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Ultraclean Si/Si Interface Formation by Surface Preparation and Direct Bonding in Ultrahigh Vacuum

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ABSTRACT

Silicon surfaces have been cleaned and bonded in ultrahigh vacuum, at a pressure in the 10^{-10} Torr range. The bonded interfaces show extremely low contamination levels as measured by secondary ion mass spectroscopy. Nevertheless, a potential barrier could be detected at the interface by spreading resistance and current vs. temperature measurements. This suggests that the barrier is caused by inevitable dislocation networks due to wafer misorientation, as well as residual oxygen at the interface.

Introduction

Room temperature silicon wafer bonding in a clean room environment relies on smooth surfaces, bringing the silicon wafers into close proximity, and a chemical interaction between adsorbed surface atoms and molecules. Direct bonding between the silicon surface atoms is not achieved until a subsequent anneal step. By going to ultrahigh vacuum (UHV) conditions, wafer bonding can be investigated without the influence of adsorbed surface species. It is well known that impurities present on the wafer surfaces are incorporated into the bonded interfaces^{1,2} thereby influencing the interface properties. An open question is what happens if two atomically clean silicon surfaces are brought into contact. In particular, the properties of interfaces formed by bonding of atomically clean surfaces are expected to be an indicator of the intrinsic properties of bonded interfaces.

To date, very little has been done on this subject.³⁻⁶ Room temperature bonding of silicon at a pressure of 10^{-8} Torr has been reported by Gösele et al.³ In that work the surfaces were prepared by heating of the samples at a pressure of 10^{-6} Torr, and a good bond was achieved as judged from a tunneling electron microscope (TEM) image. However, to prepare and maintain atomically clean surfaces for reasonable lengths of time, typical UHV pressures of 10^{-10} Torr are required. Recently, we reported the first results on direct bonding in the 10^{-10} Torr range.⁴ In this work, the direct bonding at a UHV base pressure of 1×10^{-10} Torr, after cleaning at a maximum pressure of 2×10^{-9} Torr, is further investigated. The surfaces were analyzed prior to bonding by using low energy electron diffraction (LEED) and Auger electron spectroscopy (AES). Chemical analysis of the interfaces formed by UHV bonding using secondary ion mass spectroscopy (SIMS) are presented together with electrical data obtained from spreading resistance measurements as well as current vs. voltage and current vs. temperature measurements. A slightly different approach for room temperature UHV bonding has been reported by Takagi et al.⁶ A successful bonding at room temperature was reported using surface cleaning and activation by means of an argon atom beam in vacuum. The cleaning of the surfaces were followed by surface contacting at room temperature with an applied mechanical pressure.

Experimental

The samples used in the experiments were 1×2 cm pieces of silicon wafers (mainly CZ, (100)-oriented, p-type,

