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# Multi-jet electrospinning of polystyrene/polyamide 6 blend: thermal and mechanical properties

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## Abstract

Polystyrene (PS) has high thermal resistance thus can be applied as thermally comfortable textile. However, the application is limited due its low mechanical strength. In this study, polyamide 6 (PA6) was blended with PS to improve the mechanical strength of PS, by means of a multi-jet electrospinning. Content ratio of the blend web was measured by chemical immersion test and confocal microscopy analysis. Fiber content was in accordance with the number of syringes used for PS and PA6 respectively. The effects of content ratio on the web morphology, thermal resistance, tensile behavior, air and water vapor permeability, and surface hydrophilicity were investigated. The influence of environmental humidity during electrospinning process on three dimensional (3D) web structure was also reported. PS web produced from higher humidity had more pores and corrugations at the surface. The increased surface roughness and porosity led to the increased hydrophobicity and thermal resistance. Though the blending of PA6 with PS enhanced the mechanical strength, the added PA6 decreased air/water vapor permeability and thermal resistance. The lowered thermal resistance by the addition of PA6 was mainly attributed to higher thermal conductivity of PA6 material and lowered air content with PA6 fibers.

**Keywords:** Multi-jet electrospinning, Polystyrene, Polyamide 6, Thermal resistance, Porosity

## Introduction

Electrospinning process is broadly used to obtain membrane-like webs with submicron to micron fibers (Li and Xia 2004). Electrospun nanofibers, with its large surface area and multiple pores, can be used to construct unique functional nanostructures for composites, filtration membranes, biomaterials, and breathable textile fabrics (Greiner and Wendorff 2007; Li and Xia 2004; Pham et al. 2006). Generally, an electrospinning set-up consists of a high voltage source, container (usually syringe) for polymer solution, syringe pump, capillary nozzle, and grounded collector (Pham et al. 2006). When high electric voltage is applied, the surface tension of polymer solution is overcome by the applied electric field. Charged polymer solution forms into jet, forming a Taylor cone, then gets further stretched. Meanwhile, solvent from the polymer jet continuously evaporates and solidifies to form fiber webs on a collector (Reneker and Chun 1996).

Despite the usefulness and availability of electrospinning technique for various product development, its commercial application has been limited mainly due to its poor production efficiency (Teo and Ramakrishna 2006). As ways to increase the polymer throughput and improve productivity, a multi-needle (multi-jet) (Teo and Ramakrishna 2006) setup or roller spinning electrode device (Cengiz et al. 2010; Yener and Jirsak 2012) has been tested. Due to the advantage of multi-jet electrospinning as a simple set-up for blending different fibers with desired ratio (Teo and Ramakrishna 2006), several research groups have applied multi-jet device to fabricate nanofibrous textiles. Park et al. (2013) investigated the efficacy of blending polyurethane/polyamide 6 using an angled dual-nozzle electrospinning set up. Ding et al. (2004) studied the mechanical properties of blended web with poly(vinyl alcohol) and cellulose acetate in different ratio. However, there are few studies that thoroughly examined the influence of blend ratio on the web structure and properties as clothing materials.

Polystyrene (PS) and polyamide 6 (PA6) are widely used for in textile industry (Carrizales et al. 2008; Casper et al. 2004; Marsano et al. 2010; Pai et al. 2009). PS has a potential application as breathable textile with thermal comfort thanks to its high thermal resistance, but its application is limited due to its low mechanical property. If a material such as PA6 with good mechanical property can be blended with PS, the blend web can have practical applications as thermally comfortable clothing with the enhanced mechanical property.

In this study, a multi-jet electrospinning set-up (Fig. 1) was used to produce blend webs with PS and PA6, and the effect of content ratio was investigated on the web morphology, thermal and mechanical properties, air and water vapor permeability, and surface hydrophilicity. The influence of environmental humidity during electrospinning process on the three dimensional (3D) web structure was also briefly reported.

