580	2450	31.40	6.9	/18	/14	0.8	3.1	256	6/21	1360	-	214	3920	32 80	•	1/6	1360	-	0.9	494
66414	753	-	1100	894	29.90	6.1	803	617	0.0	1.6	1.04	6/25	1220	-	343	4010	37.30	-	157	1200	-	0.8	434
66456	2100		2380	2720	24 60	15.0	546		1.2	4.0	10	18											
66484	1040	-	5090	1120	25.80	8.9	643	816	12	1.6	102	67275	1490	-	268	4410	18 10		159	1110	-	05	342
665010	1230	-	4400	1230	25 50	9.4	790	1160	-	2 1	162	67285	1660	-	232	3450	36 70		152	1140		0.3	354
												6729	1110	-	272	1390	37 90		158	1200	G.4	1.6	252
LDTI:												<b>873</b> G	901	-	1094	1330	39 50	27	:5:	1140	-	0.6	441
6653	1470	3430	6500	2140	27.40	10.8	776	926	1.1	2.9	214	67302	1030	-	862	1770	37.60	2.1	203	1200	0.2	1.0	332
66556	1100	-	3250	885	26.30	7.2	710	858	0.8	1.5	125	6733	732	1955	598	945	39.50	3.1	206	1180	•	0.8	282
665710	) 95 <del>9</del>	-	4440	1070	26.30	6.4	650	717	0.9	2.2	136	67332	986	2430	712	966	33.80	1.8	187	983	0.2	0.7	287
65008	-	-	3130		39.10	7.1		-	-		111	67345	1170	-	587	1690	32.50	2.3	197	1010	-	0.9	348
65637	1210	-	2920	-	33.00	7.0	69Z	/36	-	2.9	113	6/36		-	584		31.10	-			-	Ξ.	337
66630	11/0	-	4010	3730	29.20	- 1.1	597	913	•	2.4	183	6/361	2130	-	450	3420	33.90	٠	176	1210	÷.,	1.1	505
B00/	912	1910	3190	1000	33.00	1.1	293	869	-	1.5	13/	6/38	11/0	-	605	1690	36.60	^	207	1150	0.4	0.8	202
1012												6/37	1270	-	765	1680	33.20		201	10/0		1.2	200
66718	1660		2710	1910	12 30	. 7	612	685	-	21	100	5740	1610		855	2470	30.60		199	1070	0.3	1.4	429
66755	1030	-	2590	1790	36.90	7.3	700	928	0.6	1.4	105	57415	1480	-	903	2046	36 60	2.6	192	1180		1.0	308
										• • •		6751	1640	-	689	3050	35 20		196	1020	-	1.0	257
1#:												6752	1790	-	490	3060	36.10	3.6	197	522		0.7	200
6680	1010	-	2670	1180	33.30	8.2	640	1200	0.9	2.1	190	6753	1370	-	1360	1950	36.70	3.6	202	1050	0.5	1.7	505
66806	621	4280	1950	1030	33.90	7.4	569	847	0.7	1.7	154	67546	1400	2079	559	218C	39.40	2.9	189	997	-	0.8	368
66801	1020	3640	2740	1600	22.20	6.9	449	603	0.6	1.7	290	67558	1960	3610	804	2910	36.50	3.6	189	1030	0.2	0.8	411
6686	566	•	966	1390	30.90	-	247	363	0.3	0.6	217	6/565	1310	2180	999	1780	37.80	3.3	189	1130	0,3		341
5567	340	-	774	2310	30.50	-	359	536		0.9	100	6/5/6	3530	-	692	2200	39 43		181	596		0.9	194
6660	/09	11:0	31/	464	34.00		410	612	9.3	1.3	105	0/38/	1374	1040	84.5	1000	37.70	2.4	170	/3/	0.2	0.7	262
6690	757	3320	900	1.480	17 ^^	3.9	33/	849	0.5	0.8	282	0/33/ 676A7	2500	1210		1920	37.70	1.7	179	1010	0.3	0.0	174
6691	711		940	1050	12 00		440	721	0.5	1.2	310	67617	1800	1111	47 CA 7	951	31.30	4.7	127	684	-	0.4	220
3331			300	1010	36.30					<b>.</b>		67670	990	-	667	1360	36.00	27	181	1080	-	10	318
2#:												676-6	2340	2450	750	3750	-	-	186	1000	0.2	1.2	367
669Z	917		1100	1700	34.80	-	297	826	0.4	1.1	374	67656	1140	-	654	1870	37.90	1.9	186	1070	0.3	1.0	247
66925	971	-	1000	1120	32.30	4.2	337	934	0.5	1.7	487	67666	2420	3060	756	4010	37 50	3.2	173	927	6.3	1.0	184
6693	870	•	626	2850	31.50	4.1	301	918	-	1.2													
6694	775	3090	1130	2310	32.80	4.9	299	950	04	1.5	990												

Continued

Depth	Ha	74g	A1	C1	Ca .	۲	Min	Sr	ξų	0y	u 
411:											
6767?	1680	-	562	2960	36.90	5.3	150	1070	-	Q.7	197
67678	1820	6090	1200	2850	37.10	23	500	1050	0.4	17	-
\$7 <b>5</b> 86	1040	1701	<b>8</b> 84	1730	39,40	2.0	196	1010	0.3	1.2	180
67705	2290	•	600	3980	37.50	-	192	996	0.Z	. 0	222
67715	1930	2489	933	2900	39,20	1.7	501	1080	-	0.9	167
67726	2040	-	750	3370	38.30	2.2	178	878	•	1.2	184
\$7735	2570	2360	765	4870	35.80	-	186	1010	0.3	1.0	147
67767	2390	-	947	4250	36.70	Z.3	185	1060	0.4	1.0	316
\$7775	2360	2330	543	4110	36.40	2.3	172	1050	-	0.7	165
67765	2150	2190	647	3570	36.30	-	167	1180	-	0.9	Z05
67796	1760	•	1280	2690	38 10	2.7	187	1260	0.5	1.3	452
\$7805	2540	-	663	4600	36.80	-	155	1120	-	1.0	162
67817	1150	-	902	1800	39.6C	4.2	184	1230	0.5	1.0	486
67836	2200		642	4460	36.80	3.4	165	1000	-	1.1	392
67846	3110	-	657	5720	37, 30	2.3	147	1250	0.3	1.4	539
67857	2110		610	4620	37.60	2.3	159	1120	0.Z	0.5	383
67876	2020	3558	602	3250	39.20	1.0	151	1090		37	292
67885	2580	-	-	:630	•		124	874	-	0.5	360
5790	2010		579	3070	-	4.1	153	1130	-	1.3	205
67925	2330	-	-	4230	-	-	152	1180	-	1.0	372
67934	Z34C	2004	704	4060	39.30		150	1240	0.3	1.0	281
67944	2270	-	563	3630	35 40		155	1290	0.3	1.0	303
67956	1110	-	641	665	35 60	34	111	682	a 2	0.7	281
67964	1500	2210	805	1980	35 40	4.0	142	1110	-	0.8	256
67583	2710		-	4830	38 80	-	151	1150	03	0.9	256
68021	1450	3050	585	653	37 20		115	1100	0.4	1.1	671
68014	2140		738	1490	38 70	-	142	1340	0.5	1.2	141
68041	2350	-	365	10900	38.00	71	165	1640	0.3	1 0	196
68055	2170	1820	225	3440	-		110	1 360		0.7	375
58054		2016	450	123	15 80	2 1	140	1346	a 2	1.1	457
KRC/L	516	2250	630	-	17.80	2.6	154	1091			170
	744					<b>.</b>					
<b>C</b> .00											
-	1640	1595	643	2810		16	166	1030	0.4	1.5	264
000370		- 130		1919			1.00	1000			

# **APPENDIX IV**

# Analytical Results of Selected Drill Core Samples from TWB-8

Depth	-	Ca	Fe	s	c	Cr	Ce	2-	As	<b>I</b> r	•	Sr	54	C 3	8a	mf	Th	La.	Ce	M	Sm	Eu	fb.	10	Lu	Ce/La	La/To
UCP1: 6401	0.10	32.4	0 Z17	9 1	. 1	6.0	1.	, 23		8.3		983	-	0.1	ın	0.1	0 5	8.8	6.6	9.0	1.9	Q. J	a. 1	9.7	Q. 1	0.75	<b>13.3</b>
UDP2: 64039	0.99	33.6	0 93	6 1	2	5.7	1.	7 26	-	6. Z		967		0. I	142	Ç. I	0.4	10.6	8.4	9 Z	2.4	6 4	04	07	J 1	a. 79	18 0
LCP: 661710 66287 6630	0.11 J.10 8.12	11 7 11 11 1. 15	0 126 0 162 0 192	5 0 1 0 1 0	. I . 9 . 6	6.5 8.8 4.2	] - ] 2.	4 42 7 42 7 39	-	9.9 8.7 11.1	-	1020 1120 586	- 6.4 0.2	C.2 0.2 0.1	167 134 172	0.2 0.2 0.1	1.0 0.9 0.9	15.2 15.1 14 6	14.1 13.3 13.0	15.1 13.4 14.2	3 8 3.7 3 9	07 97 06	0.6 0.4 0.4	0 9 1.0 1.0	0 2 0 2 0 2	0.93 0.00 0.89	16 5 15 4 15 2
UBT: 66413	6,10	29.6	0 326			8.5	15	r 19	3.9	6.5		1110	0.8	Ø.3	2120	03	1.6	15.4	18.4	12.5	3.6	0.6	0.5	13	0.2	I 19	12 0
LOT : 665.3 665.7	0.19 0.12	25.8 20.9	0 52) [52 0	0 4 0 2	1	10.3 5.6	9. 6.	1 41 F 23	z. 5	13.5 10.7	-	1150 2511	0.6 4.7	0.J 0.Z	67) 635	0.4 0 z	2.3 1.4	22.5 15.4	29.4 17.3	20.3 15.2	5.7 4.2	1.0 0.6	0.6 0.5	L 5 9.9	5 Z - 0.1	: 29	15 Z 16 4
19: 560011	0.13	20. Z	6 300	<b>0</b> 1	. 5	7.0	3.	5 54		<b>8</b> . <b>1</b>	-	<b>85</b> 1	0.5	0. t	1370	0.Z	1.1	13.3	14.9	11.1	3.7	G 6	0 a	0 9	ð. L	1.12	24.5
2%: 6692 6700 6717	0,11 0,11 0,13	34.4 34.0 36.2	0 180 8 179 8 48		0	3.6 4.0 4.0	2.5.	5 70 5 25 1 17	-	10.9 13.5 9.7	J	875 1240 1350	0.2 0.4	0 I 0.I	595 90 81	0.1 0.1 0.3	0.4 3.3 9.1	9.5 10 6 7.5	7,4 7,9 4,1	6.7 8.0 5.0	2.1 2.3 1.4	0.4 0.4 0.2	0.3 0.3 0.2	0.5 0.7 0.6	0.1 0.1 0.1	0.78 0.75 0.55	17 9 15.8 12.9
39): 6751	0.21	35 5	a 55			5.4	J	<b>1</b> 5		22.7		1030		0.1	144	a. 1	0.Z	7.8	5 6	4 7	E.6	د ه	0 2		01	3 72	13 5
40; 67917 67956 68050	0.14 0.15 0.26	37.4 36.6 35.2	0 37 4 25 6 23	503070	8	4 8 3 I 2 6	7 0 1	9 23 6 20 9 21	•	17.2 19.5 37.0	-	1300 1260 1360		-	101 245	0 1 0 C 0 C	0.2 0.1	7.8 5.8 5.0	5 2 3.4 2 6	7 8 4.6 3 6	I 6 I 7 I 4	0 3 0 2 0 2	0.2 0.2 0.1	06 04 04	9.1 0.1 0.1	0 67 0 59 0 52	14.2 13.0 12.0
Other s Bryozow	angele n cha	s: Th, en	shere.	(Ste	-	) 						1188														• ••	
Gray ch	0.07 101112	38.2 onsher 37.4	e (Ste C 21	9 ( 9775) 4 (		1.6	1	7 38 0 23		4.0 1.0	•	968	<b>و</b> .پ	<b>8</b> 1		0.1 0.1	0 Z	1.1 6.2		•.J 5.9	1.4	0 2	0.2 0.2	9.6 0.5	9.L 9.1	0 61	14 0
stylein	0.03 te 0.47	37.0	0 1070	6 C	, 0	: 4 25.7	: 21	z 37 5 220	-	1.1 7.40.1		1100 1260	- 1.1	0.1 1.9		0 ' 7.0	0.2 12.5	7.3 116	4.6 193	6.1 150	1.5 34.1	0) 50	0 2 J 8	0.6 5.0	0.1 0.9	0 63 0.89	12 6 20 0

