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1 **WATER RESOURCES ADAPTATION TO CLIMATE AND DEMAND**

2 **CHANGE IN THE POTOMAC RIVER**

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8 **ABSTRACT**

9 The effects of climate change are increasingly considered in conjunction with changes in water
10 demand and reservoir sedimentation in forecasts of water supply vulnerability. Here, the relative
11 effects of these factors are evaluated for the Washington, DC metropolitan area water supply for the
12 near (2010 to 2039), intermediate (2040-2069), and distant future (2070 to 2099) by repeated water
13 resources model simulations. This system poses water management challenges due to long water
14 delivery travel times that increase uncertainty, multiple water jurisdictions that constrain potential
15 decisions, and future scenarios that simultaneously increase demand and decrease water supply
16 during the critical summer period. Adaptation strategies were developed for the system using a
17 multi-objective evolutionary algorithm. Optimized reservoir management policies were compared
18 using six distinct objectives, ranging from reservoir storage to environmental and recreational
19 benefits. Simulations of future conditions show water stress increasing with time. Reservoir
20 sedimentation is projected to more than double (114% increase) the severity of reservoir storage
21 failures by 2040. Increases in water demand and climate change are projected to further stress the
22 system, causing longer periods of low flow and a loss of recreational reservoir storage. The adoption
23 of optimized rules mitigates some of these effects, most notably returning simulations of 2070-
24 2099 climate to near historical levels. Modifying the balance between upstream and downstream

25 reservoirs improved storage penalties by 20.7% and flowby penalties by 50%. Changing triggers
26 for shifting load to off-line reservoirs improved flowby (8.3%) and environmental (4.1%) penalties
27 slightly, while changing demand restriction triggers provided only moderate improvements, but
28 with little adverse effects.

29 **Keywords:** Water resources management; optimization; climate change adaptation; drought.

30 INTRODUCTION

31 Climate research indicates that the Earth's climate is changing in response to changes in the
32 global atmospheric composition, brought about by human activities (IPCC 2014). As atmospheric
33 research improves the reliability of climate projections, water resources planners and engineers
34 must consider climatic changes as important factors for water supply planning, along with more
35 traditional non-stationary factors, such as demand change and reservoir sedimentation. Once future
36 vulnerabilities to any of these factors are identified, adaptation strategies can be developed to
37 mitigate their effects. Like many major cities, the Washington, DC metropolitan area (WMA) is
38 interested in identifying changes in water supply vulnerability due to (a) increased water demand,
39 (b) losses of storage, and (c) changes in natural water availability due to the effects of climate
40 change. This study explores these questions and demonstrates how water resources optimization
41 can be combined with projections of future conditions to develop adaptation strategies, using the
42 WMA as a case study.

43 The WMA is the 6th largest metropolitan area in the U.S. (U.S. Census Bureau 2016), housing an
44 estimated 6.1 million residents across 15 counties in Maryland (MD), Virginia (VA), and the District
45 of Columbia (DC). Each of these three regions operate under separate water suppliers, creating an
46 interesting jurisdictional challenge that was largely addressed by a unique shared decision-making
47 scheme designed to ensure equitable water access during water shortages (U.S. Army Corps of
48 Engineers 1982). Water for the region (Fig. 1) is primarily provided by withdrawals from the
49 Potomac River, whose flow can be augmented by the Jennings Randolph Reservoir, located a nine
50 to ten day travel time (300 km) upstream of the Washington, DC water supply intakes, and the
51 smaller Little Seneca Reservoir, located only one day travel time upstream, that can be used to

52 fine-tune releases (Sheer and Flynn 1983). This design, completed in 1982, allows the 38,000 km²
53 Potomac watershed to remain largely uncontrolled, but also increases the importance of effective
54 water management policies. Maryland and Virginia maintain off-line water storage, the Patuxent
55 and Occoquan reservoirs, respectively, which can supplement water extracted from the Potomac
56 River. In 2008, 31% of suburban Maryland's water production came from the Patuxent reservoirs
57 and 42% of suburban Virginia's water production came from the Occoquan Reservoir, with the
58 remainder and all of Washington DC's water supply coming from the Potomac River. For more
59 detail and history on the WMA water supply system, please refer to Stagge and Moglen (2014) or
60 Sheer and Flynn (1983).

61 Optimization of the WMA water supply system has its origins in the initial water allocation
62 studies (Palmer et al. 1979; Palmer et al. 1982) , which concluded that demand could be met
63 through coordinated operation of the existing Patuxent and Occoquan reservoirs along with the
64 Jennings Randolph and a then-proposed reservoir, which would eventually become the Little
65 Seneca reservoir. The system has been stressed several times, with water supply releases made
66 on three occasions, in 1999, 2002, and 2010. Following the 1999 drought event, specific triggers
67 were added to the management plan that guaranteed all regions (MD, VA, and DC) would enact
68 water use restrictions automatically and simultaneously to prevent jurisdictional disagreements. In
69 an optimization study of the region, Stagge and Moglen (2014) concluded that these triggers were
70 unnecessarily conservative, never engaging during simulations of the historical drought of record,
71 but that accepting infrequent use restrictions would greatly decrease the system's vulnerability.
72 Stagge and Moglen (2014) considered other water management rules, concluding that improvements
73 to reservoir storage and environmental flowby could be achieved by modifying rules that shift
74 demand from the Potomac River to the off-line reservoirs. Rules controlling the relative releases
75 from the Jennings Randolph and Little Seneca reservoir were found to be relatively well optimized,
76 though a slightly stronger reliance on releases from the Little Seneca improved overall storage and
77 downstream flow targets.

78 Projections of climate change effects in the Potomac River watershed and the mid-Atlantic

79 United States predict moderate increases in mean annual temperature, precipitation, and stream-
80 flow over the next century (Najjar et al. 2009; Pyke et al. 2008; Hayhoe et al. 2008). An evaluation
81 of the four best performing General Circulation Models (GCMs) in the Chesapeake Bay watershed
82 suggests an increase in mean annual temperature of $3.9 \pm 1.1^\circ\text{C}$ and an increase in precipitation of
83 $9 \pm 12\%$ by the end of the century under the A2 scenario (Najjar et al. 2009). This continues the
84 historical trend of precipitation increases throughout the northeast U.S. during the 20th century
85 (Groisman et al. 2001; Groisman et al. 2004). Despite projected increases in mean annual precipi-
86 tation and flow for the mid-Atlantic, variation in the seasonality and distribution of precipitation and
87 runoff is potentially more important for water resources management. Storm events are projected
88 to become both more severe and intermittent, with precipitation intensity expected to increase by
89 one standard deviation, concurrent with an increase in dry days and heat waves (Meehl and Tebaldi
90 2004; Tebaldi et al. 2006).

91 These projections suggest a moderate increase in mean flows, but with greater likelihood of
92 both flooding, due to storm intensity, and drought, due to prolonged dry periods. Seasonality is
93 also expected to shift, with the greatest increase in precipitation occurring during the winter and
94 spring (Najjar et al. 2009). Similar seasonal trends were noted in McCabe and Ayers (1989), Moore
95 et al. (1997) and Hayhoe et al. (2007). This was further supported by detailed simulations of flow
96 in the Potomac River that project a slight increase (1-7%) in mean annual flow by 2070-2099, with
97 the increase occurring during the winter and early spring peak season (Stagge and Moglen 2013).
98 At the same time, summer flows are projected to decrease, caused by a decrease in runoff from
99 large, sustained storm events, the date of the minimum flow is expected to shift earlier by 2-5 days
100 (Stagge and Moglen 2013).