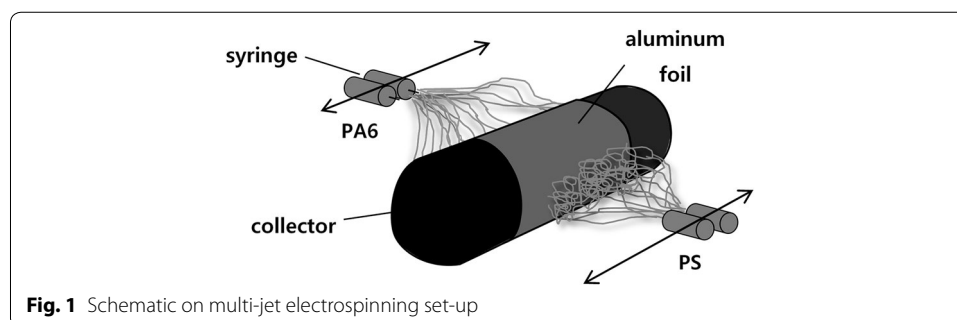
## Methods

### Materials

Polystyrene (PS,  $M_w = 350,000$  g/mol) and polyamide 6 (PA6,  $M_w = 10,000$  g/mol) were purchased from Sigma-Aldrich (USA). N,N-dimethylformamide (DMF, 99.8%), tetrahydrofuran (THF, 99.5%), formic acid ( $\geq 99.0\%$ ) and acetic acid ( $\geq 99.0\%$ ) were purchased from Daejung Chemicals (Korea) and used as solvents without further purification.

### Multi-jet electrospinning

To obtain uniform PS fibers, 18 wt% PS solution was prepared with DMF/THF mixture in a weight ratio of 3/1. 18 wt% PA6 solution was prepared with a formic acid/acetic acid



**Fig. 1** Schematic on multi-jet electrospinning set-up

mixture in a weight ratio of 4/1. ES-robot<sup>®</sup> Electrospinning/spray system (Nano NC, Korea) was used. A multi-jet electrospinning set up is illustrated in Fig. 1. Two syringes with needles (gauge 22G) were placed in the front and back side of grounded stainless drum collector respectively, and polymer solution was ejected toward the collector rotating at a speed of 100 rpm. The ejecting syringe was horizontally moved along the track with a speed of 7 m/min. Electric voltage of 20 kV was applied to the tip, and a collector to tip distance was maintained at 20 cm. Environmental temperature was kept at  $25 \pm 5$  °C and humidity was  $40 \pm 5$  RH % if not specified. To obtain the varied contents of PS and PA6 in the blend web, the number of syringes containing PS or PA6 solutions were varied as 4/0, 3/1, 2/1, 2/2, 1/2, 1/3 and 0/4, and a constant solution feeding rate of 0.2 ml/h was maintained. All webs were made in a thickness range of 56–64  $\mu\text{m}$ . Electrospun webs were collected on an aluminum foil, and dried in vacuum at room temperature for 24 h to evaporate residual solvents.

## Characterization

### *Determination of PS/PA6 blend ratio*

The blend web was observed for its PS and PA6 contents by the chemical immersion test (adjusted KS K ISO 1833 method) and confocal microscopy (LSM 700, Carl Zeiss, Germany) analysis after dyeing the respective fibers with different fluorescent dyes.

The contents of PS and PA6 in the blend electrospun web were investigated by immersing the dried blend web into formic acid to remove the PA6 component. The immersed web was thoroughly washed with formic acid and distilled water then dried. The content of PA6 was calculated by the weight loss of the web.

PS was dyed with rhodamin B ( $\geq 95.0\%$ , HPLC grade, Sigma-Aldrich) in 5  $\mu\text{g}/\text{ml}$  concentration, and PA6 was dyed with fluorescein isothiocyanate isomer I (FITC, 98.0%, HPLC grade, Sigma-Aldrich) in 5  $\mu\text{g}/\text{ml}$  concentration. The confocal microscopy was taken through the web thickness of 60  $\mu\text{m}$  in every 1  $\mu\text{m}$  sectional frames. The images were analyzed by Adobe Photoshop CS4 for the number of pixels in red PS fibers and green PA6 fibers to estimate the respective fiber contents in a blend web.

### *Web morphology*

Fiber morphology was observed by field emission scanning electron microscope (FE-SEM, JSM-7600F, JEOL, Japan). The fiber diameter of each specimen was measured by image analyzing software, Image J (National Institute of Health, USA). Web configuration with varied environmental humidity during electrospinning process was observed by the photo taken by using Digital Single Lens Reflex (EOS 650D, Canon, Japan) to draw a comparison of the appearance of each web.