# **APPENDIX V**

### Analytical Results for Samples from Drill Core E-1x Obtained by INAA. Some Data Are by XRF.

			Depth (feet	1						Depth (fe	et )		
lennt	6734 UDP1	6737	6738-5	6742- <u>5</u>	6744-5	6745 UDP2	Element	\$753-5 UDP2	6758	6760-5	6753	6767 LGP	6770
le(%)	0.45	0.26	0.25	0.32	0.24	0.20	No(1) K (1)	0.24	0.21	0 19	0 22	017	0.25 -
a(1)	17.20	32.50	31 30	36 10	33.50	34 30	Ca(X)	32 10	35.QC	36.10	35 SC	34 20	13 90
e(%)	1.06	1.41	0.26	0 19	0.29	3.22	Fe(%)	0.36	C 26	a 22	0 15	0.13	0.12
li (%) x#F	0.51	6.30	0.26	0.10	0.76	0.16	A1(1)19F	0.37	0.23	4.17	C 10	0.13	3 09
1 (ppm) 201	F 1370	170	130	80	120	78	Ta (ppe) INF	193	120	29	55	<del>6</del> 0	70
n (agas) siti	F 2050	4390	3590	3170	3050	1610	Rn(pp=)XEF	2250	1770	1670	1520	1560	1040
e(L) Liff	1.78	J. 53	Q. 18	3.12	0.18	J. 15	F : (X) 'RF	0.24	0.20	Q 14	3 13	0 11	0 10
1 (%) XRF	18 9	1.7	9.9	3.7	5.1	2.9	\$1(%)XBF	7.2	3.5	28	21	23	21.2
6(pps)38	F 19	3	3	3	3	2	10(ppn)38F	4	2	:	:		ļ
r ( ppn ) 301	F 36	6	5	3	4	3	Ir (ppm) 3019	5	4	3	3	1	5
n ( pps) 20	51	32	24	36	27	33	2n ( ppm) 100 F	29	27	23	40	11	
u ( ppm ) XXX	F 12	10	8	9	11	12	Cu(ppe)XIIF	14	12	10	11		9
( jigan ) jijar	35	,	-	•	-	•	V(ppm) INF	6	•	-	-	-	-
:(ppn)	5. L	2.3	1.7	2.0	2.9	1.5	Sc(ppm)	27	2.4	53	11	1.7	07
(ppn)	25.0	70	5.6	6.5	7.4	4.8	Cr(ppm)	94	46	53	36	43	2 B
o(ppm)	3.6	1.5	1.2	8.2	2.4	2.9	Ca(pp=)	30	3.0	24	: 7	0.5	24
1 ( <b>apa</b> )	30.6	24.6	22.0	16.2	18 1	34.6	Zn(ppp)	•	21.4	87.4	47.5	, ,	19.4
s ( appa )	6.6	7.3	-	2.7	0.8	1.5	As(ppm)	19	21	1.9	12	23	1.
r(ppn)	17.2	26.8	34.9	41 I	35.1	25 5	Ør(ppm)	28.1	35.2	25 Q	35.5	31.0	26.5
( <b>age</b> )	25.5	53	4.8	3.6	4.4	30	Rb(ppm)	5.6	3.4	2.3	-	-	1.3
(ppn)	857	1290	1260	1570	1580	1510	Sr(ppm)	1360	1500	1600	:490	1400	643
(appa)	0.3	0.2	0 I	0.2	01	C.1	Sta(ppm)	0.1	0 1	0.2	0.2	21	01
s ( ppm)	1.4	0.3	0.2	0.1	0.2	0.1	Cs(ppm)	0 3	0 2	91	9.1	a 1	0.1
(1998)	300	[84	644	164	182	120	Ba(ppm)	154	145	150	136	1,15	214
·(mm)	1.1	0.3	0.2	0.I	0.2	0.1	HT ( PERC)	67	2.1	a t	91	<u>u</u> 1	9.1
a ( page )	0.2	-	-	-	•	•	i a ( ppm)	•	•	-	-	•	-
	÷.				÷.,		Au(1990)	÷	· •				Â.
	3.4	0.9	0.8	G. 6	3.5	0.5	(h(ppm)	3.3	37		9.4	1 2	0.5
	3.1	1.1	2.1	2.1	1.7	6.10				1 5	0.1	6.7	
	0.00	U 43	0.35	9.21	U. 44	0.2U	5 <b>64</b> 0	רנפ	U. 23	3 11	0.14	V (-	9 11
(1996)	22 9	12.7	10.8	9.6	12.9	19.0	La/ppm)	12.5	11.7	14.8	7.2	10 1	51
t(ppn)	37.3	21.8	14.3	15 4	196	11 1	Ce(ppm)	20.9	16.3	16.2	• 3		/ 0
( see )	20.4	8,7	10.6	10.8	12.1	10.2	Nct(ppm)	14.4	12.5	14.7	5.5	37	3 9
-(eee)	4.4	2.4	2.2	2.4	2.9	2.3	See(pppe)	23	27	23	7.7	27	1.5
	0.9	a.s	0.4	0.5	6 6	0.5	Ec(ppm)	0 6	0 5	56	3 3	9.5	21
b( <b>#2#</b> )	0.6	0,4	G. 3	0.4	0.4	0.4	10(00000)	0 3		25	93		0.2
(هذم )ه	1.4	10	0 9	1.0	14	10	Thippen;	12	1 3	13		1.1	0.4
u(ppm)	σ2	a 2	a 1	3.1	ai	Q 1	( <b>Sign</b> )	0 I	ui	31	u i	u 1	0.1

			دا: «دمد										
Element	6774 LOP	6780-5	6703	6795	6790-5	6800-4	Element	f Dia. 2005	6007-5	5810	\$812-5 UDT	6816	6620
No(1) K (1)	0.10	0.22	0.15	0.13	6.18	0.19	No(%) E (%)	0.19	0.13	0.14	0.18	0.21	0.16
Ca(X) Fe(X)	35.50 0.19	34.70 0.25	35.10 8.18	32.90 0.27	32.30 0.22	34.90 0.24	Ca(%) Fe(%)	31.00 0.22	31.50 0.44	27.30 0.20	31.00 0.36	25.80 0.35	31.50 0.36
A1 (1) 386	0.12	0.20	0.14	<i>L</i> .0	0.28	0.25	A1 (1) 385	0.30	0.30	0.20	0.42	6.40	0.56
- Ti (ppm) 388	F 57	105	76	140	137	105	Ti (ppm) 200	170	150	136	194	247	•
الثلا (هجي )عاد	1340	1170	1100	1410	1250	1420	Her ( ppps) 101	1215	1680	1610	1540	1230	•
Fe(%)##F	8.12	0.15	0.12	0.20	0.15	G 17	Fe(%)##F	Q. 16	0.24	0.20	0.26	0.29	0.26
51(X)##	2.6	4.7	4.3	<b>0</b> .7	10.0	5.6	\$1 (X)300F	11.5	11.4	10.3	13.8	22.1	10.7
	-	z	-	2	3	2	Rb(pps)381	2	3	Z		3	4
(r(ppn))		4	3	2	•	4	(r(pps)20		4	<u>.</u>	•		
					24	21	(n( ppn) 300	21	37	n n	37	11	
V(pps)39	-	ż	1	3	•	-	2 ( ppm) 3 (Mr	- 10	4	•	3	4	10
Sc(pp)	1.3	2.1	1.9	2.0	2.5	3.1	Sc(pp)	2.0	3.5	2.5	4.0	3.8	3.0
Cr(ppn)	3.3	3.0	4.2	5.5	6.3	4.4	Cr(ppm)	5.9	5.4	5.9	5.5	6.0	5.8
Ca(ppm)	3.9	13.5	4.2	4.6	3.8	3.6	Ce(ppm)	10.8	5.8	4.5	6.9	12.7	6.7
Zn(ppn)	22.Z	40.0	34.5	-	-	-	Zn(pp)	•	-	•	-	-	-
As(ppm)	1.0	2.8	1.2	1.1	1.4	1.4	As(ppm)	-	3.4	3.1	1.3	1.9	
	35.3	37.7	31.0	16.7	30.5	26.3	Gr(pps)	19.7	11.4	16.1	15.3	13.2	12.8
경험	1.5	5.3	2.3	4.1	4./	3.3		5.4	4.7	4.2	3.5	6.6	8.5
	1304	14.34	140	0.2	1200	0.7	SP(ppm)	1140	1410	1210	:200	1140	14,99
	8.1	8.2	0.2	0.2	0.2	0.2		9.2	6.2	0.7	0.4	0.0	0.3
	13	144	157	262	87	136		197	278	203	241	116	198
Htf (mmm)	0.1	0.2	0.1	6.2	0.2	0 2	Hf (mm)	0 1	03	0.2	03	0 4	6.5
Te(mm)	-	-	-	-	-	-	Tel meni	-	-	-	-	-	-
Au(gab)	-	-	-	-	-	2.4	Au(mb)		•	-	-		-
Th(ppm)	3.6	1.3	1.1	1.0	1.7	1.2	in(ppm)	1.7	17	1.4	24	2.4	2.6
V (ppm)	2.0	2.0	1.9	0.9	9.0	0.0	u (ppm)	0.6	0.9	ð. 8	0.9	0.0	0.8
UGHC	0.12	0.16	0.20	0.14	0.13	0.12	USAC	0.13	0.14	0.12	0.15	0.25	9.17
La(ppm)	3.0	11.7	11.5	15.3	13.6	16.4	Le(pps)	15.5	15.0	13.1	16 3	18.7	17.6
	11.1	13.8	14.4	23.2	22.1	<b>(J.)</b>		<u>A.</u>	21.1	21.5	31.4	JV . 9	- <b>X</b> . J
	9.7	16.6	3.0	10.0	13.3	10.7		29.0	18.4	13.8	10.3	17.0	17.4
	6.C	3.0	3.9	6.7	Z 			7		3.7		3.9	3.3
	8.1	0.4	0 4	0.6	0.5	0.4	The second	0.5	0.0	0.5	0.0	6.7	0.7
	ōś	0 1	10	1.5	12	16	Th(mm)	1.4	1.6	1.3	1.6	17	1.6
	0.1	0.1	0.1	0.2	0.1	0.2	Lu(mm)	0.2	0.2	02	0.2	0.2	0.2

			Depth (fe	et)						Depth (fe	et ]		
lienent	6822 UBT	6826-3	6823	6433-5 LaTI	<b>6836</b> -5	6841	tienent.	6846 L071	<b>6840</b> -5	6852 LOT2	6855	6857	6861
la(1)	0.22	0.24	0 :9	0 26	0.22	9 21	Na(%)	0.15	0 19	9 25	2 12	a 19	0 13
a(X)	25 60	21 90	30 00	34.72	24 60	31 50	Call	31.50	26 1Q	26 25	34 20	27 30	33.99
e(%)	1 19	9.25	2 27	0 19	2 68	5.35	Fe(L)	0 29	\$ 35	0 32	3 23	0 21	0 23
1:(%)##F	0.32	0.50	Q 34	\$ 17	0 35	0.34	A1(%)##F	3 28	3 76	9.32	9 :9	0 33	0 25
( 1 ( <b>1998) 3</b> 8F	158	237	140	86	151	155	Trippm)XRF	119	254	139	54	129	107
h ( pps) 207	[440	1290	1250	1050	910	8/0	Mn(ppm)338F	710	aac	₩70	39-3	1930	1259
e(%)#85	C 25	9.25	3 ZO	a 13	3 34	0 20	Fe(%)ARF	G 2C	0.30	3 23	a 13	0 13	0.16
1 (X) 200F	22.2	16.4	14.8	5.	34	12 2	\$1(%)##F	12.5	. 2	7 <b>•</b>	• 3	13 6	• 3
ro (page) 101 F	2	4	3	1	2	3	Nb(ppm) XN7	2	3	2	I	Z	Z
(*(200)300		<u> </u>	4	3	4	4	Zr(ppm)XRF	4		3	2	4	2
A ( 1996) 2007	30	31	21		35	25	(n ( ppm) IRF	22	55	37	26	27	
	•		4	12		10	Cu(ppe) Air	10	10	16	19	,	15
( Children 1 Tradies	•	•		-	•	<b>`</b>	a ( bitas ) T a s	,	11	-			•
<( ppn ]	32	4.8	23	22	3 0	35	Sc(ppr)	25	4 3	23	17	26	24
r ( 1999)	4 0	4.7	10.4	15 4	97	95	Cr(ppm)	9.8	10 Z	11.5	11 7	13.8	11 4
o ( ppp)	Z5 5	71	35	21	38 7	25	Co(1994)	15 Z	3:	27 1	2.5	7.5	3 3
n (ppp)		-	-				( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )	· .			· .		
ls(pgm)	46.3			11		11	As(ppm)	3.1	11	4.5			15
(ppm)	10.3	21.4	16.6	25.5	25 4	24.6	Sr(ppm)	27.3	34	22.5	15 /	14 2	15.4
	1.1	5.0	37	3 3	4 3	4.5	40(ppm)	2.3	7 0	37	2.2	34	3 0
r (ppm)	1160	1126	1420	1 390	1530	1340	5*(ppm)	(543	1490	1763	1980	1230	1000
	33	11	0 1			03	20(ppm)	<b>C</b> 4	9.4		11	11	9 Z
	107	375	202	153	2 2	6 3		97	57	9 2		1 1	0.1
	302	2.5	202	139	107	1.0	34 ( 1998) 16 ( 1998)	201		149	1.1		
			~ .		v 2			77		33		42	<b>u</b> . c
L ( mak )	-						i ar ( parta )						
	21	,,			,,	1.4	The second	: 4			1.0		1.5
formi	a .	3 4	à,		23	37	() formal					2.7	0.6
1 DHC	0 11	ā 17	0.13	0 10	0 16	0 15	U DIIC	0 11	0 ž3	0 15	0 12	3 13	0 13
a (nem)	12 5	I <b>J 8</b>	111	14 2	26.5	17 6	Eal com)	14.5	22 6	17.2	12 1	13.9	:5.3
e(pps)	25.3	29.1	25 2	13 3	28.5	28 7	Ce(nom)	23 7	35 2	30 4	173	23 2	21 2
d(ppn)	16.6	21 0	157	15 1	16.5	18 9	Nd(nom)	15.0	23 1	17.3	14 1	14 6	16.5
Set page 1	3 8	6 2	38	4 9	4.6	5.4	54(200)	4 2	64	4.8	35		4.3
(u( ppm)	0.6	0 5	07	07	0.9	0.3	Eu(mar)	37	1.0	2.3	0.6	37	07
(b) (pom)	0.4	07	0.5	0.5	37	0.7	"b(ppm)	ā 6	0.8	2.5	3.5	0.5	0.5
(bee)	13	15	1 2	13	1.3	: .	75(000)	13	1.8	1.1	11	12	1.5
14 0001	ā 7	62	ā ī		37	0.2	1		<b>n</b> 7	Ā 7			

