

## **Reducing the sensation of electrical stimulation with dry electrodes by using an array of constant current sources**

SOLOMONS, Cassandra, SLOVAK, Martin, HELLER, Ben  
<<http://orcid.org/0000-0003-0805-8170>> and BARKER, Anthony

Available from Sheffield Hallam University Research Archive (SHURA) at:

<http://shura.shu.ac.uk/17405/>

---

This document is the author deposited version. You are advised to consult the publisher's version if you wish to cite from it.

### **Published version**

SOLOMONS, Cassandra, SLOVAK, Martin, HELLER, Ben and BARKER, Anthony (2018). Reducing the sensation of electrical stimulation with dry electrodes by using an array of constant current sources. *Medical Engineering & Physics*, 51, 91-95.

---

### **Copyright and re-use policy**

See <http://shura.shu.ac.uk/information.html>

1 **Title: Reducing the sensation of electrical stimulation with dry electrodes by**  
2 **using an array of constant current sources**

3 Cassandra D Solomons<sup>1,2</sup>, Martin Slovak<sup>1</sup>, Ben Heller<sup>3</sup>, Anthony T. Barker<sup>1</sup>

4 <sup>1</sup> Medical Physics & Clinical Engineering, Royal Hallamshire Hospital, Sheffield, S10  
5 2JF, United Kingdom

6 <sup>2</sup> SENSE School, VIT University, Vellore 632014, Tamilnadu, India (*Present address*)

7 <sup>3</sup> The Centre for Sports Engineering Research, Sheffield Hallam University, Sheffield,  
8 United Kingdom

9

10 **Corresponding author:** Dr Martin Slovak, Medical Physics & Clinical Engineering,  
11 Royal Hallamshire Hospital, Sheffield Teaching Hospitals NHS Foundation Trust,  
12 Glossop Road, Sheffield, S10 2JF, United Kingdom, tel. +44 0114 27 1160, email:  
13 [m.slovak@sheffield.ac.uk](mailto:m.slovak@sheffield.ac.uk)

14

15

16

17

18

19

20

21

22

23

24

25       **Abstract**

26 Hydrogel electrodes are commonly used for functional and other electrical stimulation  
27 applications since the hydrogel layer has been shown to considerably reduce the  
28 perception of stimulation compared to dry electrodes. However, these hydrogel  
29 electrodes must be changed regularly as they dry out or become contaminated with  
30 skin cells and sweat products, thus losing their adhesiveness and resistive properties.  
31 Dry electrodes are longer lasting but are more uncomfortable due to unequal current  
32 distribution (current hogging). We hypothesize that if current through a dry electrode  
33 is equally shared amongst an array of small sub-electrodes, current hogging and thus  
34 the sensitivity perceived due to stimulation will be reduced. We constructed an 8 x 8  
35 array of millimetre sized dry electrodes that could either be activated as individual  
36 current sources, or together as one large source. A study was performed with 13  
37 participants to investigate the differences in sensation between the two modes of  
38 operation. The results showed that 12 out of 13 participants found the new (distributed-  
39 constant-current) approach allowed higher stimulation for the same sensation. The  
40 differences in sensation between single and multiple sources became larger with  
41 higher intensity levels.

42       **Keywords:** Dry electrodes; electrical stimulation; array stimulation

## 43 **1. Introduction**

44 The application of electrical current to stimulate nerves for functional and therapeutic  
45 purposes is well established [1], [2]. Electrodes play a major role in the success of  
46 stimulation since the efficacy of intervention, avoidance of tissue injury and the  
47 associated discomfort are all determined by the stimulation waveform and type of  
48 electrode used [2]. Surface electrodes are the most commonly used electrode types  
49 in typical functional electrical stimulation (FES) application for correction of foot drop  
50 caused by damage to the brain or spinal cord. Guiraud et al reported that implanted  
51 FES devices for gait restoration have been restricted to experimental concepts, and  
52 have very little follow-up data [3]. The size, shape, material and placement of surface  
53 electrodes determines how effectively the underlying muscles and nerves are  
54 stimulated with the least amount of discomfort [4]. Good surface electrodes should be  
55 comfortable during use, easy to apply, stay in place for at least a day, re-usable, cost  
56 effective and reliable [5].

