

Physics

Electricity & Magnetism fields

Okayama University

Year 1992

Acceleration of convergence characteristic
of the ICCG method

Koji Fujiwara* Takayoshi Nakata†
Hirotsugu Fusayasu‡

*Okayama University

†Okayama University

‡Matsushita Electric Industrial Coporation Limited

This paper is posted at eScholarship@OUDIR : Okayama University Digital Information Repository.

http://escholarship.lib.okayama-u.ac.jp/electricity_and_magnetism/127

Acceleration of Convergence Characteristic of the ICCG Method

K. Fujiwara and T. Nakata
Department of Electrical Engineering
Okayama University
Okayama 700, Japan

H. Fusayasu
Information Equipment Research Laboratory
Matsushita Electric Industrial Co., Ltd.
1006 Kadoma, Osaka 571, Japan

Abstract - The effectiveness of renumbering for the incomplete Cholesky conjugate gradient solver, which is usually applied to direct solvers, is examined quantitatively by analyzing 3-D standard benchmark models. On an acceleration factor which is introduced to obtain convergence quickly, indices for determining the optimum value of the acceleration factor, which minimizes the number of iterations, are discussed. It is found that the renumbering is effective to use with the ICCG solver, and the solver using the acceleration factor gives a good convergence characteristic even in the case when the conventional solver fails to provide convergent solutions.

I. INTRODUCTION

In 3-D electromagnetic field analysis using the finite element method, the CPU time for solving linear equations is dominant in the total CPU time. Therefore, an acceleration of the ICCG solver [1,2] is significant in reducing the total CPU time. The acceleration can be obtained by reducing the number of iterations by improving preconditioning.

The improvement in preconditioning can be carried out by renumbering unknown variables [3]. It is often said that there is no total timesaving, especially in the 3-D computation which requires much CPU time, because the renumbering [4,5] is more time-consuming than the reduction in the solution time due to the renumbering. However, it has not been clarified quantitatively how the renumbering can reduce the number of iterations for the ICCG method, and how much time is required for the renumbering.

T.A.Manteuffel succeeded in improving the preconditioning by introducing an acceleration factor. However, the optimum value of the acceleration factor, which minimizes the number of iterations, was determined by trial and error [6].

In this paper, the effect of the renumbering on the number of iterations for the ICCG method is examined quantitatively by analyzing several standard benchmark models for 3-D magnetic field computations. Furthermore, a method for automatically determining the optimum acceleration factor is investigated, and various factors (a gauge condition, types of elements, etc.) affecting the acceleration factor are discussed.

II. IDEAS FOR IMPROVING CONVERGENCE CHARACTERISTIC

The number of iterations for the ICCG method can be reduced when a preconditioning matrix approaches the original coefficient matrix. Ideas for improving the preconditioning are explained.

A. Renumbering

When the incomplete Cholesky decomposition, which is

Manuscript received June 1, 1992, revised October 20, 1992. This work was supported in part by the Grant-in-Aid for Co-operative Research(A) from the Ministry of Education, Science and Culture in Japan (No.01302031).

available for a symmetric coefficient matrix, is applied, the preconditioning matrix LDL^T obtained is different from the original matrix H as follows:

$$LDL^T = H + E \quad (1)$$

where E is a matrix which describes the difference between the incomplete and complete decompositions. All non-zero entries in H are decomposed.

If LDL^T approaches H by reducing E , the convergence characteristic can be accelerated. The following objective function W is defined as a useful index which shows the amplitude of E .

$$W = \sum_{i=1}^{n_u} \sum_{j=1}^{n_u} E_{ij}^2 \quad (2)$$

where E_{ij} is an entry at a row number i and a column number j in E , and n_u is the number of unknown variables. The entries of $E_{ij} \neq 0$ appear at positions of fill-ins when an acceleration factor γ described later is equal to 1, and also at those of the diagonal entries H_{ij} of the matrix H when $\gamma \neq 1$. In the case of the complete decomposition, W is equal to zero because all E_{ij} 's are equal to zero. When the renumbering [5,6] is applied, the preconditioning matrix is improved because the number of fill-ins is reduced.