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			Death (fe	et 1						Death Ife	et )		
Elamont	6064-5 LD72	5855	5858-4	6872	6676-4 19	6879-6	Element	6001-6 1#	<b>585</b> 2	6897-)	6496 20	6998	<b>690</b> 1
<b>1.</b> (1)	0.16	3 23	2 14	3 /0 3 57	0 12	0.10	He(I)	• :1	0 67	0 14	ə 11	0 17	0.14
	75 30	10.00	35.00	12 63	30 13	30 20	Calat	38.00	35 40	34 32	36 10	35 30	30.64
Fe(I)	0 27	2.57	0.60	2 32	0.29	1 10	Fe(%)	0.13	0 37	3 67	5 67	0.00	8.06
al (7) II	0.26	2 74	3 44	-	3 29	0.00	A1(%)#8F	0 11	0.34	3 38	3 95	0.96	8 94
<b>تبلد (مربع )</b> 1	134	396	194	31	30	36	T: (ppm)38F	34	16	33	20	21	14
بين (معلم ) مي	1200	1150	1162	573	540	490	Min ( pagen ) JUCA	490	400	192	349	340	256
e(1))	6.72	0 44	0 31		0.06	0.07	P ( 1, 1997	Q Q/	0.04	365	0.04	9 65	9 23
	12.1	- 13.3		•	: 3		31 ( A) AND Mb. (	1.6				9.9	9.4
		;	;			1	Te(man) XBC	4					
	-	Ś			1,	74	Ta/ anni XRE		71	14	,,	76	22
		16				:0	Cu(and)285	10			- Y	;-	ià
(ppn)36	-	12	ŝ		-	-	¥(ppn)3%	•		-	:	-	-
Sc ( ppm)	24	4.6	4 2	12 7	15	1.9	Sc(ppm)	1.0		1.4	39	11	0.5
Cr(apm)	• 3	15 U	11 4	34-3	15 0	11.9	Cr(ppm)		34	87	<b>9</b> J	10 9	96
Ce(ppn)	2.2	12 2	15.5	34 2	56	11	Co (ppm)	3.8	35	07	35	۵,	0 6
(n(ppm)	-		· · ·				En (apm)		·	•	35	-	:0
			24 3					5.0	1 1				
	28	11 4		21 2		11 3		13.0	10.3		4	17	
	1610	590	1860	780	1446	1510	Setemat	1850	:632	1680	17:5	:	1850
Sal anni	A 2	3.6	a 7	2.6	1 1	01	Sib( man)	83	3 1	ē 1	1 I	a 2	0 1
Cs(mm)	0.1	93	ā 2	1.5	0 1	<b>0</b> .1	Cs(app)	ā 1				01	
le(ggm)	125	246	124	260	76	89	Bu(ppm)	<b>M</b>	106	92	84	135	93
wf (ppm)	ð. 2	5.4	03	22	01	01	197 ( ppm)	Q 1	-	91	•	3 E	•
Ta(ppm)	•	<b>2</b> .1	-	-	-	-	Ta(appm)	•	•	-		-	-
fu(ppb)	-	•	÷		÷	÷	Au(ppb)	÷		÷	2.5		
TP-( ppm)	1.5	4.7	2.4	12 :	63		1 <b>11 ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( </b>	84		<b>a</b> ,		= 3	
	0 13	3.37	3.23	J.J I 03	9.5 2.41	0.63		1 52	0 35	G 49	0 63	0.76	348
Lafonat	18.7	25.5	18.1	B2 6		19.2	Lefam:	18.7	6.7				\$7
Ce(ppm)	18.9	52.4	34.4	1:5	51	11.7	Ce(ppm)	11.8	6 2	9 2	15	÷ 5	5.2
ld(ppn)	12.5	42 3	23 3	35 2	\$ 1		Ref( pages)	74	a 3	9 3	94	10 7	67
Sea( pppa)	33	71	51	25 I	23	27	Sm(ppm)	29	17	2.4	5 0	2.4	13
Eu( <b>200</b> )	05	15	1 5	45	0.4	9.5	Eu(22)	04	0 2	94	03	94	a.2
[a(pp)	3.4	11	Q 8	33	5.3	54	Th(ppm)	33	4 Z	0.3	Q.2	3 3	6.2
70(ppn)	1.1	2.2	16	4.0	10	11	T1(2720)	11	97	0 9	39	13	06
Lu( <b>99</b> #;	0 I	0.2	37	2.7	3.1	9. L	Lu( <b>ppm</b> )	91	0 I	3 I	a 1	0 l	01

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# **APPENDIX VI**

Well-Logging Data for TWB-8. Depth Is in Feet, Asterix (\*) Gives the Average Value of Two Neighbouring Values, and Values in Parenthesis Suggest Overflow.

Depth	68	52	NPH I	tur	ILS	CILO	SFLA	Jest	4	9	SPer-	: <b>.</b> #	21.3	:::3	SFLA
	(991)	( 101 )	(1)	(0he m)	(014 =)	(as salas) 	(Cha =)		(GPT)	(ali) 	(%)	(3787 =)	(0748 x.	(* etc.)	(0148 ±
uopi								6702 3	a + 32	247	3 235	:: )	14 4	<b>66</b> 3	4 52
6594.00	6.63	254	9 315	118	(2000);	-7 23	6.96	5734 3	1 7 23	236	1 26.7	3 45	11.3	<b>80</b> 3	4 13
6597. CR	1 7.1	744	9.291	15.5	26.2	39.2	7 🗰	6754 9	3 <b>8 8</b> 5	221	3 245	12.3	0.55	116 3	3 96
6375 36	0.94	231	3 201	<u> </u>	24.2	413	12	\$795.5	3 8 57	215	2 234	11 7		114 2	3 13
6661.00	6.33	$n_{n}$	9.245	31 7	30.6	22.6	1.20	6797 3	9 7 46	211	3 366				3 11
MM2.00	0.01	233 233	0 200	33.4	23.5	42.5	7.48	6710 3	3 9 92	224	2 3/ 3	<b>13</b> 7	14.2	•4 2	1.21
								6711 0		213	5 196		12.4	32 /	1.79
	)" /.448 . 7.11	230		11 .	13 4	/3 4		6/15 0			3 43/			9 41	( ))
1613 UN	6.33	211	8.103	.• •	20 /	34.0	4 98	6/14 3		124	3 412		4 74	38.4	1 17
		716	8 244		\$ 17	187		6713 G	y <u>y</u> #/	114	7 441	7	7.17	-	
		213	0 261	9 14	7 1		7.74	4717 A		21.0	5 855	4 45	10.1	<b>4</b>	2 04
1478 48	7.85	796	8 3-77			104	2.44	6718.0	r 3.33 6 5.36	198	0.445	• • •	107	- 7 ir	1.4
421 25	- 74	201	0 101	772	ã.	1.44	3 8	6718 G	2 2 2 1	197	3 447	1 14	23.2	41 1	: 17
621 7		201	8 101	7 14	6 77	1.49	2.15	6719 6	7 75	194	1 455	1.0	13.4		1.54
474 0	• 11	196	6 313	7 67		iss	2 11	6720 0	6 6 64	191	476	1 12	5 73	:15	1 47
1627 BD	10.5	184	5 202	11.5	12.5	77 4	2 23	6721 0	8 5 57	1.78	0 867	1 54	4 17	747	1 12
636 06	8.99	207	1 253	8 31	7 54	132	2 16	6725 0		116	0 454	3.42	3.5"	200	1 11
101															
5631 25	* 9 29	223	5 272	6 27	6 27	160	2.12	\$777 5	a 5 63	: 14	2 398	2 44	273	366	5 564
634 50	8 43	176	0.209	6 79	5 90	145	2 09	6728 5	ŭ 776	110	0 386	2 57	2 82	357	3 974
5637.00	0.00	100	0 261	6 41	5 (3	195	1.97	6729 9		103	0 400	2 H	2 84	347	0 94
5641.25	· 0.32	182	0.272	10 3	7 45	135	2 43	6730 0	0 0 30	90	0 400	2 47	3 25	327	0.93
6643.33	)" B IO	208	0 285	5 28	5.63	172	2 54	6730 2	5" 7 <b>80</b>	89	3 400	252	3.37	299	0.91
6645 SK	9.54	210	0 244	8 35	6 64	151	2 25	6733 3	G 970	737	0.454	7 22	2.47	454	8.79
<b>6640</b> .33	i" 9 21	209	a 272	6 <b>3</b> 3	553	181	2.25	6733 2	0° 3 25	76.3	3 467	2 16	23:	435	5 78
5650 BJ	i* 9.87	193	G. 266	5 92	5 29	190	Z 24	6734 5	0 721	- 75 4	0.437	i 94	I #5	542	5 74
011								6736 0	6 773	- 54 4	1 3 379	: 93	I 64	ŝ	0.72
6653 OC	6.91	132	0 293	8 87	6 61	151	2 31	6736 2	0" <b>4</b> 15	- 49 3	0 390	2 31	1.85	540	5 72
6655 56	6.03	199	3 3 3 6	10 5	7 [4	140	2.38	6738-0	0 6 55	21 3	0 453	2 45	1.94	515	0.72
<b>1657</b> .41	1° 745	213	0 267	9 43	7 18	140	2.46	6739 0	G 9,04	21.4	2 4 3 3	2.4	2.12	47;	0 72
5660 6J	9.93	139	0 201	8 32	6.55	157	2.46	\$739 2	3" 7 90	28 3	2 419	1 33	2.73	475	3 12
100.3. X	17 7 NG	132	0 259	10 1	13 66		2.94	6740 0		563	9 402	12	1.94	212	0 /2
144 J M	7.07	173	0 2 39	10 3	13 00	/3.4	2.94	6/41 3	e /15	/1 4		1 11		100	3/3
- AT 1.		- C.M	9.679	/ 33	<b>8</b> . 63	124	6.39	6/31.0		14 3		- 93	1 14	174	6 6 5
10'4 1873 61				( 2000 )		~ ^	1.61	6/3C U				1 70	2 34	40	9 36
66.76 AS		258	0 121	27 1	27.2	37 4	5 15	9/33 U			1 U 3/9	15	2 10	4(3	6.00
138 138		( 13	9 141		41 6	37.4	3.63	6/34 3	· · · · ·	17 4	0 6 376 0 374	1 71	7 73	101	0.49
6680 W	7 94	230	0 220	12 6	13.2	75.9	4 76	6758 A	4 7 16	10	6 36.4		1 67	60E	0.40
<b>6680</b> 50	់ភ្ល	277	0 226		10.7	33.2	4 86	4757 5					1 40	i uz	0 44
-	• 7 12	274	0 227	11 7	10 7	93 4	4 82	6744 4			A 0 ATA	1 72	1 13	\$77	0.44
MAC 0		241	0 254	20.0	in j	ű í	4 95	6764 6	4 6 94		5 0 411	i n	1 78	447	0 44
6687 OC	9.17	241	0.75	10.5	16 6	ũ .	4 55	6760 5	·		G G 397	1.61	1.84	545	- G AM
	9 9	240	6 241	16 1	12.5	80 C	5.10	6761 6	a. 6 m	-2	23 2 427	1 54	i 73	579	0.00
1649 0	i i i	240	0 259	17 1	15 4	65 0	5 69	6782 9	6 6.15	-4	6 0 399	1 44	1 62	610	0.40
690 a	6 90	236	0 231	20 B	13 6	13 1	5.01	6764 5	4 9 13	-79	5 0 457	14	1 63	615	0 47
6691 OC	្រាំមើ	233	0 232	23 0	16.3	61.3	5.16	6765 5	6 6 94	-42	0 0 459	i 40	: 70	588	0.47
(F)			-	-			-	6766 5	a* i 70	-41	0 424	1.30	177	566	0.46
1692 QC	10.0	234	0 243	37 5	14.8	67.4	5.21	48	_						
1492.5¢	9 72	238	0 234	473 2	15.8	63 2	5.43	6767 5	4° 6 91	-51 9	0 384	: 34	1 73	578	0 45
1693. DI	9.17	241	0 233	45 2	15 4	64.8	5 52	6767 5	e 51	-51	9 0 384	1 38	173	578	0.74
5654 00	1 8 87	z 44	0 251	367	20 8	48 1	5.85	6768 5	a* 7.10	-60 4	5 384	1 32	1 54	609	0 44
1695 QC	9 12	245	0 273	24 7	17.4	57 5	6 22	5770.5	0 7.74	-65	3 0 396	1 17	1 33	755	0.42
6696.0	3 8.04	1 253	0 259	20.3	20 L	49 8	6 47	6771 3	6.89	-71 (	5 0 361	117	1 28	784	0.42
5697.00	3 8 31	251	0 255	<i>t</i> i 9	20.0	50 0	6 39	6772 6	3* 730	-97	I 0 431	1. 2Z	1 31	763	5 41
6490 Q	9.41	Z 46	0 230	26.2	56.9	14.9	5.39	6773 5	a 577	-117	0 424	E 25	1 35	740	0 41
6699 O	1 1 1	238	0 248	34 3	(2000)	-15 5	6.09	6776 0	7.91	-98	2 0 434	1 18	1 45	694	0.40
5700 00	7.99	24[	0 261	20.1	73 6	13.6	5.60	6777 4	6* 7.35	-97	1 0 461	112	1.42	707	0.40
5/01 00	្រុំទ	744	C 215	14 6	20 1	45 8	4 98	6778 5	HT 6.35	-113	0 410	1 12	1 41	112	0.39
6/01 S	3 3.66	s 745	0 211	11 2	18.9	52.9	4,72	6779 5	10 746	-116	0 441	1 10	1 44	595	0.39

Cantinued

<b>Cupt</b> h		9		IUN	_ 1.a	CIUB	SFLA
	( <b>GP</b> T)	( <b>ک</b> مب)	(36)	(386 s)	196 2	(# #**)	( <b>CR</b> •)
	7.94	-126	8 447	1 11	1.46	-	0.39L
361.28.	5. <b>6</b> t	-เม	8.448	1 11	1 33	754	8. XX
30) M.	1.13	-140	8. 4D1	1 1)	1 75	701	8.372
<b>764. 54</b> **	8.95	-142	4.467	112	1 20	761	0.371
366 66	6.39	-145	0.396	: 38	1.26	795	0.371
W. 97	8.30	-134	8 419	1 1)	1 41	788	0 300
JUR. 39*	7.19	-145	8.487	1.17	1 33	756	0.367
<b>799.25</b> °	8.45	-143	6 425	1 12	1.8I	994 -	8.364
797.46*	5.95	-116	0.423	: 12	3 92 3		8 376
ינו נוד	7.99	-132	8.449	1 20	1.11	987	8.30
794 33°	7.50	-151	8.428	I 45	1 36	739	8.481
255.58	8. W2	-127	8.443	1.49	1.45	680)	8.48
796.42**	0.33	-92.6	8.427	1.41	1 37	ກມ	0.411
<b>***</b>	7.63	-35.8	8.426	1.17	1.02	990	8.419
882 L7*	7.91	-120	0.413	154	1.72	824	8.452
<b>60 N°</b>	6.92	-99 0	8 416	1.45	1.24	812	8.42
APA 27"	6.48	-65.2	8.443	1.48	1.39	775	0.472
885 <u>9</u> 8 -	8 M	-38 2	8 462	1.41	3.02	331	8.482
	7 📾	-33.6	8.488	142	3.47	294	0.475
<b>867 54</b> *	9.Ū7	-531	0.363	1 65	4.18	214	1 44
an) 10°	7.39	-457	8.414	1.92	2.75	455	0.40
ata 33*	0.25	-47 2	8 427	170	1.63	546	1.45