57 In the past, carbon-rubber electrodes were commonly used. However, these require  
58 the application of electrode gel which can be messy and inconvenient. Therefore low-  
59 cost self-adhesive hydrogel electrodes are currently use as standard. As the resistivity  
60 of the hydrogel layer increases, the stimulation-induced discomfort decreases [6].  
61 Though high resistivity hydrogel electrodes possess most of the desired properties  
62 required for good electrodes, they have poor reusability. Using old, dried out and dirty  
63 electrodes increases the chances of causing skin irritation, reduces self-adhesiveness  
64 and increase electrode-tissue impedance. Regular replacement of these electrodes  
65 increases the costs of therapy, especially when more sophisticated and costly  
66 electrodes are required [8].

67 Taking these issues into consideration, dry electrodes appear attractive for long-term  
68 applications. However, dry electrodes may cause pain or discomfort when high  
69 intensity electrical stimulation is applied. At low current intensities, stimulation evokes  
70 a sensory reaction without muscle contraction; as the current intensity is increased in  
71 order to evoke a muscle contraction, this sensory response increases and can cause  
72 pain and skin irritation [9]. Hair follicles, sweat pores and other structures beneath the  
73 skin form paths of low resistance for the current passing through the electrodes and  
74 thereby cause uneven current densities (“current hogging”). It is thought that the local  
75 high current densities due to current hogging lead to the greater pain associated with  
76 surface stimulation [6]. We hypothesise that if current can be more evenly distributed  
77 across the stimulated area (thus avoiding current hogging) then stimulation will be  
78 more comfortable. One way to achieve this even distribution is to use a high  
79 impedance hydrogel electrode [6]; However, Cooper et al. conducted a study on the  
80 properties of high resistivity hydrogel samples and concluded that they became  
81 contaminated with skin products and lost their desired properties if they were used for  
82 several days [7], causing significant problems in long term applications. An alternative  
83 approach to achieve equal distribution of the current within the electrode is to use  
84 multiple constant current sources, each connected to one of an array of small, adjacent  
85 mini electrodes.

## 86 **2. Material and methods**

### 87 Participants

88 Ethical approval for the study was obtained from the Sheffield Hallam University  
89 Research Ethics Committee and participants were recruited from students and staff  
90 within the University. After obtaining informed consent, thirteen adults, (11 male and

91 2 female) were recruited to the study. Participants were excluded if they had any prior  
92 adverse responses to any form of electrical stimulation or had any skin conditions such  
93 as eczema.

#### 94 Equipment and Materials

95 A 64 channel, constant current stimulator, Shefstim, was used to provide stimulation  
96 [10]. The parameters of stimulation i.e., pulse width, amplitude and frequency were  
97 controlled by custom software and PC. A commercially available hydrogel electrode  
98 (StimTrobe 5x5cm, Axelgaard Manufacturing Ltd., USA) was used as the anode. The  
99 cathode was a dry electrode array of 64 electrodes (in an 8 x 8 matrix), constructed  
100 from stainless steel paper pins. The heads of the pins were approximately 1mm in  
101 diameter and were used as the electrodes. The pins were placed through a piece of  
102 stripboard with spacing of 2.54 mm and a 5 mm thick foam backing. The pins were  
103 then soldered onto another piece of stripboard via which the electrodes were  
104 connected to the outputs of the stimulator. The whole electrode formed a square of  
105 30 mm x 30 mm.

106 A breakout box was constructed so that each of the 64 channels could either act as  
107 individual electrodes (multiple sources) or all could be shorted to act as a single  
108 electrode (single source). This allowed the same electrode array to be placed on the  
109 same location and used to compare conventional (single source) and the novel  
110 (multiple sources) stimulation techniques, without having to remove the electrode. The  
111 participant was blinded as to the nature of stimulation, and the two stimulation types  
112 were delivered alternately.

