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Title: Liquid digestate recycled utilization in anaerobic digestion of pig manure: Effect on methane production, system stability and heavy metal mobilization

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Abstract: To improve bioenergy, methane, production in the anaerobic digestion plant application, the effects of recycled liquid digestate on anaerobic digestion of pig manure were investigated. Two continuous stirred tank reactors were operated for 230 days with varying organic loading rates (OLRs, from 1.5 to 6 g VS L⁻¹ d⁻¹); one reactor was implemented with liquid digestate recirculation and the other was set as the control without recirculation. It was demonstrated that the recirculation operation improved methane production and system fermentation stability, particularly for OLRs below 5 g VS L⁻¹ d⁻¹. The inhibition of methane production was found under an OLR of 6 VS L⁻¹ d⁻¹, which was caused by significantly increased viscosity from 30 to 1000 mPa·s and decreased mass transfer characteristics. The previously reported negative effects of accumulated ammonia and VFA on anaerobic digestion under digestate recirculation were not found in the present investigation of pig manure treatment. However, the heavy metals Pb, Mn, Cu and Zn accumulated in both liquid and solid fractions of the generated digestate in the digestate recycled reactor. The stable carbon isotope analysis of $\delta^{13}\text{C}\text{CO}_2$ and $\delta^{13}\text{C}\text{CH}_4$ produced the biogas may indicate different methanogenic pathways between the anaerobic reactors with and without digestate recirculation.

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Beijing, 13.03.2017

Dear Editor,

We hereby submit the enclosed manuscript entitled “Liquid digestate recycled utilization in anaerobic digestion of pig manure: Effect on methane production, system stability and heavy metal mobilization”, to be considered for publication in *Energy*.

To improve bioenergy, methane (biogas), production in the anaerobic digestion plant application, the effects of recycled liquid digestate on anaerobic digestion of pig manure were investigated. The operatized operation mode (digestate recirculation) of pig manure anaerobic digestion to improve the methane production and system stabilization were confirmed. However, the heavy metal accumulation and methanogenic pathways were shifted after the operation. The finding can further inspire the application. The paper help to develop the renewable energy production, optimize the energy processes, and mitigate the environmental pollutants. Thus, the paper perfectly fit the aims and scope of this journal.

We thank you for considering our manuscript and we hope it will be of your interest. All authors have seen this manuscript and approved to submit to your journal. This paper describes an original work and it is not being submitted to any other journal. The manuscript has been checked by English native speakers with expertise in the field.

Looking forward to hearing from you, I remain respectfully yours.

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Highlights

- Digestate recycling on AD can promote renewable energy production under low OLR
- Digestate recycling can improve the AD system stability under low OLR
- Increased viscosity decreased mass transfer and lowered renewable energy production
- Stable isotopic analysis of biogas indicated different methanogenic pathways
- Heavy metal accumulation under digestate recycling may influence land application

1 Liquid digestate recycled utilization in anaerobic digestion of pig
2 manure: Effect on methane production, system stability and heavy
3 metal mobilization

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12 **Abstract**

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14 the effects of recycled liquid digestate on anaerobic digestion of pig manure were
15 investigated. Two continuous stirred tank reactors were operated for 230 days with varying
16 organic loading rates (OLRs, from 1.5 to 6 g VS L⁻¹ d⁻¹); one reactor was implemented with
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21 significantly increased viscosity from 30 to 1000 mPa·s and decreased mass transfer
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23 on anaerobic digestion under digestate recirculation were not found in the present
24 investigation of pig manure treatment. However, the heavy metals Pb, Mn, Cu and Zn
25 accumulated in both liquid and solid fractions of the generated digestate in the digestate

1 recycled reactor. The stable carbon isotope analysis of $\delta^{13}\text{C}_{\text{CO}_2}$ and $\delta^{13}\text{C}_{\text{CH}_4}$ produced the
2 biogas may indicate different methanogenic pathways between the anaerobic reactors
3 with and without digestate recirculation.

4 **Keywords:** Biogas; Process stability; Recirculation; Swine manure; Stable isotope

5

6 **1. Introduction**

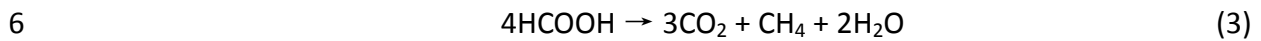
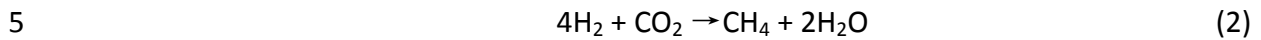
7 Anaerobic digestion (AD) has been recognized as a cost-effective biological
8 technology for bioenergy production using various bio-waste, such as livestock manure [1,
9 2]. The traditional crude oil consumption has reached 388 million t in 2009 in China, and
10 over 50% of that was imported, thus, Chinese government is heavily promoting the
11 renewable energy production plant to offset the energy needed [3-4]. The renewable
12 energy production has accounted around 10% of the China's primary energy consumption,
13 and the contribution is tremendously increasing in these years [3]. China, as one of the
14 leading pork production countries in the world, has built more than 90,000 AD plants with
15 a total treatment capacity of 14 million m^3 [4]. Thereafter, large amounts of anaerobic
16 digestate have been generated as by-products from AD plants along with the energy
17 production. The digestate is rich in nutrients and traditionally used as bio-fertilizer for
18 agriculture [2]. However, the quantity of digestate production often exceeds the
19 consumption ability of surrounding farmland, and digestate transport from the point of
20 surplus to distant farmlands is not economically feasible. More important, the anaerobic
21 digestate always still contain considerable amounts (25-30%) of methane potential under
22 short hydraulic retention time in AD plant [5]. Thus, in order to fulfil the throughout
23 energy recovery and methane production, the proper disposal method of AD plant
24 digestate is urgently required.

25 The recycled utilization of digestate has preliminarily been demonstrated as an
26 efficient method for recovering energy and reducing digestate discharge from some AD

1 plants [5-8]. The recycling operation could introduce the residual methane potential and
2 methanogenic bacteria back to the AD plant, which can theoretically significantly improve
3 the methane production of the applied AD plant. However, the concerns surrounding
4 recycling of digestate in AD plants are the accumulation of key chemical inhibitors to
5 methane production in AD plant, such as ammonia and volatile fatty acids (VFAs) [9, 10]. It
6 is commonly accepted that excessive ammonium accumulation can increase the
7 proportion of free ammonia, which is toxic for methanogenesis and results in lower
8 methane production. However, this process might also be highly dependent on feeding
9 materials. For example, Estevez et al., 2014 [7] observed a 16% increase in methane yield
10 with liquid digestate recycling of cow manure with *Salix*, whereas Wu et al., 2016 [8]
11 reported a decrease of 43% in methane production under liquid digestate recycling of
12 chicken manure due to ammonia accumulation. In addition, viscosity may also increase
13 with digestate recirculation and decrease methane production due to imperfect substrate
14 movement in AD plants. Until now, the implications of digestate recirculation have been
15 studied in AD of dairy manure [6], chicken manure [8] and co-digestion of cow manure
16 with *salix* [7] or grass silage [5]. To our knowledge, the renewable energy, methane,
17 production performance of pig manure anaerobic digestion under digestate recycling
18 operation has not been studied.

19 Besides the energy production efficiency, the deep understanding of methane
20 generation mechanisms change under the digestate recycled utilization would be
21 important to support the recycling application in AD plant. Molecular analysis methods,
22 such as next generation high-throughput sequencing, can accurately identify the dominant
23 methanogenic *Archaea* [11], but are insufficient for quantifying specific metabolic activity
24 [12]. Carbon isotope analysis has become an important tool for studying specific metabolic
25 activity from hydrogenotrophic and acetotrophic methanogens in AD plants [13, 14]. It is
26 well accepted that methane (CH_4) is primarily produced from acetate by acetotrophic
27 methanogens (Eq. 1) and from CO_2 and H_2 by hydrogenotrophic methanogens (Eq. 2) in AD

1 reactors. Additionally, formate may also play an important role as a substrate (Eq. 3) for
2 formatotrophic methanogens [15]. Notably, formate (Eq. 3) usually acts as a precursor for
3 hydrogenotrophic methanogens (Eq. 2) due to CO₂ production.