101 In addition to climate change, demand increases and loss of storage due to sedimentation will
102 further stress the system. The population of the WMA was predicted to increase by approximately
103 1 million people (25%) between 2010 and 2040, which corresponds to a projected water demand
104 increase of 23% (MWCOG 2009). According to the most recent Census estimates (U.S. Census
105 Bureau 2016), the region's population has already increased by 460,000 during the first 5 years

106 of this period (2010-2015). Adding to this potential system stress, reservoirs in the WMA water
107 supply system are projected to lose 7-15% of their usable storage volume due to sedimentation in
108 the 30 years between 2010 and 2040 (Ahmed et al. 2010).

109 This study has two primary objectives: first, to estimate future water supply vulnerability
110 in the Potomac River and WMA, and second, to optimize water system rules based on future
111 conditions and thereby provide adaptation strategies. The WMA represents an interesting challenge
112 for this approach, given its tranboundary jurisdictional constraints and uncertainty due to the
113 lag between reservoir releases and water delivery. Future conditions are simulated using the
114 best available projections of demand change and reservoir sedimentation, while climate change
115 effects are based on stochastically generated flows (Stagge and Moglen 2013) driven by Coupled
116 Model Intercomparison Project Phase 3 (CMIP3) projections (Meehl et al. 2007). Adaptation
117 strategies are derived by considering several conflicting objectives using start-of-the-art multi-
118 objective evolutionary algorithm optimization. The advantage of this approach is greater flexibility
119 in objectives and system models, while allowing decision-makers to easily compare alternatives
120 by metrics that are used in practice. The resulting strategies show how current levels of service in
121 the WMA could be maintained in the future using only better management, avoiding the need for
122 physical modification to the system. This demonstrates an approach merging climate projections
123 and optimization that could be replicated in other water systems to develop adaptation strategies.

124 **METHODS**

125 This study extends prior research on optimal water management on the Potomac River under
126 current conditions Stagge and Moglen (2014) to instead test the vulnerability of the WMA water
127 supply system to projected future climate, demand, and storage change and then to address the
128 critical topic of adaptation to these future conditions. Future vulnerability was tested by comparing
129 system performance using current conditions to three future climate periods (2010-2039, 2040-
130 2069, 2070-2099) and projections of demand and reservoir sedimentation at five year intervals
131 from 2010 to 2040. Vulnerability was estimated for each of these scenarios separately and together,
132 while performance was quantified using six objective functions considered in previous studies of the

133 system. Adaptation strategies were determined by optimizing system rules using a multi-objective
134 evolutionary algorithm approach and highlighting how optimal rules might mitigate vulnerabilities
135 identified in the first part of the study.

136 **Washington Metropolitan Area Water Supply Model**

137 This study uses the water supply model developed and described in detail by Stagge and
138 Moglen (2014). Hydraulic routing and reservoir operations were simulated using OASIS (Version
139 3.09.033), developed by Hydrologics, Inc (Hydrologics Inc. 2009). OASIS is a water management
140 simulation and decision model, which uses a node-arc architecture to model reservoirs, reaches,
141 inputs and withdrawals. Operating rules are expressed as goals or constraints and solved via
142 linear programming using a daily time step, mimicking the imperfect foresight of daily operational
143 decision-making.

144 The OASIS model was developed in conjunction with the Interstate Commission on the Potomac
145 River Basin (ICPRB) and water suppliers to ensure that all data, operating rules, and assumptions
146 were accurate. Reservoir details, including stage-storage curves, sedimentation rates, and existing
147 operational rule curves, were provided by the ICPRB, as well as the current Potomac channel
148 routing and travel time estimates. Daily demand among the three major WMA water suppliers was
149 simulated using a set of multivariate regression equations, incorporating an autoregressive–moving-
150 average (ARMA) error term, provided in Ahmed et al. (2010). Municipal water needs of the WMA
151 are managed by three major suppliers:

152 **Washington Suburban Sanitary Commission (WSSC)**, which serves the Maryland suburbs,

153 **Fairfax Water**, which serves Fairfax County and other northern Virginia suburbs, and

154 **Washington Aqueduct**, which provides water to the District of Columbia.

155 The current water supply system (Fig. 1) is the result of several design iterations and collab-
156 oration among the numerous levels of government, water suppliers and citizen groups. Details
157 of the system are provided by Stagge and Moglen (2014) and Ahmed et al. (2010). This system

158 relies predominantly (approximately 78% annually, Ahmed et al. 2010) on flow from the Potomac
159 River to satisfy water demands, with the remainder of water provided by two off-line reservoirs:
160 the Patuxent Reservoir system operated by WSSC and the Occoquan Reservoir operated by Fairfax
161 Water (Table 1). Flow in the Potomac is augmented by two reservoirs. The Jennings Randolph
162 Reservoir is the larger of the two ($109 \times 10^6 \text{ m}^3$), but is located approximately 9-10 days hydrologic
163 travel time upstream of the WMA intakes (Table 1). The Little Seneca Reservoir is located only a
164 day upstream of the MWA intakes, but has significantly smaller usable storage and a smaller wa-
165 tershed area. These two reservoirs are, therefore, operated in concert, with the Jennings Randolph
166 providing primary releases and the Little Seneca used to "fine tune" flows immediately upstream
167 of the intakes. The Savage Reservoir, located eight kilometers downstream from the Jennings
168 Randolph Reservoir, is operated to satisfy local North Branch low flow requirements and to
169 supply water to the nearby town of Westernport, Maryland. It was not considered for optimization
170 because it operates independently; however, the Savage Reservoir does make water supply releases
171 during severe droughts according to a matching relationship with Jennings Randolph releases and
172 therefore is also included in the model. While allowing the main stem of the Potomac River to
173 remain relatively uncontrolled, this system layout possesses considerable uncertainty, as release
174 decisions must be made in advance of accurate weather forecasts.

175 **Climate Change Flow Simulation**

176 The effect of climate change was simulated by stochastically generating daily climate-adjusted
177 streamflow and precipitation time series using the method described in Stagge and Moglen (2013).
178 Five GCM models (Table 2) from the CMIP3 experiment (Meehl et al. 2007) were used to generate
179 flows for three emissions scenarios (SRES A2, A1b, and B1). Projections of GCM-scale climate
180 variables were related to discrete monthly climate states identified from the historical record for
181 the study region. The Markov chain transition probabilities between these climate states are
182 then adjusted based on GCM climate projections. The parameters of a daily streamflow model,
183 similar to Aksoy (2003) and Szilagyi et al. (2006), are defined by the monthly climate state and
184 ultimately used to generate climate-adjusted daily streamflow. Daily flow is modeled using a

185 two-state (increasing/decreasing) Markov chain, with rising limb increments randomly sampled
186 from a Weibull distribution and the falling limb modeled as an exponential recession. This model
187 was demonstrated to accurately reproduce historical streamflow statistics at the daily, monthly and
188 annual time step in the Potomac River (Stagge and Moglen 2013) and to produce climate-adjusted
189 streamflows that match the general findings of classical climate downscaling studies (Najjar et al.
190 2009; Milly et al. 2005; Hayhoe et al. 2007).

191 Daily streamflow was generated for USGS stream gauge 01646500, located on the Potomac
192 River near the Little Falls pumping station in Washington, DC and spatially disaggregated to
193 daily streamflow and precipitation values at the necessary upstream sites using the "Method of
194 Fragments" (Srikanthan and McMahon 1982; Porter and Pink 1991), as in Stagge and Moglen
195 (2014). Flows were bias-corrected using quantile-quantile mapping to remove residual model bias,
196 particularly at the upstream sites.

197 **Demand and Sedimentation Projections**

198 Demand projections (Table 3) were based on the most recent population and demand projections
199 for the WMA (Ahmed et al. 2010). This projection evaluates demand change through the year 2040,
200 modeling beyond the 20 year forecast legally mandated to be performed once every five years. These
201 predictions are based on recent water use information provided by the WMA water suppliers and
202 demographic projections from the most recent Metropolitan Washington Council of Governments
203 (MWCOG) Round 7.2 Cooperative Forecast (MWCOG 2009). Demand change beyond year 2040
204 is not considered in this study, as water demand forecasts tend to become unreliable beyond the 30
205 year horizon in this region (Ahmed et al. 2010), given the added uncertainty of population change
206 and innovations in water efficiency.

