

## Comparative in vitro study and biomechanical testing of two different magnesium alloys

Journal of Biomaterials Applications  
2014, Vol. 28(8) 1264–1273  
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DOI: 10.1177/0885328213506758  
jba.sagepub.com  


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### Abstract

In this in vitro study, magnesium plates of ZEK100 and MgCa0.8 alloy similar to common titanium alloy osteosynthesis plates were investigated as degradable biomedical materials with a focus on primary stability. Immersion tests were performed in Hank's Balanced Salt Solution at 37°C. The bending strength of the samples was determined using the four-point bending test according to ISO 9585:1990. The initial strength of the noncorroded ZEK100 plate was 11% greater than that of the MgCa0.8 plate; both were approximately 65% weaker than a titanium plate. The bending strength was determined after 48 and 96 h of immersion in Hank's Balanced Salt Solution; both magnesium alloys decreased by approximately 7% after immersion for 96 h. The degradation rate and the Mg<sup>2+</sup> release of ZEK100 were lower than those of MgCa0.8. Strong pitting and filiform corrosion were observed in the MgCa0.8 samples after 96 h of immersion. The surface of the ZEK100 plates exhibited only small areas of filiform corrosion. The results of this in vitro study indicate that the ZEK100 alloy may be more suitable for biomedical applications.

### Keywords

In vitro, corrosion, magnesium, orthopedic, implants

### Introduction

Magnesium and its alloys were rediscovered at the end of the 20th century as promising degradable biomaterials for orthopedic applications.<sup>1–3</sup> Researchers are attracted by the prospect of avoiding a second surgery for implant removal, which is necessary with titanium implants.<sup>4</sup> In addition, magnesium alloys provide desirable mechanical properties, close to those of natural bone, which prevent the “stress shielding” phenomena.<sup>5</sup> Magnesium reportedly stimulates new bone formation (osteoinductive) and also supports the adherence of bone tissue to its surface (osteoconductive).<sup>5–8</sup>

In human body fluids and blood plasma with high Cl<sup>-</sup> concentrations, the degradation of magnesium alloys is accompanied by a loss of mechanical stability. The resulting surface layer consists mainly of the corrosion product magnesium hydroxide (Mg(OH)<sub>2</sub>), which is locally dissolved into soluble MgCl<sub>2</sub>. In addition, calcium phosphate salts<sup>9</sup> and MgCO<sub>3</sub><sup>10</sup> precipitate on the surface of magnesium alloys resulting in a corrosive protective effect. During the corrosion process, Mg<sup>2+</sup> ions are released from the metal.

Magnesium is a natural component of the human body and it is mainly stored in bone (60–65%).<sup>11</sup> Furthermore, it is the second most abundant cation in cells and an important cofactor for many enzymes that are involved in metabolic pathways and DNA repair processes.<sup>11,12</sup> The concentration of Mg<sup>2+</sup> in the blood serum of human adults comprises 0.7–1.1 mol/l;

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serum  $Mg^{2+}$  levels exceeding this amount are excreted by the kidneys.<sup>11</sup>

In this *in vitro* study, two different magnesium alloys were investigated: one containing rare earth elements (REEs) (ZEK100) and MgCa0.8. Both alloys were chosen because of their promising biomechanical properties, and both had been evaluated *in vivo* in previous studies.<sup>13–21</sup> ZEK100 pins have shown promising initial mechanical stability.<sup>15,20</sup> Lensing et al. reported good biocompatibility and an osteoconductive effect of ZEK100 in the middle ear of rabbit.<sup>17</sup> In contrast, some studies have shown that the biocompatibility of the ZEK100 alloy appears to be questionable.<sup>16,22</sup>

Pure magnesium possesses insufficient mechanical properties.<sup>23</sup> The alloying of magnesium with a large variety of elements was introduced to solve this issue. These alloying elements influence the corrosion film composition and therefore the corrosion properties.<sup>24</sup> Magnesium alloyed with passivating elements, such as the REE (yttrium and neodymium), exhibits enhanced corrosion resistance.<sup>18,24</sup> Magnesium alloys containing REE were first investigated at the beginning of the 1980s.<sup>25</sup> The addition of REE contributes to solid solution strengthening and grain boundary strengthening, and therefore enhances the ductility of the alloy.<sup>1,25</sup>

Several studies have investigated the properties and corrosion behavior of binary magnesium–calcium alloys.<sup>13,14,18,19,26–30</sup> The addition of calcium provides solid solution strengthening and contributes to grain refinement owing to grain boundary strengthening.<sup>1</sup> It was observed that the addition of calcium above the solubility limit of approximately 1.34 wt% Ca enhanced the corrosion rate.<sup>18,19,26</sup> The addition of less than 1 wt% Ca demonstrated a low corrosion rate with an appropriate elastic modulus.<sup>18</sup>