7 General criteria has demonstrated that methanogenesis by CO₂-reduction (Eq. 2) will lead
8 to strongly depleted $\delta^{13}\text{C}_{\text{CH}_4}$ values in comparison to methanogenesis by acetate cleavage
9 (Eq. 1). The fractionation factor of $\delta^{13}\text{C}_{\text{CO}_2}$ and $\delta^{13}\text{C}_{\text{CH}_4}$ ($a\text{C} = (\delta^{13}\text{C}_{\text{CO}_2} + 10^3) / (\delta^{13}\text{C}_{\text{CH}_4} + 10^3)$)
10 is another possible indicator to approximately identify dominant methanogenic pathways.
11 Published literature suggests that lower aC values indicate that acetotrophic methanogens
12 would be the more dominant pathway of methane production in AD reactors [16]. The
13 inorganic and organic compounds, as well as bacterial biomass, will refill AD plants after
14 digestate recycling operations, which might change the methanogenic pathways [17].
15 Nevertheless, the impacts of digestate recirculation on methane production mechanisms
16 in AD reactors have never been investigated.

17 Another knowledge gap hypothesis is the dynamics of heavy metals in digestate
18 from AD plants might also influence the operation of digestate recirculation; heavy metal
19 concentration will regulate the digestate application by agriculture. Thus, to achieve the
20 full success application of this optimized digestate recycled AD plant, the accumulation
21 and mobilization of heavy metals in digestate effluent under liquid digestate recirculation
22 need to be monitored.

23 The aims of the study presented here were to assess the liquid digestate
24 recirculation operation on the energy production performance and mechanisms of pig
25 manure anaerobic digestion. For this purpose, laboratory-scale CSTRs for treating pig
26 manure at variable OLRs (increased from 1.5 to 6 g VS L⁻¹ d⁻¹) were implemented under

1 mesophilic conditions. The influences of AD reactor digestate recirculation on methane
2 production, and the characteristics of the digested substrate, were investigated to evaluate
3 methane production and system stability. Additionally, to assess the risk potential for
4 agricultural utilization of the final digestate effluent, the dynamics of heavy metals
5 accumulation and mobilization were determined in both the liquid and solid fractions.
6 Moreover, to understand the impact of recirculation on predominantly methanogenic
7 pathways, the composition of $\delta^{13}\text{C}_{\text{CO}_2}$ and $\delta^{13}\text{C}_{\text{CH}_4}$ associated with the molecular analysis
8 method were monitored.

9 **2. Material and methods**

10 **2.1 Materials and inoculums**

11 The pig manure used in this study was collected from a larger-scale pig farm
12 located in Beijing, China. The raw pig manure was naturally dried, followed by
13 pulverization treatment. Then, the homogenized samples were frozen at $-20\text{ }^\circ\text{C}$ to prevent
14 biological decomposition. The frozen substrates were thawed in a refrigerator at $4\text{ }^\circ\text{C}$ for 1
15 day prior to introduction to the reactor. The sludge inoculum was collected from a biogas
16 plant (located in Shun Yi district, Beijing, China) with mesophilic pig manure AD by CSTRs.
17 The characteristics of the pig manure and inoculum sludge are summarized in Table 1.

18 **2.2 Experiment set-up and operation**

19 Two laboratory-scale CSTRs were implemented in two identical glass cylinders with
20 a total volume of 15 L and effective volume of 10 L. The feeding and discharge ports were
21 set at the top and bottom of the reactors, respectively. The gas outlet was at the top and
22 connected with a plastic gasbag. Both CSTRs were intermittently stirred at 120 r/min for 1
23 h on and 1 h off. The whole experiment lasted 230 days, and the experiment was
24 maintained at $37 \pm 1\text{ }^\circ\text{C}$ in a temperature-controlled chamber. Once a day, approximately
25 660 mL of digestate was drawn out through the outlet port at the bottom of the CSTRs,
26 and the same amount of raw material was fed in via the feeding port. The hydraulic

1 retention time (HRT) of both CSTRs was maintained at around 15 days through the entire
2 experiment. To investigate the effect of various OLRs and recirculation on the performance
3 of the CSTR reactors, the experiment was divided into two phases with eight OLR levels
4 (Fig. 1). The initial OLR was $1.5 \text{ g VS L}^{-1} \text{ d}^{-1}$ during the start-up experimental period. Then,
5 the OLR gradually increased until reaching $6 \text{ g VS L}^{-1} \text{ d}^{-1}$. In phase I, both CSTR reactors (R1
6 and R2) were established without recirculation until day 57 under an OLR of $2.5 \text{ g VS L}^{-1} \text{ d}^{-1}$.
7 In phase II, R2 was set to 60% effluent liquid digestate recirculation from day 58 to the end
8 (day 230) while R1 was un-recirculated as the control.

9 **2.3 Sampling and analysis**

10 The pH was determined using a digital pH meter (FE20, Mettler-Toledo,
11 Switzerland). The methane production volume was measured with a wet-type precision
12 gas meter (LML-1, Changchun, China). Moreover, CH_4 and CO_2 contents were analysed
13 using a biogas analyser (Eheim Visit 03, Messtechnik Eheim, Germany). Total solids (TS),
14 volatile solids (VS) and total ammonia nitrogen (TAN) of all samples were determined using
15 standard methods [18]. Total inorganic carbon (TIC) and volatile fatty acids (VFAs) were
16 analysed by titration with $0.1 \text{ NH}_2\text{SO}_4$ to endpoints of pH 5.0 and 4.4, following the
17 procedure of Zhang et al., 2014 [19]. The sludge viscosity was determined using a
18 rotational viscometer (NDJ-1, Shanghai China) at a shear rate of 60 min^{-1} as described by
19 Chang et al., 2007 [20]. Cellulose and hemicellulose were determined using the sequential
20 analysis method developed by Soest et al., 1985 [21]. All the above parameters were
21 collected from each sample every 1-2 days for routine analyses in the present study.

22 Additionally, the concentrations of heavy metal elements, including lead (Pb),
23 manganese (Mn), copper (Cu) and zinc (Zn), in both liquid and solid fraction of the effluent
24 were determined using inductively coupled plasma mass spectrometry (ICP-MS, Elan 9000,
25 Perkin Elmer, USA) approximately every 2 days from day 100 to 230 in the experiment. The
26 stable isotopic enrichments of CH_4 and CO_2 were carried out as described by Nikolausz et
27 al., 2013 [13]. Briefly, an isotope ratio mass spectrometry system (Finnigan MAT 253,

1 Thermofinnigan, Bremen, Germany) was coupled to a gas chromatograph (HP 6890 Series,
2 Agilent Technology, USA) via a combustion device for carbon analysis. The isotope analyses
3 were conducted on day 47 and 118 with six replicates of each measurement to represent
4 the performance in phases I and II, respectively.

5 **2.4 Microbial community analysis**

6 In order to investigate the microbial difference between reactors, 16S rDNA
7 characterization was carried out to analyse the microbial communities at the end of the
8 experiment. A sample (20 g) of substrate from each CSTRs (R1 and R2) were used to
9 extract microbial DNA using the FastDNA[®] SPIN Kit (MP Biomedicals, Santa Ana, CA)
10 according to the manufacturer's instructions. The extracted soil DNA was first detected by
11 agarose gel electrophoresis (1.0% agarose in 0.5× TAE) to examine its integrity and
12 approximate concentration. Then, the quality and quantity of DNA samples were
13 determined using a NanoPhotometer[®] Spectrophotometer (IMPLEN, Carlsbad, California,
14 USA) and a Qubit[®] RNA Assay Kit in a Qubit[®] 2.0 Fluorometer (Life Technologies, Carlsbad,
15 California, USA). The 16S rDNA gene amplification was carried out according to Kozich et
16 al., 2013 [22]. Briefly, the extracted DNA was amplified with a universal primer set
17 (314F/805R) targeting the V3+V4 hypervariable region. The detailed PCR conditions were
18 adopted as described by Kozich et al., 2013 [22]. The amplicons were purified using a
19 Wizard[®]SV Gel and PCR Clean-up System (Promega, Madison, Wisconsin, USA) after gel
20 extraction. The purified 16S rDNA amplicons were sequenced using the Illumina Miseq
21 platform (Illumina Inc., San Diego, CA) at Anoroad Bio. Tech. Inc. (Beijing, China). After
22 trimming the low quality sequences, residual sequences were aligned using MOTHUR. The
23 aligned sequences were checked for chimera using USEARCH 6.1 in QIIME and classified
24 into Operational taxonomic units (OTUs) within a 0.03 difference (97% similarity) using the
25 de novo OTU picking workflow in QIIME.