207 Sedimentation rates (Table 4) were based on historical trend analysis (Ahmed et al. 2010) using
208 the Kendall-Theil Robust Line (Sen 1968). This non-parametric method is a popular alternative to
209 linear regression and is more robust to outliers. The rate of sedimentation was assumed to remain
210 constant for all future time steps, but was only projected until 2040 to match demand changes. This
211 limit on the time horizon was meant to account for uncertainty in sediment capture methods or land

212 cover change.

213 **Optimization of Operating Rules**

214 Optimization of system operating rules was carried out in a manner similar to Stagge and
215 Moglen (2014), using SMS-EMOA (Emmerich et al. 2005; Beume et al. 2007), a steady-state
216 multi-objective evolutionary algorithm designed to maximize the multi-dimensional hypervolume
217 (S-metric) dominated by a finite number of points. Hypervolume metrics, developed by Zitzler and
218 Thiele (1998) and Fleischer (2003), are invariant to objective scaling, tend to converge on the Pareto
219 set, and assign a greater weight to regions with unique points or high curvature in the objective
220 space. Optimization was carried out using the EMOA R package (Mersmann 2011) with simulated
221 binary crossover (SBX) and polynomial mutation. This optimization scheme has proven efficient
222 and effective relative to other multi-objective evolutionary algorithms in benchmark studies (Beume
223 et al. 2007).

224 Within the range of available water resources optimization techniques, evolutionary, or genetic,
225 algorithm solvers have proven successful because of their robustness and flexibility (Chen 2003;
226 Momtahn and Dariane 2007; Oliveira and Loucks 1997; Wardlaw and Sharif 1999). Evolutionary
227 algorithms are capable of searching large and complex decision spaces and evaluating nonlinear
228 and non-convex objective functions. Multi-objective evolutionary algorithm optimization solves
229 for a set of compromise solutions, termed the Pareto optimal front, that represent optimal solutions
230 which cannot be improved without affecting the other objectives.

231 Six objective functions were developed in conjunction with water suppliers and the ICPRB and
232 designed to cover the range of potential benefits within the Potomac River system. Target volumes
233 and flows were often based on legal agreements, such as the Low Flow Allocation Agreement
234 (U.S. Army Corps of Engineers 1982). Because the functional limit of current multi-objective
235 evolutionary algorithms has been shown to be approximately 10 objectives (Reed et al. 2013), this
236 optimization model uses six objectives. Each objective is followed by the units of that objective in
237 parentheses.

- 238 1. **Shortage**, which minimizes delivery shortages to the water suppliers (volume)
- 239 2. **Storage**, which minimizes low storage volumes in any of the reservoirs (volume)
- 240 3. **Flowby**, which minimizes days when flow in the Potomac does not exceed low flow require-
- 241 ments (days of violation)
- 242 4. **Rec Season**, which minimizes days during the recreation season that Jennings Randolph
- 243 levels fall below recreation facilities (days of violation)
- 244 5. **Whitewater**, which minimizes days when whitewater releases cannot be made due to low
- 245 storage volume (days of violation)
- 246 6. **Env Flows**, which minimizes days when flow in the Potomac falls below recommended
- 247 environmental levels for three consecutive days (days of violation)

248 These objectives are presented as a constrained multiobjective optimization problem, identical

249 to that posed in Stagge and Moglen (2014):

250
$$\text{Minimize } Z = Z_{\text{Short}}, Z_{\text{Stor}}, Z_{\text{Flowby}}, Z_{\text{Rec Season}}, Z_{\text{WW}}, Z_{\text{Env Flows}} \quad (1a)$$

$$Z_{\text{Short}} = \sum_i \sum_{t=0}^n \begin{cases} \frac{\text{Dem}_i(t) - \text{Del}_i(t)}{\text{Dem}_i(t)} & \text{if } \text{Dem}_i(t) > \text{Del}_i(t) \\ 0 & \text{otherwise} \end{cases} \quad (1b)$$

$$Z_{\text{Stor}} = \sum_j \sum_{t=0}^n \begin{cases} 100 - 6 \times \text{Stor}_j(t) & \text{if } 0 \leq \text{Stor}_j(t) < 10\% \\ 60 - 2 \times \text{Stor}_j(t) & \text{if } 10 \leq \text{Stor}_j(t) < 20\% \\ 40 - \text{Stor}_j(t) & \text{if } 20 \leq \text{Stor}_j(t) < 40\% \\ 0 & \text{if } \text{Stor}_j(t) \geq 40\% \end{cases} \quad (1c)$$

$$Z_{\text{Flowby}} = \sum_k \sum_{t=0}^n \left(\frac{Q_k(t) < Q_{\text{Flowby}}}{n} \right) \quad (1d)$$

$$Z_{\text{Rec Season}} = \sum_{t=0}^{n_{\text{Rec Season}}} \left(\left(\frac{\text{Elev}_{\text{JR}}(t) > \text{Elev}_{\text{Beach}}}{n_{\text{Rec Season}}} \right) + 2 \times \left(\frac{\text{Elev}_{\text{JR}}(t) > \text{Elev}_{\text{WV}}}{n_{\text{Rec Season}}} \right) + 5 \times \left(\frac{\text{Elev}_{\text{JR}}(t) > \text{Elev}_{\text{MD}}}{n_{\text{Rec Season}}} \right) \right) \quad (1e)$$

$$Z_{\text{WW}} = \sum_{t=0}^{n_{\text{WW}}} \left(\frac{Q_{\text{WW}}(t) = 0}{n_{\text{WW}}} \right) \quad (1f)$$

$$Z_{\text{Env Flows}} = \sum_{t=0}^n \left(\frac{((Q_{\text{LF}}(t) \text{ and } Q_{\text{LF}}(t-1) \text{ and } Q_{\text{LF}}(t-2)) < 200 \text{ MGD})}{n} \right) \quad (1g)$$

251 where each of the Z terms represent individual objective functions. For all objective functions, n
252 represents the total number of days in the time series, i represents the 5 individual water suppliers,
253 and j represents the 6 reservoir storage accounts: (1) Jennings Randolph Water Quality, (2)
254 Jennings Randolph Water Supply, (3) Savage, (4) Patuxent, (5) Occoquan, and (6) Little Seneca.
255 Z_{Short} (Eq. 1b), sums the percent water delivery shortage at all supply points, including WSSC,
256 Fairfax Water, the USACE, the city of Westernport, and the city of Rockville, where Dem_i refers to
257 daily demand, Del_i refers to daily delivery. Z_{Stor} calculates a penalty when reservoir usable storage
258 falls below 40% of the usable storage in the baseline year 2012. Penalties increase as storage
259 approaches zero using a piecewise function which approximates the existing drought restriction
260 setpoints (MWCOG 2000). Z_{Flowby} , which sums all days when the legally prescribed flowby,
261 Q_{Flowby} is not satisfied by flow, Q_k , at each of the k locations. The pertinent flowbys are 227

262 $\times 10^3$ m³/d at Luke, 1140×10^3 m³/d at Great Falls and 379×10^3 m³/d at Little Falls. $Z_{\text{Rec Season}}$
263 (Eq. 1e), refers to the summer Recreation Season, which occurs each year between May 1 and
264 Aug 31, represented in the function by $T_{\text{Rec Season}}$. During this period, water managers strive
265 to maintain water levels in the Jennings Randolph Reservoir, represented as Elev_{JR} , above three
266 recreation access points. These points, termed E_{Beach} , E_{WV} , and E_{MD} , are 443 m, 440 m, and
267 433 m, respectively. Z_{WW} (Eq. 1f) calculates the ratio of days when whitewater releases, Q_{WW} ,
268 cannot be made due to low storage volume. Whitewater releases are set to occur on the 15th and
269 30th of April and May, whose set is represented as T_{WW} . $Z_{\text{Env Flows}}$ (Eq. 1g), uses a measure to
270 summarize water supply activity's effect on the ecological health of the Potomac River. While the
271 legal flowby requirement below Little Falls is set at 757×10^3 m³/d, the Potomac Basin Large River
272 Environmental Flow Needs study stated that there "is strong concern that a continuous, multi-day
273 period of flows at or very close to 379×10^3 m³/d MGD would be injurious to the biota" (Cummins
274 et al. 2010). This function sums the number of occurrences when flow below Little Falls, Q_{LF} ,
275 remains below 757×10^3 m³/d for 3 or more consecutive days.