Previous studies have demonstrated good biocompatibility of MgCa0.8 *in vivo*.<sup>13,28</sup> The production of high amounts of gas in a short time due to high corrosion rates is undesirable for clinical applications. The accumulation of gas associated with MgCa0.8 implants was mild to moderate *in vivo*, with no harmful effects toward the animal.<sup>14</sup>

In this *in vitro* study, we investigated the corrosion behavior and mechanical properties of two different alloys (MgCa0.8 and ZEK100) in Hank's Balanced Salt Solution (HBSS). The results were compared with a titanium alloy plate (Ti6Al4V) of similar sample size and shape. This study is focused on primary stability and the effects of degradation during the first days of immersion. In addition,  $Mg^{2+}$  release from the alloy was determined, and the corrosion rate was evaluated according to the mass loss method. Alloy surfaces were investigated using scanning electron microscopy (SEM), and high-energy synchrotron radiation was applied for microstructural characterization.

## Methods

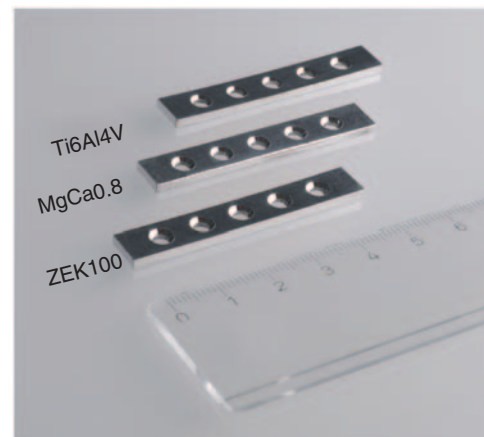
### Material and preparation

Two different magnesium alloys were examined in this study: ZEK100 (1 wt% zinc, 0.1 wt% zirconium, and 0.1 wt% rare earth metals) and MgCa0.8 (0.8 wt% calcium). The plates were 50 mm long, 8 mm wide, and 2 mm thick. They were manufactured by face slab milling. Five screw holes were drilled and counterbored in each plate. The resulting screw holes had an inner diameter of 3 mm on the bone-facing side and a counterbore diameter of 5 mm (Figure 1). The samples had a surface of 898 mm<sup>2</sup>. Two titanium alloy plates with the same dimensions were manufactured from a Ti6Al4V rod (Goodfellow GmbH, Bad Nauheim, Germany).

The surfaces of the magnesium samples were pickled prior to immersion testing with a solution of 5 ml 65% nitric acid (Merck, Darmstadt, Germany), 20 ml 85% glycerol (Merck, Darmstadt, Germany), and 5 ml 100% acetic acid (Merck, Darmstadt, Germany) for 30 s. Next, the samples were ultrasonically cleaned for 2 min with isopropanol and then dried in a vacuum drying oven (Heraeus Vacuum oven, Thermo Scientific, Bonn, Germany) at 50°C for approximately 20 min.

### Immersion testing

The static immersion test was performed in HBSS (Biochrom AG, Berlin, Germany) to simulate the normal ion concentration under physiological conditions at 37.5°C. The corrosion media contained 8.00 g/l NaCl, 0.4 g/l KCl, 0.04 g/l Na<sub>2</sub>HPO<sub>4</sub>, 0.06 g/l KH<sub>2</sub>PO<sub>4</sub>, 0.20 g/l MgSO<sub>4</sub>·7H<sub>2</sub>O, 0.14 g/l CaCl<sub>2</sub>, 1.00 g/l glucose, and 0.35 g/l NaHCO<sub>3</sub>. The plates were placed into 500 ml HBSS by a nonresorbable



**Figure 1.** Picture of the plates (length: 50 mm, width: 8 mm, thickness: 2 mm) used in this *in vitro* study.

wire (Ethicon™Prolene™, 4-0, Johnson & Johnson GmbH, Neuss, Germany). The pH of the solution was monitored during the immersion test using a pH meter (Schott® Instruments Lab850, SI Analytics GmbH, Mainz, Germany). After immersion, the samples were dried and the corrosion layer was removed with chromic acid. Two samples were used per interval of each magnesium alloy. The degradation rate was evaluated according to the weight loss method<sup>31</sup>

$$\Delta W = \frac{W_{\text{before}} - W_{\text{after}}}{At}$$

where  $\Delta W$  is the weight loss,  $W_{\text{before}}$  (mg) is the weight of each sample before corrosion, and  $W_{\text{after}}$  (mg) is the weight of each sample after corrosion.  $A$  is defined as the sample's surface area (cm<sup>2</sup>) and  $t$  is the immersion time (d). This weight loss rate was converted into an average corrosion rate (mm/y) using<sup>31,32</sup>

$$P_w = 2.1\Delta W$$

#### Detection of Mg<sup>2+</sup> release through inductively coupled plasma optical emission spectroscopy (ICP-OES)

The ICP-OES (Spectro Ciros Vision EOP, Spectro Analytical Instruments, Kleve, Germany) was applied to quantitatively determine the release of magnesium ions from the plates during the corrosion process. Two plates of each alloy were immersed in 100 ml HBSS at 37°C for 158 h. At fixed time intervals (the first after 45 min), 1 ml was taken for analysis and replaced with the same amount of fresh corrosion media. The pH of every analysis sample was monitored.