26 **2.5 Statistical analysis**

27 Differences between parameters from R1 (control) and R2 (recirculated reactor)

1 were evaluated using the repeat measured student T test at 95% confidence level ($p < 0.5$)
2 of significant differences. Principal Component Analysis (PCA) was used to identify
3 different treatment performance patterns between R1 and R2 under each experimental
4 phase with different OLRs. PCA was conducted using all measured parameters, which
5 includes pH, methane production, VFA, TIC, TAN, viscosity, TS, VS, hemicellulose and
6 cellulose. For PCA analysis, data was standardized (to a Z score with a mean = 0 and S.D. =
7 1) to ensure that each variable had the same influence in the analysis. Sigmaplot software
8 (version 12.5, Sigma, Inc.) and XLStat Pro® (XLStat, Paris, France) were used for plotting
9 and data analyses, respectively.

10 **3. Results**

11 **3.1 Methane production**

12 The methane production of the two CSTR reactors (R1 and R2) was compared as
13 time progresses in the experiment (Fig. 2). Operation conditions were the same for R1 and
14 R2 during phase I, and methane production performance were also similar between the
15 two reactors ($P > 0.05$). Both daily (Fig. 2a) and volumetric methane production (Fig. 2b)
16 increased along as OLRs increased with value ranges from approximately $2\text{-}5 \text{ L d}^{-1}$ and 0.5-
17 $0.9 \text{ m}^{-3} \text{ m}^{-3} \text{ d}^{-1}$, respectively. Subsequently, in phase II, R2 changed to the liquid digestate
18 recirculation mode and R1 was maintained in the un-recirculated mode. Methane
19 production (both daily and volumetric) increased in R2 compared to R1 until the OLRs
20 increased to $5 \text{ g VS L}^{-1} \text{ d}^{-1}$. The average daily and volumetric methane production reached
21 11 L d^{-1} and $2.0 \text{ m}^{-3} \text{ m}^{-3} \text{ d}^{-1}$ for R1 and 13 L d^{-1} and $2.2 \text{ m}^{-3} \text{ m}^{-3} \text{ d}^{-1}$ for R2, respectively. When
22 the OLR increased to $6 \text{ g VS L}^{-1} \text{ d}^{-1}$, the methane production fluctuated strongly in R2.
23 Average values decreased to around 11 L d^{-1} and $2 \text{ m}^{-3} \text{ m}^{-3} \text{ d}^{-1}$ for daily and volumetric
24 methane production, respectively, which were even lower than that of R1. Additionally,
25 regarding methane and CO_2 content, no obvious difference was found between two
26 reactors ($P > 0.05$). The average methane content of R1 and R2 was around 61.2%, and the
27 corresponding average CO_2 content was about 36.9% throughout the entire experiment

1 (Fig. 2a).

2 **3.2 Anaerobic digestate characteristics**

3 **3.2.1 Dynamics of pH, TAN, VFA and TIC**

4 The pH, TAN, VFA and TIC were similar between the two reactors in phase I, with
5 average values of 7.1, 600 mg L⁻¹, 350 mg L⁻¹ and 3800 mg L⁻¹, respectively (Fig. 3). However,
6 all these parameters increased tremendously in R2 after liquid digestate recirculation and
7 reached 7.5, 1600 mg L⁻¹, 1200 mg L⁻¹ and 1000 mg L⁻¹ for pH, TAN, VFA and TIC,
8 respectively. Notably, pH in R2 stabilized at 7.5 after OLR reached 4 g VS L⁻¹ d⁻¹. TAN
9 concentration in R2 decreased to around 600 mg L⁻¹ when the OLR reached 6 g VS L⁻¹ d⁻¹.
10 Nevertheless, these values were significantly higher in R2 as compared to R1, which only
11 showed a slight improvement with increasing OLRs. At the end of this experiment under
12 an OLR of 6 g VS L⁻¹ d⁻¹, the pH, TAN, VFA and TIC in R1 achieved 7.2, 600 mg L⁻¹, 600 mg L⁻¹
13 and 5800 mg L⁻¹, respectively.

14 **3.2.2 Dynamics of viscosity, cellulose and hemicellulose, VS and TS**

15 The viscosity, cellulose and hemicellulose, VS and TS were also similar between the
16 two reactors in phase I (Fig. 4). However, it is clear that the R2 viscosity increased
17 exponentially up to around 1000 mPa·s, while it still kept below to 30 mPa·s in R1 as the
18 OLRs increased from 2.5 to 6 g VS L⁻¹ d⁻¹ in phase II (Fig. 4a). The average cellulose and
19 hemicellulose contents in the R1 and R2 digestate reached up to 4.1% and 9.8%,
20 respectively (Fig. 4b). The average VS (Fig. 4c) and TS (Fig. 4d) contents achieved 6.7 % and
21 4.2 % for R1, 9.9% and 15% for R2, respectively, at the end of the experiment.

22 **3.3 Performance patterns of the two CSTR reactors**

23 Methane production (MP), as well as the substrate characteristics, including pH,
24 VFA, TIC, TAN, viscosity, TS, VS, hemicellulose and cellulose (H&C) of both CSTR reactors
25 throughout the experiment were analysed using principal component analysis (PCA) to
26 assess the performance patterns (Fig. 5). Independent PCA analyses were completed

1 separately for experimental phases I (Fig. 5a) and II (Fig. 5b). The first two principal
2 components accounted for a variation of 64.9% and 79.0% for phases I and II, respectively.
3 In phase I, the R1 and R2 patterns generally overlapped and did not show clear group
4 differences under each OLR (Fig. 5a), suggesting the two systems had good parallelism.
5 However, in phase II clear group differences between R1 and R2 were found (Fig. 5b). Both
6 R1 and R2 showed the same tendency and indicated an up-right direction as the OLRs
7 increased. Moreover, the methane production also showed a direct loading effect.
8 However, R1 moved close to and was concentrated in the positive direction of PC2 and R2
9 moved close to and was concentrated in the positive direction of PC1 along as OLR
10 increased. The values of pH, TAN, TIC, VFA, viscosity, TS and VS showed high positive
11 loadings on the PC1 axis, which indicates a positive correlation with R2 with increasing
12 OLRs (Fig. 5d).

13 **3.4 Heavy metal mobilization**

14 The heavy metals, including Pb, Mn, Cu and Zn, were analysed in both the solid and
15 liquid fractions of the anaerobic digestate effluent for both R1 and R2 in experimental
16 phase II (Fig. 6). All of these heavy metals were generally more than 10 times higher in the
17 solid than liquid fraction for both R1 and R2. Moreover, the contents of Pb, Mn, Cu and Zn
18 in the solid fraction digestate of R2 were significantly higher than R1, and reached
19 approximately 0.7, 90, 120 and 300 mg L⁻¹, respectively. However, the heavy metals in the
20 liquid fraction were only slightly higher (not significant) in R2 as compared with R1. The
21 concentrations of Pb, Mn, Cu and Zn were maintained below approximately 0.08, 4, 8 and
22 9 mg L⁻¹, respectively, for both R1 and R2.