113 Experiment design

114 The participants were asked to sit on a chair and rest their left arm on a table in front  
115 of them. The electrode array was placed approximately 5 cm below the elbow on the  
116 extensor aspect of the left forearm and was secured with two Velcro straps. The anode  
117 was placed on the wrist of the same arm. The experimental protocol consisted of two  
118 parts:

119 *a) Identification of comfort threshold (CT):* This was defined as the threshold at which  
120 the participant felt that the sensation was at a maximum level that would be just  
121 tolerable for long periods of stimulation. This threshold stimulation current was  
122 identified for both single and multiple sources in random order by slowly increasing the  
123 intensity of stimulation and repeated twice more for each stimulation type. The  
124 maximum current of the three measurements was taken as the comfort threshold.

125 *b) Difference in sensation:* For each participant, stimulation was applied at 25%, 50%,  
126 75% and 100% of the largest comfort threshold current identified above, starting at the  
127 lowest intensity. Stimulation was randomly switched between single source (type A)  
128 and multiple sources (type B), whilst keeping intensity constant. The participant was  
129 asked to mark the difference in perceived sensation on the visual analogue scale  
130 provided (Figure 2). Switching between A and B was repeated until the participant was  
131 confident about his decision.

132 Outcome measures

133 *a) Identification of comfort threshold (CT):* After the stimulation intensity was set to the  
134 appropriate level for the measurement being made, current stimulation intensity was  
135 recorded (measured by ShefStim). At the same time the delivered charge was  
136 measured as the voltage ( $V_C$ ) across a  $1\ \mu\text{F}$  capacitor ( $C$ ) connected in series with the

137 participant in the anode path using a battery operated oscilloscope (Tektronix THS  
138 720). The delivered charge was calculated as  $Q [\mu\text{C}] = C [\mu\text{F}] * V_C [\text{V}]$  and applied  
139 current for in one pulse as  $I [\text{mA}] = \frac{Q [\mu\text{C}]}{t_{200} [\mu\text{s}]} * 10^3$

140 *b) Difference in sensation:* The perceived sensation was measured using the Visual  
141 Analogue Scale (VAS). The VAS values are expressed as percentage measured on  
142 10 cm line between 'no difference' and 'much more uncomfortable' for either A (single  
143 source) or B (multiple sources).

144 Analysis

145 *a) Identification of comfort threshold (CT):* The Wilcoxon matched-pair signed rank test  
146 was used for the current threshold measurements. All values are expressed as mean  
147 values with confidence intervals unless indicated differently on the graphs.

148 *b) Difference in sensation:* The Wilcoxon signed rank test was also used to compare  
149 the differences in sensation to a hypothetical value of 0% i.e. no difference in  
150 sensation.

### 151 **3. Results**

152 The results of the comfort threshold measurements showed that 12 out of 13  
153 participants had a higher comfort threshold for multiple current sources. The median  
154 comfort threshold for multiple sources was 14.5 mA (10.4 to 22.1, 97.75% CI of  
155 median) in comparison to 12.4 mA (8.3 to 18.6, 97.75% CI of median) for a single  
156 source. The Wilcoxon non-parametric test gave a highly-significant p value of 0.0017  
157 with median difference of 2.0 mA (0.7 to 4.9 mA, 97.75% CI of median).

158 The magnitude of the differences between the comfort thresholds varied across the  
159 participants (mean 19%) but was as high as 93% more current delivered for one



160 participant (Pt #8). Only one participant (Pt #7) had a higher comfort threshold for the  
161 single source (6% lower for the multiple source). Figure 3 shows a graphical  
162 representation of the results obtained in this test.