UP1:         CT0:         5.33         145         165         2.97         2.18           6394.00         1.77         5.39         147         165         2.75         2.47         670:50         1.76         5.63         144         165         2.13         2.40           6601.00         1.75         5.99         149         181         2.44         670:50         1.77         6.27         143         181         2.40         2.40           6602.00         1.78         5.70         189         172         2.57         2.45         670:50         1.84         144         144         3.54         2.57           6602.00         1.79         7.56         112         113         114         2.45         671:50         1.86         6.13         1.44         144         134         135         2.15         2.45         671:50         1.86         6.21         133         131         2.16         2.55         2.45         671:50         1.86         6.21         133         131         2.16         2.55         2.45         671:50         1.86         6.31         132         145         2.55         2.45         671:70         1.85         6.43	Depth	8408 (g/cm <sup>3</sup> )	PEF	DT (us/f)	LITH (cps)	AMPL (mV)	(9/cm <sup>3</sup> )	Depth	1008 (g/cm <sup>3</sup> )	PEF	DT (us/f)	LITH (cps)	/₩₽L (124)	RHG1_3 (g/cm <sup>3</sup> )
6894 00         1.77         6.39         1.47         165         2.17         2.47         6702 00         1.78         5.80         1.44         165         2.13         2.24           6507 00         1.74         5.39         1.47         1.84         2.17         2.41         6704 00         1.77         6.31         1.14         1.25         2.44         2.44         6707 00         1.64         4.40         1.33         1.64         2.43         6707 00         1.64         4.40         1.34         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.44         1.45         1.45         1.45         1.45         1.45         1.44         1.44         1.45         1.44         1.44         1.45 <th1.45< th=""> <th1.45< th="">         1.45</th1.45<></th1.45<>								6701.50	1.77	5.93	145	165	2.97	2.38
6597 60       1 74       3.64       2.17       3.44       2.17       2.43       6764 00       1 76       6.27       1.43       164       2.10       2.44         6507 50       1.75       5.59       1.64       1.07       2.44       6764 00       1.76       6.31       142       153       163       2.10       2.44         6400 50       1.77       5.79       1.78       5.79       1.78       6.19       1.44       3.54       2.57         6403 50       1.78       7.45       1.00       1.86       6.19       1.44       1.45       3.10       2.65         6403 50       1.78       7.45       1.00       1.86       6.19       1.44       1.45       3.10       2.65         1097       1.89       6.25       1.21       1.57       2.54       6716 00       1.86       6.39       1.34       1.65       3.10       2.64         6423 60       1.89       6.71       1.33       1.30       2.64       6716 00       1.86       6.39       1.34       1.65       2.64       6.39       1.33       1.39       3.77       2.64         6423 60       1.87       6.71       1.93       9.69	6594.00	1.77	6.39	147	165	2.75	2.47	6702.00	1.78	5.90	144	165	2.13	2.28
Seps. 50         174         5.59         147         184         2.37         2.41         676 50         1.75         6.51         142         140           660 1         0.77         5.39         147         180         122         2.44         670 500         1         6.50         131         141	6597.00	1.74	5.86	140	179	3.68	2.43	5704.00	1.76	5.27	143	166	2.10	2.43
4601.00         1.75         5.59         1.95         1.81         2.44         2.45         670.700         1.86         6.49         1.34         1.31         2.41         77         6.30         1.35         1.31         1.34         2.41         74         1.35         1.31         1.34         2.55         1.31         1.34         2.55         1.31         1.34         2.55         1.31         1.34         2.55         1.31         1.34         2.55         1.31         1.30         2.64         2.64         2.64         2.64         2.64         2.64         2.64         2.64         2.64         2.64         2.64         2.64         2.64         2.64         2.65         2.67         2.64         2.70         1.34         1.44         1.15         2.64         2.65         2.67         2.64         2.70         2.64         2.70         2.64         <	6599.50	1.74	5.59	147	184	2.37	2.41	6704.50	1.75	6.51	142	170	2.68	2.40
4602.00       1.77       5.70       195       172       2.97       2.45       6707.00       1.81       6.4       134       153       2.10       7.46         6407.00       1.87       1.78       7.38       1.70       1.78       7.38       1.70       1.85       6.15       1.44       1.44       1.54       2.55         647.00       1.86       6.25       1.21       1.55       7.47       2.50       671.00       1.86       6.15       1.41       1.41       1.54       2.55         647.00       1.86       6.27       1.33       1.31       1.61       2.46       6.71       1.85       6.43       1.34       1.45       3.50       2.61         6423.27       1.55       7.61       1.23       1.07       1.15       2.54       671.00       1.86       6.33       1.35       1.46       4.14       2.44         6423.07       1.55       7.61       1.23       1.07       1.15       2.54       671.00       1.86       6.33       1.35       1.37       2.44       2.76         6427.00       1.86       6.77       1.33       3.9       2.77       6.45       1.21       1.33       3.77 <td< td=""><td>6601.00</td><td>1.75</td><td>5.59</td><td>149</td><td>181</td><td>2.46</td><td>2.44</td><td>6705.50</td><td>1.77</td><td>6.30</td><td>139</td><td>161</td><td>3.41</td><td>2.41</td></td<>	6601.00	1.75	5.59	149	181	2.46	2.44	6705.50	1.77	6.30	139	161	3.41	2.41
UD72:         C <thc< th="">         C         <thc< th=""> <thc< th=""></thc<></thc<></thc<>	\$602.00	1.77	5.70	145	172	2.97	2.45	6707.00	1.81	6.48	134	153	2.10	. 46
defs         1.73         7.36         120         1.64         0.876         2.46         6711.00         1.87         6.15         1.41         1.41         3.54         2.55           100	UDP2:	_						6710.00	L.86	6.19	144	144	3.54	2.57
Add 1. OD       1. 78       6. 46       133       164       2. 59       2. 47       671 0. 00       1. 68       6. 73       1. 42       1. 18       3. 10       2. 51       2. 45         6417.400       1. 68       6. 57       1. 31       1. 11       3. 61       2. 51       2. 51       2. 55       571 6. 00       1. 68       6. 57       1. 31       1. 11       3. 61       2. 55       562       571 6. 00       1. 68       6. 53       1. 31       1. 51       5. 50       5. 53       1. 55       7. 61       1. 13       1. 15       2. 56       671 6. 00       1. 68       6. 53       1. 31       1. 44       2. 44       2. 44       2. 44       2. 44       2. 44       2. 44       2. 44       2. 44       2. 44       2. 45       6. 71       1. 13       1. 57       2. 54       671 6. 00       1. 68       6. 13       1. 13       1. 37       2. 45       645       1. 31       1. 37       2. 44       4. 24       2. 45       4. 44       2. 44       4. 44       2. 44       4. 44       2. 44       4. 44       2. 45       4. 44       2. 45       4. 44       2. 45       4. 44       2. 45       4. 44       2. 45       4. 44       2. 45       4. 44       4.	6609.75*	1.79	7.36	150	149	0.876	2.46	6711.00	1.87	6.15	141	141	3.54	Z.59
	6613.00	1.78	6.45	133	164	2.59	2.47	6713.00	1.88	6.91	142	136	3.10	2.65
6417.68       1.68       6.21       1.33       1.11       3.61       2.63         6417.60       1.68       6.21       1.33       1.44       1.62       2.63         6420.58       1.68       6.21       1.31       1.44       1.02       2.63         6420.58       1.68       6.21       1.31       1.44       1.02       2.63         6420.58       1.58       7.61       1.23       1.00       1.55       2.54       6715.00       1.66       6.33       1.33       1.45       3.80       2.64         6420.59       1.59       7.61       1.23       1.00       1.55       2.54       6715.00       1.66       6.35       1.33       1.35       2.65         6400.00       2.00       5.70       94.8       1.06       1.37       2.60       6727.00       1.65       6.57       1.22       1.34       2.46       6727.50       1.57       2.21       2.46       4.27       2.24       4.44       2.61       3.67       2.21       6.57       5.27       1.33       3.55       2.65       6.77       1.33       3.55       2.66       6.77       1.33       3.56       2.64       6.77       1.21       3.66 <td>LDP:</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>6714.00</td> <td>I. 66</td> <td>6.75</td> <td>[ 38</td> <td>130</td> <td>2.51</td> <td>Z.6Z</td>	LDP:							6714.00	I. 66	6.75	[ 38	130	2.51	Z.6Z
Halls CO       1.30       6.40       122       1.92       2.54       671,600       1.65       6.27       1.31       1.44       4.10       2.45         GEG3.287       1.53       7.61       1.33       107       1.15       2.56       671,600       1.65       6.39       134       145       4.10       2.45         GEG3.277       1.53       7.61       113       107       1.15       2.56       671,600       1.66       5.93       133       137       2.65         GEZ7.00       1.87       6.53       108       1.92       2.54       672,00       1.66       6.15       130       133       3.55       2.66         GEZ7.00       1.87       6.53       0.70       9.8       6.71       2.65       672,70       1.95       6.57       1.22       1.34       1.25       2.66         GEA1.27       2.05       6.71       9.8       6.71       2.65       672,70       1.95       6.57       1.22       1.34       1.25       2.65         GEA1.27       2.05       6.71       9.8       6.70       0.71       0.55       2.67       0.136       6.16       1.77       1.16       2.76       1.45	6617.83*	1.85	6.25	121	135	1.77	2.50	6715.00	1.89	6.21	133	131	3.61	2.65
Back 3: 3*         1.8*         6.82         1.3         1.30         2.06         2.54         671, 00         1.65         6.3         1.34         1.63         3.90         2.64           Back 3: 2*         1.55         7.61         1.23         1.07         1.15         2.56         671, 80         1.66         6.41         1.33         1.30         3.77         2.64           Back 3: 2*         1.35         7.61         1.23         1.25         2.60         6771, 80         1.67         6.41         1.33         3.35         2.67         6771, 80         1.65         6.55         1.22         1.44         2.60         6772, 80         1.95         6.57         1.24         1.25         2.66           G431, 2*         2.05         6.71         9.8         9.8         9.87         1.41         2.61         377         1.44         2.61         377         1.44         2.61         377         1.44         2.61         377         1.44         2.61         377         1.44         2.61         372         1.35         2.65         6.57         1.23         3.65         2.65         1.30         1.15         2.46         2.71         3.77         2.44	6619.00	1.90	6.60	122	129	1.92	2.54	6716.00	1.86	6.27	133	144	4.10	Z.63
6423.27°       1.55       7.61       123       107       1.15       2.58       6718.00       1.67       6.37       133       133       337       2.45         6623.26°       1.28       6.71       119       97.8       0.971       2.50       6715.00       1.67       6.31       133       133       337       2.45         6627.00       1.28       6.57       104       104       6.18       0.18       6.15       132       133       337       2.45         6617.00       2.00       6.70       94.8       104       1.97       6.43       147       2.60       6773       00       1.96       6.15       122       133       3.59       2.66         6631.287       2.70       7.28       9.50       7.47       0.550       2.66       6772       50       1.96       6.51       127       113       3.76       2.66         6643.30       2.11       6.76       5.6       6.77       133       1.97       6.23       133       1.77       7.83       3.0       7.50       2.66       6.50       131       118       4.21       2.67         6443.30       2.11       6.34       1.59 <td< td=""><td>6620.50°</td><td>1.46</td><td>5.<b>6</b>2</td><td>133</td><td>130</td><td>2.06</td><td>2.54</td><td>6/17.00</td><td>1.85</td><td>6.49</td><td>134</td><td>145</td><td>3.90</td><td>2.63</td></td<>	6620.50°	1.46	5. <b>6</b> 2	133	130	2.06	2.54	6/17.00	1.85	6.49	134	145	3.90	2.63
bb21.4*       1.55       7.61       123       107       1.15       2.58       b719.00       1.94       6.14       1.33       1.33       3.77       2.48         b622.00       1.92       6.35       105       123       1.07       2.54       6719.00       1.46       6.15       130       133       3.55       2.65         b627.00       1.92       6.35       105       1.23       1.77       2.54       6720.00       1.46       6.15       130       133       3.55       2.65         b031.00       2.05       6.71       99.8       94.7       1.41       2.61       9715.00       1.90       6.73       1.26       1.25       1.65       6.57       1.21       1.33       3.57       2.65         b333.00       2.21       6.44       95.5       643.3       3.25       2.66       6778.00       1.99       6.54       1.30       118       4.21       2.67         b443.30       2.22       6.21       1.67       7.20       3.24       6730.00       1.99       6.56       130       108       4.21       2.77         b453.00       2.20       6.36       1.00       1.65       2.71       6733.00	6623.25*	1.95	7.61	123	10/	1.15	2.50	6/18.00	1.86	6.39	136	140	4.14	2.84
back 100       1.39       b / 1       1.12       1.37       3.74       2.60         back 2       00       6.70       94.8       100       1.39       2.60       6715       00       1.85       6.45       105       134       1.55       2.66         ball 25*       2.00       6.77       94.8       106       1.42       2.61       6775       00       1.85       6.57       114       1.65       2.64         ball 25*       2.20       6.71       95.8       95.7       1.42       2.61       577       50       1.97       6.73       122       112       3.59       2.66         644.15*       2.20       6.42       95.6       95.7       6.73       0.19       6.51       1127       113       3.76       2.66         644.35*       2.22       6.21       107       65.4       1.59       2.67       6730.070*       1.96       6.51       130       116       4.21       2.77         645.30       2.22       6.21       106       1.65       2.71       6730.071       196       6.55       130       108       4.21       2.77         6453.30       2.22       7.12       1.20	6623.26*	1.35	7.61	123	107	1.15	6.5	6719.00	1.8/	0 41	133	139	3.77	2.64
back (b)       1.20       6.33       103       1.23       1.07       2.54       672       100       1.39       1.37       1.35       1.25       2.65         back (b)       1.7       2.05       6.71       99.8       94.7       1.41       2.61       975.50       1.90       6.73       1.24       1.26       4.44       2.70         back (b)       2.71       7.26       9.56       6.13       1.35       2.26       6.77       50       1.95       6.57       1.21       1.33       55       2.65         back (b)       2.70       6.32       9.5       9.5       6.72       50       1.95       6.51       1.27       1.113       3.76       2.66         back (b)       2.22       6.21       107       6.3       0.330       2.18       6730.00       1.96       6.41       130       118       4.21       2.77       6443.50       2.22       6.21       1.06       2.64       2.61       6730.00       1.99       6.56       130       100       4.21       2.77       6445.50       2.22       6.21       1.01       3.23       2.44       6.33       1.02       2.77       6455       1.01       1.99       5	6623.00	1.90	•./ <u>1</u>	119	99.8	0.971	7.60	6/19.00	1.00	D. JO	132	139	3.70	2.03
Bash. Ob         2.00         6.70         94.8         1.00         1.39         2.00         671.00         1.90         6.70         1.11         1.12         1.21         2.00           Bash. Sol         2.17         2.18         3.0         96.7         1.41         2.65         377.50         1.96         6.77         1.21         3.58         2.65           Bash. Sol         2.27         2.80         97.75         1.96         6.77         1.33         3.59         2.66           Bash. Sol         2.27         6.16         1.37         6.27         1.13         3.78         2.65           Bash. Sol         2.27         6.73         0.77         1.56         6.16         1.37         1.18         4.21         2.67           Bash. Sol         2.22         6.71         100         69.4         1.59         2.67         6730.00         1.99         6.50         131         116         4.21         2.77           Bash. Sol         2.22         7.7         7.03         2.64         6733.70°         1.99         6.56         130         100         4.21         2.73           Bash. Ob         2.01         2.24         2.25 <th< td=""><td>6627.00</td><td>1.30</td><td>6.33</td><td>105</td><td>123</td><td>1.07</td><td>2.34</td><td>6721.00</td><td>1.05</td><td>5.17</td><td>130</td><td>114</td><td>3.33</td><td>2 69</td></th<>	6627.00	1.30	6.33	105	123	1.07	2.34	6721.00	1.05	5.17	130	114	3.33	2 69
DDI:         OF 1         OF 2         OF 3         DI:         DI: <thdi:< th="">         DI:         DI:         <thdi:< <="" td=""><td>0639.90</td><td>2.90</td><td>0.70</td><td>34.0</td><td>108</td><td>1.33</td><td>2.00</td><td>6725.00</td><td>1.05</td><td>6 70</td><td>127</td><td>176</td><td>1.23</td><td>2.03</td></thdi:<></thdi:<>	0639.90	2.90	0.70	34.0	108	1.33	2.00	6725.00	1.05	6 70	127	176	1.23	2.03
BESLE 30         C-107         P-14         P-16         P-16     -16         P-16         P-1	6631 7.9	2.05	£ 71		05 7	1 41	3 E1	300	1.30	Q.73				
SS77 00       5.11       6.48       2015       6.43       1.54       2.03       6.75       6.73       1.27       1.23       1.26       1.12       3.66       2.66         SS47 5.00       1.27       1.23       1.27       1.23       3.76       2.50       6.16       1.27       1.13       3.76       2.66         SS47 5.00       1.26       6.16       1.27       1.13       3.76       2.66       1.26       6.16       1.27       1.13       3.76       2.66         SS45 5.03       2.21       6.20       1.25       2.71       6730 00       1.96       6.50       1.30       1.86       4.21       2.77         SS50 0.37       2.11       6.47       1.19       7.7       2.03       2.14       6735 00       1.96       6.55       1.30       1.05       2.77       6730 00       1.96       6.54       1.21       1.77       6.75       6730 00       1.96       6.54       1.21       1.11       3.76       2.76       6730 00       1.96       6.54       1.22       1.11       3.76       2.76       6730 00       1.96       6.54       1.21       1.11       3.76       2.76       6730 00       1.96       6.54	6634 50	2.03	7.76	33.0	76 8	1.65	2.01	6727 50	1 96	6 57	. 7	13	1 59	2.55
Ext:         To:         To: <thto:< th=""> <thto:< th=""></thto:<></thto:<>	5637 00	2 21	6.44	95.6	68.3	1.05	2.03	6728 50	1.97	6 23	:26	112	3 66	2 65
540 33*       2:17       6:26       553       0:350       2:56       6730 00       1:96       6:41       130       118       4:21       2:67         6645 50       2:22       6:21       107       634       1.59       2:67       6730 00       1.99       6:56       130       108       4:21       2:67         6645 50       2:22       6:21       107       634       1.59       2:67       6730 00       1.99       6:56       130       108       4:21       2:67         6650 130       1:64       2:61       6736 20°       1.99       6:56       130       109       4:21       2:76         6655 130       1:20       164       2:61       6736 20°       1.99       6:54       122       110       3:28       2:86         6655 19       1:31       1:4       2:02       2:57       6738 00       1.99       6:54       122       112       3:80       2:46         6655 19       1:5       1:64       1:66       2:55       6739 200       1.95       6:44       120       3:80       2:46         6657 10       1:97       6:46       1:22       1:6       6:65       1:20       120	6641 25°	2 20	6 12	87 0	74 7	0.550	2 64	6729 00	1 98	5 16	127	113	3.78	2 64
E45.5         5.2         2.47         6730.207         1.96         6.50         111         118         4.36         2.67           E460.37         2.14         6.47         118         79.7         2.03         2.14         6733.207         1.99         6.65         130         108         4.21         2.76           E450.307         2.01         6.36         130         108         4.21         2.76           E453.50         2.02         6.36         130         108         4.21         2.76           E453.50         2.01         6.28         120         105         2.56         6.77         1.99         6.56         120         103         2.82         2.66           E453.50         2.02         6.59         115         114         2.02         2.57         6738.00         1.99         6.54         120         117         3.90         2.76           E463.56         2.02         6.59         115         104         1.66         2.56         6779.207         1.95         6.54         120         117         1.96         117         1.06         2.76           E467.0         1.96         6.71         109         119 <td>6643 33*</td> <td>2 17</td> <td>6 28</td> <td>96.9</td> <td>83 3</td> <td>0 930</td> <td>2 18</td> <td>6730.00</td> <td>1.96</td> <td>6.41</td> <td>130</td> <td>118</td> <td>4.21</td> <td>2.67</td>	6643 33*	2 17	6 28	96.9	83 3	0 930	2 18	6730.00	1.96	6.41	130	118	4.21	2.67
E488 33*         2 28         7 22         112         56 0         1.65         2 71         6731 00         1.99         6.56         130         108         4 21         2 .77           650 0.3*         2.11         6.47         118         79         7         2.03         2.64         6731 20*         1.99         6.55         135         109         3.74         2.73           653.00         2.02         6.36         120         106         2.64         6736 20*         1.99         6.55         123         110         3.74         2.75           653.0         2.01         6.36         120         104         2.01         2.61         6736 20*         1.99         6.54         123         110         3.74         2.76           653.0         121         113         114         2.02         2.57         6739 00         1.95         6.44         120         120         3.60         2.86           6667.0         1.92         6.30         121         121         1.20         2.54         6740 00         1.95         6.44         120         170         4.63         2.76           6473.77*         1.96         6.71         109 </td <td>6645.50</td> <td>2 22</td> <td>6 21</td> <td>107</td> <td>69 4</td> <td>1.59</td> <td>2 67</td> <td>6730.20*</td> <td>1.96</td> <td>6.50</td> <td>131</td> <td>118</td> <td>4.36</td> <td>2.67</td>	6645.50	2 22	6 21	107	69 4	1.59	2 67	6730.20*	1.96	6.50	131	118	4.36	2.67
6450       0.3*       2.11       6.47       118       79.7       2.03       2.64       6731.20*       1.99       6.65       136       109       4.21       2.73         6453.00       2.02       6.36       120       106       2.64       2.61       6736.00       1.99       6.56       123       110       3.28       2.66         6453.50       2.01       6.28       120       104       2.01       2.61       6736.00       1.99       6.54       123       110       3.28       2.66         6453.60       2.02       6.59       115       104       1.68       2.55       6730.00       1.95       6.44       120       117       3.98       2.76         6463.67**       2.02       6.59       115       104       1.68       2.56       6740.00       1.94       6.55       120       120       4.05       2.66         6471.07*       1.96       6.11       109       119       119       110       1.03       2.76         64667.00       1.92       6.50       121       104       1.68       2.53       6751.00       2.06       7.31       125       9.5       2.74         6473.67*	5549.33*	2.24	7.22	112	58.0	1.65	2.71	6733.00	1.99	6.68	130	108	4.21	2.77
L071:       L0.0	6650 83*	2.11	6.47	118	79 7	2.03	2 54	6733.20°	1.99	6.65	136	109	4.21	2.76
ibits         00         2.02         6.36         120         106         2.68         2.61         6736.00         1.99         6.58         123         110         3.28         2.66           6555         50         2.01         6.28         120         104         2.01         2.61         6736.00         1.99         6.54         122         111         3.40         2.67           6660.67         1.97         6.46         122         117         1.29         2.57         6738.00         1.95         6.44         120         117         3.96         2.74           6663.68         2.02         6.59         115         104         1.68         2.56         6779.20         1.95         6.44         120         120         2.66         2.66           6677.0         1.92         6.30         121         121         1.20         2.54         6741.00         1.94         6.55         120         120         4.63         2.74           6476.42"         2.12         7.00         121         103         3.52         2.63         6752.00         2.06         7.31         123         91.4         4.63         2.71           6460.00	LOTI		••••		••••		• • • •	6734,50	1.99	6.96	130	109	3.74	2.73
6455       50       2.01       6.21       6736       70       1.99       6.54       122       111       3.40       2.67         6457       1.97       6.46       122       117       1.29       2.77       6738.00       1.95       6.54       120       117       3.96       2.76         6463.54       2.02       6.59       115       104       1.68       2.56       6739.00       1.95       6.54       120       120       3.60       2.65         6463.56       2.02       6.59       115       104       1.68       2.56       6740.00       1.94       6.55       120       120       4.03       2.65         6463.67*       1.96       6.71       109       119       1.84       2.53       6752.00       2.06       7.31       125       95       5       5.29       2.74         6476.42*       2.02       7.00       121       103       2.52       2.63       6753.07       2.06       7.31       125       95       5       5.29       2.72         6476.42*       2.02       7.00       121       103       2.52       2.63       6755.37       2.01       7.01       120       10	\$653.00	2.02	6.36	120	106	2.68	2.61	6736.00	1.99	6.58	123	110	3.28	2.66
6457. 03       1.99       6.31       113       114       2.02       2.57       6738.00       1.96       6.61       119       116       4.29       2.74         6660.67       1.97       6.46       122       117       1.29       2.57       6738.00       1.95       6.44       120       117       3.98       2.76         6663.58       2.02       6.59       115       104       1.68       2.56       6739.20*       1.95       6.54       120       120       3.60       2.58         6467.00       1.92       6.30       121       121       1.20       2.54       6741.50       1.98       6.55       120       120       4.05       2.65         6473.67*       1.96       6.71       109       119       1.86       2.53       6752.00       2.06       7.21       123       91.4       4.63       2.71         19*       .       1.86       2.53       6753.00       2.06       7.31       120       100       5.34       2.68         6467.00       2.13       7.25       129       79.9       2.65       2.60       6735.64*       2.04       7.33       120       99.1       5.33       2.72<	6655.50	2.01	6.28	120	104	2.01	2.61	6736.20*	1.99	6.54	122	111	3.40	2.67