#### Biomechanical testing

To specify the mechanical properties of the specimens, they were tested according to ISO 9585:1990. The four-point bending test setup (Figure 2) was designed for tests with a uniaxial material testing machine (Mini Bionix 858, MTS Systems in Minneapolis, MN, USA). The test system consisted of four rollers with a diameter of 8 mm. The distance between the lower and outer rollers was 32 mm, and the distance between the upper and inner rollers was 10 mm. The plates were positioned on the lower rollers according to the protocol of ISO 9585:1990. The distance between the outer and inner rollers was 11 mm, including a screw hole of the demonstrators. The central screw hole and another screw hole were positioned between the inner rollers. The test rig was produced by the Research Workshop of the Medical School, Hannover, Germany.

#### Microstructural characterization

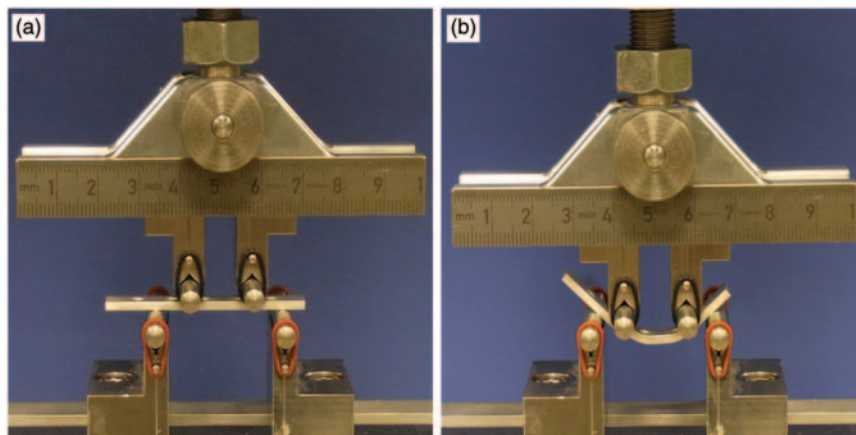
After the corrosion products were removed from the surface with chromic acid, the magnesium plates were analyzed with a Zeiss EVO 60 VP SEM.

Diffraction experiments were performed using high-energy synchrotron radiation ( $E \sim 100$  keV,  $\lambda = 0.12561$  Å). A Perkin-Elmer area detector (400 mm × 400 mm, 200 μm pixel size) was used with a sample-detector distance of 1430 mm.

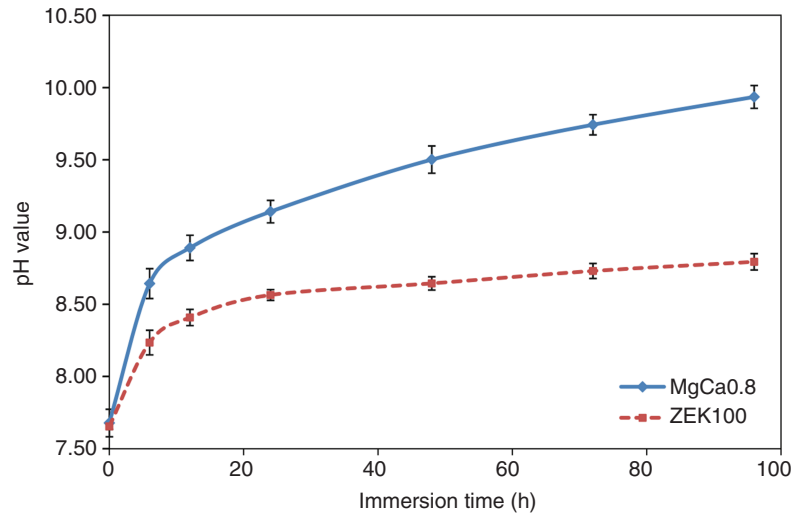
## Results

#### Immersion test and corrosion properties

The pH of HBSS was measured during the immersion of the plates (Figure 3). The pH of the HBSS increased rapidly during the first hours of exposure. After 12 h of



**Figure 2.** Picture of the four-point bending setup. The samples were tested according to ISO 9585:1990.



**Figure 3.** pH value versus immersion time of MgCa0.8 and ZEK100 plates in 500 ml Hank's solution. The dots represent mean values and standard deviation. Sample size for each alloy:  $n = 4$  for 0–48 h,  $n = 2$  each for 72 and 96 h.

**Table 1.** Corrosion rates of the magnesium alloy plates according to the mass loss method.<sup>31</sup> Sample size: Two of each alloy per interval.