23 **3.5 Microbial community**

24 The microbial community diversity in R1 and R2 were analysed and compared using
25 16S rDNA Pyrosequencing. After quality trimming, 15,998 and 16,134 valid
26 Pyrosequencing reads of the 16S rDNA gene were obtained for R1 and R2, respectively
27 (Table S1). Rarefaction curves, based on the OTUs at 3% dissimilarity (Fig. S1), indicated

1 that the sequences were sufficient to reflect the diversity of the microbial communities.
2 The microbial diversity (Shannon and Simpson index) was similar in R1 and R2 (Table S2).
3 The microbial communities of both reactors showed high diversity at the levels from
4 phylum, class (Fig. S2) to genus (Fig. 7). *Bacteroidetes* and *Firmicutes* were the two
5 dominant phyla; *Bacterioidia* and *Clostridia* were the two dominant classes in both CSTR
6 reactors (Fig. S2).

7 As shown in Fig. 7, at a genus level, the dominant genus in R1 was *Clostridium* (accounting
8 for 43.3%) which belongs to the phyla *Firmicutes*. Moreover, *SMB53* (16.2%) and *YRC22*
9 (12.2%) were next most dominant genus types in R1. However, the genus *Candidatus*
10 *Cloacamonas* and *Syntrophus* were the dominant bacterial communities in R2, accounting
11 for 36.2% and 22.4%, respectively. The corresponding values were significantly lower in R1,
12 accounting for 7.1% and 2.1%, respectively.

13 **3.6 $\delta^{13}\text{C}_{\text{CH}_4}$ and $\delta^{13}\text{C}_{\text{CO}_2}$ compositions**

14 The isotopic compositions of ^{13}C in CO_2 and CH_4 were analysed and the
15 fractionation factor of aC was calculated for biogas production in phases I and II (Table 2).
16 In phase I, the average values of $\delta^{13}\text{C}_{\text{CO}_2}$ and $\delta^{13}\text{C}_{\text{CH}_4}$ for both R1 and R2 were similar and
17 maintained approximately 6‰ and -44‰, respectively. As the OLRs increased from phase I
18 to phase II, the averaged of $\delta^{13}\text{C}_{\text{CO}_2}$ and $\delta^{13}\text{C}_{\text{CH}_4}$ in R1 changed to 5.03‰ and -42.20‰,
19 respectively. For R2 in phase II, the averaged of $\delta^{13}\text{C}_{\text{CO}_2}$ and $\delta^{13}\text{C}_{\text{CH}_4}$ in R1 changed to 6.40‰
20 and -48.21‰, respectively. The average fractionation factors of $\delta^{13}\text{C}_{\text{CO}_2}$ and $\delta^{13}\text{C}_{\text{CH}_4}$ for R1
21 were 1.052 and 1.049 in phase I and II, respectively. However, the values for R2 were 1.052
22 and 1.057 in phase I and II, respectively.

23 **4. Discussion**

24 The main objective of this study was to provide the first comprehensive assessment
25 of the performance anaerobic digestion of pig manure with liquid digested recirculation. In
26 the present study, all parameters for both R1 and R2 were similar in experimental phase I.

1 The results demonstrated that the two AD reactors performed well as parallel, thus, the
2 two reactors were comparable in phase II when R2 was modified to digestate recirculation
3 mode. An increased pH was observed in both R1 and R2, which was attributed to the
4 increasing OLRs applied to system [23]. The pH value is a pivotal factor that may affect
5 methane production efficiency. However, the pH in both R1 and R2 was in the range of 6.5-
6 7.5 until the end of the experiment, which was still suitable for active methane-forming
7 microorganisms [24].

8 When the OLR was below $5 \text{ g VS L}^{-1} \text{ d}^{-1}$, higher methane production was clearly
9 found in R2 as compared with R1 (Fig. 2a). The results indicate that recirculation promoted
10 AD system efficiency under relative low OLRs. It was also demonstrated by the previous
11 study from Estevez et al., 2014 [7], methane yields increased 16% compared to the control
12 in co-digestion of cow manure and Salix under an OLR of $2.6 \text{ g VS L}^{-1} \text{ d}^{-1}$. The methane was
13 generated from the degradation of biodegradable organic substances in the AD reactor
14 and the methane production can be used to indicate AD system efficiency. The explanation
15 for the increased methane production may be an incomplete degradation of organic
16 substances and biofilm reintroduced to the reactor during recycling [7, 17].

17 The inhibition of methane production due to ammonia and VFA accumulation was
18 not found, which may due to the pig manure material used for AD in the present study. It
19 has been shown that ammonia accumulation can introduce negative effects on methane
20 production in plant AD [9]. A rise in TAN level with initiation of digestate recirculation has
21 been observed in investigations of mesophilic AD of silages using stirred tank reactors [17],
22 and hyper-thermophilic-mesophilic AD of waste activated sludge in two-stage systems [25].
23 TAN concentration accumulation is also heavily aggravated with digestate recirculation
24 operation in AD of chicken manure [8]. In the present study, the TAN level in AD effluent
25 increased with the initiation of digestate recirculation. However, the levels were still far
26 below an inhibitory concentration, suggested as above 3000 mg/L, and showed no signs of
27 inhibiting the system throughout the experiment. An inhibition due to accumulated VFA in

1 an AD reactor with recirculation was found in a previous study [10]. However the
2 accumulated VFA in this study was also lower than the limit concentration, suggested as
3 2000 mg HAC/L [26], which provided AD stability in the present study.

4 Additionally, the potential for improved system stability has been found in pig
5 manure AD under recirculation operations. AD system stability can be enhanced by
6 incremental alkalinity (TIC) concentration as well as lower VFA/TIC ratios, which are the
7 most important contributors to buffering capacity in the AD process [24]. In this study, the
8 R2 VFA/TIC ratios maintained 0.11 ± 0.03 , which indicates a strong buffering capacity
9 during digestate recirculation. The improvement of system buffering capacity and pig
10 material properties can be explained by the recycling digestate.

11 Methane production in R2 under digestion recirculation showed strong fluctuations
12 and the average value was lower than R1 under the highest OLR of $6 \text{ g VS L}^{-1} \text{ d}^{-1}$. Because
13 the TAN and VFA concentrations were clearly below inhibitory concentrations, the
14 hypothesis for methane production inhibition is high viscosity. The TS, VS, cellulose and
15 hemicellulose contents contributed to high viscosity in the AD reactor [27]. The continually
16 increasing content of such factors were especially apparent in R2 under recirculation. The
17 viscosity increase during the AD processes causes a foaming problem by decreasing the
18 mass transfer ability [28]. The digested recirculation might accelerate the accumulation
19 process, because part of the recalcitrant compounds remained in the discharged digestate
20 was recycled and thus accumulated in the recirculating reactors [7]. Therefore, it is crucial
21 to decrease the TS, VS, cellulose and hemicellulose contents and maintain an appropriate
22 viscosity level in the AD reactor for methane production.

23 The accumulation of heavy metals in agriculture soil due to long-term land
24 application of digestate is a cause for concern because of potential environmental risks.
25 The contents of Pb, Mn, Cu and Zn were 10 times higher in the solid fraction digestate
26 than the liquid fraction digestate in this study, similar to values reported by Zhang et al.,
27 2011 [29]. In addition, the Pb, Mn, Cu and Zn contents in both the solid and liquid fraction

1 digestate of R2 was higher than R1, showing that heavy metal accumulation was promoted
2 by the digestate recirculation in the AD reactor. The results indicate that the effluent
3 coming from a recirculating system may post a threat to the environment due to the high
4 content of heavy metals. Consequently, to protect the soil environment, it is advisable to
5 test for heavy metals prior to applying digestate effluent from a recirculating anaerobic
6 digestion system to arable land.