### *Mechanical properties*

Tensile properties were assessed by a universal test machine (UTM, WL 2100, Withlab Co. Ltd., Korea) for a specimen in  $40 \times 10 \times 0.06 \text{ mm}^3$  in accordance with ASTM D5035 strip method. The gauge length and crosshead speed were 20 mm/min and 10 mm/min, respectively. The average of five measurements was used for analysis.

### Air and water vapor permeability

Pore size and distribution of the web were measured using capillary pressure tester (CFP-1500 Porometer, PMI, USA) at the maximum pressure of 200 psi and the maximum flow rate 25,000 ml/min. The apparent density of blend webs was measured by Eq. 1:

$$\text{Apparent density [g/m}^3\text{]} = \text{mass of web/volume of the web} \quad (1)$$

Air permeability of the web was characterized using capillary flow porometer (CFP-1200, PMI, USA), at the maximum pressure of 200 psi and the maximum flow rate of 25,000 ml/min. In this method, the amount of air (ml/s) passing through the specimen was measured as the applied air pressure was increased up to the set maximum pressure.

Water vapor transmission rate (WVTR) was measured according to ASTM E 96 desiccant method. A custom-designed cup was filled with calcium chloride, and the web specimen was fixed onto its opening. Then the assembly was kept at 40 °C, 90% RH. After 1 h, the evaporation of water through the specimen was measured by the weight change of the cup.

### Surface hydrophilicity

Surface hydrophilicity of the blend web was measured by static contact angle (SCA) measurement using a contact angle measurement device (Theta Lite, Attention, KSV Instrument, Finland). 4 µl droplets of distilled water was placed on five different positions on the sample surface, and the SCA on specimens were measured. SCA changes were recorded for 60 s of water contact time on the web surface.

### Thermal properties

Thermal conductivity of an electrospun web was measured by KES-F7 System (Thermal Labo II: Kato Tech Co. Ltd, Japan). Thermal resistance was measured using a sweating hotplate device (SGHP-8.2, Measurement Technology Northwest, USA), according to the modified ISO 11,092 sweating guarded-hotplate test method. For measurement of thermal resistance, electrospun web specimen was placed 10 mm above the hotplate to simulate a micro-environment of still air between human skin and clothes (Kim and Park 2013).

## Results and discussion

### Blend Ratio of PS/PA6 Webs

Content ratio of PS/PA6 of the developed web was measured by the chemical immersion test and the confocal microscopy analysis (Table 1). Overall, the ratio of the number of syringes containing PS to PA6 was similar to blend ratio calculated by immersion test and confocal microscopy analysis. Slight differences were noticed between immersion test and confocal microscopy analysis results. As confocal microscopy was taken for every 1 µm of the nonwoven web sections, errors could come from the overlooked areas between the sections. Therefore, the immersion test was considered as more reliable method because the test allows us to measure the whole area of the specimen. Moreover, PA6 fibers were much finer than PS fibers, thus PA6 fibers had larger surface area which might have affected pixel counting. We calculated weight of webs using weight

**Table 1 Characteristics of the electropsun webs**

Code	Number ratio of jets (PS/PA6)	Weight ratio (confocal microscopy analysis)	Blend ratio (immersion test)	Calculated weight <sup>a</sup> (g/m <sup>2</sup> )	Measured weight (apparent density) (g/m <sup>2</sup> )	Error <sup>b</sup> (%)	Thickness (μm)
S4A0	4/0	100/0	100/0	–	8.1 ± 0.4	–	60 ± 4
S3A1	3/1	74/26	76/24	9.2	8.7 ± 0.5	6	60 ± 3
S2A1	2/1	64/36	67/33	9.6	9.2 ± 0.5	4	60 ± 2
S2A2	2/2	48/52	51/49	10.4	9.5 ± 0.4	9	60 ± 4
S1A2	1/2	34/66	33/67	11.2	10.0 ± 0.7	12	60 ± 1
S1A3	1/3	22/78	24/76	11.6	10.1 ± 0.5	15	60 ± 2
S0A4	0/4	0/100	0/100	–	12.7 ± 0.5	–	60 ± 1

<sup>a</sup> Weight was calculated on the assumption that PS weight is 8.1 and PA weight is 12.7 on 6th column

<sup>b</sup> Error (%) = (calculated weight – measured weight)/measured weight\*100