	Mean corrosion rate (mm/y)	
	48 h immersion	96 h immersion
MgCa0.8	3.62	2.89
ZEK100	0.70	0.63

immersion, the alkalization of the corrosion medium progressed at a slower pace. However, the immersion of MgCa0.8 plates resulted in a higher HBSS pH than the immersion of ZEK100 plates. After 96 h of immersion, the pH of HBSS rose to 9.9 for MgCa0.8 plates compared with 8.8 for ZEK100 plates.

The corrosion rate was determined after 48 and 96 h using the weight loss method (Table 1). ZEK100 demonstrated a five-fold lower corrosion rate than MgCa0.8.

### Release of $Mg^{2+}$ from the magnesium plates

The  $Mg^{2+}$  concentration dissolved into the HBSS from the magnesium samples was determined using ICP-OES (Figure 4(a)). The MgCa0.8 plates exhibited rapid  $Mg^{2+}$  release during the first 20 h of immersion. The ZEK100 plates exhibited a more consistent increase of  $Mg^{2+}$  concentration throughout the exposure time. The rate of  $Mg^{2+}$  release from the MgCa0.8 plates during the first 24 h of immersion was 1.082 mg/h ( $1.2 \times 10^{-3}$  mg/h  $mm^2$ ), nearly eight-fold higher than the rate

of ion release from the ZEK100 plates: 0.143 mg/h ( $1.592 \times 10^{-4}$  mg/h  $mm^2$ ) (Figure 4(b)). Moreover, the pH of HBSS increased more rapidly as a result of the immersion of the MgCa0.8 samples than the ZEK100 samples. After 20 h, the MgCa0.8 corrosion media reached a stable pH of approximately 10 (Figure 4(c)).

### The effect of corrosion on bending strength

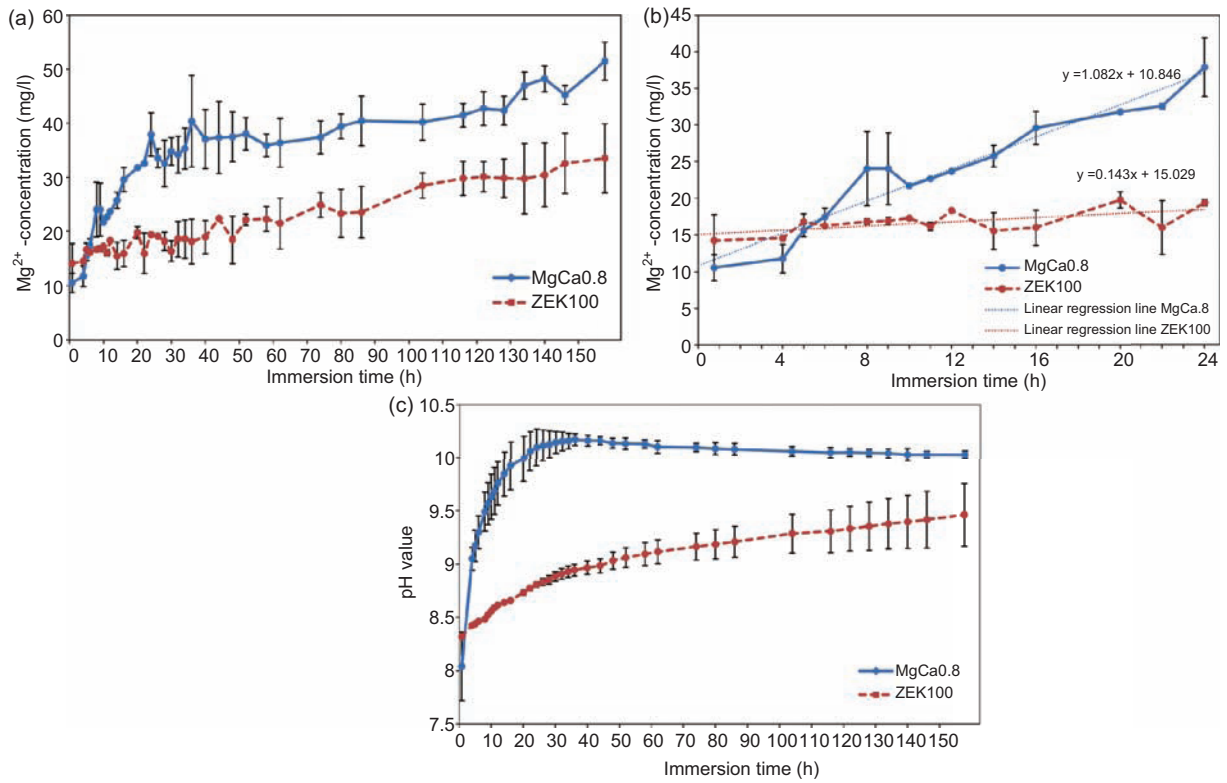
Figure 5 shows the bending strengths of the magnesium and titanium plates. Uncorroded samples of ZEK100 ( $0.306 \pm 0.003$  Nm) were stronger than MgCa0.8 ( $0.272 \pm 0.00005$  Nm). In contrast, the bending strength of titanium plates with the same dimensions was higher ( $0.803 \pm 0.001$  N m).