6660.67         1.97         6.46         122         117         1.29         2.57         6739.00         1.95         6.44         120         117         3.98         2.76           6663.58         2.02         6.59         115         104         1.68         2.56         6779.00         1.94         6.55         120         120         3.60         2.66           6667.00         1.92         6.50         120         1.60         2.66         6779.00         1.94         6.55         120         120         3.60         2.65           667.00         1.92         6.50         124         102         4.05         2.74           657.00         2.02         7.00         121         103         3.52         2.63         6753.00         2.06         7.31         125         95         5.45         2.74           6670.50         2.05         7.41         129         91.8         2.86         2.57         6755.50         2.04         7.33         120         99.1         5.39         2.72         6590.92         2.05         7.41         128         91.8         2.86         2.57         6755.50         2.04         7.31         180 <td< td=""><td>6657.83</td><td>1.99</td><td>6.31</td><td>113</td><td>114</td><td>2.02</td><td>2.57</td><td>6738.00</td><td>1.96</td><td>6.61</td><td>119</td><td>116</td><td>4.29</td><td>2.74</td></td<>	6657.83	1.99	6.31	113	114	2.02	2.57	6738.00	1.96	6.61	119	116	4.29	2.74
6463.5         6.9         115         104         1.68         2.56         6739.20°         1.95         6.54         120         120         3.60         2.56           6463.67         2.02         6.59         115         104         1.68         2.56         6740.00         1.96         6.55         120         120         4.05         2.66           6473.67°         1.96         6.71         109         119         1.86         2.53         6750.00         2.02         6.80         124         102         4.74         2.75           6476.42°         2.02         7.00         121         103         3.52         2.83         6750.00         2.06         7.21         123         91.4         4.63         2.71           7880.00         2.13         7.25         129         90.8         2.45         2.56         6756.63°         2.03         7.01         120         100         5.38         2.72           6490.00         2.95         7.41         128         91.8         2.88         2.55         6756.4°         2.04         7.33         120         99.1         5.33         2.72           6490.00         1.91         6.95	<b>666</b> 0.67	1.97	6.46	122	117	1.29	2.57	6739.00	1.95	6,44	120	117	3.98	2.70
6663.67"         2.02         6.59         115         104         1.66         2.56         6740.00         1.94         6.53         120         120         4.05         2.65           6647.00         1.92         6.30         121         121         1.20         2.54         6741.50         1.96         7.15         117         110         4.03         2.66           6476.42"         2.02         7.00         121         103         3.52         2.63         6753.00         2.06         7.21         123         91.4         4.63         2.71           1W:         7.00         121         103         3.52         2.63         6753.00         2.06         7.31         120         99.1         5.36         2.66           5600.00         2.13         7.25         129         99.9         2.85         2.66         6755.66"         2.04         7.33         120         99.1         5.39         2.72           6560.00         1.91         6.79         122         17         1.01         2.52         6739.56"         2.04         7.33         120         99.1         5.39         2.72           6560.00         1.88         6.05 <t< td=""><td>6663.58</td><td>2.02</td><td>6.59</td><td>115</td><td>104</td><td>I.60</td><td>2.56</td><td>6739.20*</td><td>1.95</td><td>6.54</td><td>120</td><td>120</td><td>3.60</td><td>2.58</td></t<>	6663.58	2.02	6.59	115	104	I.60	2.56	6739.20*	1.95	6.54	120	120	3.60	2.58
6667.00         1.92         6.30         121         121         1.20         2.54         6741.50         1.96         7.15         117         110         4.03         2.66           6673.67"         1.96         6.71         109         119         1.86         2.53         6752.00         2.06         7.31         125         95.6         5.23         2.74           6676.42"         2.02         7.00         121         103         2.52         2.63         6752.00         2.06         7.21         123         91.4         4.63         2.74           5460.00         2.13         7.25         129         95.9         2.65         2.60         6756.63"         2.03         7.01         120         100         5.39         2.76           5600.50         2.05         7.41         129         91.8         2.88         2.57         6757.50         2.04         7.35         118         103         3.89         2.72           6695.00         1.91         6.73         1.22         117         1.01         2.52         6759.58"         2.03         7.57         116         103         3.67         2.74           6696.00         1.90	6663.67*	2.02	6.59	115	104	1.68	2.56	6740.00	1.94	6.55	120	120	4.05	2.65
Larrz:         6/31.00         2.02         8.00         124         102         4.74         2.72           6473.67*         1.96         6.71         109         119         1.86         2.53         6752.00         2.06         7.21         123         91.4         4.63         2.74           6476.42*         2.02         7.00         121         103         2.52         2.63         6753.00         2.06         7.21         123         91.4         4.63         2.71           5600.2         2.05         7.41         129         9.9         2.65         2.60         6756.63*         2.03         7.01         120         100         5.34         2.69           6605.00         2.05         7.41         128         91.8         2.86         2.57         6735.56*         2.04         7.33         120         99.1         5.39         2.72           6667.00         1.91         6.79         122         117         1.01         2.52         6736.59*         2.03         7.57         118         103         3.457         2.72           6667.00         1.80         6.51         141         125         4.02         6750.59*         2.03	6667.00	1.92	6.30	121	121	1.20	2.54	6741.50	1.98	7.15	117	110	4.03	Z.68
6473.67"       1.96       6.71       109       119       1.86       2.53       6752.00       2.06       7.31       125       39.6       5.27       2.71         1W:       2.02       7.00       121       103       3.52       2.63       6753.00       2.06       7.31       123       39.4       4.63       2.71         1W:       2.02       7.00       121       103       3.52       2.63       6753.00       2.06       7.21       123       39.4       4.63       2.71         5600.00       2.13       7.25       129       79.9       2.65       2.60       6756.45"       2.04       7.33       120       99.1       5.39       2.72         6500.92       2.05       7.47       128       91.8       2.48       2.55       6756.59"       2.01       6.75       118       97.0       5.32       2.72         6697.00       1.88       6.05       161       126       4.06       2.50       6759.59"       2.03       7.57       116       101       4.69       2.74         6689.00       1.88       6.05       161       125       132       3.09       2.47       6760.59"       2.03       7.	L072:							6751.00	2.02	6.80	124	102	4.74	2.75
68/6.47"       2.02       7.00       121       103       2.32       2.63       b735.00       2.06       7.11       123       31.4       4.63       2.74         5460.00       2.13       7.25       129       99.9       2.65       2.60       6755.63"       2.03       7.01       120       100       5.34       2.65         6560.50       2.06       7.41       129       98.8       2.65       2.66       6756.46"       2.04       7.35       118       97.0       5.39       2.72         6560.50       1.91       6.79       122       117       1.01       2.52       6738.58"       2.04       7.35       118       97.0       5.32       2.76         6687.00       1.90       6.72       135       132       2.16       2.49       6761.58"       2.04       7.10       117       96.3       4.57       2.71         6689.00       1.80       6.59       135       136       2.66       2.47       6762.59"       2.03       7.52       116       99.7       4.12       2.71         6499.00       1.80       6.59       135       136       2.66       2.47       6762.50       2.03       7.52	66/3.6/*	1.96	6.71	109	119	1.86	2.53	6/52.00	2.06	7.31	125	32.0	5.29	2.14
Inf:         0.34         24         2.04         0	66/6.42"	2.92	7.00	121	103	3.52	Z.6J	B/33.UU	2.00	1.61	123	31.4	4.03	2.71
Seed. 00         2.13         7.43         1.29         8.13         2.60         1.23         6.13         7.01         1.20         1.00         1.24         2.05           6580. 50         2.06         7.41         1.29         80.8         2.46         2.56         6755. 50         2.04         7.36         1.18         97.0         5.32         2.72           6580. 50         2.05         7.47         1.28         91.8         2.46         2.57         6757. 50         2.04         7.36         1.18         97.0         5.32         2.72           6687.00         1.98         6.05         141         126         4.06         2.5G         6759.58*         2.03         7.57         116         101         4.65         2.74           6689.00         1.88         6.05         141         125         132         2.19         2.49         6761.54*         2.04         7.10         117         96.3         4.57         2.71           6699.00         1.88         5.99         135         131         1.86         2.48         6764.50         2.03         7.52         116         99.7         4.12         2.71           6499.00         1.88 <td>1771</td> <td></td> <td>2.24</td> <td>1.20</td> <td></td> <td></td> <td></td> <td>5/34.3V 5765.53*</td> <td>2.04</td> <td>7 01</td> <td>120</td> <td>1/00</td> <td>5.45</td> <td>2.00</td>	1771		2.24	1.20				5/34.3V 5765.53*	2.04	7 01	120	1/00	5.45	2.00
Constrain         Constrain <thconstrain< th=""> <thconstrain< th=""> <thc< td=""><td>7000.00</td><td>2.13</td><td>1.23</td><td>129</td><td>79.9</td><td>2.65</td><td>2.00</td><td>6756 A6*</td><td>2.03</td><td>7 33</td><td>120</td><td>99.1</td><td>5.34</td><td>2 72</td></thc<></thconstrain<></thconstrain<>	7000.00	2.13	1.23	129	79.9	2.65	2.00	6756 A6*	2.03	7 33	120	99.1	5.34	2 72
0.300, 24, 2       0.30, 1, 27       120       91, 0       2.40       137       0.21, 29       1.00       <	6680.00	2.00	7.41	129	00.0	2.40	2.30	6757 50	2.04	7 36	118	97 0	5 37	2 80
Seed of the transmission of the transmission of the transmission of transmissi transmission of transmission of transmissi transmission	6685 00	1 01	6 78	122	31.0	2.00	2.3/	6758 58*	2 01	6 79	118	103	3.89	2 72
Seene         Diago         Constrained         Constrained <thconstraine< th="">         Constane         <thconstane< t<="" td=""><td>6687 00</td><td>1.51</td><td>6.05</td><td>141</td><td>126</td><td>4.06</td><td>2.50</td><td>6759 52*</td><td>2.03</td><td>7.57</td><td>116</td><td>101</td><td>4.69</td><td>2.74</td></thconstane<></thconstraine<>	6687 00	1.51	6.05	141	126	4.06	2.50	6759 52*	2.03	7.57	116	101	4.69	2.74
6669         00         1.80         6.11         135         132         3.09         2.69         6761         133         2.03         7.04         116         99.3         4.55         2.76           6499.00         1.88         6.59         135         136         2.68         2.47         6762.50         2.03         7.04         116         99.3         4.55         2.71           6490.00         1.88         6.99         135         131         1.66         2.48         6764.50         2.03         7.02         116         99.3         4.72         2.71           6492.00         1.89         6.33         138         129         2.42         2.49         6766.59         2.07         7.73         123         90.5         4.73         2.83           6492.00         1.89         6.30         141         133         3.51         2.47         49         6765.59         2.06         6.91         121         89.5         5.03         2.72           6493.00         1.82         6.67         1.44         3.54         2.46         6767.59*         2.06         6.91         121         89.5         5.03         2.72           6495.00	5588 00	3 90	6 72	135	132	2 18	2 49	5750 58°	2.04	7.10	117	96.3	4.57	2.71
6699 00         1.88         5.99         135         136         2.68         2.47         6762 50         2.03         7.52         116         99.7         4.12         2.71           6491 00         1.88         6.89         135         131         1.86         2.48         6762 50         2.03         7.52         116         99.7         4.12         2.71           6492 00         1.89         6.33         136         129         2.42         2.48         6765 50         2.07         7.73         123         90.5         4.73         2.83           6492 00         1.89         6.30         141         133         3.51         2.47         444         471         2.83           6492 00         1.85         6.59         142         144         3.54         2.46         6767 59*         2.06         6.91         121         89.5         5.03         2.72           6493 00         1.82         6.51         142         144         2.97         2.46         6767 59*         2.06         6.91         121         89.5         5.03         2.72           6496 00         1.82         6.69         143         1.74         2.46 <th< td=""><td>5589.00</td><td>1.88</td><td>\$ 11</td><td>135</td><td>132</td><td>3 09</td><td>2 49</td><td>6761.63*</td><td>2.03</td><td>7.04</td><td>118</td><td>99.3</td><td>4.55</td><td>2.78</td></th<>	5589.00	1.88	\$ 11	135	132	3 09	2 49	6761.63*	2.03	7.04	118	99.3	4.55	2.78
669:00         1.00         6.09         135         131         1.06         2.48         6764.50         2.03         6.90         120         103         5.18         2.83           278:         6765.50         2.02         7.22         120         99.4         4.71         2.83           649:         00         1.89         6.33         138         129         2.42         2.49         6765.50         2.07         7.73         123         99.5         4.71         2.83           6492.50         1.80         6.30         141         133         3.51         2.47         44           6493.00         1.85         6.59         143         144         2.54         2.46         6767.59*         2.06         6.91         121         89.5         5.03         2.72           6495.00         1.82         6.67         143         144         2.97         2.46         6767.59*         2.06         6.91         121         89.5         5.03         2.72           6495.00         1.82         6.67         144         147         2.64         2.47         6768.59*         2.06         6.91         121         89.5         5.03         2.72<	6690.00	1.88	6 59	135	136	2 68	2 47	6762.50	2.03	7 52	116	99.7	4.12	2.71
2mi         6765.50         2.02         7.72         120         99.4         4.71         2.83           6492.00         1.89         6.33         138         125         2.42         2.49         6766.58*         2.07         7.73         123         90.5         4.73         2.80           6492.50         1.80         6.30         141         133         3.51         2.47         44           6493.00         1.85         6.59         142         144         3.54         2.46         6767.59*         2.06         6.91         121         89.5         5.03         2.72           6495.00         1.82         6.67         144         147         2.64         2.47         6769.59*         2.06         6.91         121         89.5         5.03         2.72           6495.00         1.82         6.67         144         147         2.64         2.47         6769.59*         2.06         7.34         123         92.2         4.79         2.73           6495.00         1.82         6.69         145         150         0.379         2.42         6771.50*         2.08         6.80         124         100         4.63         2.67	669:.00	1.00	6.89	135	131	1.86	2.48	6764.50	2.03	6.90	120	103	5.18	2.83
6452         00         1.89         6.33         138         129         2.42         2.49         6766.58"         2.07         7.73         123         90.5         4.73         2.80           6452.50         1.89         6.30         141         133         3.51         2.47         4H         6766.58"         2.07         7.73         123         90.5         4.73         2.80           6492.50         1.85         6.58         142         144         3.54         2.46         6767.59"         2.06         6.91         121         89.5         5.03         2.72           6454.00         1.82         6.57         1.44         1.47         2.64         6767.59"         2.06         6.91         121         89.5         5.03         2.72           6459.00         1.82         6.57         1.44         1.47         2.64         6767.59"         2.06         6.91         121         89.5         5.03         2.72           6459.00         1.82         6.67         1.44         1.74         2.46         6770.50"         2.02         6.80         124         100         4.63         2.67           6459.00         1.80         6.73	211:							6765.30	2.02	7.22	120	99.4	4 71	2.83
6692.50         1.80         6.30         141         133         3.51         2.47         44           6693.00         1.85         6.58         142         144         3.54         2.46         6767.59*         2.06         6.91         121         89.5         5.03         2.72           6693.00         1.82         6.59         143         144         2.97         2.46         6767.59*         2.06         6.91         121         89.5         5.03         2.72           6495.00         1.82         6.57         144         147         2.64         2.47         6766.59*         2.06         6.91         121         89.5         5.03         2.72           6495.00         1.82         6.67         144         147         2.64         2.47         6766.59*         2.06         6.91         121         89.5         5.03         2.72           6495.00         1.82         6.64         145         150         2.75         2.45         6770.50*         2.02         6.80         124         100         4.63         2.67           6499.00         1.80         6.51         1.42         150         0.3*9         2.42         6773.50	6692.00	1.89	6.33	138	129	2.42	2.49	6756.58*	2.07	7.73	123	90.5	4.73	2.80
6693.00         1.85         6.58         142         1.44         3.54         2.46         6787.58*         2.06         6.91         121         89.5         5.03         2.72           6694.00         1.82         6.59         143         148         2.97         2.46         6787.58*         2.06         6.91         121         89.5         5.03         2.72           6495.00         1.82         6.67         1.44         147         2.64         6787.59*         2.06         6.91         121         89.5         5.03         2.72           6496.00         1.82         6.67         1.44         1.74         2.46         6787.59*         2.06         6.91         121         89.5         5.03         2.72           6496.00         1.81         6.62         147         1.48         1.74         2.45         6771.50         2.02         6.80         122         102         4.63         2.67           6497.00         1.82         6.69         1.45         150         0.379         2.42         6771.50         2.03         6.35         124         100         4.63         2.67           6499.00         1.78         6.51         142	6692.50	1.80	6.30	141	133	3.51	2.47	414						
6696         1.82         6.59         1.43         1.49         2.97         2.46         6787.59*         2.06         5.91         121         89.5         5.03         2.72           6495.00         1.82         6.67         1.44         147         2.64         2.47         6789.59*         2.08         7.34         123         92.2         4.79         2.73           6495.00         1.81         6.62         147         1.44         1.74         2.64         2.47         6789.59*         2.08         7.34         123         92.2         4.79         2.73           6497.00         1.81         6.52         147         1.44         1.74         2.45         6770.50*         2.02         6.80         124         100         4.63         2.70           6499.00         1.82         6.69         1.45         150         9.75         2.42         6772.63*         2.02         6.66         124         105         4.75         2.75           6499.00         1.78         6.51         1.42         156         0.796         2.42         6773.50         1.99         6.90         124         105         4.75         2.75           6700.00	6693.00	1.85	6.58	142	144	3.54	2.46	6767.58"	2.06	6.91	121	89.5	5.03	2.72
6495.00         1.82         6.67         144         147         2.64         2.47         6768.58°         2.08         7.34         123         92.2         4.79         2.73           6696.00         1.81         6.62         147         148         1.74         2.45         6770.50°         2.02         6.80         124         100         4.63         2.70           6697.00         1.82         6.60         145         150         2.75         2.45         6771.50         2.03         6.54         125         102         4.68         2.67           6699.00         1.80         6.73         144         150         0.379         2.42         6773.50         1.99         6.80         124         105         4.75         2.75           6790.00         1.78         6.51         142         156         0.262         6773.50         1.99         6.90         124         107         4.36         2.72           6700.00         1.75         6.43         143         166         1.28         2.42         6776.67°         2.00         6.85         126         107         4.95         2.72           6701.00         1.76         6.11	6694.00	1.82	6.59	143	148	2.97	2.46	6787.59*	2.06	6.91	121	89.5	5.03	2.72
6495         00         1.81         6.62         147         1.46         1.74         2.46         6770.50"         2.02         6.80         124         100         4.63         2.70           6497.00         1.82         6.69         1.45         150         2.75         2.45         5771.50         2.03         6.54         125         102         4.68         2.67           6499.00         1.80         6.73         144         150         0.379         2.42         6772.63"         2.02         6.66         124         105         4.75         2.75           6499.00         1.78         6.51         142         156         0.786         2.42         6773.50         1.99         6.60         124         107         4.35         2.75           6499.00         1.75         6.43         142         156         1.28         2.42         6776.67"         2.00         6.80         124         107         4.35         2.75           6700.00         1.76         6.11         1.65         1.29         2.38         6776.67"         2.00         6.80         126         107         5.02         2.31           6770.00         1.76         <	6695.00	1.82	6.67	144	147	2.64	2.47	6768,58*	2.08	7.34	123	92.2	4.79	2.73
6497.00         1.82         6.69         145         150         2.75         2.45         6771.50         2.03         6.54         125         102         4.68         2.67           6699.00         1.80         6.73         144         150         0.379         2.42         6772.63         2.02         6.66         124         105         4.75         2.75           6699.00         1.78         6.51         142         156         0.796         2.42         6773.50         1.99         6.50         124         107         4.35         2.72           6700.00         1.75         6.43         143         165         1.28         2.42         6773.64"         2.00         6.95         126         107         4.35         2.72           6701.00         1.76         6.11         145         165         1.29         2.38         6777.64"         2.00         6.95         126         107         4.95         2.63           6701.00         1.76         6.11         146         165         1.29         2.38         6777.64"         2.00         6.95         126         107         5.07         2.81           6701.07         6.77         <	6696.00	1.81	6.62	147	148	1.74	2.46	6770.50"	2.02	6.80	124	100	4.63	2.70
6599         00         1.80         6.73         1.44         1.50         0.379         2.42         6772.63"         2.02         6.86         124         105         4.75         2.75           6599         00         1.76         6.51         1.42         156         0.766         2.42         6773.50         1.99         6.90         124         107         4.35         2.72           6700.00         1.75         6.42         143         165         1.28         2.42         8776.67"         2.00         6.85         125         109         4.95         2.69           6701.00         1.76         6.11         146         166         1.29         2.38         6777.46"         2.00         6.83         126         107         5.07         2.81           6778.54"         2.01         6.83         127         106         5.23         2.71           6779.50         2.01         6.83         127         102         4.94         2.78           8790.44"         2.01         6.83         127         102         4.94         2.78           6779.50         2.01         6.83         127         102         4.94         2.78 <td>6697.00</td> <td>1.82</td> <td>6.50</td> <td>145</td> <td>150</td> <td>9.75</td> <td>2.45</td> <td>6771.50</td> <td>2.03</td> <td>6.54</td> <td>125</td> <td>102</td> <td>4.68</td> <td>2.67</td>	6697.00	1.82	6.50	145	150	9.75	2.45	6771.50	2.03	6.54	125	102	4.68	2.67
Bestry UQ         1.78         6.51         142         156         0.786         2.42         6773.50         1.99         6.50         124         107         4.36         2.72           6700.00         1.75         6.42         143         166         1.28         2.42         6776.67*         2.00         6.65         125         109         4.95         2.69           6701.00         1.76         6.11         146         165         1.29         2.38         6777.64*         2.00         6.95         125         109         4.95         2.81           6701.00         1.76         6.11         146         165         1.29         2.38         6777.64*         2.00         6.95         126         107         5.07         2.81           6778.54*         2.01         6.88         127         106         5.23         2.71           6799.50         2.01         6.88         127         105         5.01         2.78           8790.44*         2.01         5.83         127         105         5.01         2.78	6698.00	1.80	6.73	144	150	0.319	2.42	6772.63*	2.02	6.86	124	105	4.75	2.75
b/pu.uu         1.75         b.43         143         165         1.28         2.42         b/f6.9/ <sup>2</sup> 2.00         6.95         125         109         4.95         2.63           6701.00         1.76         6.11         146         165         1.29         2.38         6777.46 <sup>4</sup> 2.00         6.90         126         107         5.07         2.81           6701.00         1.76         6.11         146         165         1.29         2.38         6777.46 <sup>4</sup> 2.01         6.94         127         105         5.23         2.71           6701.50         2.01         6.83         127         105         5.23         2.71         6779.50         2.01         6.83         127         102         4.94         2.78           879n.444         2.01         6.84         127         102         4.94         2.78         879         6.01         6.83         127         102         4.94         2.78	6699.00	1.78	6.51	142	156	0.786	2.42	6773.50	1.979	6.90	124	107	4.35	2.72
07/01.00 1.75 5.11 145 155 1.29 2.38 5777.45 2.00 5.50 120 107 5.07 2.81 6778.54° 2.01 6.98 127 106 5.23 2.71 6779.50 2.01 6.88 127 102 4.94 2.78 8780.44° 2.01 6.83 127 102 4.94 2.78	6/00.00	1.75	6.43	143	166	1.20	2.42	6//6.6/*	2.00	0.05	120	109	6.95	2.09
6779.50 2.01 6.83 127 102 4.94 2.78 6779.50 2.01 6.83 127 102 4.94 2.78 8780.487 2.01 6.87 127 105 4.01 2.78	e/ut.00	1.76	6.11	146	196	1.29	2.30	0///.40" #778 #4*	2.00	0.3U 4.04	127	106	5.0/	2.01
0779.34 2.55 5.500 127 102 4.57 2.7 8780 487 2.01 8.67 132 105 6.01 2.78								6,776 40	2.01	6 82	127	102	4 94	2 78
								5790 AL*	2 01	5.00	127	105	5 01	2 70