276 Five operating rule modifications were considered based on recommendations by water sup-
277 pliers and stakeholders. These rule modifications span a range of typical water management and
278 conservation approaches and are identical to those considered by Stagge and Moglen (2014): (1)
279 the "buffer equation" which shifts load between the upstream (Jennings Randolph) and downstream
280 (Little Seneca) mainstem Potomac reservoirs, (2) "load shifting" which shifts load from the Po-
281 tomac to the off-line reservoirs, (3) metropolitan demand restrictions, and seasonal reservoir release
282 rule curves for the (4) Jennings Randolph and (5) Patuxent reservoirs. Each candidate rule was
283 optimized separately to determine their potential adaptation effect. Adaptation rules were gen-
284 erated using both the historical record and the Commonwealth Scientific and Industrial Research
285 Organisation (CSIRO) (Gordon et al. 2002) A2 scenario (2070 to 2099), both subject to year 2040
286 levels of demand and sedimentation. The CSIRO output was chosen as representative of SRES A2
287 conditions at the end of the next century, while the A2 scenario was chosen as the most extreme
288 case. In verification tests, the CSIRO model consistently produced good statistical agreement with

289 the historical record across daily, monthly and annual time steps.

290 **RESULTS**

291 **Projected Changes to WMA Reliability**

292 Three major processes are projected to affect the reliability of the WMA water supply system
293 over the next century. These are demand change, reservoir sedimentation, and climate change.
294 To identify the relative impact of these processes on the system, the system was simulated while
295 adjusting to each parameter in isolation.

296 *Vulnerability due to Demand Change*

297 Demand forecasts predict a population increase of approximately 1 million (25%) between 2010
298 and 2040, which corresponds to a projected water demand increase of 430 m³/d (23%) (Table 3,
299 MWCOG 2009). The greatest increase in population, and therefore water demand, is projected
300 to occur within the Fairfax Water service area of Northern Virginia. Demand increase for Fairfax
301 Water is projected to increase by 31% between 2010 and 2040, while the WSSC and Washington
302 Aqueduct service areas are expected to increase demand by 19% and 18%, respectively. The City
303 of Rockville, MD which maintains a separate water supply, is projected to have a relatively large
304 increase in demand by percent (31%), but this remains a small portion of the total WMA water
305 supply because of Rockville's small service area.

306 This projected increase in demand will produce a consistent increase in Storage penalty failures,
307 Z_{Stor} , and Recreation Season failures, $Z_{\text{Rec Season}}$ (Fig. 2). However, it is important to note that
308 impacts are different, with sedimentation strongly affecting available storage (Fig. 2a) and increased
309 demand strongly affecting recreation season storage (Fig. 2b). By the year 2040, this increase in
310 demand alone will result in an additional loss of approximately 0.5 days/year with access to the Beach
311 (2.0% increase) and 0.9 days/year with access to the West Virginia boat ramp (58.3% increase).
312 While this loss of recreation time may not appear large, a 58.3% increase in the more severe WV
313 boat ramp failures suggests that demand will drive a loss of recreation revenue. Additionally,
314 recreation failures tend to occur in extended groups, rather than a single instance. In this way, the

315 additional failures may have a considerable effect on individual recreation seasons. While increased
316 demand does not dramatically affect WMA storage across all reservoirs (Fig. 2a), by year 2030 it
317 begins to adversely affect storage in the Little Seneca Reservoir, shown as an increased deviation
318 between sedimentation only scenarios and combined sedimentation and demand.

319 *Vulnerability due to Sedimentation*

320 Usable reservoir storage volume is expected to decrease due to the deposition of sediment
321 carried by reservoir inflows over time. Reservoirs in the WMA water supply system are projected
322 to lose 7 to 15% of their usable storage volume due to sedimentation in the 30 years between
323 2010 and 2040. Based on the most recent survey, the sedimentation rate in the Jennings Randolph
324 Reservoir is particularly high relative to the other reservoirs (Table 4), and much greater than
325 the original "design" sedimentation rate of 25 m³/yr (Burns and MacArthur 1996). By year
326 2040, the storage capacity loss in the Jennings Randolph Reservoir is projected to be 25% of the
327 original storage volume (14.1% between 2010 and 2040). Despite these predictions of storage loss,
328 sedimentation rates tend to change with time, as the sediment contribution of upstream watersheds
329 change. Increased development tends to increase sediment load per area (Allmendinger et al. 2007),
330 though this effect may be mitigated by improvements in non-point source runoff treatment. It is
331 important to note that the Jennings Randolph watershed, historically home to coal mining, has seen
332 a decrease in this industry and has been subject to increased oversight with respect to non-point
333 source runoff.

334 As expected, reservoir sedimentation is expected to increase the frequency and severity of
335 reservoir storage failures, defined as usable storage less than 40% by Z_{Stor} (Fig. 2). This noted
336 increase is due primarily to storage failures in the Patuxent and Savage reservoirs. Interestingly, the
337 Jennings Randolph and Little Seneca water supply reservoirs do not develop storage failures until
338 the year 2040 sedimentation level. This suggests that there may be opportunities for improving Z_{Stor}
339 as storage is lost to sedimentation through changes in how load is allocated among the reservoirs.
340 Because $Z_{\text{RecSeason}}$ is strongly tied to storage in the Jennings Randolph, it is not surprising that
341 $Z_{\text{RecSeason}}$ is relatively unaffected by sedimentation losses (Fig. 2). Further, sedimentation has little

342 impact on the flow measures, Z_{Flowby} and $Z_{EnvFlows}$.

343 *Vulnerability due to Climate Change*

344 Output from five GCM simulations (Table 2) was used to generate streamflow and precipitation
345 throughout the Potomac watershed at 30 year intervals (2010 to 2039, 2040-2069, 2070 to 2099).
346 These simulations predict a slight increase (1-7%) in mean annual flow over the next century, with
347 increases during the winter and early spring, followed by decreased flow during summer (Stagge
348 and Moglen 2013; Najjar et al. 2009; Hayhoe et al. 2007). Projections also show that summer
349 flows will be characterized by longer periods of low flow (Tebaldi et al. 2006), with shorter but
350 more intense storm events and an earlier occurrence of the annual minimum flow. As expected, the
351 highest emission scenario, SRES A2, produced the most severe shifts in streamflow, while the low
352 emission scenario, SRES B1, produces a more modest change.

353 The effect of climate change alone on water supply reliability in the WMA region is shown
354 graphically in Fig. 3. Climate change simulations project an increase (worsening) for nearly all
355 objective functions over the next century. Results presented in Fig. 3 account for model bias by
356 using quantile-quantile bias correction and always comparing projections against current conditions
357 simulated using the same GCM. Interestingly, the greatest change for most objective functions
358 occurs during the first part of the upcoming century (2010 to 2039), despite streamflow trends
359 continuing consistently until 2099 (Stagge and Moglen 2013).