The strength of both magnesium alloys decreased with immersion time. The bending strength after 96 h of immersion was approximately 7% lower than the initial bending strength (0 h immersion).

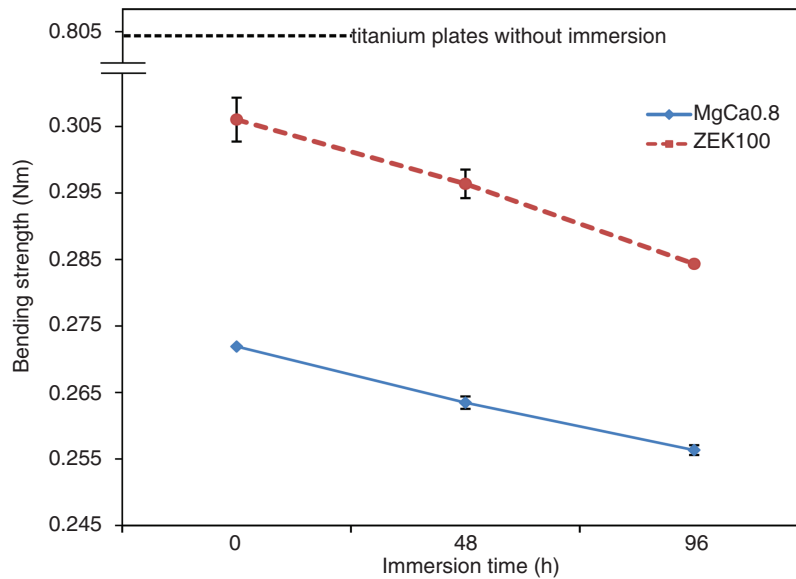
### Microstructural characterization and phase identification

Figure 6 shows the surface of the magnesium plates after removal of the surface corrosion products that resulted from 96 h of immersion. Filiform and pitting corrosion were observed on the surface of the MgCa0.8 alloy. The surface of the ZEK100 plates showed only small areas of filiform corrosion (Figure 6(a) and (b)).

The diffraction diagram and the diffraction rings of both alloys are displayed in Figure 7. The diffraction rings of both alloys demonstrated an inhomogeneous intensity distribution (Figure 7(b) and (e)). The diffraction diagram of the MgCa0.8 alloy is shown in Figure 7(c) and (d). In addition to the measured intensities



**Figure 4.** (a) Mg<sup>2+</sup> release from the ZEK100 and MgCa0.8 plates as a function of time. (b) Average Mg<sup>2+</sup> release during the first 24 h. (c) pH of the analyzed corrosion media sample. The dots represent mean values and standard deviation. Two samples were tested per alloy.

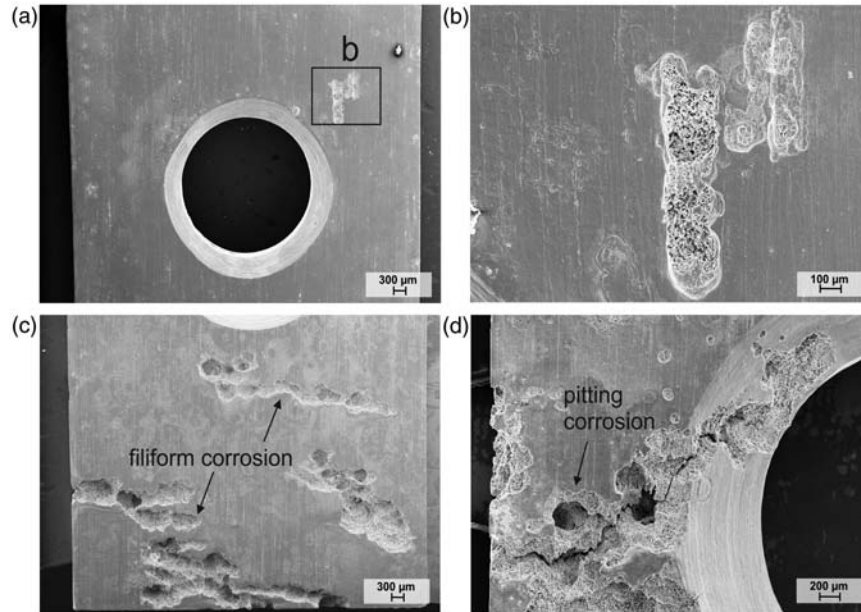


**Figure 5.** Bending strength versus immersion time. The bending strength of both alloys decreased with immersion time. The dots represent mean values and standard deviation. Two samples were tested per alloy and immersion time.