÷	(a/cm <sup>3</sup> )	ж,	10 (1/57)	(chs)	5Ì	5
-191.56*	8	3	8	112	5.15	2.74
-1.2	8	3	2	8	5.16	2.74
-15.74	2,01	8	127	107	5.75	2.71
8	8.1	3	<b>R</b> 1	==	97. S	3~~
	8	3	R	112	5.73	<u>م</u>
	8	1.13	821	112	5.17	<b>8</b> .2
-22.96	1.97	6.75	8.1	110	5.11	2.70
	1.97	2	ß	9	3	2.70
	*	2.3	2	511	5.8	2.74
DA ME		7.14	122	011	4	2.2
225.26	R	8.2	117	ğ	3	2.75
	8.7	2.8	611	8	4.27	<b>3</b> .5
	3	<b>2</b> 3	124	511	5.27	2.70
-11. 20m	8~	10.7	115	J.X	16.9	2.77
	2.01	2	115	8	5.17	2.7
2.7	8	3	611	8	5.18	2.75
3.50		5 2	116	8	3	2.67
106.42	2.01	8.~	114	ă	<b>5</b> .5	3.2
- 17. (Q.1	<b>3</b> .6	10.4	115	6.78	£7.4	<b>69</b> .2
5	1		311		5	
				B		: 1
	8.2		•		16.0	51.7