360 When examined in greater detail, the climate change scenarios result in an increase in the
361 frequency of Patuxent and Savage storage failures, though the severity of these failures actually
362 tends to decrease throughout the century. This is partially because load is shifted to other reservoirs
363 such as the Little Seneca and the Occoquan, which previously did not produce storage failures, but
364 begin to once subjected to climate change streamflows. Though storage in the Jennings Randolph
365 Reservoir is never low enough to be considered a storage failure, climate change conditions greatly
366 decrease the number of days with access to the Jennings Randolph beach by 3.9-5.2 days/year.
367 Access to the WV boat dock is decreased by an average of 0.4 to 1.3 days/year. Whitewater releases
368 are predicted to be curtailed an additional 4-14 days over the simulation period, an increase of 18%

369 to -41%.

370 **Adaptation Strategies**

371 As expected based on the vulnerability portion of the study, runs combining the climate pro-
372 jections of the 2070-2099 A2 emissions scenario with 2040 demand change and sedimentation
373 was the most challenging scenario for the WMA system. The value of implementing adaptation
374 strategies to this extreme case was determined by comparing system penalties (objective function
375 values) using optimized rules to current rules (Table. 5). These results show that adjustments to the
376 Buffer Equation can produce the greatest improvement under future conditions for most objectives.
377 Load shifting to reservoirs off the mainstem offers modest improvements, primarily to the flowby
378 penalty, while modifying demand restricts produces the smallest impact. Modification of the Jen-
379 nings Randolph rule curve is effective for addressing objectives related to recreation storage and
380 Potomac low flows, while Patuxent rule curve modifications decrease reservoir storage penalties.
381 No system shortage failures were noted and were, therefore, not included in the discussion. This is
382 because the existing operating rules prioritize satisfying daily demand at the expense of violating
383 the other objectives.

384 *Buffer Equation*

385 Within the WMA water supply operating rules, the Buffer Equation is designed to balance
386 storage levels between the reservoirs on the main-stem of the Potomac River, the upstream Jennings
387 Randolph Reservoir and downstream Little Seneca Reservoir. Reservoir releases are calculated
388 based on estimated demand; however, the buffer equation adds a so-called "buffer flow" to Jennings
389 Randolph releases to account for imbalance in percent usable storage between the Jennings Ran-
390 dolph Water Supply volume and downstream Little Seneca storage. The existing Buffer Equation is
391 represented by a black diagonal line in Fig. 4), in which a negative storage imbalance recommends
392 a larger than necessary release from the Jennings Randolph to reduce load on the Little Seneca.
393 The right side of these plots (positive imbalance) reduces Jennings Randolph releases under the
394 assumption that the deficit will be satisfied through releases from the downstream Little Seneca
395 Reservoir. Under the current policy, the slope of the Buffer Equation (Fig. 4) is linear for both of

396 these situations, with a maximum buffer flow of 568 m³/d.

397 Modification of the Buffer Equation produced the largest improvement of the considered mod-
398 ifications for future conditions, reducing the frequency of missed flowby targets (Z_{Flowby}) and the
399 number of consecutive days with extreme low flows (Z_{EnvFlows}) (Table. 5). Buffer equation adjust-
400 ments were partially capable of mitigating the impact of climate change, reducing most penalties for
401 the 2070 to 2099 scenario to levels simulated with only demand and sedimentation. However, no
402 version of the Buffer Equation is capable of reducing system-wide penalties under climate change,
403 demand increase and sedimentation to current levels.

404 The Buffer Equation reduces Z_{Flowby} and Z_{EnvFlow} failures by increasing the buffer flow when
405 usable Little Seneca storage (%) is lower than Jennings Randolph (Fig. 4a). Under these optimized
406 rules, a much greater release is made from the Jennings Randolph Reservoir in this situation, which
407 in turn reduces load on the Little Seneca Reservoir and acts as a pulse in the Potomac River to
408 prevent extreme low flows downstream of Little Falls. Similar recommendations were made for
409 current climate conditions (Stagge and Moglen 2014) and the shape of the optimal Buffer Equation
410 does not change substantially with time between current conditions and the 2070 to 2099 projection.

411 Although the right side of the equation has little effect on Z_{Flowby} , it is important for improving
412 $Z_{\text{RecSeason}}$ (Fig. 4b), particularly for the 2070-2099 projection. This extreme scenario produced the
413 most stress on the Jennings Randolph storage, where Recreation Storage is measured. Therefore,
414 it follows that a lower Buffer Equation on the right side would reduce Jennings Randolph releases
415 when storage is low relative to other reservoirs, thereby protecting recreation storage.

416 *Load Shifting*

417 While the Buffer Equation deals with balancing releases along the Potomac River, Load Shifting
418 controls how demand is allocated to the offline reservoirs, the Patuxent and Occoquan. When
419 predicted flow in the Potomac River is not sufficient to satisfy predicted demand, production at the
420 Patuxent and Occoquant water treatment plants is temporarily increased above typical production
421 levels. Following this load shifting event, production at the offline reservoirs is curtailed an
422 equivalent amount, to replenish storage. Load shifting occurs only when storage in the Jennings

423 Randolph, Little Seneca, Occoquan and Patuxent remains above trigger points, called Load Shift
424 Storage Indices.

425 Modification of the Storage Indices and Load Shift equation has relatively little impact on
426 the WMA system in simulations of future demand/sedimentation conditions and climate change
427 (Table 5). While changes to load shifting generally results in better performance than the current
428 policy, this improvement cannot completely mitigate the effects of either climate change or of
429 demand and sedimentation change. No trends exist over time among the optimized load shifting
430 parameters, suggesting that the effectiveness of load shifting has been maximized and that no
431 further improvements will be realized with time.

432 Adjustments to the load shift equation were shown to be effective under current conditions
433 because the Occoquan Reservoir had unused storage which could be used to reduce load on the
434 already stressed Patuxent Reservoir (Stagge and Moglen 2014). However, as future conditions
435 further constrain and stress the WMA system, the additional Occoquan storage is not as readily
436 available, as shown by increases in Occoquan storage penalties (storage < 40 %). Increasing
437 the Load Shift Storage Indices was another method of decreasing load on the stressed Patuxent
438 Reservoir under current climate conditions (Stagge and Moglen 2014). However, under future
439 conditions, it puts undue strain on the Little Seneca Reservoir, suggesting that the benefits of this
440 approach are already maximized.

441 *Monthly Rule Curves*

442 All reservoirs in the WMA water supply system operate, at least during a portion of the year,
443 according to zone-based rule curves, except for Little Seneca which maintains a full storage volume
444 throughout the year. To determine adaptation potential, operating rule curves for the Jennings
445 Randolph and Patuxent Reservoirs were evaluated using multiobjective optimization. The Jennings
446 Randolph Reservoir was chosen for evaluation because it is the primary water supply reservoir on
447 the Potomac River, while the Patuxent Reservoir was most vulnerable to storage failures. Jennings
448 Randolph water quality storage is managed by the Baltimore District of the U.S. Army Corps
449 of Engineers and uses 3 zone-based rule curves (high, medium, and low) to guide water quality

450 releases during the non-Recreation Season months (September through April). These releases are
451 designed to approximate the natural contribution of the Potomac River's impounded North Branch,
452 while refilling the reservoir prior to the summer recreation season.

453 Modifications of the Jennings Randolph rule curves primarily improved objectives related to
454 Jennings Randolph storage (Table 5), reducing $Z_{\text{Rec Season}}$ by 0.1-9.2% and Z_{WW} by 83.3-98%. It
455 had little effect on storage failures, as these primarily occurred in other reservoirs or during the
456 summer season when the seasonal rule curves are not in effect. The projected climate change shift
457 towards higher flows during the winter and spring, followed by lower flows in the summer and
458 early fall was mirrored by the optimized Jennings Randolph Reservoir rule curves. The optimized
459 curves increased trigger points between March and May, immediately prior to the recreation season,
460 forcing the Jennings Randolph Reservoir to operate more conservatively, making smaller releases
461 during this time. In this way, the increase in spring flows is used to increase the storage buffer prior
462 to a summer flow regime characterized by more severe low flows.