B. Acceleration Factor

As shown in (3), an acceleration factor γ is introduced into the incomplete decomposition [6-8].

$$L_{ij} = \begin{cases} \gamma H_{ij} - \sum_{k=1}^{i-1} L_{ik}^2 D_{kk} & (i = j) \\ H_{ij} - \sum_{k=1}^{j-1} L_{ik} L_{jk} D_{kk} & (i > j) \end{cases} \quad (3)$$

$$D_{ii} = 1 / L_{ii} \quad (5)$$

where L_{ij} and D_{ii} are entries in L and D respectively. The case of $\gamma=1$ corresponds to the conventional ICCG method.

From (1) and (3)-(5), it is noted that E_{ij} shown in (2) is a function of γ , and hence can be controlled by γ . Therefore, the acceleration factor can improve the preconditioning matrix.

III. CONVERGENCE CHARACTERISTICS

The convergence characteristics are examined by solving the basic models.

A. Models Analyzed and Method of Analysis

The effects of the renumbering and the acceleration factor γ on the number of iterations for the ICCG method are investigated by analyzing several 3-D standard benchmark models i.e. the linear magnetostatic and ac steady state linear

eddy current models [9,10] proposed by the Institute of Electrical Engineers of Japan (IEEJ) and shown in Fig.1. The coefficient matrices of the respective models are real and complex. The finite element method using the magnetic vector potential is applied. Both edge and nodal elements are investigated. All meshes used are regularly subdivided. The calculations are performed in double precision using the NEC SX-1E supercomputer whose maximum speed is 285 MFLOPS.

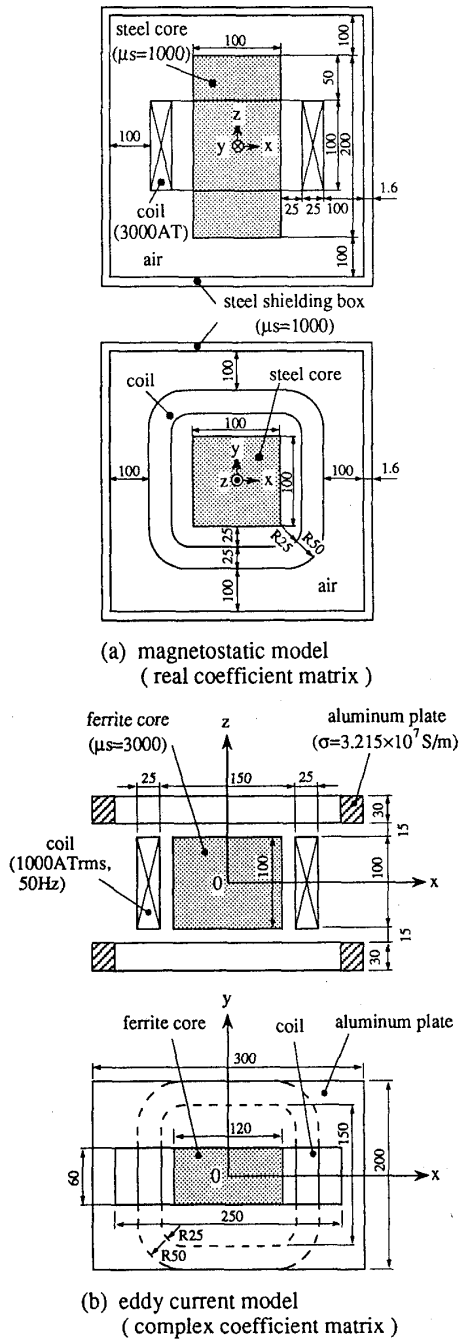


Fig.1 IEEJ standard benchmark models.