# **APPENDIX VII**

### Well-Logging Data for E-lx. Depth in Feet.

Depth	GR (GAPI)	CAL1 (inch)	DT (us/f)	ЯН08 <sub>3</sub> (g/cm <sup>3</sup> )	SNP (PU)	SP (mV)	SN (Ohm m)	IL (Chaine)	LL (0hma as)	PILL (Chun st)	N(SN) (Chun m)	NOR (Den m)
UOP1:												
6734.00	14.7	11.8	100	2.27	26.3	29.2	1.96	1.79	1.76	3.93	1.39	1.76
6737.00	12.8	11.9	112	2.09	34.5	12.3	1.55	1.09	I.24	Z.90	1.03	1.24
5738.42°	11.3	11.9	109	2.05	36.7	0.881	1.34	0.885	I.14	Z.35	0.972	1.08
5742.42"	11.7	11.9	108	Z.10	35.6	0.861	1.10	0.649	0.922	1.58	0.967	0.922
5744.42" JOP2:	12.0	12.0	106	2.07	38.7	0.764	1.07	0.715	0,854	1.75	1.00	0.854
749.00	13.3	11.8	108	2.08	37.8	8.91	1.05	0.714	0.830	1.75	1.08	0.830
753.42"	11.3	11.8	107	Z.09	37.0	0.627	1.04	0.710	0.862	1.74	1.15	0.862
758.00	12.0	11.9	111	2.06	37.9	7.21	0.968	0.664	C.839	1.83	1.12	0.839
5763.42"	10.1	11.8	108	2.05	38.7	0.803	0.996	Q. 601	0.805	1.53	1.15	0.805
5763.00 .0P:	10.6	11.5	107	2.09	36.6	1.21	1.06	0.782	0.850	1.50	1.09	0.850
5767.00	8.81	11.8	108	2.08	33.6	7.33	1.11	0.762	1.37	2.33	1.18	1.07
5770.00	11.3	12.0	106	2.07	36.0	9.04	1.09	0.753	0.858	1.91	1.01	0.856
5774.00	11.1	11.7	102	2.13	33.5	8.96	1.27	0.908	1.09	1.05	0.936	1.09
5780.42"	11.4	11.9	103	2.08	37.7	0.692	1.61	1.16	1.26	2.41	0.917	1.25
5783.00	12.9	11.9	112	2.12	34.2	8.33	1.37	0.919	1.32	2.48	0.850	1.32
5795.00	13.4	11.9	95.2	2.16	33.0	11.4	1.49	1.05	1.10	2.25	C.952	1.10
5798.42*	12.0	11.9	98.5	2.21	31.9	16.3	1.53	1.15	1.42	Z.76	0.978	1.42
500.33°	11.2	11.9	104	Z. 10	36.9	12.4	1.32	0.897	1.13	2.11	0.556	1.13
500Z.00	11.6	11.9	99.0	Z.08	36.4	11.0	1.34	0.8/7	1.10	1.78	0.780	1.10
HEU7.42"	12.1	12.2	98.9	Z.18	33.6	13.3	1.54	1.08	1.22	2.5/	1.01	1.22
NG10.000 NDT:	13.0	12.0	86.7	2.22	29.0	10.2	1.90	1.38	1,45	2.47	0.994	1.45
ið 12 . 42*	13.4	12.1	85.2	2.24	30.6	17.0	2.28	1.80	1.84	3.35	1.16	E.84
5815.00	12.6	12.0	78.0	2.36	22.5	25.0	3.11	2.88	2.45	6.12	1.86	2.45
5820.00	13.2	12.1	84.0	2.33	19.3	25.8	2.90	2.44	2.70	3.96	1.62	2.70
5822.00	11.7	12.1	80.1	2.33	23.7	25.3	2.90	2.32	2.33	6.09	1.80	2.33
5826.25*	12.9	12.0	81.I	2.33	21.9	24.3	2.75	2.43	2.36	4.07	1.75	2.36
5829.00 .DT1:	13.5	11.9	87.6	2.34	22.5	22.9	2.47	1.95	2.43	5. <b>3</b> I	1.46	2.43
5833 42*	11.3	11.9	95.7	2.19	32 0	16.7	1.94	1.31	1.65	3 32	1.17	1.66
5836 42*	11.9	11.9	93.8	2.18	33.8	12.0	1.99	1.30	1.69	7.86	1.01	1.59
5841.00	10.0	11.9	88.1	2.19	33.7	11.0	2.10	1.42	1.31	2.17	1.03	1.31
5846.00	10.1	11.9	94.4	2.15	31.0	11.9	1.81	1.11	1.37	3.17	1.41	1.37
5848.42*	11.1	12.1	96.5	2.16	30.8	13.2	1.86	1.21	1.43	2.34	1.47	1.43
5852.00	12.2	11.8	85.4	2.42	21.4	25.9	2.34	1.98	2.08	3.34	1.64	2.08
5855.00	13.3	11.8	96.9	Z.20	28.1	21.4	1.85	1.34	1.85	2.42	1.08	1.85
5857.00	11.3	12.1	98.0	2.20	32.0	22.1	1.61	1.15	1.38	2.81	1.08	1.38
5861.00	14.1	12.0	95. O	Z. 19	29.6	19.3	1.81	1.22	1.79	2.83	1.05	1.79
5864.42*	10.6	11.7	90.2	2.24	28.8	15.1	1.85	1.27	1.40	2.50	0.922	1.46
5866.00	12.4	11.6	83.1	2.30	24.5	20.Z	2.23	1.72	1.67	1.99	1.07	1.67
5568.35*	14.7	12.0	96.2	2.31	20.8	21.3	2.76	2.14	2.36	2.89	1.24	2.36
58/2.00 LH:	12.6	11.9	90.3	2.28	29.2	17.9	2.52	1.82	1.87	2.65	1.12	1.87
5876.25*	8.39	12.0	77.8	2.42	21.0	14.3	3.24	2.16	2.69	5.20	1.06	2.69
5879.50	10.7	11.8	86.4	2.31	26.5	9.93	2.49	1.59	2.34	26.2	1.14	2.34
5881.50	11.5	11.8	88.9	2.28	27.7	9.00	2.12	1.39	1.83	2.76	0.946	1.83
6890,00	12.4	12.8	92.9	2.19	28.9	7.63	1.73	1.20	1.39	3.10	0.936	1.39
5892.25" 2H:	10.8	13.0	86.0	2.20	31.6	7.75	1.82	1.27	1.34	3.10	0.868	1.34
5895.00	11.4	12.6	90.0	2.21	31.7	7.10	1.60	1.02	1.38	2.83	0.711	1.38
00.8666	9.08	12.6	96.4	2.14	34.2	7.17	1.42	0.959	1.22	2.81	0.551	1.22
6901.00	10.8	12.8	97.4	2.13	30.9	5,74	1.29	0.890	1.09	2.67	0.601	1.09
												-