7 The difference of the microbial community structure and relative abundances
8 between the two reactors (Fig. 7) can be explained by a difference in feeding stratagem. It
9 was previously reported that digestate recycling can heavily influence bacterial
10 communities [30]. As a dominant genus in the recirculated AD reactor for R2, *Candidatus*
11 *Cloacamonas* is a hydrogen-producing syntrophic bacterium, which is widely present in
12 many anaerobic digesters and constitutes the most dominant taxon at the genus level in
13 AD reactors [31]. As a member of WWE1, *Candidatus Cloacamonas* can utilize several
14 sugars and amino acids and might be involved in cellulose hydrolysis and utilization of
15 fermentation products [32]. *Syntrophus* is an anaerobic bacterium that degrades VFAs and
16 benzoate in *syntrophic* association with hydrogen-using microorganisms [33]. Thus, it
17 shows the more abundant hydrolytic bacteria were existed in R2, operating in digestate
18 recirculation mode. However, the dominant genus in R1 was *Clostridium*, which belongs to
19 the phyla *Firmicutes*, capable of fermenting cellulose and various carbohydrates to acetate,
20 butyrate and hydrogen [34].

21 The isotope fractionation can be used as an indicator for identifying the
22 predominant methanogenic pathway in anaerobic digesters, which can strongly support
23 molecular analysis [12]. The different $\delta^{13}\text{C}_{\text{CO}_2}$ (‰) and $\delta^{13}\text{C}_{\text{CH}_4}$ (‰) fraction ratios (aC)
24 detected in the present study may have resulted from different predominant
25 methanogenic pathways in R1 and R2 under different experimental phases. Laukenmann
26 et al., 2010 [15] found that methane preferentially hydrogenotrophic methanogens by CO_2
27 reduction (Eq. 2) with a lower $\delta^{13}\text{C}_{\text{CH}_4}$ (‰) value at higher concentrations of TAN and VFA in

1 AD plant. This effect may be the reason that $\delta^{13}\text{C}_{\text{CH}_4}$ (‰) in R2 significantly decreased from
2 phase I to II under higher OLRs, which corresponded to higher TAN and VFA concentrations
3 compare with R1. However, $\delta^{13}\text{C}_{\text{CH}_4}$ (‰) in R1 were not significantly different between
4 phase I and II, which may due to the relative stable TAN and VFA concentrations (Fig. 3).
5 The result indicated that hydrogenotrophic may be more dominant in R2 for
6 methanogenesis compare with R1. The decrease in aC values in R1 indicated that
7 acetotrophic methanogens were a more important methanogenesis process in phase II
8 compared with phase I for the control AD reactor, without recirculation. The previous
9 finding supports this hypothesis that at the beginning of incubation, methane was
10 preferentially produced by CO_2 reduction (Eq. 2). Later, methane production by acetate
11 cleavage (Eq. 1) might play a dominant role [35]. However, the aC value in R2 showed
12 contrasting behaviour compared with R1, which increased from phase I to phase II. This
13 result again demonstrated that hydrogenotrophic methanogenesis was the more
14 dominant pathway in R2. Overall, stable isotope analysis results clearly showed an
15 influence of digestate recirculation on methanogenesis pathways in pig manure AD.
16 Nevertheless, continuous monitoring of changing $\delta^{13}\text{C}_{\text{CO}_2}$ (‰) and $\delta^{13}\text{C}_{\text{CH}_4}$ (‰) by stable
17 isotope analysis should be further implemented to evaluate the long-term performance of
18 AD reactors.

19 **5. Conclusions**

- 20 ■ The effects of recycled liquid digestate utilization in mesophilic anaerobic digestion of
21 pig manure were investigated in the present study. It was demonstrated that
22 recirculation operation improved methane production and system fermentation
23 stability for OLRs below $5 \text{ g VS L}^{-1} \text{ d}^{-1}$.
- 24 ■ Long-term recycling of liquid digestate significantly increased viscosity from 30 to
25 1000 mPa·s, which decreased mass transfer characteristics in AD reactors and further
26 decreased methane production, particularly for an OLR of $6 \text{ g VS L}^{-1} \text{ d}^{-1}$. The negative
27 effects of accumulated ammonia and VFA on AD treatment of pig manure under

1 digestate recycling were not found in the present study.

- 2 ■ The liquid digestate recycling intensified the accumulation of heavy metals, including
- 3 Pb, Mn, Cu and Zn, in both the liquid and solid fractions of the digested effluent,
- 4 which may impact future application to farmland.
- 5 ■ Stable carbon isotopic analysis of the biogas produced demonstrated different
- 6 methanogenic pathways between anaerobic reactors with and without liquid
- 7 digestate recirculation.

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Figure 1

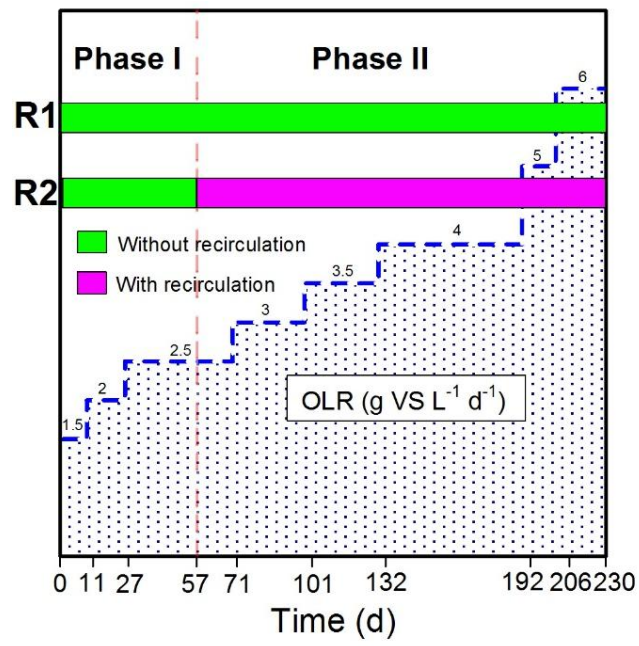


Fig. 1. The operating conditions of the two CSTRs (R1 and R2) for the entire experimental period.

Figure 2

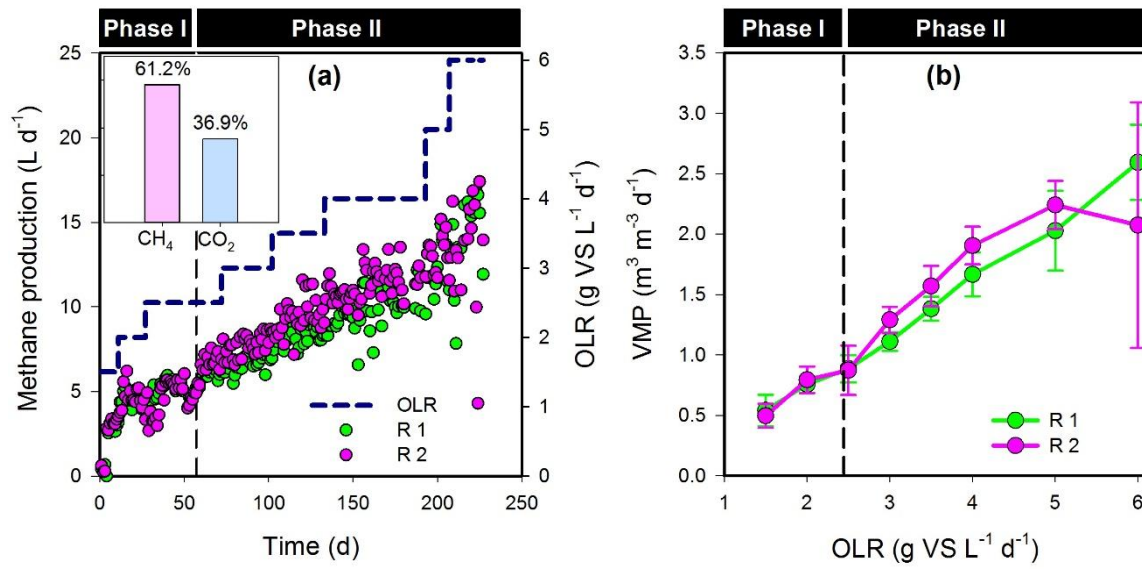


Fig. 2 Dynamics of methane production for the two CSTR reactors (R1 and R2) throughout the experimental phases (a) and the relationship between volumetric methane production (VMP) and organic loading rates (OLRs) (b).