Table I shows the discretization data for the case using the brick element and without the gauge condition. The number of unknowns for the edge element is nearly the same as that for the nodal element. However, the number of non-zero entries in the original coefficient matrix H for the edge element is much less than that for the nodal element. The number of non-zero entries in E with $\gamma = 1$ defined in (1) and the size of profile are also shown in Table I. They are discussed in the next section.

B. Investigation of Renumbering Method

1) Distribution of non-zero entries in coefficient matrix: Fig.2 shows the distribution of non-zero entries obtained by various renumbering methods for the magnetostatic model discretized by the brick edge element. A non-zero entry is illustrated by a dot (·) symbol. REG and RAN mean that the unknown variables are renumbered regularly and at random. REG is available for only the regularly subdivided mesh. RCM and GPS mean the reverse Cuthill-McKee and Gibbs-Poole-Stockmeyer renumbering algorithms [4,5] were used

Table I Discretization data

model	magnetostatic		eddy current	
	edge	nodal	edge	nodal
number of elements	13,750		14,400	
number of nodes	15,548		16,275	
number of unknowns	39,072	38,496	41,060	42,885
number of non-zero entries in H	621,852	1,434,642	653,718	1,734,684
number of non-zero entries in E with $\gamma = 1$	RAN	1,427,148	3,700,806	1,493,876
	REG	799,950	1,760,485	842,514
	RCM	1,093,633	1,894,520	1,150,437
	GPS	875,701	1,721,295	921,045
size of profile	RAN	547,755,119	506,771,474	584,806,256
	REG	46,766,858	68,560,372	56,574,742
	RCM	83,517,245	97,494,507	78,214,869
	GPS	71,821,938	100,994,751	67,279,953

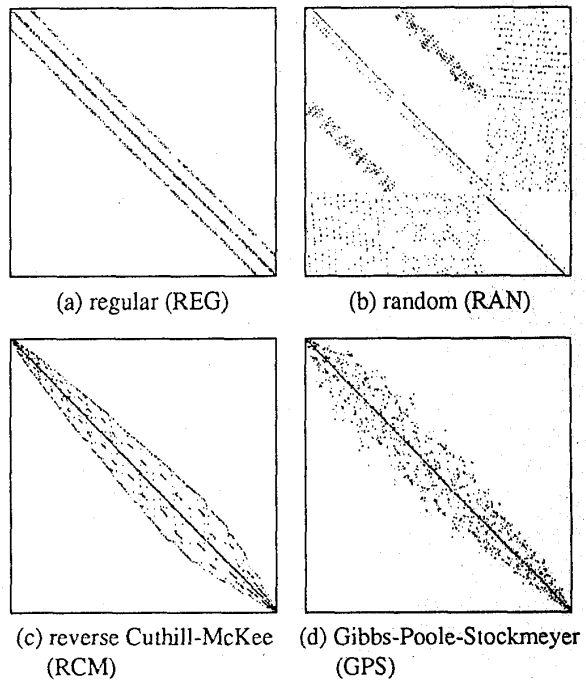


Fig.2 Positions of non-zero entries in coefficient matrix (magnetostatic model, edge element).

respectively. When RCM and GPS are applied, the non-zero entries are concentrated around diagonal entries. In the case of the eddy current model, a similar distribution is obtained. The nodal element also gives a similar distribution.

The number of non-zero entries in the original coefficient matrix H shown in Table I is identical for all renumbering methods. The size of the profile, which is defined as the summation of the half bandwidth of each row, is different for each renumbering method. When a direct solver such as the Gaussian elimination method is applied, the size of the matrix H is approximately equal to that of the profile. Therefore, the direct solver requires an extremely large memory space compared with the ICCG solver.

2) *Effect of renumbering methods on convergence characteristic:* Fig.3 shows the effect of the renumbering methods on the number of iterations for the ICCG method. The acceleration factor γ of 1.2 is used, which is discussed in the next section. The number of iterations using RCM and GPS is reduced by about 40% compared with that using RAN, and are nearly the same as that using REG. The reason is, as shown in Table I, the number of non-zero entries in the matrix E , which describes the difference between the incomplete and complete decompositions and corresponds to the number of fill-ins, are much less for REG, RCM and GPS than for RAN.