463 Modification of the Patuxent rule curve is designed to maintain adequate storage in the highly
464 stressed Patuxent Reservoir while providing additional water supply for the WSSC. Simulations
465 suggest that the Patuxent Reservoir is vulnerable during future droughts, typically entering low
466 storage (< 40%) conditions before the remaining WMA reservoirs and thereby contributing to the
467 Z_{Stor} penalty. For future conditions, adjusting the Patuxent rule curves improves Z_{Stor} by 6.1-6.4 %
468 (Table 5). The Patuxent Reservoir operates using 2 rule curves which control daily water treatment
469 withdrawals based on storage zone. The adaptation improvement is attributed to an increase of
470 approximately $1,000-1,500 \times 10^3 \text{ m}^3$ in both the upper and lower rule curves between the months of
471 September and February. This modification allows the Patuxent Reservoir to refill more effectively
472 if storage is low during the fall and winter by decreasing water treatment rates and shifting load
473 back to the Potomac River. While this shift is similar in both the climate change simulation and the
474 sediment and demand change simulation, the optimal rule curves deviate in mid-summer. Likely
475 because of increased summer drought severity due to climate change, the optimized upper and lower
476 Patuxent rule curves for this scenario tend to be approximately $300 \times 10^3 \text{ m}^3$ higher through the

477 months of July and August. This allows the Patuxent Reservoir to operate even more conservatively
478 for the most extreme scenario.

479 *Demand Restrictions*

480 The Metropolitan Washington Council of Governments standardized the implementation of
481 water use restrictions by setting three demand restriction levels: voluntary, mandatory and emer-
482 gency, each with a unique storage trigger (MWCOG 2000). As part of the MWCOG agreement, all
483 regional governments have agreed to abide by these triggers, declaring restrictions simultaneously.
484 Voluntary restrictions are triggered when combined storage in the Jennings Randolph and Little
485 Seneca reservoirs falls below 60%. Trigger points for mandatory and emergency restrictions are
486 set at 25 and 5% for Jennings Randolph or Little Seneca storage, respectively (Table 6). This is a
487 simplification of the actual MWCOG demand restriction rules, but matches actual operation very
488 well.

489 In a review of the WMA under current conditions, Stagge and Moglen (2014) found that the
490 existing MWCOG demand restriction triggers would never be implemented during a repeat of the
491 historical streamflow record with current demand levels. As stress on the WMA water supply
492 increases with time, the likelihood of demand restrictions increases, highlighting the importance of
493 an effective demand restriction policy. Under the existing MWCOG policy and 2040 demand and
494 sedimentation levels but no climate change, the WMA service area would experience Voluntary
495 restrictions once every 26 years, on average. Simulations based on the CSIRO 2070-2099 A2
496 climate scenario with demand change and sedimentation increase this frequency to once every 20
497 years, with 75% of Voluntary restriction years ultimately requiring Mandatory demand restrictions.

498 Improvements due to demand restrictions are limited and primarily focus on Z_{Flowby} and
499 $Z_{EnvFlows}$. With regard to storage, these changes particularly improve storage in the Patuxent
500 and Occoquan Reservoirs. System performance is improved by increasing the Voluntary trigger
501 from 60% of Jennings Randolph and Little Seneca storage to 74-85% (Table 6). Operations also
502 improved when the Mandatory restriction trigger point was decreased from 25% to 17-25% for
503 Jennings Randolph storage but increased from 25% to 24-59% for Little Seneca storage (Table 6).

504 The trigger point is higher for the Little Seneca because it is more vulnerable due to its small
505 size and slow refill rate. Trigger points for Emergency restrictions were also increased, although
506 these were so infrequently used that there is significant uncertainty in the results. The benefits of
507 these adaptation strategies are tempered by an increase in the frequency of demand restrictions, for
508 example doubling the frequency of Voluntary restrictions from once every 20 years to once every
509 10 years.

510 Modifying the percent demand restrictions during the summer season (June-Sep) did not pro-
511 duce significant improvement in the objective functions. However, some improvements for Z_{Flowby}
512 and $Z_{\text{Env Flows}}$ were realized by increasing the percent demand restrictions outside of the summer
513 period to resemble summer restrictions. Continuing the more severe restrictions outside the sum-
514 mer drought period allowed reservoirs to refill prior to the next summer, better handling multi-year
515 droughts.

516 **DISCUSSION**

517 This study utilizes evolutionary algorithms to optimize water management strategies. However,
518 other alternatives exist and could be substituted into this framework to identify adaptation strategies.
519 More traditional optimization techniques such as linear or nonlinear programming have the benefit
520 of quick convergence to the global optima, but would require several simplifying assumptions with
521 regard to constraints, objectives, and adaptation strategies (Labadie 2004). More recent heuristic
522 optimization techniques could also be considered, such as particle swarm optimization (Reddy and
523 Nagesh Kumar 2007; Taormina and Chau 2015), fuzzy programming (Chen and Chang 2010), or
524 simulated annealing (Li and Wei 2008). Similar to the evolutionary algorithm approach used here,
525 these alternative optimization approaches add a great deal of flexibility, sacrificing the guarantee
526 of finding global optima and requiring more processing time. More detailed comparisons of
527 modern optimization techniques are available in several methodology overviews (Ahmad et al.
528 2014; Sahinidis 2004; Labadie 2004).

529 From among these alternatives, we chose to use evolutionary algorithms because they are one
530 of the most common heuristic optimization techniques and are proven to be robust, flexible, and

531 capable of searching large and complex decision spaces (Reed et al. 2013). Flexible optimization
532 schemes are important in complex systems like the WMA because they can be directly linked to
533 hydrologic models and can handle uncertainty due to time lags in water delivery and complex
534 objective functions.

535 The objectives in this study were selected in close collaboration with the water suppliers and
536 were designed to closely match the goals of the system as codified in legal agreements. However,
537 there would be a benefit to considering new and more complex objective functions to determine
538 how the set of optimal solutions would change. For example, the environmental and low flow
539 objectives are based on quite simple legal requirements, but the objectives could be better targeted
540 to ecological health by collaborating with ecologists and fisheries experts. Similarly, there may
541 be some benefit to considering more complex economic drivers and objectives, using a framework
542 similar to Harou et al. (2009).

543 This study utilized CMIP3 projections downscaled to daily streamflow using the method of
544 Stagge and Moglen (2013) rather than more traditional approaches, such as statistical or dynamical
545 downscaling. The benefit of the Stagge and Moglen (2013) approach is that it generates a suite
546 of ensemble members to better test vulnerability over a wider range of feasible flows and does not
547 require a full hydrologic model. As described by Stagge and Moglen (2013), the existing Potomac
548 River model performed poorly for low flows, whereas the alternative approach better captured
549 these. The CMIP3 set of GCM runs has been updated with CMIP5 output (Wuebbles et al. 2013).
550 It would be helpful to consider CMIP5 output in the future, although the two experiments agree
551 well with regard to precipitation and drought near the Potomac River (Wuebbles et al. 2013). The
552 largest improvements have been for simulation of monsoon precipitation, which mainly affects
553 more southern and western parts of the United States (Cook and Seager 2013).

554 **CONCLUSIONS**

555 The effects of climate change are increasingly considered in conjunction with demand change
556 and reservoir sedimentation in forecasts of water supply vulnerability. This study provides an
557 example of how this can be accomplished, using the Washington, DC metropolitan area water supply

558 as a case study. First, system vulnerability due to projected changes was evaluated using repeated
559 simulation and then these vulnerabilities were addressed using multi-objective optimization to
560 develop a set of optimized rules under future conditions. These rules form the basis for an
561 adaptation strategy, using efficient management without the need for physical improvements.