# **APPENDIX VIII**

## Selection of Abbreviations Used in Well-Logging.

A	Amount of ell/ges in unit volume of reservoir ruck A seresty "hydrocaroon saturation	FACTOLOS	Interpretation method using electrofacies
100 L	Santo lag Amalitude fran EZ	FCIIIL.	CDL log Far detector
ĸ	Boratale Componsated Samic Log perestly increases Dt values	FIC	Formation Density Componsated Top modium-energy games rays (Compton scattering) two detectors
CAL I	Caliger		ail dats not change the the value significantly presence of gas will lower the apparent the
CBL.	Senic leg El ambitude for CBL	61,0841	A statistical interpretation method
CER	Corructed Gome Ray Total GR minus Uransum	687	Hestron log detector sensitive to both high-energy capture gamma rays and to thermal newtrees encortantion in common bulkers
cu	Induction tool conductivity		run excentric to ennimize beruhale effects
Cn.B	Indiction Top Doep conductivity	68	Gamma ray lag gress caunt rate APE units
	Comparisoned neutron log (perusity determinations) dual spectra, thermal neutrons ratio af counting rates from two detectors	615	Gome rey log spectrumetry for U_Th.K
	16 Curie source (little statistical fluctuation) radial death of investigation		Hydragen index of Hydracorbons
	ret good in gas-filled beins often run in cambination with FDC	h <sub>es</sub>	Thickness of mud cake
CORISHIND	Cashinad program	н Т	Hydrogen index of solt weler H = 1 - 0.4"P T Pr McCl companymentian in ana <sup>2</sup> 10 <sup>-6</sup>
CS	Cable spadd		
Ct	Total conductivity		Induction Electrical Survey Induction Tag
91L	Buol Induction Log includes: Dean Induction Tax: ILd	11	conductivity messired
	Andium Linduction Log: ILD Laterolog 8, LLO Log: ILP	ILO	Deep-reading induction device
	5P SFL (SFLU) gives the A of the flushed zone ID indicates A of flushed and invade? zones ID gives the A of the uncontamineted zone (A <sub>g</sub> )	Tun TSF/SQNEC	Pladium induction device Combination log includes: Itd SFL co
	Bulk density correction determined frum RDC		MCSonic GR
0t-81 01	Delta t - travel time of an acoustic wave in SONIC log	11	Senic leg Internal transit time
Dt f	Transit time in pone fluid Transit time in rock matrix	ĸ	absolute permembility
<b></b> ES	Electrical Survey (resistivity logs)	×.	effective permobility for oil
	50 16" Hermal: shellewest peretration 64" Hermal	ĸ	relative permeability K <sub>ré</sub> = K <sub>é</sub> / K
	10'0" Lateral: deepest penetration	× <sub>rw</sub>	relative permeability for dil-water system K <sub>man</sub> = K <sub>m</sub> / K
F	Formation registivity factor F = a / Phi a - determined ampirically m = commitation factor? Sands: F = 0.81 / Dhi Compacted formation: F = 1 / Phi	۲.,	effective permoobility for motor

Laterolog 3	Fecusing-electrode teal (electrical teg) LL3 Jacom electromite are used		Neutron perestay determined by CNL
	hetter resolution and more detail than LL7 after recorded with GR	T ARM	Newtran ratia fran CN. NCNL/FCNL
Laterslag 7	Focusing electrode tool (electrical log) Contor electrode plus 3 peres of electrodes	,	NaC: cuncentration
	107	₩Ę ł	Photo-electric factor
		Pag.	Photo electric cross section index per unit of mass
Lateralog B	Focusing-plactrode test (electrical log)		
	similar to LL7	Pha	peresity
	shallow		Phy + fraction of total volume accupied by pares
	received with small electrodes on the Dus! (multism Laterales		Phy = {St > Dt } / (St = St ) Dt = reading on the same ling Draws from an anti-trait table
L07	Litme Genuity Teel		Ot -= 105 usec/ft
	Hearly massering Pr		Phy = (Bho - Bhob) (Bho - Bho, )
			Phi + R. / R
LIM	Lithelagy window count rate		Phy + 1 <sup>2</sup> , / 3,
		<b>Ph</b> :	apparent netrix perosity
u	Long lower window count rate	•	from densityeneutron crossplat
15	Long-spoking computed count rate		
	lialuz	Peresity	eutek visual interpretation
COMPR	Long-spectrag man	over 1 av	
			•
1.0	tant unter 1.3 mades cont rate	Proster Cy. (45	Log te determine 4
			Statier to the attractional
เหา	tent unter 1 window count rate		Besistivity of a net-thair formation
		73	Maratian Charles and a service constraint
1.112	Long upper 2 window count rate	R <sub>at</sub>	Resistivity of mud cake
LUIN	Long upper MOD	1.4	Resistivity of mut filtrate
Nicrelateralog	Hicroresistivity device to monoure R <sub>ad</sub> influence of mod cake depressed	8463	Grain density from cross-plot porosity
	well working in salt-base muds	Red	Bulk density (g/cm <sup>2</sup> )
	$17 h \Rightarrow (3/0)$	IPC8	Rhob + Phs"Rho, + (1-Phs)"Rho
	where the sector determination of the sector determination		· · · · · · · · · · · · · · · · · · ·
	°' "#0	Rhof	Fluid density (g/cm.)
Ricroles	Sector with meturalett.	<b>*</b> >	M. downships downsta
	accurate deitnestion of permeable beds	a a b	mportal ar work warrant y
	readily detection of multicakes	ite.	Batrix density (g/c8)
	not quantitatively interpretable		from densitymentron crossplat
	satisfactorily R_n and peresity if		1
	R/R < 15 <sup>110</sup>	Rho,	Liquid density (g/cm²)
	h = = = = = = = = = = = = = = = = = = =		
	depth of investor > 4	f.	frue resistivity
	The and an in the second to particular the	•	determined by Laterbiog 7
MSFL	selectically focused looking		Laterolog 3 11d Dual Laterolog
#(0	Matrix Identification Plot	۹_	Formation water resistivity
	·	-	1000 saturated brine
14 1 14 14 14 14 14 14 14 14 14 14 14 14	micro towerse resistruity, ones		From SP curve
<b>10</b> 1	Mil marateurtu alma		Annual state of the Richard seas
	The rearativity, prince	"×0	
MICR	Micro normal resistrvity, alws		"x0 " "mf <sup>( )</sup> x0
		CT BH	Shert-sharing E density
n	Seturation exponent	*****	and a speed of a second
	usually n = 2	Sand Time	Set by the longer in the SF log
NCIN.	CRL tog	SARABARO	Combination program
	Near detector		
~~~	Beb and down downloaded to	SFL	Spherically-focused Log
#u5	Metural Gamma Spectrometry log		part of the ISE/Sonic combination

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STLE.	Spherically-focused log Averaged sver 2.5
5 <b>9</b> . u	Spherically-Recused log
Ergma	Represt neutres capture cross section
<b>h</b>	hydrocarbon soluriotion: $S_{\mu}$ = fraction of game volume filled with hydrocarbons: $S_{\mu}$ = 1 = $S_{\mu}$
Shale base Trap	Shale line in SP log, set by the lagger
<b>5</b>	Residual hydrocarbon saturation in the fluchul zone $S_{her} \approx 1 - S_{H\bar{h}}$
54	Shart normal from IEL, in alma
	Restrim log (persetty determinations) mastrem source and detector mainted on a shifl propertional counter mastrem absorbers such as (iffacts of strong mastrem absorbers such as (I and B are minimized) actimatically correction for solinity Teo Teo Teo reading if ges is present
SONIC	Sentc Log travel time OC is determined
<b>5</b> 4	Spantaneous periorital log - detect permoble bods - detecmine R - qualitative impression of shaliness - qualitative impression of shaliness nud cake present if caliper reading depressed
SAAT	Sanic Tag ratio
551	Shert-spacing I window count rate
552	Shart-spacing 2 window count rate
554	Static SP
S <sub>int</sub>	$S_{\mu 0} = sert (F^{+} H_{\mu f} / R_{\mu 0})$
s_	Fraction of pers volume accupied by formation materials lager seturation $S_{-}^{*} = S \rightarrow J / B_{-}$ $S_{-}^{*} = set (T_{-}^{*} + B_{-}^{*} / B_{-}^{*})$ $S_{-}^{*} = set (B_{-}^{*} / B_{-}^{*})$ $S_{-}^{*} = (I_{-} / B_{-}^{*})/(B_{-}^{*}/B_{-})$ $T_{-}^{*} = (I_{-} / B_{-}^{*})/(B_{-}^{*}/B_{-})$ if $B_{-}^{*}$ defines
Swirr	[reducible water saturation
s <sup>w</sup>	Mud filtrate saturation $S_{s0} = \frac{1}{2} - S_{hr}$
TENS	Tension
TOT	Thermal decay time
U	Photo electric cross section per unit of volume product Pe <sup>+</sup> density
u <sub>f1</sub>	U fluid
Ulang.	$u_{log} = (1 - m_{i_a})^* u_{ma} + m_{i_a}^* u_{i_1}$
U <sub>rre</sub>	U metrix

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I.

### **Bibliographic Data Sheet**

T-the and authors Geochemical Criteria for Reservoir Quality Variations in Challs from The North Sea H. Kunzendorf and P. Sørensen

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Abstract (Max. 2000 characters)

The research project (EFP-86) systematically investigates the influence of chalk geochemistry on petrophysical parameters determining hydrocarbon reservoir quality, i.e. porosity and permeability. Two wells of the North Sea Tyra gas field were chosen for the present investigation: the central well TWB-3 and eastern marginal well E-lx. Geophysical logging data with interpretations exist for both wells. Drill core sections of Upper Maastrichtian and Danian chalk were selected for the geochemical investigations. Chemical data on chalk samples were gathered by using both conventional (X-ray fluorescence) and special instrumental analytical techniques (instru mental neutron activation). The geochemical data are compared with the well-logging results. Geophysical logging suggests that there is reduced porosity in the Danian reservoir units LDP and UDT in both the central and marginal wells. The chalk drill core samples from the section with reduced porosity also show a lower Ca content. At the same time, a high Si content is observed in these samples and a number of trace elements in chalk show a similar distribution with depth. Silicon diagenesis is therefore regarded as being responsible for reservoir quality variations in Tyra rochs. A linear dependence is observed between chalk porosity and silicon content of chalk, i.e. reservoir porosity may be estimated from the Si content of chalk. Chalk permeability may also be determined by Si content but the linear dependency is less significant. Geochemically, depth distribu-tions of elements Al, Fe and Sc show the same trends as that for Si. Therefore, diagenetic changes in chalk also include clay minerals. Other features of the Tyra gas reservoir are displayed through the chemical data. The gas zone in TWB-8 is characterized by low contents of Na and Cl, i.e. lower water saturation is indicated. Low concentrations of rare earths in all chalk samples show a shale-normalized pattern that is characteristic of marine sediments laid down under oxic conditions. Some changes that occur with depth in the Ce anomaly probably indicates a slight change in the depositional environment. A most pronounced feature of the Tyra chalk is the Cepth distribution of manganese: the content continuously decreases with depth, i.e. from Danian (about 2000 ppm) to Maastrichtian strata (less than 200 ppm). In this respect, no other chemical element in chalk correlates with Mn. At present, there is no indication as to which mineral or mineral phase one is likely to find the element.

#### Descriptors INIS/EDB

ALUMINIUM; CALCIUM; CLAYS; DEPTH; DIAGENESIS; DRILL CORES; ELEMENTS; EXPERIMENTAL DATA; GEOCHEMISTRY; GEOLOGIC DEPOSITS; GEOPHYSICS; IRON; LIMESTONE; MANGA-NESE; NATURAL GAS; NEUTRON ACTIVATION ANALYSIS; NORTH SEA; PERMEABILITY; POROSITY; RARE EARTHS; SILICON; SPA-TIAL DISTRIBUTION; TRACE AMOUNTS; WELL LOGGING; X-RAY FLUORESCENSE ANALYSIS

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