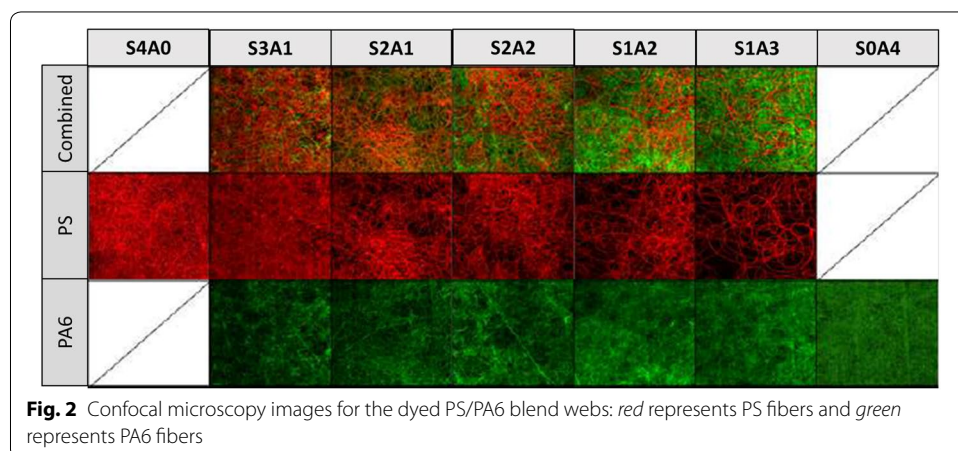
ratio measured by immersion test (5th column in Table 1) and compared the values to the measured weight (6th column in Table 1). Insignificant error was noticed from our calculated values (7th column in Table 1), but as PA6 content increases error increased as well. This might stem from our calculation based on the measured weight of S4A0 and S0A4 webs. S4A0 weight was underestimated but S0A4 weight was overestimated.

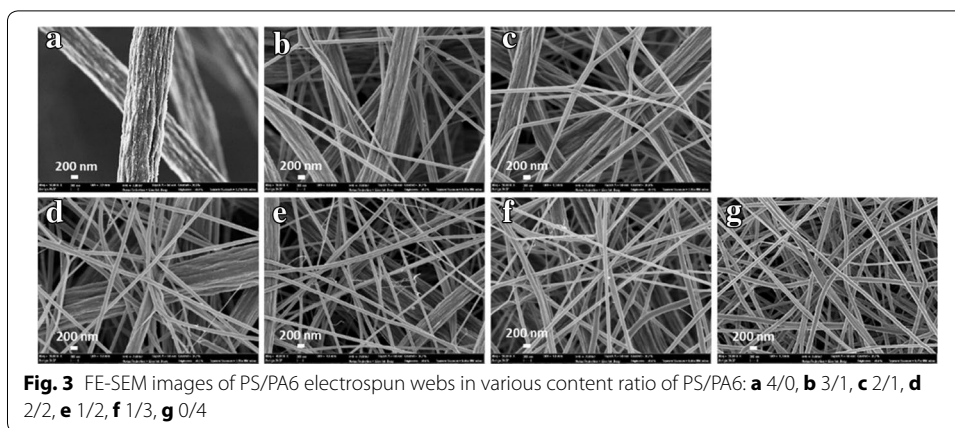
However, confocal microscopy can be applied as a useful quality control technique to examine the fiber uniformity, because it provides the visual image (Fig. 2) of the compositional distribution in blend fiber webs.

**Electropsun web morphology**

SEM images of electropsun web with various content ratios of PS to PA6 are shown in Fig. 3. At the same spinning condition, PS fibers were in larger diameter ( $0.90 \pm 0.19 \mu\text{m}$ ) than PA6 fibers ( $0.10 \pm 0.03 \mu\text{m}$ ).

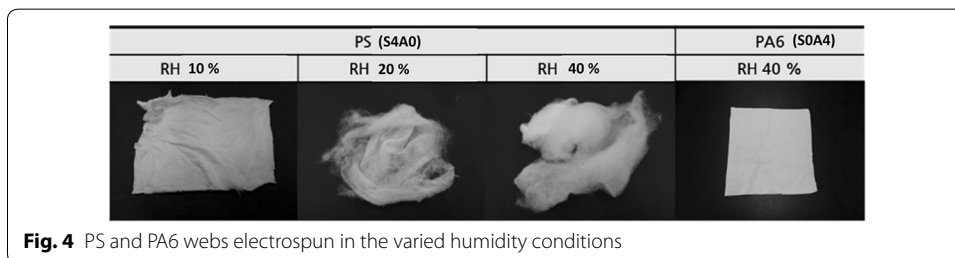
In addition to the diameter difference, more distinctive difference between PS and PA6 fibers was observed from the surface configurations as in Fig. 3a, where PS fiber surface shows corrugations and small pores. The surface configuration is a result of interactions among polymer molecule, solvent, and moisture in the environment. A polymer solution