562 A system-wide increase in demand of 23% by the year 2040 is projected to decrease available
563 storage in the Jennings Randolph Reservoir, decreasing the number of Recreation days, measured
564 above lake access points. Increased demand is also projected to increase the load on downstream
565 reservoirs, resulting in an increase in consecutive low flow days. WMA reservoirs are projected to
566 lose 7 to 15% of their usable storage volume due to sedimentation between 2010 and 2040, causing
567 an increase in storage failures, particularly in the Patuxent Reservoir. By year 2040, the effects of
568 sedimentation alone will begin to cause occasional storage failures in the Jennings Randolph and
569 Little Seneca Reservoirs as well.

570 Climate change is also projected to increase water supply vulnerability in the WMA. Climatic
571 trends in the region are towards higher flows in the winter and early spring, followed by more
572 extreme low flows in the summer. Simulations of five GCMs predict an increase in storage failures
573 within the system, with storage failures beginning to occur in the Little Seneca and Occoquan
574 reservoirs, where historically they did not occur. An increase in storage penalties is accompanied
575 by a decrease in whitewater releases and a doubling of Recreation Season failures.

576 Five potential modifications to existing operating rules were evaluated using the multi-objective
577 evolutionary algorithm optimization scheme. None of the optimized operating rules were able to
578 completely mitigate the combined effects of demand change, sedimentation and climate changes.
579 However, some, such as the Buffer Equation, were able to mitigate the effect of climate, with respect
580 to the objectives. Flowby and environmental flow penalties were decreased by modifying the
581 Buffer Equation to allow separate equations controlling upstream and and downstream imbalances.
582 Results for the load shift equation remain very similar to the optimized load shift equation found
583 for current conditions (Stagge and Moglen 2014). This suggests that the effectiveness of this
584 rule is maximized. Optimization of the zone-based rule curves suggests that Jennings Randolph

585 storage should be managed more conservatively during March, April and May in the future, while
586 storage in the Patuxent could be improved by managing the reservoir more conservatively during
587 the refill period (September to February). Evaluation of demand restriction triggers suggests that
588 system-wide operation could be slightly improved by increasing the reservoir storage triggers for
589 the minor, voluntary restriction. For the more severe, mandatory restriction, the optimized rules
590 suggest a decrease in the Jennings Randolph trigger and an increase in the Little Seneca trigger. In
591 this latter case, the increase in the Little Seneca trigger is due to its relatively small size and long
592 refill rate.

593 Using a combination of synthetic streamflow generation, water resources decision modeling
594 and multi-objective optimization, the potential vulnerabilities of the WMA water supply system
595 were evaluated. The adaptation strategies outlined here could be implemented in the WMA,
596 though several would require greater coordination and flexibility. This is a common challenge for
597 trans-boundary and shared watersheds. Further, this work provides a framework for developing
598 and comparing strategies to mitigate the effects of projected demand and climate change with an
599 appropriate adaptation strategy.

600 **ACKNOWLEDGMENTS**

601 This study was conducted while author, James Stagge, was a Via Doctoral Fellow in the
602 Department of Civil and Environmental Engineering at Virginia Tech. He gratefully acknowledges
603 support from the Via program and the Institute for Critical Technology and Applied Science
604 (ICTAS) at Virginia Tech. The authors would also like to thank the Interstate Commission on
605 the Potomac River Basin (ICPRB) and Hydrologics, Inc. for providing data access and research
606 support.

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617 The authors would like to thank two anonymous reviewers for their constructive comments
618 regarding this paper.

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TABLE 1. WMA operational characteristics.

Reservoir	Manager	Total Storage 10^6 m^3	Available Storage 10^6 m^3	Watershed Area km^2	Upstream Distance km	Travel Time days
Jennings Randolph	CO-OP,USACE	109	51	681	320	9
Little Seneca	CO-OP	16	14	54	25	1
Savage	UPRC	24	23	272	320	9
Patuxent	WSSC	51	39	342	-	-
Occoquan	Fairfax	31	30	1,533	-	-

TABLE 2. Global Climate Models (GCMs) considered.

Model	Institution	Location	Reference
CCSM3	National Center for Atmospheric Research (NCAR)	USA	Collins et al. (2006)
CGM_3.1	Canadian Centre for Climate Modeling and Analysis	Canada	Flato (2005)
CSIRO_MK3	CSIRO Atmospheric Research	Australia	Gordon et al. (2002)
MIROC_3.2	Center for Climate System Research	Japan	Watanabe et al. (2011)
PCM1	National Center for Atmospheric Research (NCAR)	USA	Washington et al. (2000)

TABLE 3. Projected WMA population and demand change (2010-2040). Percent change from 2010 is presented in parentheses.

	Population (in Millions)		Water Demand (10 ³ m ³ /d)			
	2010	2040	2010	2020	2030	2040
Fairfax	1.54	2.03 (32.0%)	663	755 (13.8%)	826 (24.5%)	866 (30.7%)
WSSC	1.72	2.01 (16.6%)	651	707 (8.6%)	746 (14.7%)	771 (18.6%)
Aqueduct	0.98	1.23 (26.0%)	571	624 (9.2%)	652 (14.1%)	673 (17.8%)
Rockville	0.05	0.06 (37%)	18	20 (10.4%)	22 (20.8%)	24 (31.3%)
Total WMA	4.28	5.33 (24.5%)	1,903	2,106 (10.7%)	2,246 (18.0%)	2,335 (22.7%)

TABLE 4. Projected sedimentation and storage loss (2010-2040). Percent change from 2010 is presented in parentheses.

Reservoir	Usable Storage (10^6 m ³)		Sed Rate (10^3 m ³ /yr)	Source
	2010	2040		
Jennings Randolph	102.5	88.1 (-14.1%)	481	U.S. Army Corps of Engineers (1963)
Little Seneca	13.8	12.1 (-12.3%)	57	Hagen et al. (1998)
Occoquan	29.5	25.0 (-15.4%)	151	CDM (2002)
Patuxent	38.1	35.4 (-7.2%)	91	Ortt et al. (2007)
Savage	23.3	21.2 (-8.8%)	68	Ahmed et al. (2010)

TABLE 5. Optimization results for future conditions (CSIRO A2, 2070-2099 climate). All values represent the maximum % improvement relative to simulations using existing operating rules.

	Z_{Stor}	Z_{Flowby}	$Z_{\text{Rec Season}}$	Z_{WW}	$Z_{\text{Env Flows}}$
Buffer Eq	20.71	50	37.79	88	15.20
Load Shifting	1.29	8.33	0	0	4.09
JR Rule Curve	1.27	16.67	9.24	98	15.20
Patux Rule Curve	6.39	4.17	0	0	2.34
Demand Res	1.46	4.17	0.52	0	5.26

TABLE 6. Optimized demand restriction triggers, in % usable storage. Current demand restriction triggers are presented as a single value, termed "MWCOG", while optimized results for the 2040 Demand and Sedimentation case "2040" and the CSIRO A2 2070-2099 case, "2070", are presented as a range across all non-dominated solutions.