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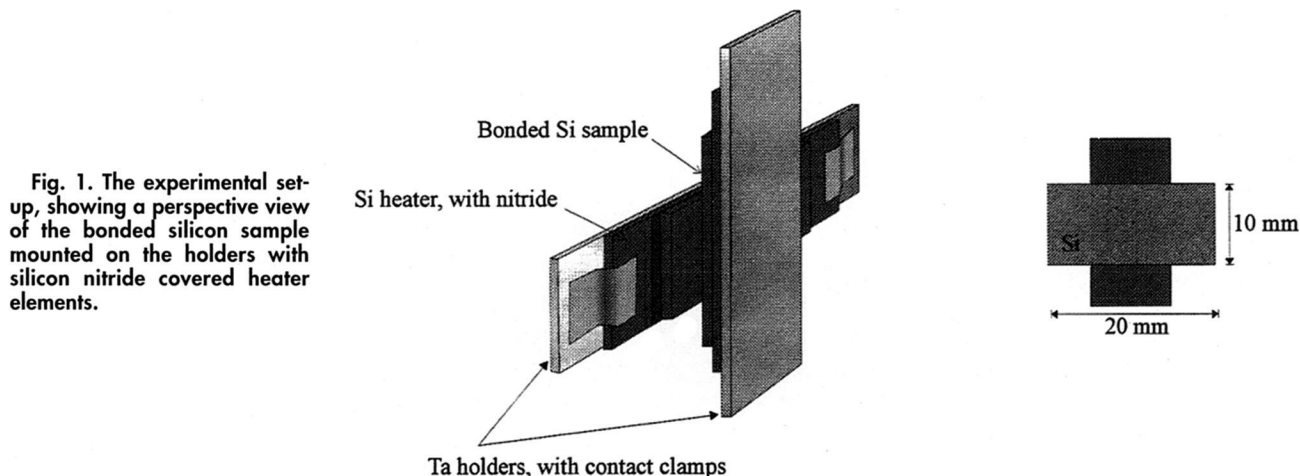
5–30 Ω -cm), cleaned in sulfuric peroxide mixture [(SPM) of $\text{H}_2\text{SO}_4(97\%):\text{H}_2\text{O}_2(30\%)$, 4:1] for 10 min, and rinsed in deionized (DI) water. The chemical oxide was removed by a 1 min etch in 10% aqHF, after which the wafers were water rinsed, and blow dried in nitrogen. This procedure terminates the surfaces with hydrogen. Immediately after blow-drying, the surfaces were contacted, and a room temperature bond was formed. The samples could thus be transported to the UHV chamber, not situated in a clean room environment, without becoming oxidized or contaminated by particles. In the UHV chamber the samples were mounted on special sample holders made of ceramics and tantalum. The samples were mounted on top of silicon strips used to heat the samples. The heater silicon strips were covered with silicon nitride to form the insulation between the heater element and the sample. Thereby a direct current through the samples⁴ could be avoided. The sample mounting is schematically shown in Fig. 1. After reaching the base pressure (1×10^{-10} Torr), the samples were debonded.

In order to prepare a clean and reconstructed silicon surface the following procedure was performed: after debonding the samples were outgassed at 600°C for several hours. After cooling, the surfaces were cleaned by “flashing” to 850°C during short periods of 10–60 s, to a total time of about 10 min. The use of small samples instead of entire wafers was necessary to maintain a low pressure (below 2×10^{-9} Torr) while heating the samples. After “flashing,” the samples were allowed to cool for some minutes before the surfaces were brought together, using a micrometer screw feed through to apply a slight pressure. While pressing the surfaces together a second heat-treatment at approximately 450°C was performed.

The UHV Prepared Silicon Surface

During and after surface preparation, characterization of the surface condition was performed, using LEED and AES, to make sure that the surfaces were clean at the moment of bonding.

Immediately after debonding it was concluded that the silicon surfaces had not oxidized, since a (1×1) LEED pattern from an unreconstructed H-terminated surface could be observed. The samples were then outgassed at about 600°C for several hours, while keeping the pressure in the chamber below 2×10^{-9} Torr. This should remove the surface hydrogen.⁷ However, after this procedure, no diffraction pattern could be obtained with LEED, indicating a contaminated and/or disordered surface. AES



showed increased amounts of oxygen as well as carbon on the surface.

After a short additional heating for only 2 min at 850°C, a diffraction pattern was again obtained, showing a (2×1) reconstruction of the clean silicon surface. The diffraction pattern is shown in Fig. 2. This observation indicates that the degradation that takes place during heating to 600°C, whether it be a contamination layer or a disordering of the surface structure, can be removed at a higher temperature. The 850°C is chosen to be above the silicon dioxide sublimation temperature.⁸

Characterization of the Bonded Interface

The bonded interfaces achieved high mechanical strength, qualitatively judged from the fact that they could withstand a polishing at a beveled angle, as described below. Bonding was not achieved if no pressure or heating was applied. The reasons for this are still not clear, presumably it reflects the need for substantial atomic diffusion to obtain silicon/silicon bonding across the entire interface. The formed interfaces were characterized electrically by spreading resistance, current vs. voltage, and current vs. temperature measurements, and chemically by SIMS analysis.

Spreading resistance measurements.—The UHV-bonded interfaces were electrically characterized using spreading resistance measurements. A reference sample was made in the clean room by HF etching, bonding, and annealing in a conventional furnace (1000°C, 30 min in N_2). The samples were polished to a beveled angle of 11.54° or 5.45° as a preparation for the spreading resistance measurements. As shown in Fig. 3, a small resistance peak is observed at the location of the bonded p-type/p-type interface in both samples. No clear differences could be found between

UHV and clean room samples. This means that the surface potentials and the majority carrier concentrations at the bonded interfaces are approximately equal in the two samples.