such as PS in a mixture solvent of a highly volatile THF and a less volatile DMF can create porosity and/or corrugations by the vapor-induced phase separation (VIPS) (Casper et al. 2004; Fashandi and Karimi 2012; Lin et al. 2010). When a fluid jet of PS solution is exposed to humid environment, the polymer solution undergoes phase separation into polymer-rich and solvent-rich regions. Then the polymer-rich phase solidifies quickly, whereas the solvent-rich phase delays the solidification. Highly volatile THF in solvent-rich region contributes to creating small pores at the surface upon its rather faster evaporation, while low volatile DMF contributes to forming corrugations and grooves at the surface by the growth of pores and evolution of channels.

In addition to the effect of binary solvent system, it was also found that 3D configuration of the web could be controlled by the environmental humidity during electrospinning process. Figure 4 presents pure PS and PA6 electrospun webs produced from the varied environmental humidity during electrospinning process. A4 formed a smooth membrane-like surface in all the humidity conditions; however, S4A0 web configuration was highly dependent on humidity condition. With the increased humidity, PS web formed a bulkier and fluffier structure having more air content. This phenomenon can be explained by the repulsive interactions between neighboring PS fibers when they are dissolved in an electrically conductive solvent like DMF and a solvent-rich phase is formed in humid environment (Bonino et al. 2012; Sun et al. 2012). Thus, by choosing the right condition for environmental humidity during electrospinning process and solvent system, 3D web configuration and surface morphology can be controlled for the relevant application. For example, a bulky and porous PS web that is produced in humid and solvent rich condition would make a good material for thermal insulation with large air content in its structure.



### Tensile properties

Tensile property with the varied ratio of PS/PA6 is shown in Fig. 5. PS web had low tensile strength (0.4 MPa) and relatively high strain at break (78%), while PA6 web showed five times higher strength (2.0 MPa, 32% strain) than PS. The mechanical strength of blend web was enhanced as PA6 content was increased. In the earlier work by Park et al. (2011), lower mechanical strength of PS was attributed to the lack of bonding of PS fibers, fibers being easily slipped when extended. Good mechanical strength of PA6 web may be stem from better bonding by the layers of individual fibers resulting from a slow evaporation of solvent. A relatively high strain at break of S2A2 blend (strain 96%) can be explained by the lack of bonding in PS fibers in the web, where the fiber slippage and extension occurred up to 96% strain.

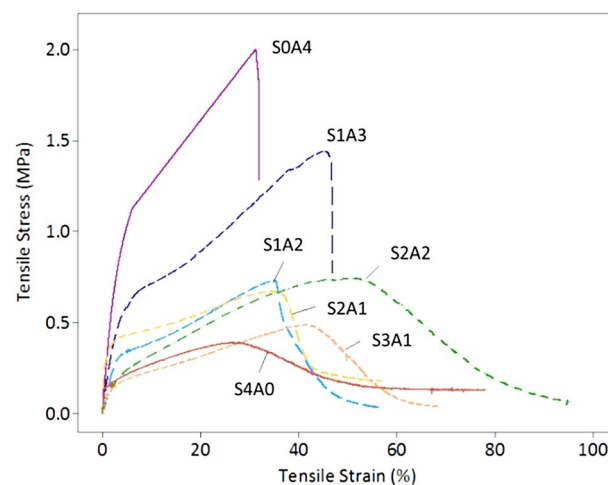
### Porosity

Table 2 shows the total pore volume and % porosity. S4A0 electrospun web exhibited the largest pore size distribution, pore volume, and porosity due to its relatively bulkier structure (Fig. 3). A4 showed the least pore size distribution, pore volume, and porosity. The total pore volume significantly decreased with the increase of PA6 contents within the blend web, because the smaller size PA6 fibers filled up the large pores formed by PS fibers. Likely, the porosity calculated from the web density was highly influenced by the PA6 content.