	Jennings Randolph			Little Seneca		
	MWCOG	2040	2070 A2	MWCOG	2040	2070 A2
Voluntary	60	74-85	74-83	60	73-82	72-83
Mandatory	25	17-25	18-25	25	24-53	26-59
Emergency	5	11-17	11-15	5	4-15	3-14

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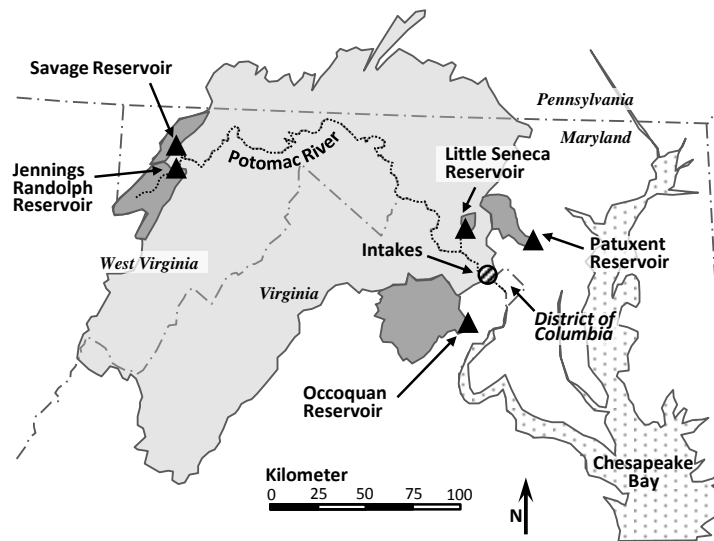
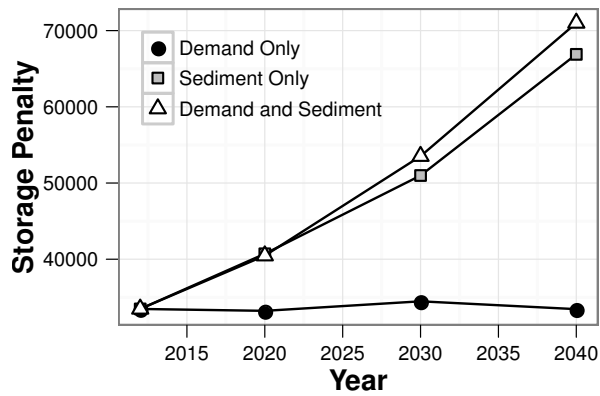
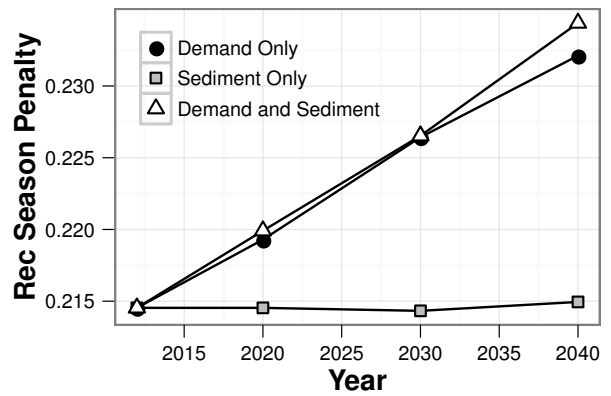


FIG. 1. Potomac watershed and Washington, DC, water supply; Potomac watershed shown in lighter shade, with reservoir watershed shown in a darker shade; reservoirs shown as triangles and intakes for the Washington, DC, metropolitan area shown as a hashed circle.

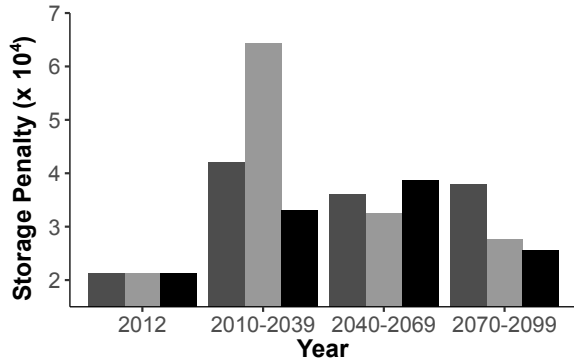


(a) Storage

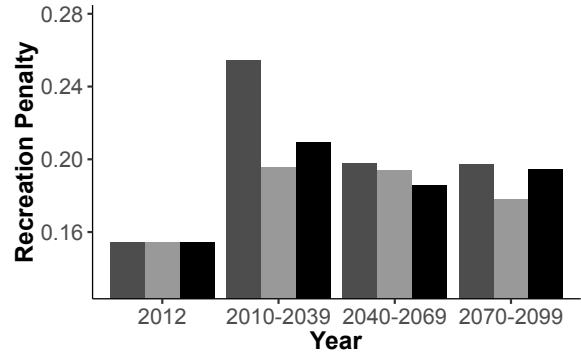


(b) Recreation Season

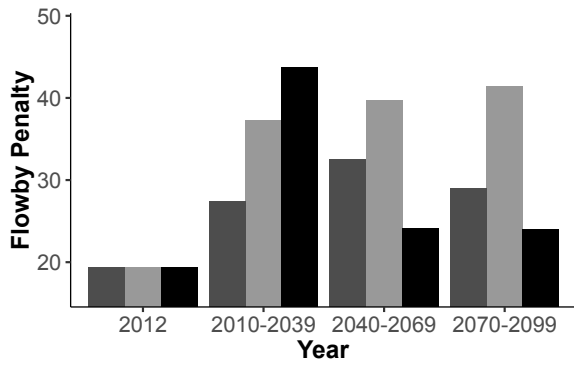
FIG. 2. Effect of demand increase and reservoir sedimentation on Storage (a) and Recreation Season (b) objectives.



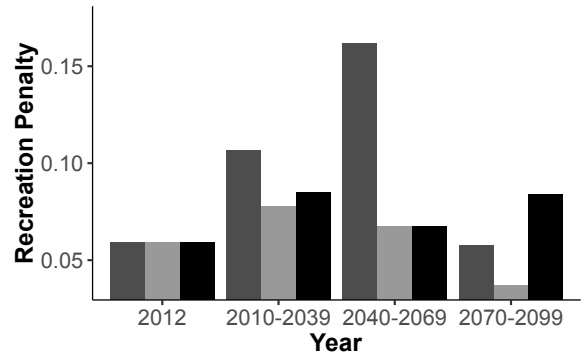
(a) Storage



(b) Recreation Season



(c) Flowby

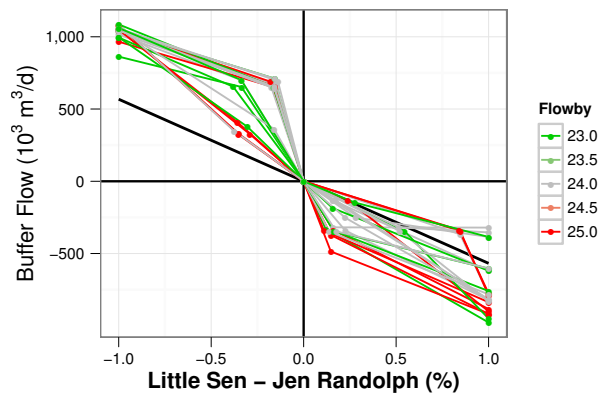


(d) Whitewater

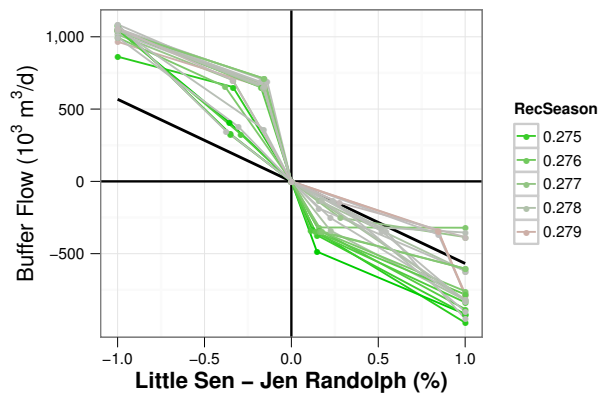
Scenario

■ A2 ■ A1b ■ B1

FIG. 3. Effect of climate change on system objectives. Lines represent the mean of all five considered GCMs for the SRES A2, A1b, and B1 emission scenarios.



(a) Flowby



(b) Recreation Season

FIG. 4. Optimized buffer equation under 2070-2099 climate change conditions with respect to Flowby (a) and Recreation Season (b). Current operating rules are shown by the diagonal, black line. Each non-dominated solution is presented with the color scale corresponding to improvement (green) or worsening (red) of the objective function relative to current policy.