A more detailed analysis of the data shows that in both cases the increase in spreading resistance corresponds to a barrier caused by an interfacial sheet charge of about 10^{11} positive elementary charges per centimeter squared. This corresponds to an energy barrier of the order of 0.1 eV, which should have a noticeable influence on the carrier transport through the sample at room temperature.

Current vs. voltage and current vs. temperature measurements.—To verify the results in the spreading resistance analysis, the bonded Si/Si p-type/p-type junctions were characterized using conventional current vs. voltage and current vs. temperature measurements. The current vs. voltage curves of the UHV bonded samples showed the presence of an interfacial barrier influencing the current. Figure 4 shows an activation plot of the current across the bonded interface obtained from current vs. temperature measurements at different applied voltages. It is obvious from this figure that the current is thermally activated at lower temperatures. The activation energy is found to be voltage dependent, corresponding to a potential barrier that decreases with the applied voltage. This is what one should expect for a bonded Si/Si interface where the potential barrier is caused by a sheet charge due to interface states, being filled to the position of the Fermi level at the interface.⁹ From Fig. 4, an activation energy of 0.11 eV is deduced for the curve corresponding to an applied voltage of 0.1 V. This activation energy is in agreement with the results of the spreading resistance analysis. At temperatures between approximately 170 and 270 K the current becomes approx-

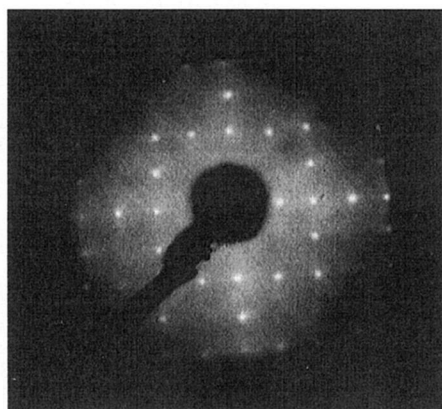


Fig. 2. LEED pattern showing a (2×1) reconstructed silicon surface after heating to 850°C in UHV.

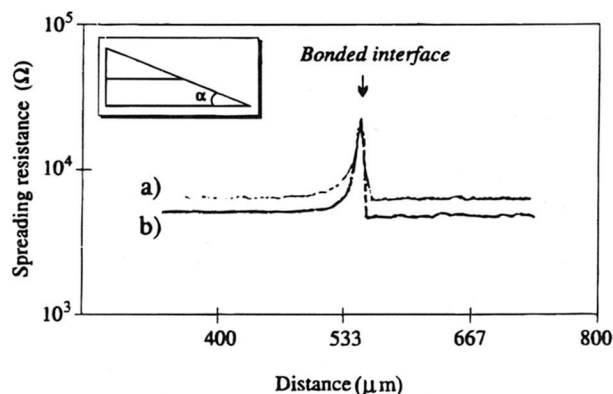


Fig. 3. The measured spreading resistances for samples (a) cleaned, bonded, and annealed in UHV, and (b) bonded and furnace annealed in the clean room.

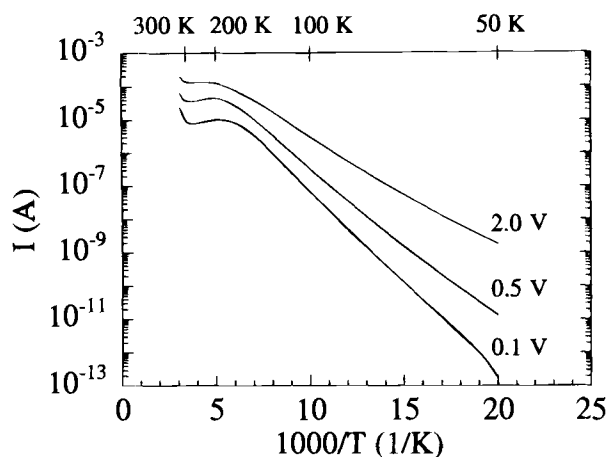


Fig. 4. Activation plot at different applied voltages for a Si/Si p-type/p-type junction formed by wafer bonding in UHV.

imately temperature independent, but again shows indications of becoming thermally activated at the highest investigated temperatures. The current vs. voltage characteristics also change from emission type at the lowest and highest temperatures, to an approximately ohmic character at the intermediate temperatures. However, at these temperatures the current across the structure is too small to be explained by the bulk resistivity of the silicon.