### Air permeability and water vapor permeability

Air permeability of the web was measured by the volume of air passing through the web per second with the incremental pressure up to 300 psi (Fig. 6). S4A0 required the lowest pressure to pass the same amount of air, indicating the highest air permeability. Adding PA6 decreased the air permeability. It appears that the porosity is correlated to the air permeability of the web.

Water vapor transmission, however, was not directly associated with the porosity of the web (Fig. 7). Instead, it was influenced both by the porosity and the surface

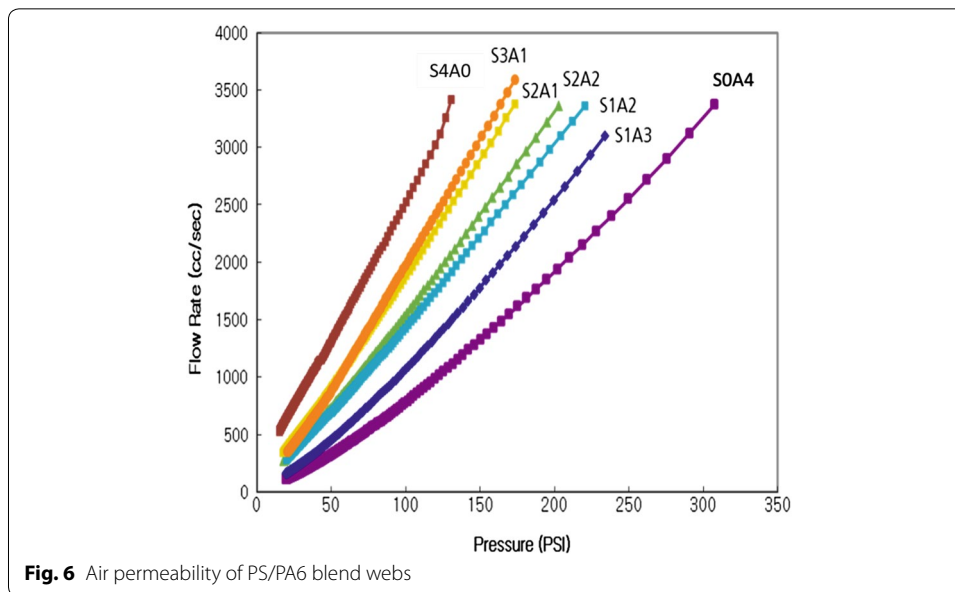


**Fig. 5** Stress-strain curve for various contents PS/PA6 webs: **a** 4/0, **b** 3/1, **c** 2/1, **d** 2/2, **e** 1/2, **f** 1/3, **g** 0/4

**Table 2 Pore size range, total pore volume and porosity of PS/PA6 blend webs**

Sample	Pore size range ( $\mu\text{m}$ )	Sample density ( $\text{g}/\text{cm}^3$ )	Total pore volume ( $\text{ml}/\text{g}$ )	Porosity <sup>a</sup> (%)
S4A0	0.47–10.20	0.123	6.473	79.62
S3A1	0.11–9.95	0.153	4.878	74.63
S2A1	0.05–9.91	0.170	4.214	71.63
S2A2	0.03–7.23	0.217	3.198	69.39
S1A2	0.01–4.16	0.221	3.001	66.33
S1A3	0.01–5.18	0.257	2.398	61.62
S0A4	0.01–3.75	0.321	1.898	60.92

<sup>a</sup> Porosity = sample density  $\times$  total pore volume  $\times$  100