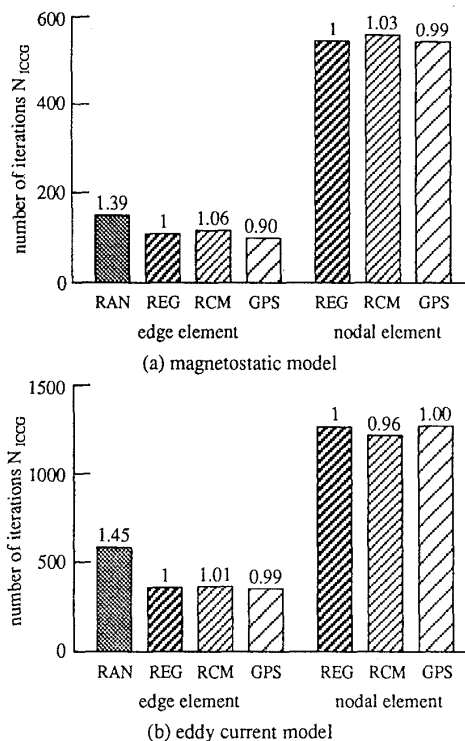


Fig.3 Effect of renumbering method ($\gamma = 1.2$).

Table II CPU time (s) for renumbering and ICCG method ($\gamma = 1.2$)

model	magnetostatic		eddy current		
	edge	nodal	edge	nodal	
renumbering	RCM	3.9	8.6	4.1	9.2
	GPS	4.8	9.6	5.1	10.3
ICCG	RCM	87.1	686.5	542.4	3420.7
	GPS	77.2	679.7	531.3	3605.7

Table II shows the CPU times for the renumbering method and the ICCG solver. As much CPU time is required to find a starting node in the original RCM [4], a technique developed in GPS [5] is adopted to find the starting node quickly. The CPU time for the renumbering method is negligibly small compared with that for the ICCG solver. Therefore, it may be concluded that the renumbering is effective to use with the ICCG solver.

C. Investigation of Acceleration Factor

1) *Determination of acceleration factor:* Fig.4 shows the number of iterations N_{ICCG} for the ICCG method. The optimum value γ_{opt} of γ , which minimizes N_{ICCG} , strongly depends on the type of element used. When γ is less than γ_{opt} , N_{ICCG} is greatly increased. Therefore, the conventional incomplete decomposition ($\gamma=1$) should not be used.

Fig.5 shows the objective function W defined in (2). The W - γ curves have forms similar to the N_{ICCG} - γ curves shown in Fig.4. The W - γ curves, however, are not enough to estimate γ_{opt} , because in the case of the nodal element, a great number of iterations is needed for γ which minimizes W as shown in Fig.4.

The maximum value $(L_{ii})_{max}$ of the diagonal entries in L is shown in Fig.6. The γ which minimizes $(L_{ii})_{max}$ is nearly the same as γ_{opt} . Therefore, γ_{opt} can easily be determined by finding the minimum value of $(L_{ii})_{max}$.

2) *Effect of acceleration factor on convergence characteristic:* Fig.7 shows the effect of the gauge conditions on the number of iterations. The magnetostatic model is analyzed using RAN and REG methods, shown in Fig.2. In the case without gauge, $\gamma=1$ with RAN gives the converged result shown in Fig.7(a). In the case with gauge, however, both renumbering methods fail to provide convergent solutions at $\gamma=1$, as shown in Fig.7(b).