SIMS analysis of the UHV bonded interfaces.—SIMS analysis was used to investigate the presence of impurities at the bonded interfaces and to find out the origin of the observed interfacial barrier. The following elements were analyzed for all samples: H, C, O, F, S, Cl (Cs^+ primary ions) and Na, Al, K, Ca, Cr, Fe, Mn, Ni, Cu, Ta (O^- primary ions). The samples were polished in the same way as for the spreading resistance measurements, thereby exposing the bonded interface.

Table I summarizes the SIMS results for one clean room bonded and several UHV-bonded samples. The value Δ_{signal} given after each element is defined as the approximate ratio of the signals (counts/s) from the peak at the bonded interface and from the bulk part of the sample. Figure 5 shows the peaks from the detected nonmetallic and metallic contaminants, respectively, in the UHV sample "UHV(v)" and in the clean room sample "RR" of Table I.

By doing the SIMS analysis in a spot located slightly above the bonded interface on the beveled sample, bulk silicon is analyzed before passing the bonded interface. Since the sample has a bevel, the cross section of the interface will pass over the analyzed area during sputtering.

Table I. SIMS data for differently prepared samples, bonded in UHV and in the clean room. The value Δ_{signal} given after each element is defined as the ratio of the signals (counts/s) from the peak at the bonded interface and from the bulk part of the sample.

Bonded in (Name)	Clean room chemistry	Result SIMS analysis (Δ_{signal})
UHV [UHV(i)]	SPM + 10% aqHF	K(30), Ca(4)
UHV [UHV(ii)]	SPM	H(10), C(3), O(10), F(10), S(100)
Clean room [RR]	SPM + 10% aqHF	Na(8), K(5), Ca(4)
		H(40), C(130), O(50), F(10), S(80), Cl(10)
		Na(1000), K(2000), Ca(1500), Cr(20)
UHV [UHV(iii)]	SPM + 10% aqHF	H(5), C(2), O(10), Cl(10)
UHV [UHV(iv)]	SPM + 10% aqHF	H(3), C(4), O(3), F(2), S(10)
		Na(200), K(500), Ca(200), Cr(20), Mn(10)
UHV [UHV(v)]	SPM + 10% aqHF	H(6), C(18), O(4), F(5)
		Na(100), K(150), Ca(10)

This is the reason for the broad appearance of the peaks in Fig. 5. An attempt was made to determine the absolute values of some important impurities by use of known reference samples. This relatively rough estimate gave the result that the concentrations, assuming that they are present in a volume element around the interface, are at least of the magnitudes shown in Table II. The spread in impurity concentrations between different UHV-bonded samples were found to be less than an order of magnitude.

Clearly, the UHV-bonded interfaces are less contaminated than the clean room ones, although a large spread in results is observed. The samples UHV(iv) and UHV(v) in Table I were prepared and room temperature bonded in the clean room at the same occasion. The samples show considerable larger levels of, Ca, Na, and K as compared to the other UHV-bonded samples, pointing to possible influences of differences in the wet cleaning procedures on the contamination levels also after cleaning in UHV. The SIMS results taken together are clear evidence of the effectiveness of the UHV cleaning procedure.