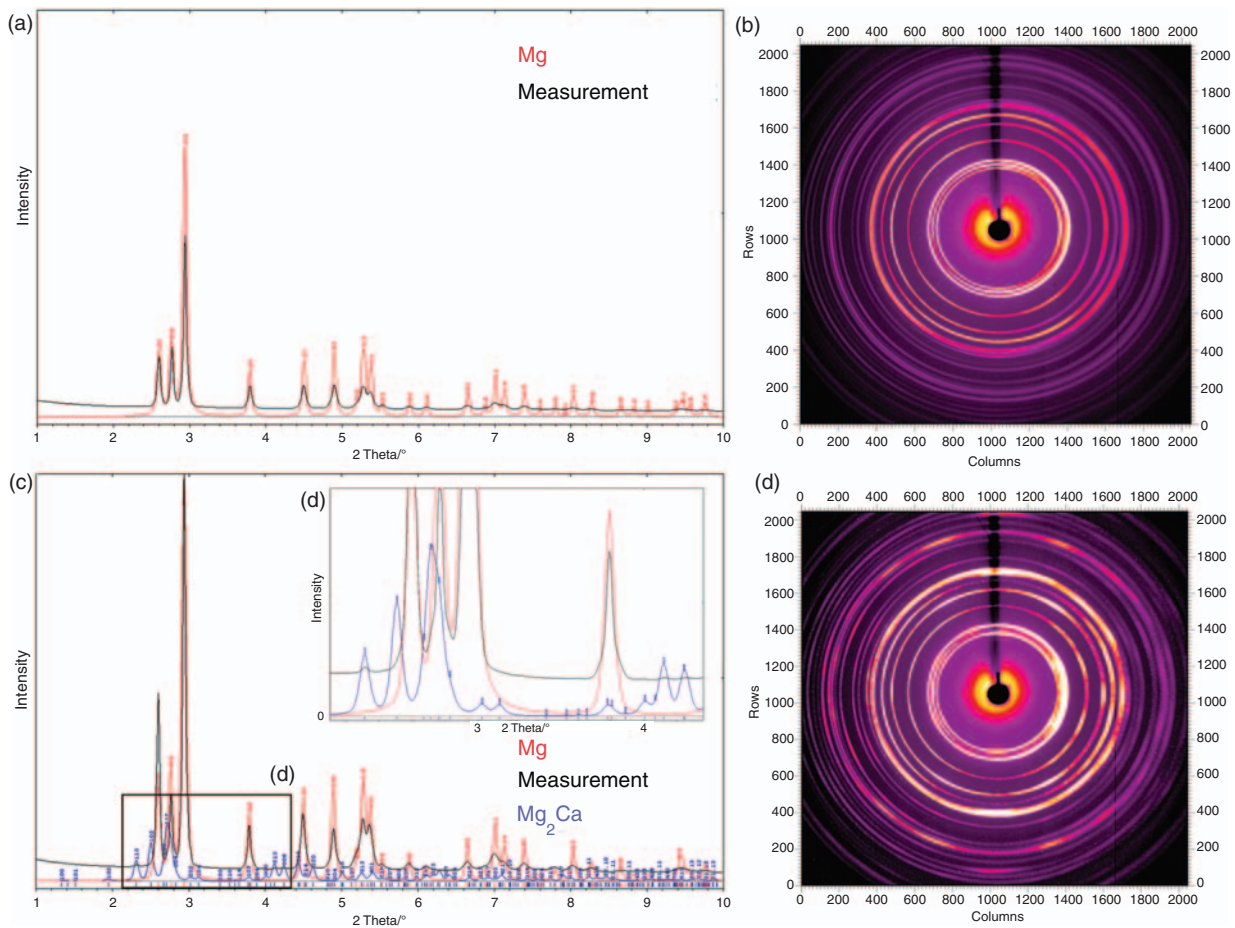
(black line), simulated diffraction diagrams are also provided for Mg (solid solution, red line) and Mg<sub>2</sub>Ca (intermetallic compound, blue line). Both simulated phases fit the position of the measured reflection lines

quite well, but not the intensity. The measured intensities of the ZEK100 samples also differed strongly because of the material's texture. No intermetallic phases were detected.





**Figure 6.** SEM pictures of the plates after 96 h immersion and removal of the corrosion layer. (a) and (b): ZEK100 and (c) and (d): MgCa0.8.



**Figure 7.** Diffraction diagram and diffraction rings of ZEK100 and Mg<sub>2</sub>Ca0.8 alloy samples. (a) and (b): ZEK100 and (c) to (e): Mg<sub>2</sub>Ca0.8.

## Discussion

Fracture healing is dependent on the fracture gap and achieved stabilization. Plates are a common orthopedic implant and are usually attached to the bone with screws.<sup>33</sup> The fixation of a plate should supply sufficient stability to enhance fracture healing. High primary stability is important and should not decrease greatly during the first days after the placement of the plate. Therefore, in this *in vitro* study we focused on the initial strength of the magnesium implants versus titanium implants and investigated the implant stability specifically during the first days of immersion. The currently used plates are made of stainless steel or titanium alloys<sup>5</sup> and are available in a wide range of sizes. In this study, five-hole plates from two different magnesium alloys were examined after immersion in HBSS and compared with titanium plates.