163 Two out of the 52 VAS measurements were not collected due to an operator error.  
164 These measurements were at 25% CT for Pt #2 and Pt #8. The values reported below  
165 are differences in VAS values expressed in percent. Positive values indicate the extent  
166 that multiple source stimulation is more comfortable than single source, whereas  
167 negative values indicate the single source is more comfortable. The 25% of comfort  
168 threshold (CT) measurements showed median difference of +5% (0% to +39%,  
169 98.83% CI) and a Wilcoxon signed rank test compared the values to a hypothetical  
170 value of 0 with  $p = 0.089$ , the 50% of CT measurement showed a median difference  
171 of 16% (4% to 28%, 97.75% CI,  $p = 0.0164$ ), the 75% CT measurement showed a  
172 median of 20% (3% to 69%, 97.75% CI,  $p = 0.0083$ ) and maximum intensity showed  
173 a median of 32% difference (0% to 61%, 97.75% CI,  $p = 0.0020$ ).

174 The differences in sensations between single and multiple sources became larger with  
175 higher intensities levels (50%, 75% and max.) in participants Pt#1, Pt#,3, Pt#9 and  
176 Pt#13. However in some participants the differences were consistent typically in Pt#2,  
177 Pt#4, Pt#5, Pt#6 as shown on Figure 4. Participant #7 perceived the single source as  
178 more comfortable than multiple sources at lower currents, but reported the opposite at  
179 maximum CT, similarly Pt #8, at 25% CT.

#### 180 **4. Discussion**

181 We hypothesised that if current is more evenly distributed across the stimulated area  
182 then the stimulation will be more comfortable. The results of the study show that  
183 participants were able to tolerate higher stimulation intensities with multiple sources of

184 stimulation. We expected multiple sources to be increasingly more comfortable than  
185 single source stimulation as stimulation levels increased. Indeed this was the case  
186 globally and some participants clearly showed this phenomena individually. However,  
187 some participants did not perceive much difference between the two stimulation types  
188 and two found multiple sources to be only more comfortable only at the highest levels.  
189 An explanation for this could be due to differing perceptions of sensation for sub-  
190 maximum stimuli. It could also be that the pitch of the electrodes was not small enough  
191 to optimise the control of current hogging. Another factor that could be influential is  
192 that there was no skin preparation, such as hydration of the skin, prior to the  
193 application of the dry electrode to the participants' forearms, and that varying degrees  
194 of skin hydration explain the wide variation in comfort thresholds. It is also possible  
195 that those participants with thicker hair, more sweat glands and naturally drier skin  
196 could have found multiple sources to be more comfortable, although this was not  
197 measured.

198

199 Although the multiple-source constant current stimulation is more comfortable than a  
200 single constant-current source, there was no attempt in this study to stimulate at  
201 functional levels, so we do not know if it is comfortable enough at the currents required  
202 for functional use. The minimum tolerable current intensity (Pt #2) was 9 mA, through  
203 an approximate 6.25 cm<sup>2</sup> contact area. As electrodes in common clinical use are often  
204 25 cm<sup>2</sup>, a larger electrode area may allow a minimum of 36 mA tolerable current, which  
205 is sufficient for most foot-drop applications.

206 Although the *Shefstim* stimulator is very compact for its capabilities (it measures  
207 142mm x 50mm x 14mm and weighs 125 g including batteries), the necessity of having  
208 64 individual constant-current sources makes it larger and more expensive than a well-

209 designed single-channel stimulator. An alternative, lower-cost approach would be to  
210 use resistors to impose near constant-current for each channel. For a maximum  
211 current inequality of 10%, each resistance would have to be of the order of nine times  
212 greater than the maximum skin resistance presented by a single channel, so this would  
213 require an approximately 10 times higher stimulation drive voltage to compensate for  
214 the drop across the resistors, leading to a higher power consumption. Increasing the  
215 tolerance for current inequality would lower this wasted energy.

216

217 The experimental electrode array used in this study is too bulky and inconvenient to  
218 use clinically. A smaller, flexible design integrated into an elasticated garment to hold-  
219 it in place on the skin would be required for this to be a clinically usable approach.