Discussion

The most striking result is that although there is a clear difference (about an order of magnitude) between the interface impurity concentrations in samples bonded in UHV, as compared to samples bonded in the clean room, the spreading resistance data are very similar. That is, the electrical behavior as indicated by the spreading resistance measurement is about the same, regardless of the impurities at this level. The results show that O and S are present at the bonded interfaces, although the differences are large between the clean room bonded and the UHV-bonded samples. Those impurities may act as donors in silicon, which would give rise to a barrier of the observed type. However, the spreading resistance data for the two cases are very similar. A possible explanation is the different anneal temperatures. A barrier of the observed type would occur if impurities acting as donors, e.g., O or S, were present. Since activation and deactivation of different donors occur at different temperatures, it is possible that some of the impurities are electrically active only after the 450°C anneal but not after the 1000°C anneal. It is reported that in CZ material, O could getter and precipitate at the bonded interface during heating.¹⁰ A parallel can be made with so-called thermal donors, observed to appear at 450°C, and deactivate above about 650°C, in materials created using the separation by implantation of oxygen (SIMOX) technique.¹¹ Another possible explanation to the similarities in the electrical behavior is that the potential barrier at the interface is due not to contamination but rather to "intrinsic" factors, such as inevitable misorientation between the wafers and miscut of the individual wafer surfaces, causing dislocation networks in the interface region.

To achieve a better understanding of the properties of UHV-bonded interfaces also FZ silicon and silicon of crystallographic orientation (1-1-1) should be investigated in the future. The use of FZ silicon should for instance allow an investigation of interfacial properties in the case of a lower oxygen content in the silicon bulk material. Since the silicon (1-1-1) surface shows different reconstructing properties to the (1-0-0) surface, interesting information may be added. Very preliminary results show that FZ silicon as well as (1-1-1) oriented silicon are possible to bond

Table II. Estimated concentrations of impurities at UHV-bonded Si/Si interfaces.

Element	Concentration (cm^{-3})	Element	Concentration (cm^{-3})
Hydrogen	1×10^{20}	Sodium	4×10^{17}
Carbon	4×10^{19}	Potassium	2×10^{17}
Fluorine	2×10^{17}	Calcium	2×10^{17}
Oxygen	2×10^{20}	Chromium	2×10^{16}
Sulfur	5×10^{17}		