The biomechanical results of the magnesium-based plates were compared with those of a plate made from the titanium alloy Ti6Al4V, which is commonly used in orthopedic trauma surgery. Titanium alloys exhibit minor biocorrosion with the release of metallic ions, which normally do not compromise plate stability.<sup>34</sup> The corrosion products, released metallic ions, have been associated with proinflammatory, cytokine-induced, enhanced osteoclastic activity, which in turn causes bone resorption.<sup>34</sup>

We assume that the loss of stability of titanium alloys is negligible within the short period of time (96 h) observed in our study. Therefore, the biomechanical examinations of the titanium plates were performed to their initial conditions without immersion tests.

The bending strength of the titanium plates is comparable to that of a 2 mm mini-fragment plate, which was also tested according to ISO 9585:1990.<sup>35</sup> In this study a bending strength of 0.53 Nm was determined. The biomechanical parameter of the tested 2 mm mini-fragment plate is lower than the bending strength of the titanium plates evaluated in our study (0.803 Nm). The reason for this slight deviation might be explained by the difference in plate design.

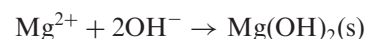
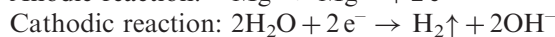
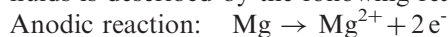
The initial strengths of both magnesium alloys were approximately 65% lower than that of the titanium alloy. Of the two magnesium alloys, the ZEK100 plates exhibited greater initial stability. Therefore, ZEK100 plates may be considered more suitable for osteosynthesis applications than MgCa0.8 plates. The degradation of magnesium alloys is known to be high in the first hours of exposure to the corrosion media. This is mainly due to the fact that the corrosion protective layer needs some time for formation. Therefore, we particularly investigated the first hours of corrosion and its effect on the stability of the magnesium plates.

The study of Waizy et al. showed that between week 2 and week 6 of immersion of ZEK100 in HBSS no considerable change in bending strength was reported.<sup>36</sup> Our study showed that in the first 96 h of degradation the bending strength of both magnesium alloys decreased about 7%. ZEK100 still have a higher stability and is therefore based on the biomechanical results of the preferred magnesium alloy. Many studies have shown that the degradation of magnesium alloys in *in vitro* experiments is higher than in comparable *in vivo* studies.<sup>37–39</sup> A decreased loss of stability *in vivo* compared to the results in this study is assumed.

Alloy plates are used in clinical practice as internal splints to hold fractured ends of bone together; additional fracture stabilization with lag screws is common. According to the biomechanical results, the preferred use of these magnesium-based plates is the fixation of non-weight-bearing bones (e.g. fracture of the metacarpal bones). Sufficient stability of degradable plates *in vivo* must be ensured during the first 6–8 weeks after implantation.<sup>40</sup>

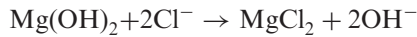
The magnesium alloy ZEK100 contains REE and zirconium in low concentrations. The alloying elements are used to improve the mechanical and corrosion properties of the biomaterial.<sup>41</sup> These alloying elements are known to have adverse effects and potential long-term risks,<sup>42–45</sup> although some studies have reported good biocompatibility.<sup>46,47</sup> Allergic hypersensitivity, reduction of hemoglobin oxygen affinity, and fatty liver are some potential adverse effects of these elements at toxic doses.<sup>43,45</sup> Chelated REE are easily excreted in the urine, and mortality studies have revealed that REE are not highly toxic.<sup>43</sup> However, bone is one of the main target organs of REE because REE are of a radius similar to Ca<sup>2+</sup> ions, which may lead to REE accumulation in the environment directly surrounding the implant.<sup>43</sup> Because implants made of degradable magnesium alloys are not removed after implantation, *in vivo* biocompatibility studies should focus on the long-term effects of these implants. In an animal study with 12 months of observation time, a good biological response to a REE-containing alloy (MgYREZr, similar to WE43) and its degradation products was observed.<sup>48</sup>

The degradation of magnesium and its alloys in biofluids is described by the following reaction



Degradation is accompanied by an alkalization of the corrosion media due to the production of hydroxide ions (OH<sup>-</sup>). These experiments were performed without CO<sub>2</sub> gas application. HCO<sub>3</sub><sup>-</sup>/CO<sub>2</sub> is the main buffering

system in blood and in HBSS. The high proportion of hydroxide ions supports the formation of magnesium hydroxide, which in turn acts as a protective layer against corrosion. The greater tendency toward film formation is reportedly associated with local pH > 10.5 and is believed to have a corrosion-inhibiting effect.<sup>49</sup> Magnesium hydroxide is disrupted by chloride ions with the release of OH<sup>-</sup>