220 Further work should compare comfort levels between stimulation through multiple  
221 sources and a single source using a hydrogel electrode. This will give us a clear picture  
222 of whether the hydrogel electrode could be replaced with an array of dry electrodes.  
223 Additional work should also investigate the tolerable level of current mismatch  
224 between channels.

225 Although stimulation with multiple sources was shown to be more comfortable, it is  
226 clear that there is a large difference in response between participants. Further work  
227 should seek to identify the reasons for these differences, e.g., it is possible that  
228 participants with thicker hair and drier skin found multiple current sources more  
229 comfortable than participants with less hair and more hydrated skin. Understanding  
230 these parameters may help to improve the technique further.

## 231 **5. Conclusions**

232

233 The purpose of this study was to see whether the sensation associated with the use  
234 of dry electrodes could be reduced. Stimulation through multiple sources showed  
235 improved comfort levels compared to single source stimulation in most subjects,  
236 suggesting that it may avoid current hogging.

237 **Conflict of interest:** None

238 **Funding:** Internal departmental – Sheffield Teaching Hospital NHS Foundation Trust,  
239 Sheffield, UK

240 **Ethical approval:** Ethical Approval obtained from Sheffield Hallam University by Dr  
241 Ben Heller in October 2013

242

## 243 **References**

244 [1] P. H. Peckham and J. S. Knutson, "Functional Electrical Stimulation for  
245 Neuromuscular Applications," *Annu. Rev. Biomed. Eng.*, vol. 7, no. 1, pp. 327–  
246 360, 2005.

247 [2] L. R. Sheffler and J. Chae, "Neuromuscular electrical stimulation in  
248 neurorehabilitation," *Muscle Nerve*, vol. 35, no. 5, pp. 562–590, 2007.

249 [3] D. Guiraud, C. Azevedo Coste, M. Benoussaad, and C. Fattal, "Implanted  
250 functional electrical stimulation: case report of a paraplegic patient with complete  
251 SCI after 9 years," *J. Neuroeng. Rehabil.*, vol. 11, no. 1, p. 15, 2014.

252 [4] T. Keller and A. Kuhn, "Electrodes for transcutaneous (surface) electrical  
253 stimulation," *J. Autom. Control*, vol. 18, no. 2, pp. 35–45, 2008.

254 [5] T. Bajd and M. Munih, "Basic functional electrical stimulation (FES) of

255 extremities: An engineer's view," *Technol. Heal. Care*, vol. 18, no. 4–5, pp. 361–  
256 369, 2010.

257 [6] N. Sha, L. P. J. Kenney, B. W. Heller, A. T. Barker, D. Howard, and W. Wang,  
258 "The effect of the impedance of a thin hydrogel electrode on sensation during  
259 functional electrical stimulation," *Med. Eng. Phys.*, vol. 30, no. 6, pp. 739–746,  
260 2008.

261 [7] G. Cooper, A. T. Barker, B. W. Heller, T. Good, L. P. J. Kenney, and D. Howard,  
262 "The use of hydrogel as an electrode-skin interface for electrode array FES  
263 applications.," *Med. Eng. Phys.*, vol. 33, no. 8, pp. 967–972, Oct. 2011.

264 [8] L. P. Kenney *et al.*, "A review of the design and clinical evaluation of the  
265 ShefStim array-based functional electrical stimulation system," *Med. Eng. Phys.*,  
266 vol. 38, no. 11, 2016.

267 [9] J. R. de Kroon, M. J. Ijzerman, J. Chae, G. J. Lankhorst, and G. Zilvold, "Relation  
268 between stimulation characteristics and clinical outcome in studies using  
269 electrical stimulation to improve motor control of the upper extremity in stroke.,"  
270 *J. Rehabil. Med.*, vol. 37, no. 2, pp. 65–74, 2005.

271 [10] B. W. Heller *et al.*, "Automated setup of functional electrical stimulation for drop  
272 foot using a novel 64 channel prototype stimulator and electrode array: results  
273 from a gait-lab based study.," *Med. Eng. Phys.*, vol. 35, no. 1, pp. 74–81, Jan.  
274 2013.

275