Figure 3

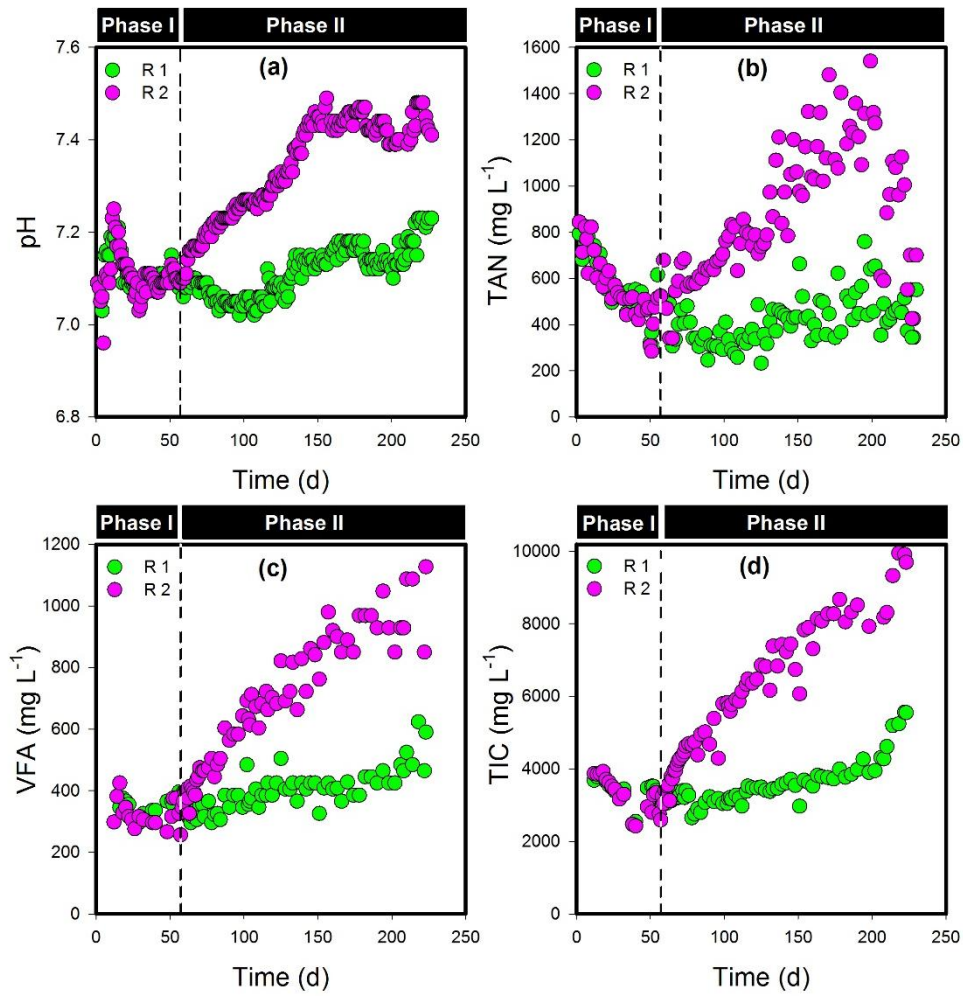


Fig. 3 Dynamics of pH and TAN, VFA and TIC values from the two experimental reactors without (R1) and with (R2) recirculation throughout the experiment.

Figure 4

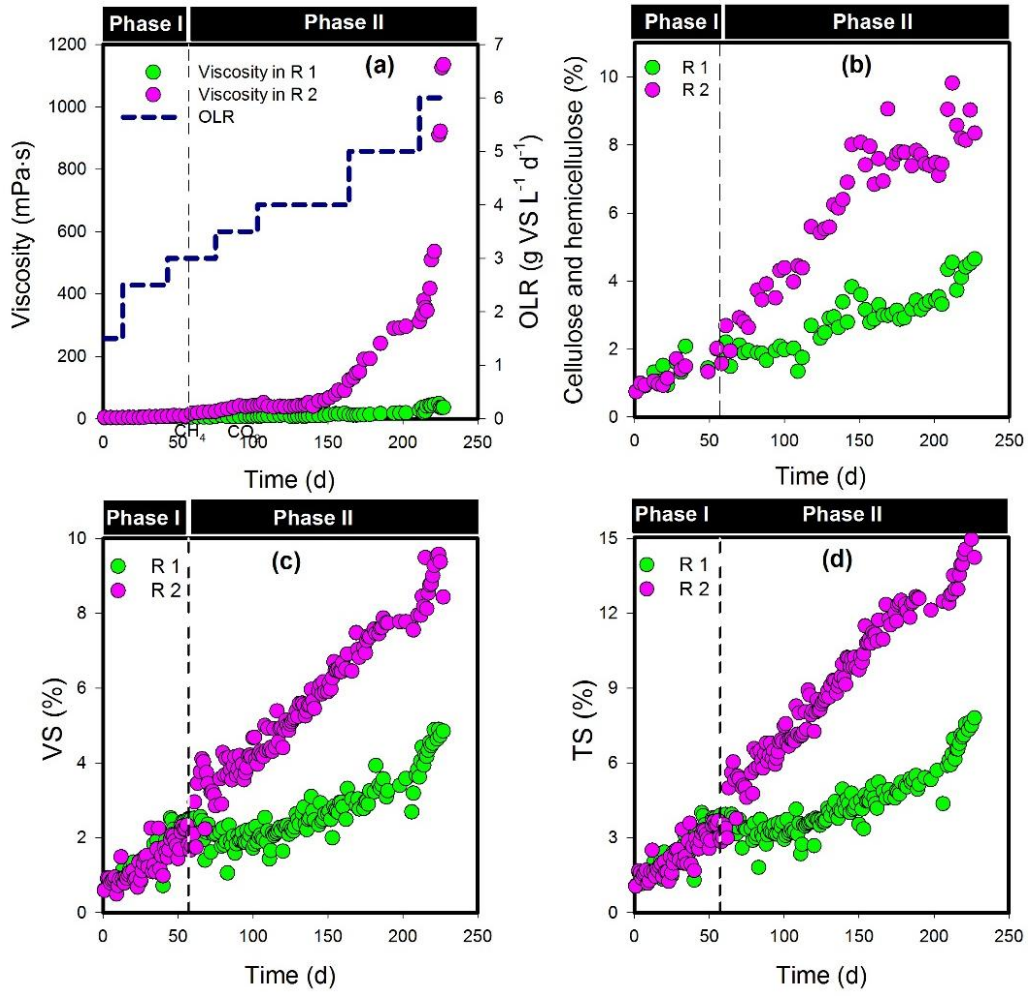


Fig. 4 Dynamics of viscosity, and cellulose and hemicellulose, VS and TS for the two CSTR reactors without (R1) and with (R2) recirculation throughout the experiment.