**Fig. 6** Air permeability of PS/PA6 blend webs

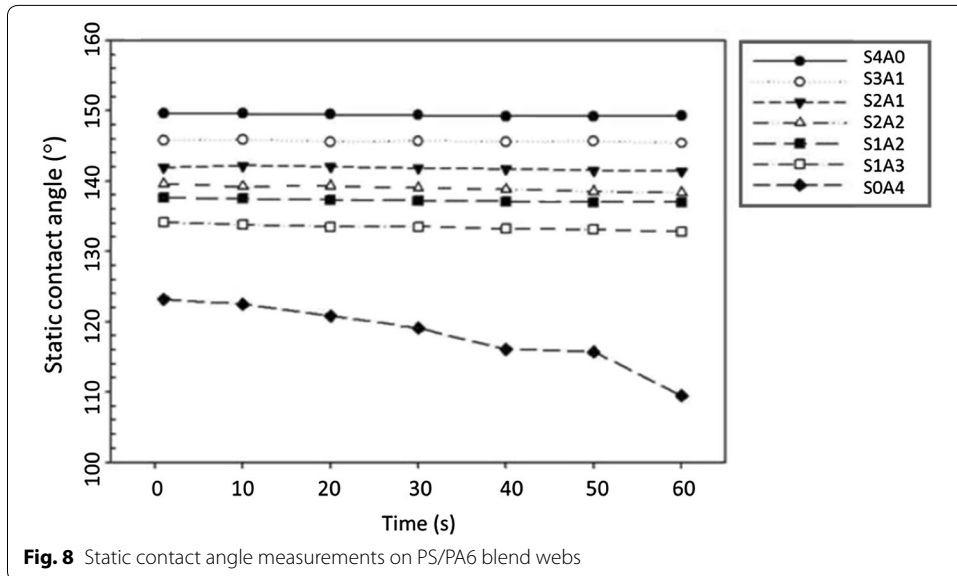
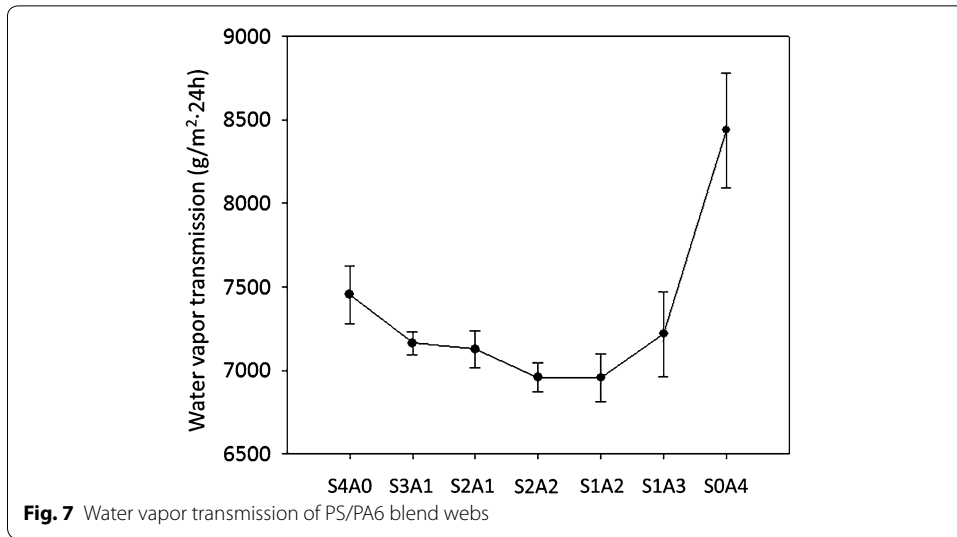
hydrophilicity of webs. Many researchers (Ahn et al. 2011; Gibson 1993; Wehner et al. 1988) have agreed that water vapor travels through air spaces of textiles and experiences absorption and desorption within fibers.

The effect of porosity on water vapor transmission was dominant for S4A0, S3A1, S2A1, S2A2, and S1A2; that is, the increased PA6 content reduced the web porosity, and thus lowered the water vapor transmission. However, when PA6 was further increased in the web content, hydrophilicity by PA6 contributed more to the water vapor transmission, significantly enhancing the water vapor transmission for A4. Thus, when PA6 is blended with PS web, it should be understood that certain comfort properties such as air permeability and water vapor transmission can be compromised in exchange of improved mechanical strength.

### Surface hydrophilicity

Surface hydrophilicity of PS/PA6 blend webs were investigated through static contact angle (SCA) measurements (Fig. 8). S4A0 had high SCA value of  $150^\circ$  due to the low surface energy and surface roughness coming from PS fiber's wrinkled surface (Fig. 3)





(Miyachi et al. 2006). As the PA6 composition increased, SCA was decreased accordingly. It was because PA6 has higher surface energy (45.3 mN/m) (Gotoh 2004) than that of PS (40.7 mN/m) (Harris et al. 2003). Also the phenomenon may be caused by the fact that PA6 fibers were finer and smoother, giving less surface roughness than PS fibers (Fig. 3). All samples except S0A4 maintained consistent SCA for 60 s of time. Park et al. (2014) suggested that PA6 plain textiles may wet more quickly than PA6 film, because wetting can be facilitated at the textile surface by the wicking through fiber interfaces. Densely packed PA6 fibers of S0A4 sample can possibly promote wicking and spreading, giving a decreasing SCA with 60 s of time.