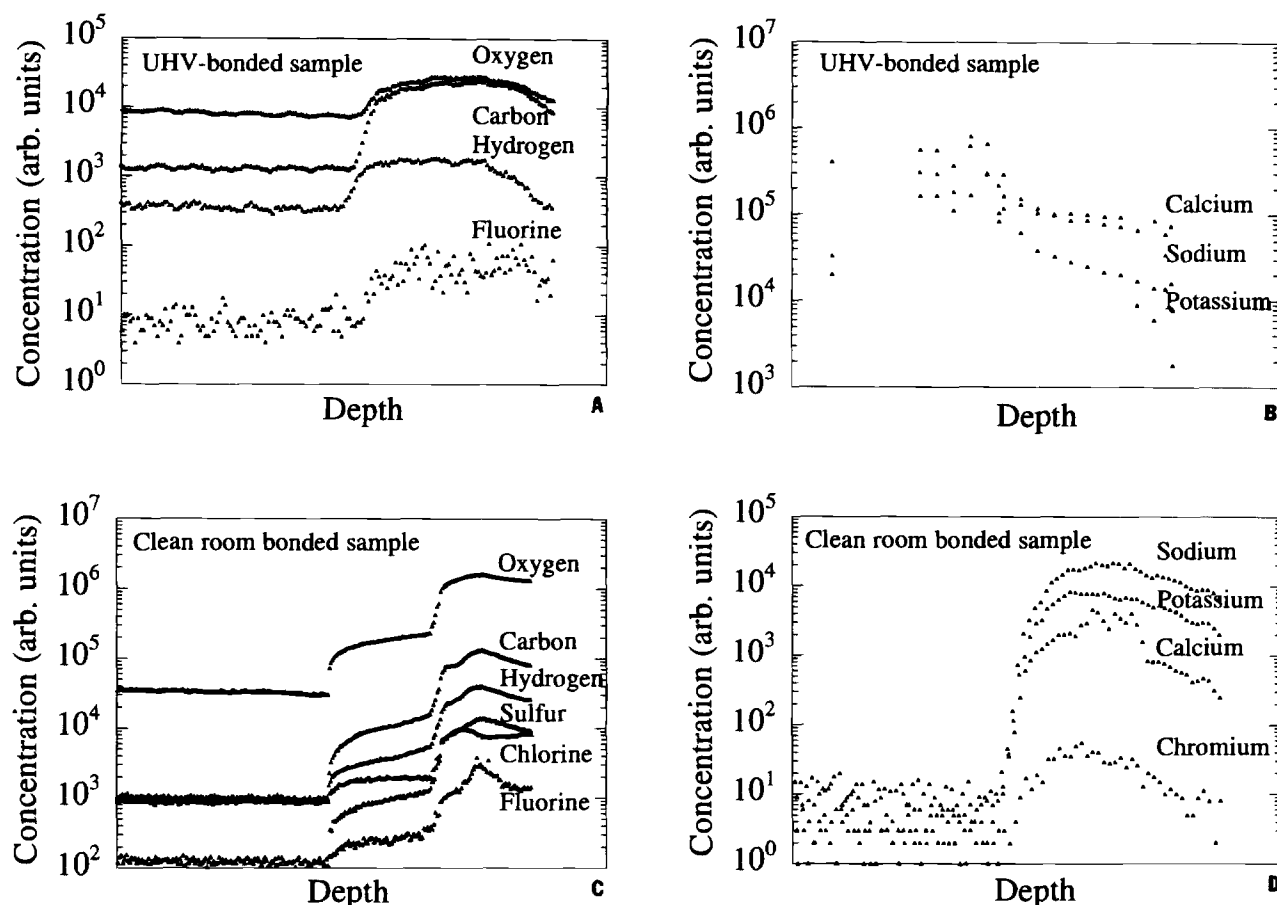


Fig. 5. Nonmetallic and metallic contaminants, respectively, as obtained from SIMS in the UHV sample UHV(v) and in the clean room sample RR of Table I.

by the same method as described above, but reliable analysis data of these interfaces are not yet available.

Apparently, the current across the sample is restricted by a potential barrier.¹² This potential barrier is relatively low, and affects the current across the bonded interface at room-temperature. Potential barriers at bonded Si/Si interfaces range in amplitude from almost zero to about 0.5 V depending on the cleaning procedure used before wafer bonding.^{9,12} The barrier found from the spreading resistance measurements agrees with the activation energy obtained from the current vs. temperature measurements (Fig. 4). The current vs. temperature curve shows a peculiar behavior at temperatures between 170 and 270 K. Also the current vs. voltage characteristic differ at these temperatures as compared to the characteristics at lower and higher temperatures. The reason for this is not understood. One may speculate that different parts of the junction are active at different temperatures.

Another interesting result is that the surfaces are seen to degrade upon heating to 600°C in UHV. This indicates that the surface is disordered (not able to reconstruct) and/or it gets contaminated with some species during the outgassing, that destroys the diffraction pattern. The latter theory is supported by the observation of increased amounts of oxygen as well as carbon on the surface (AES). Sticking of carbon monoxide to the surface could thus be a possible explanation, although the increase in both carbon and oxygen monitored by AES are small. The lack of any visible LEED spots after the 600°C anneal implies that the contaminated or disordered layer at the surface is more than one atomic layer thick. One possible explanation is diffusion of oxygen and other elements from the ends of the 2×1 cm samples, which are not protected after clean room bonding, into the 1×1 cm central region of the samples where a clear (1×1) LEED pattern is seen prior to annealing. A clean but not ordered (reconstructed) sur-

face could be another possible explanation. Heating to 850°C gives a LEED pattern again, due to removal of carbon and oxygen and/or ordering of the surface structure. Hence, to obtain true Si-Si bonding between the two crystals, the surfaces should be cleaned at about 850°C, at very low pressure. Wafer bonding in UHV does allow studies of direct bonding between surfaces cleaner and more atomically ordered than is possible by any other method invented so far. An interesting perspective of this work is to attempt to preserve surface reconstructions such as the (7×7) reconstruction of Si(111) at such bonded interfaces, to study their effect on the electrical characteristics of the interface.