Figure 5

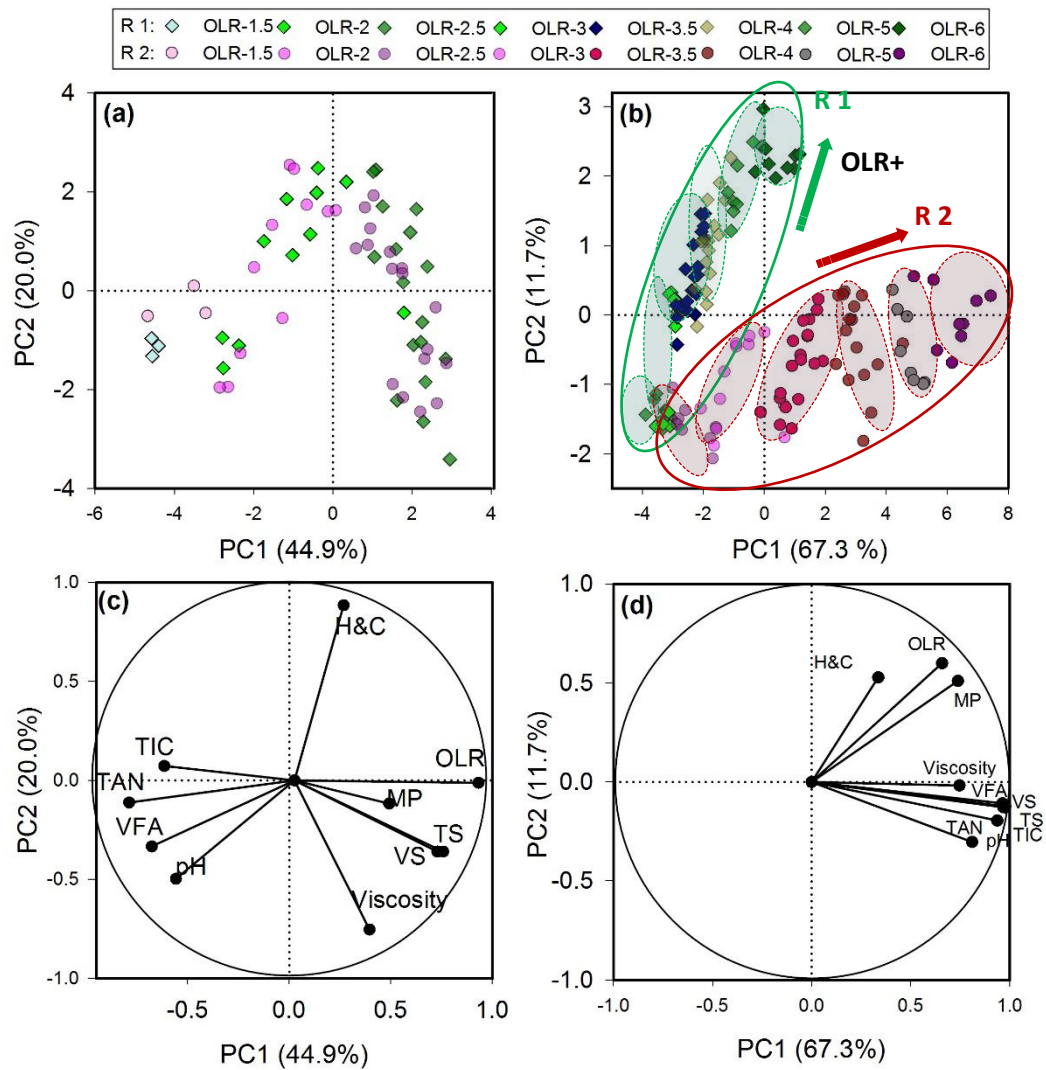


Fig. 5 Principal component analysis of results from the two CSTR reactors without (R1) and with (R2) recirculation in experimental phases I (a) and II (b). Plots (c) and (d) represent the factor loading plots for each principal component analysis in experimental phases I and II, respectively.

Figure 6

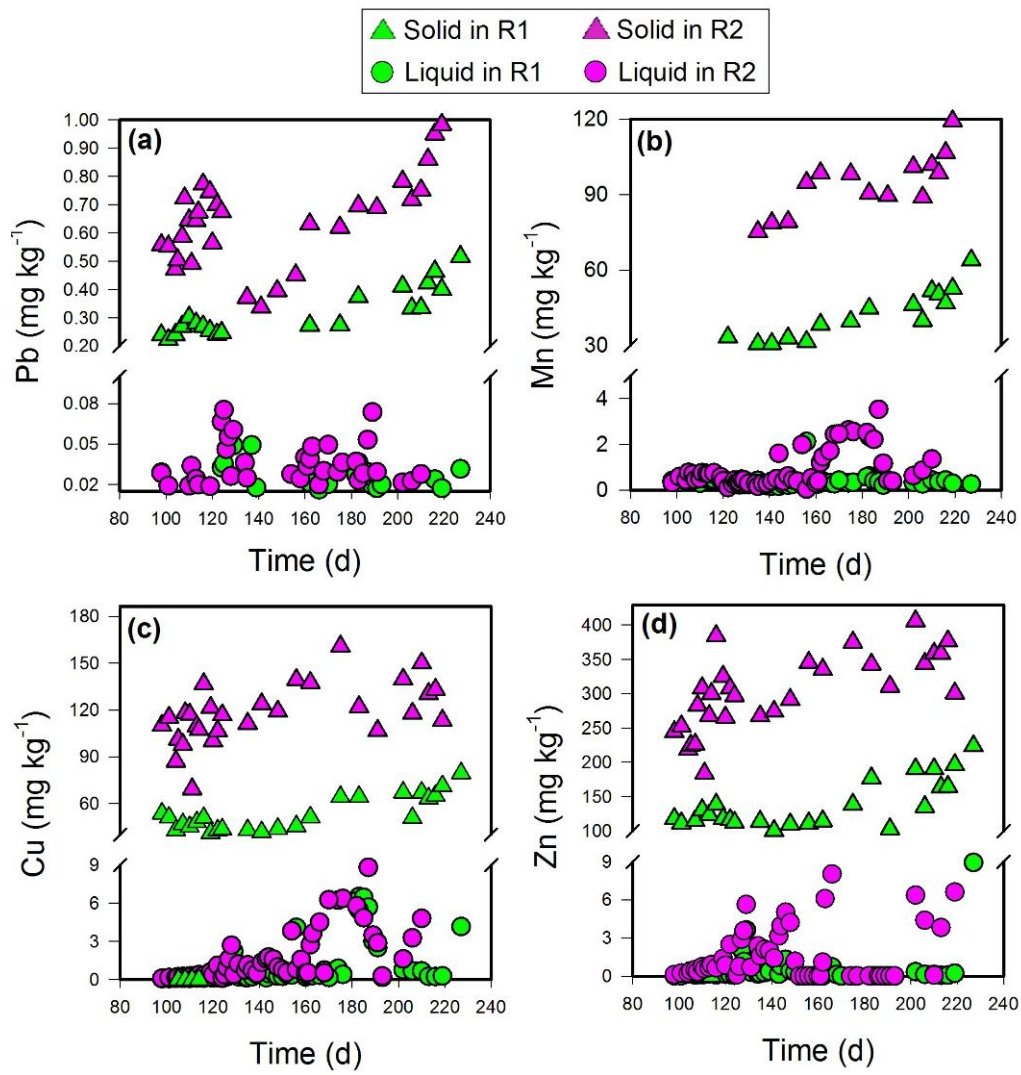


Fig. 6 Dynamics of heavy metal concentrations (Pb, Mn, Cu and Zn) from the two CSTR reactors without (R1) and with (R2) recirculation in experimental phase II.