### Thermal properties

As the thermal conductivity of air is as low as 0.025 W/m K, thermal conductivity of textile material is largely influenced by air content (Kim and Park 2013). Thermal conductivity for PS film is reported to range in 0.10–0.13 W/m K (Han and Fina 2011; Hu et al. 2001) and that of PA6 film to be 0.25 W/m K (Han and Fina 2011). Also, a material with higher density and lower air content is likely to have higher thermal conductivity, deteriorating thermal insulation.

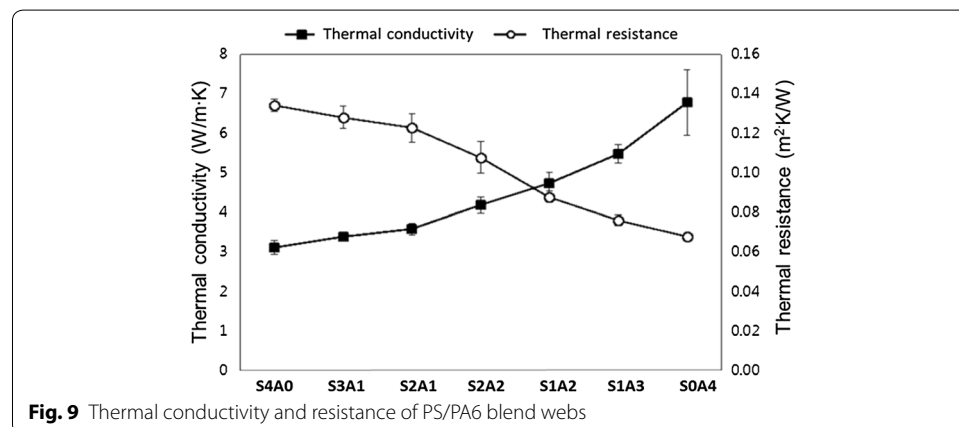
In Fig. 9, as PA6 content increased, thermal conductivity of the web increased, due to PA6's higher thermal conductivity and the lowered porosity (or lower air content). PS fibers not only had larger porosity but also had corrugations on fiber surfaces, resulting in a larger air content for the PS web.

Thermal resistance of the web was linearly reduced with higher PA6 content (Fig. 9). As shown in Fig. 3, finer PA6 fibers appeared to interlace with larger PS fibers, forming a complicated and dense pore structure. The results show that the addition of PA6 can enhance the mechanical strength of the web in the expense of comfort factors in terms of thermal resistance, air permeability, and water vapor transmission.

### Conclusion

To obtain fibrous webs with the high thermal resistance and reasonable mechanical strength, blend webs with PS and PA6 contents were produced by the multi-jet electrospinning process. Confocal microscopy can be used to examine fiber contents and distribution in the web, while immersion test gave more accurate fiber contents of the blend web. Fiber morphology and 3D structure of PS fibrous web were influenced by the environmental humidity during electrospinning process and solvent selection. PS web produced in higher humidity generated more pores and corrugations at the surface. The increased surface roughness and porosity led to the increased hydrophobicity and thermal resistance.

The addition of PA6 to PS enhanced the mechanical strength. However, the added PA6 deteriorated the comfort properties including air permeability, water vapor transmission rate, and thermal resistance. Water vapor transmission of 100% PA6 web, however, was significantly better than that of blend web due to higher surface hydrophilicity of the web. The lowered thermal resistance by the addition of PA6 is attributed to (1)



higher thermal conductivity of PA6 material and (2) lowered air content for compact PA6 structure.

The blend ratio of PS/PA6 influenced on blend web structure, morphology, and properties. Future study is needed for the environmental parameters in electrospinning to produce an optimal 3D web structure to achieve the highest thermal resistance. It is recommended to examine the ways to enhance the mechanical strength of the PS web, probably by lowering the rate of solvent evaporation to allow more time for fiber bonding.

#### Authors' contributions

All authors were involved in the design of experiments and result discussion. Also, all authors read and approved the final manuscript.

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#### Competing interests

On behalf of all authors, the corresponding author states that there is no competing interests.

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