In response to the immersion of both magnesium alloys (ZEK100 and MgCa0.8), the pH of the HBSS increased sharply during the first hours of exposure. An accelerated pH increase during the first hours of immersion was reported by several *in vitro* studies.<sup>50–53</sup> The decelerated increase of pH after 6 h may be attributed to the formation of magnesium hydroxide and other phosphate- and calcium-containing salts, which precipitated on the surface of the magnesium samples. Interestingly, the pH of the HBSS increased more with the immersion of MgCa0.8 plates than ZEK100 plates. This finding indicated the more progressed and faster corrosion of the MgCa0.8 plates. These observations were supported by the determined corrosion rates for both magnesium alloys according to the mass loss method (Table 1). The corrosion rates were approximately five-fold greater for the MgCa0.8 plates than for the ZEK100 plates. The corrosion rate was slower after 96 h of immersion than after 48 h, which can be explained by the protective effect of the formed surface films (resulting from the precipitation of calcium phosphate salts and magnesium hydroxide). Song et al. reported the formation of a magnesium hydroxide film on the surface of an AZ31 within 2 h after immersion.<sup>23</sup> Similar to our results, Zhu et al. reported a reduction of the corrosion rate with progressing immersion time for a AZ31 alloy.<sup>54</sup> A study by Walker et al. reported lower corrosion rates for MgCa0.8 than were observed in the present study (1.937 mm/y in MEMp, 1.291 mm/y in MEM, and 0.795 mm/y in EBSS).<sup>38</sup>

Several studies have shown that the corrosion rates *in vivo* differ from those determined *in vitro*.<sup>39,55</sup> Many different parameters influence the *in vitro* corrosion rate (e.g. choice of corrosion media, temperature, CO<sub>2</sub> gas application, etc.).<sup>3,56,57</sup> Therefore, the alteration of parameters makes it difficult to compare different *in vitro* tests.

The release of Mg<sup>2+</sup> from the metal was measured using ICP-OES analysis (Figure 4). Only a few studies have analyzed the release of Mg<sup>2+</sup> from magnesium alloys.<sup>51,52</sup> These results confirm the observations of the immersion test and the determination of the corrosion rate. The release of Mg<sup>2+</sup> decelerates with immersion time as a consequence of protective surface layer

formation. This analysis is influenced by the formation and degradation of Mg(OH)<sub>2</sub>. Some of the dissolved Mg<sup>2+</sup> ions from the metal form insoluble magnesium hydroxide Mg(OH)<sub>2</sub>, and therefore are excluded from the analysis, although as mentioned previously, Mg(OH)<sub>2</sub> can be transformed into soluble MgCl<sub>2</sub> by Cl<sup>-</sup> ions and is therefore again accessible for ICP-OES analysis. However, the speed of this accumulation and degradation process is unknown. Notably, the high rate of MgCa0.8 corrosion appears to result in a faster loss of biomechanical stability.

The microstructural characterization of the MgCa0.8 plates revealed the presence of the intermetallic Mg<sub>2</sub>Ca phase, which is consistent with other studies.<sup>26,58</sup> Intermetallic phases form during the solidification of the cast alloys and mainly distribute at the grain boundaries.<sup>59</sup> Most of the intermetallic second phases reportedly possess a corrosion-accelerating effect.<sup>60</sup> This reduction of corrosion resistance is mainly attributed to galvanic corrosion between the anodic α-Mg and the intermetallic phases, which act as a cathode.<sup>60</sup> Kirkland et al. report that this phase is very reactive, with faster dissolution rates than Mg.<sup>26</sup> The Mg<sub>2</sub>Ca phase is described as a more efficient anode than α-Mg.<sup>26</sup>

Analysis of the ZEK100 plate revealed no intermetallic phases. Here, a combined Rietveld texture analysis would have given very precisely the amounts of the present phases and the texture (to calculate the anisotropic behavior of the material). Small amounts of other phases might also be found using this method, because of the improved alignment of the measured intensities. MgZn and Mg<sub>2</sub>Zn are the most prominent intermetallic phases that would be expected according to an analysis of a similar magnesium alloy.<sup>51,61</sup>

## Conclusion

Magnesium plates made of different magnesium alloys were investigated after *in vitro* corrosion in HBSS. Biomechanical tests demonstrated a continuous loss of mechanical strength by osteosynthesis plates made of magnesium alloys. Although the initial bending strength of the uncorroded ZEK100 plate was greater than that of the MgCa0.8 plate, both were approximately 65% weaker than a titanium plate. The degradation rate and the Mg<sup>2+</sup> release of ZEK100 were lower than those of MgCa0.8.

## Acknowledgments

The authors gratefully acknowledge the financial support provided by the German Research Society (DFG) within the collaborative research project (SFB 599). We thank Markus Badenhop for excellent technical support and Christopher Müller for the design of Figure 1.



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