Figure 7

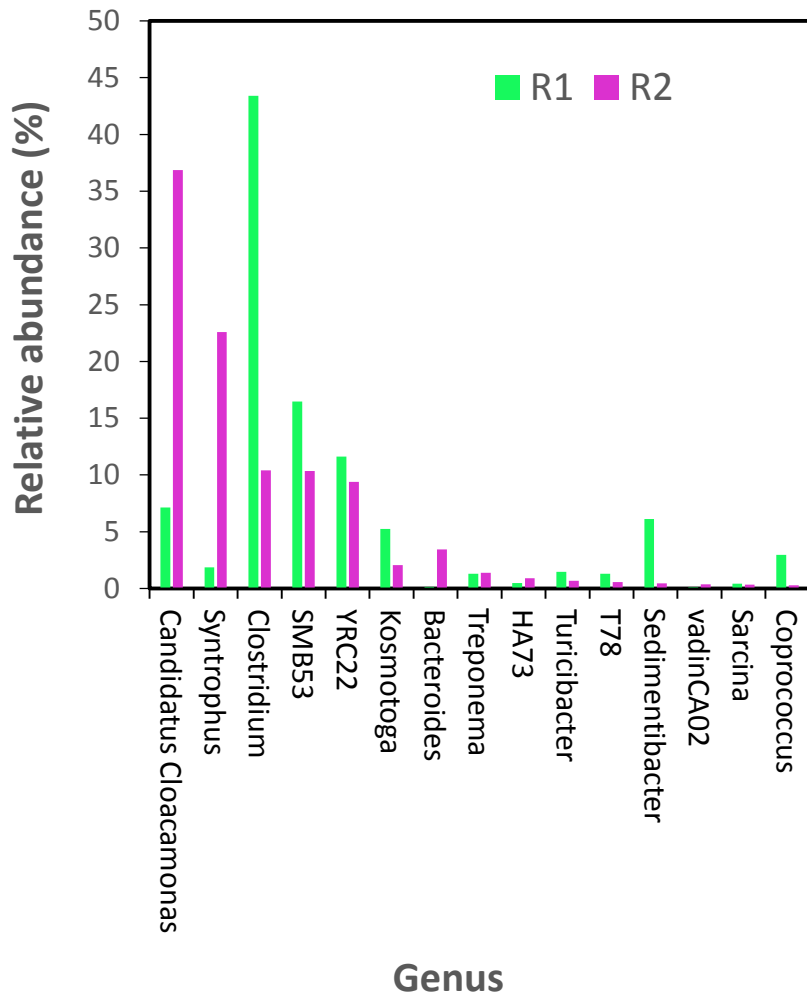


Fig. 7 Taxonomic classification of bacterial 16S rDNA gene reads of the substrate sample from the two CSTR reactors with (R2) and without recirculation (R1) at the genus level (the relative abundances of bacterial 16S rDNA gene reads less than 0.1% are not shown).

Table 1

Characteristics of pig manure and sludge inoculum.

Materials	TS (%)	VS (% TS)	C (% TS)	N (% TS)	H (% TS)	S (% TS)
Pig manure	89.70	68.46	34.38	2.27	5.47	0.58
Sludge inoculum	4.11	54.01	ND	ND	ND	ND

Values are expressed as mean. ND = Not determined.

Table 2

The compositions of $\delta^{13}\text{C}_{\text{CO}_2}$ and $\delta^{13}\text{C}_{\text{CH}_4}$ in the biogas of the two CSTR reactors without (R1) and with (R2) recirculation in experimental phase I (47 d) and II (118 d).

	$\delta^{13}\text{C}_{\text{CO}_2}$ (‰)		$\delta^{13}\text{C}_{\text{CH}_4}$ (‰)		aC	
	Phase I	Phase II	Phase I	Phase II	Phase I	Phase II
R1	5.94 ± 0.45^a	$4.45 \pm 0.24^{b*}$	-44.23 ± 0.91^a	$-44.20 \pm 0.63^{b*}$	1.052 ± 0.005	$1.050 \pm 0.004^*$
R2	6.05 ± 0.16	6.00 ± 0.24	-43.90 ± 0.87	-48.21 ± 0.40	1.052 ± 0.003	1.057 ± 0.002

Different letters beside the values from different experiment phases for the same reactor and gas represent significantly different; *beside the values represent significantly different values between different reactors for the same experimental phase and gas.

Supplementary Materials

Liquid digestate recycled utilization in anaerobic digestion of pig manure: Effect on methane production, system stability and heavy metal mobilization

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Table S1

The number of observed valid pyrosequencing reads, OTUs, Shannon-wiener diversity index (Shannon) and Simpson diversity index (Simpson) of the sludge samples from R1 and R2.

Sample	Valid pyrosequencing reads	OTUs	Shannon	Simpson
R1	15,998	840	4.6	0.92
R2	16,134	892	4.1	0.89

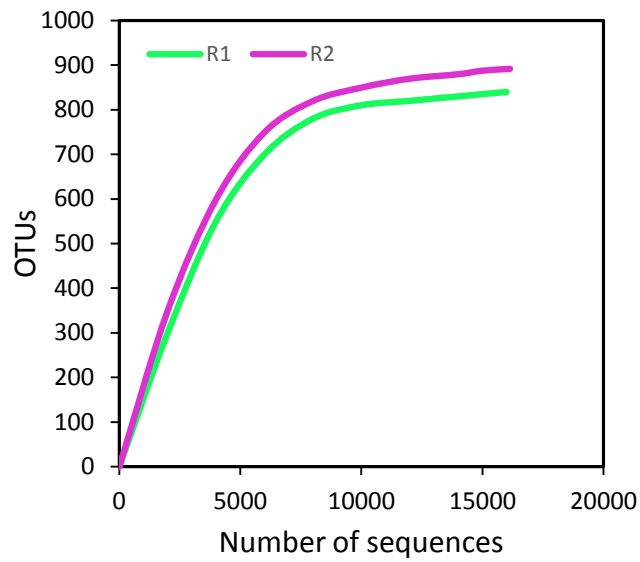


Figure S1. Rarefaction analysis of the sludge samples from R1 and R2. Rarefaction is shown for OTUs with differences that do not exceed 3% OTUs with $\geq 97\%$ pairwise sequence identity are assumed to form the same species and genus, respectively.

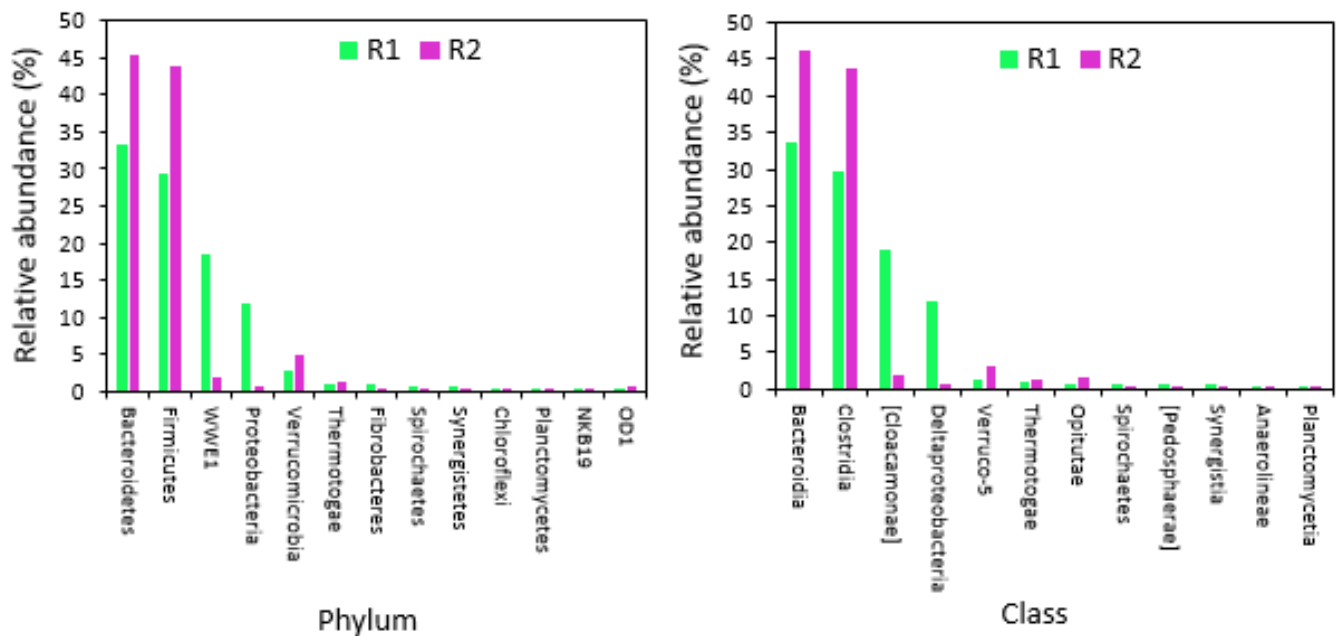


Figure S2. Taxonomic classification of bacterial 16S rDNA gene reads of the substrate sample from two CSTR reactors with (R2) and without recirculation (R1) at phylum and family levels (the relative abundances of bacterial 16S rDNA gene reads less than 0.1% are not shown).