Fig.8 shows the effect of the types of elements on the number of iterations. Tetrahedral and brick nodal elements are

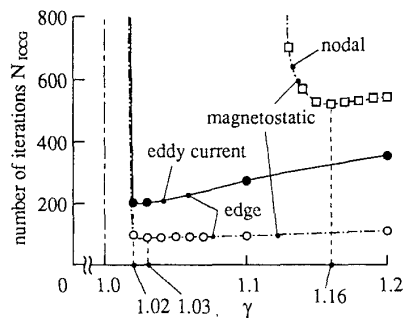


Fig.4 Number of iterations for ICCG method (REG).

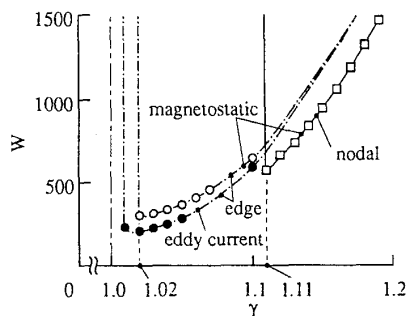


Fig.5 Error index W (REG).

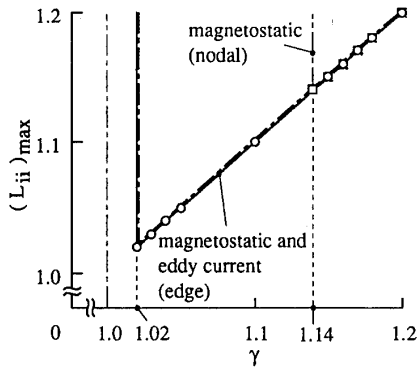


Fig. 6 Maximum value among diagonal entries in lower triangular matrix (REG).

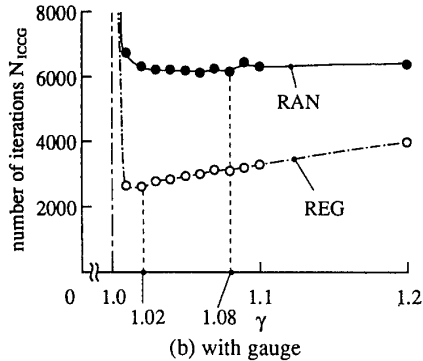
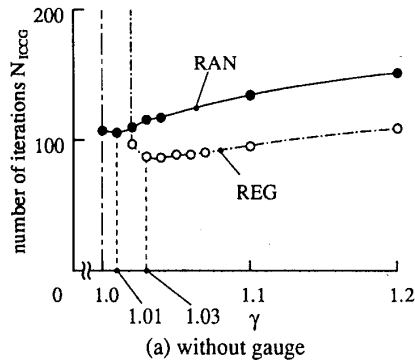


Fig. 7 Effect of gauge conditions on number of iterations for ICCG method (magnetostatic model, edge element).

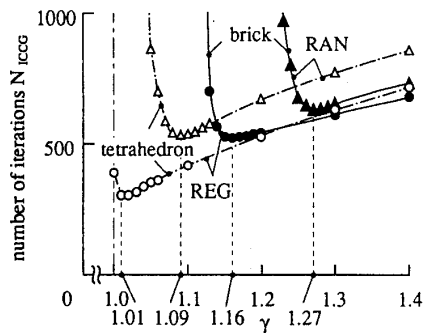


Fig. 8 Effect of types of elements on number of iterations for ICCG method (magnetostatic model, nodal element).

compared. The unknown variables for both elements are the same because the tetrahedral mesh is generated by subdividing a brick into six tetrahedrons. γ_{opt} depends on the types of elements and the renumbering methods.

IV. CONCLUSIONS

In order to accelerate the convergence characteristic of the ICCG solver, improvements by renumbering and the acceleration factor were investigated. The results obtained are summarized as follows:

- (1) As the renumbering can decrease the solution time, it is recommended to execute the renumbering before solving problems.
- (2) The acceleration factor is robust and gives a good convergence characteristic, and its optimum value can be easily determined.