Conclusions

We have shown results on silicon structures formed by wafer bonding in UHV, at a pressure in the 10^{-10} Torr range. To obtain clean silicon surfaces before UHV-bonding the surfaces should be cleaned at about 850°C in a pressure below 10^{-9} Torr. As measured by SIMS, the UHV-bonded interfaces contain more than an order of magnitude less impurities compared to interfaces prepared in the clean room. Nevertheless, a potential barrier could be detected at the interface by spreading resistance and current vs. temperature measurements. The energy barrier from both of these analysis is in the 0.1 eV range. It is suggested that the barrier is caused by inevitable dislocation networks due to wafer misorientation, as well as residual oxygen at the interface.

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Novel Low k Dielectrics Based on Diamondlike Carbon Materials

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ABSTRACT

Hydrogenated diamondlike carbon (DLC) and fluorine containing DLC (FDLC) were investigated for their potential applications as low k dielectrics for the back end of the line interconnect structures in ultralarge scale integrated circuits. It was found that the dielectric constant (k) of DLC can be varied between <2.7 and >3.4 by changing the deposition conditions. The thermal stability of the DLC films was found to be correlated to the values of the dielectric constant, decreasing with decreasing k . Only DLC films having dielectric constants $k > 3.3$ appeared to be stable to anneals of 4 h at 400°C in a nonoxidizing environment. However these films were characterized by stresses higher than 600 MPa. FDLC films, thermally more stable at 400°C than the DLC films with $k > 3.3$, could be prepared with dielectric constants below 2.7 and internal stresses <200 MPa. Such FDLC films are thus promising candidates as a low k interconnect dielectric.

Introduction

The reduction of electrical device dimensions and increased integration in ultralarge scale integrated (ULSI) circuits results in increased resistance of the back end of the line (BEOL) metallization and increased interlevel and intralevel capacitances, which cause an increase in the signal delays. In order to improve the switching performances of future ULSI circuits insulators with dielectric constants (k) significantly lower than that of SiO_2 are needed in to reduce these capacitances. Dielectrics with low k values are available, e.g., polytetrafluoroethylene (PTFE) with $k = 2.0$, but these materials are not stable at temperatures above 300–350°C. However, integration of the dielectrics in ULSI chips requires thermal stability at temperatures of at least 400°C.¹ Diamondlike carbon (DLC) has been considered a possible low k dielectric, but the films have either been found not to be stable above 350°C,^{2–4} or have dielectric constants of about six.⁵ Matsubara et al. have demonstrated the integration feasibility of fluorine containing DLC (FDLC) films in a multilevel structure using Al metallization, but only at temperatures below 350°C.⁴

In order to integrate a new low k dielectric material in ULSI devices, such a material has to satisfy a number of requirements, among which are: electrical (low dielectric constant, low dissipation factor), thermal (stability at 400°C), mechanical (low stresses), adhesion, and compatibility with other materials, etc.¹ The present paper describes DLC and FDLC films as potential candidates for a low k interconnect dielectric. The films have been prepared by plas-

ma-assisted chemical vapor deposition (PACVD) and have been characterized by whether they satisfy some of the requirements mentioned above.

Experimental

Hydrogenated DLC and FDLC films have been prepared by radio-frequency (rf) plasma-assisted CVD (PACVD) in a parallel plate reactor, at pressures of 100 to 300 mTorr and rf powers of 25–150 W. The deposition was performed on Si substrates placed on the powered electrode, thus being at a negative self-bias. The DLC films were deposited from a pure hydrocarbon, while the FDLC films were deposited from fluorinated hydrocarbon ("fluorocarbon" in the following), or mixtures of the fluorocarbon with hydrogen. The films were characterized in the as-deposited state and after annealing at 400°C in helium or nitrogen for various amounts of time. The films were characterized by Fourier transform infrared spectroscopy (FTIR), Rutherford backscattering (RBS), and forward recoil elastic scattering (FRES). The hydrogen content of the films was determined by FRES, while RBS was used to determine the fluorine concentration $[\text{F}/(\text{C} + \text{F})]$. Both RBS and FRES data were analyzed with a RUMP program (Computer Graphic Services-CGS-Ithaca, NY), which was used to simulate theoretical film compositions and fit them to the experimental spectra. The stresses in the films were determined from the radius of curvature induced on the substrate by the deposited films.

The thermal stability of the investigated materials was initially investigated by measuring changes of film thickness as a result of annealing. Such changes were determined

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