REFERENCES

- [1] J.A. Meijerink and H.A. van der Vorst, "An iterative solution method for linear systems of which the coefficient matrix is a symmetric M -matrix," *Math. Comp.*, vol. 31, no. 137, pp. 148-162, January 1977.
- [2] D.S. Kershaw, "The incomplete Cholesky-conjugate gradient method for the iterative solution of systems of linear equations", *J. Comp. Phys.*, vol. 26, pp. 43-65, 1978.
- [3] S.R.H. Hoole, Z.J. Cendes and P.R.P. Hoole, "Renumbering and preconditioning in the conjugate gradients algorithm," *Computational Electromagnetics*, Elsevier, pp. 91-99, 1986.
- [4] E. Cuthill and J. McKee, "Reducing the bandwidth of sparse symmetric matrices," *Proc. ACM National Conference*, Association for Computing Machinery, pp. 157-172, 1969.
- [5] N.E. Gibbs, W.G. Poole, Jr and P.K. Stockmeyer, "An algorithm for reducing the bandwidth and profile of a sparse matrix," *SIAM J. Numer. Anal.*, vol. 13, no. 2, pp. 236-250, April 1976.
- [6] T.A. Manteuffel, "An incomplete factorization technique for positive definite linear systems," *Math. Comp.*, vol. 34, no. 150, pp. 473-497, April 1980.
- [7] P.J. Leonard and D. Rodger, "Finite element scheme for transient 3D eddy currents," *IEEE Trans. Magn.*, vol. 24, no. 1, pp. 90-93, January 1988.
- [8] R. Albanese and G. Rubinacci, "Numerical procedures for the solution of nonlinear electromagnetic problems," *ibid.*, vol. 28, no. 2, pp. 1228-1231, March 1992.
- [9] T. Nakata, N. Takahashi and K. Fujiwara, "3-D finite element analysis of magnetic fields of IEEJ model," *Electromagnetic Fields in Electrical Engineering*, International Academic Publishers, pp. 285-288, 1989.
- [10] T. Nakata, N. Takahashi, K. Fujiwara and P. Olszewski, "Verification of softwares for 3-D eddy current analysis using IEEJ model," *Advances in Electrical Engineering Software*, Springer-Verlag, pp. 349-360, 1990.

Koji Fujiwara (M'90) was born in Hiroshima Prefecture, Japan, in 1960. He received the B.E. and M.E. degrees in electrical engineering from Okayama University in 1982 and 1984 respectively.

From 1985 to 1986, he was with Mitsui Engineering and Shipbuilding Co., Ltd. Since 1986, he has been an Assistant Professor at the Department of Electrical Engineering, Okayama University. His major fields of interest are the applications of the 3-D finite element method to electromagnetic field computations and the acceleration of solvers for large scale simultaneous equations.

Takayoshi Nakata (M'72, SM'91) was born in Ehime Prefecture, Japan, in 1930. He received the B.E. and Ph.D. degrees in electrical engineering from Kyoto University in 1953 and 1971 respectively.

From 1953 to 1962, he was with Fuji Electric Manufacturing Co., Ltd., where he was engaged as a design and development engineer of large transformers. Since 1963, he has been a Professor at the Department of Electrical Engineering, Okayama University. His major fields of interest are the applications of the finite element method to electrical machines and electronic instruments, magnetic characteristics of transformer cores and magnetic measurements.

Dr. Nakata was awarded the 1983 Book Award, the 1985 Paper Award and the 1989 Electric Power Award of the Institute of Electrical Engineers of Japan. He established the IEEE Magnetics Society's Tokyo Chapter in 1977. He is a member of the international steering committee of the COMPUMAG conference and a member of the working group on recommended practices for field computation and analysis in electric machinery of the IEEE Power Engineering Society.

Hirotsugu Fusayasu was born in Tottori Prefecture, Japan, in 1967. He received the B.E. and M.E. degrees in electrical engineering from Okayama University in 1990 and 1992 respectively.

Since 1992, he has joined Matsushita Electric Industrial Co., Ltd.