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H. Zabel I. K. Robinson (Eds.)

# Surface X-Ray and Neutron Scattering

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# Analytical Calculation of the Resolution Correction Function for X-Ray Surface Structure Analysis at High Exit Angles

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**Abstract.** The analysis of rod scans in surface x-ray diffraction provides information about structure parameters normal to the sample surface. In order to achieve high resolution the measurements have to extend to momentum transfers  $q_z$  as large as possible. The proper correction of the measured intensity data for the resolution function of the detector is a prerequisite for obtaining reliable structure information. We have developed an analytical expression for the resolution correction of rod scan intensity data which take into account an anisotropic detector resolution  $T(\Theta, \Phi)$ , the domain size of the sample,  $\zeta$ , and the primary beam divergence parallel to the sample surface  $\Delta\tau$ .

## 1. Introduction

Glancing incidence angle x-ray scattering is now a well established technique for surface structure analysis [1,2]. So far work has been concentrated on measurements of 'in plane' data providing only the projection of the structure. In order to obtain information about the structural parameters normal to the sample surface, measurements along the reciprocal lattice rods up to high momentum transfer  $q_z = \ell \cdot c^*$  have to be performed. However, in all diffraction experiments the measured intensities have to be corrected for the instrumental resolution. For in plane structure analysis this is simply done by multiplying the intensity by a factor  $\Delta q_z$  corresponding to the length of the rod accepted by the detector [1,2].

The correction factors become complicated for rod scans, when the scattering plane is no longer parallel to the sample surface. In the following we shortly outline the intensity correction due to the detector resolution for our z-axis diffractometer with two independent detector angles. Subsequently we discuss the results by considering different detector arrangements, where the primary beam divergence and the finite domain size of the sample are taken into account.

## 2. Calculation

Experimentally, the integrated intensity is measured by rotating the sample around the surface normal keeping the detector at a fixed position out of plane. In Fig.1 this procedure is shown in projection to the  $\ell=0$  plane when the reciprocal lattice rod is swept through the detector's aperture. The integrated intensity is given by the convolution of the reflectivity with the transmission function:

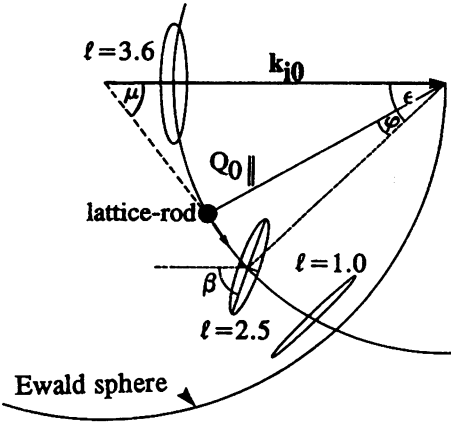


Fig. 1: Projection of the diffraction geometry on the  $l=0$  plane, illustrating the measurement of the integrated intensity. The sample is rotated around the surface normal. Diffraction is obtained when the rod intersects the detector aperture. The angular range of  $\varphi$  where the rod remains within the detector changes at different  $l$  values. The measured intensities must therefore be corrected due to the different shapes of the resolution ellipse.

$$E(Q_0) \propto \iiint i(k_i - k_{i0}) \cdot |F(q)|^2 \cdot T(q - Q_0 - \Delta Q_1(k_i - k_{i0}) - \Delta Q_2(\varphi)) dq^3 dk_i^3 d\varphi \quad (1)$$

In Eq. 1  $i(k_i - k_{i0})$  describes the intensity distribution in the primary beam around the incident beam  $k_{i0}$ . Gaussian functions are assumed for the primary beam intensity distribution  $i$ , the transmission function  $T$  and the rod profile parallel to the surface  $|F(q)|^2$ . The parameters  $q$  and  $Q_0$  represent vectors in reciprocal space, the latter indicates the reflection under consideration. The primary beam divergence and the rotation angle  $\varphi$  of the crystal are taken into account by the arguments  $\Delta Q_1(k_i - k_{i0})$  and  $\Delta Q_2(\varphi)$ . The calculation is based on three assumptions: (1) a grazing incidence geometry is used, (2) the radiation is strictly monochromatic and (3) the lateral extensions of the reciprocal lattice rod and the detector acceptance are small as compared to the radius of the Ewald sphere. The analytic solution of Eq. (1) is simple but tedious and will be described elsewhere [3]. Finally we are left with an expression  $E(Q_0) \propto |F(Q_0)|^2 \cdot L(Q_0)$ , where

$$L(Q_0) = \frac{\lambda \cdot \Delta\theta \cdot \Delta\phi}{d^{1/2} \cdot a \cdot b \cdot |Q_0|} \{ 1 + m \cdot \Delta\tau^2 \cdot \Gamma^2 + m/\zeta^2 \}^{-1/2} \quad (2)$$

indicates the Lorentz factor which describes the dependence of the integrated intensity on pure geometric parameters, particularly on the acceptance angles of the detector  $\Delta\theta$  and  $\Delta\phi$ . The parameters  $d$ ,  $m$  and  $\Gamma$  are given by

$$c = \cos(\beta - \epsilon) \cdot \cos(\beta - \epsilon) \cdot (1/a^2 - 1/b^2) \quad (3)$$

$$d = (\sin(\beta - \epsilon))^2 / a^2 + (\cos(\beta - \epsilon))^2 / b^2 \quad (4)$$

$$e = (\cos(\beta - \epsilon))^2 / a^2 + (\sin(\beta - \epsilon))^2 / b^2 \quad (5)$$

$$m = \lambda^2 \cdot (e - c^2/d) \quad [ \text{\AA}^2 ] \quad (6)$$

$$\Gamma = (\cos \mu) / \lambda - |Q_{0\parallel}| \cdot \cos(\mu + \epsilon), \quad [ \text{\AA}^{-1} ] \quad (7)$$

where  $a/\lambda$  and  $b/\lambda$  [  $\text{\AA}^{-1}$  ] are the short and the long axis of the projected resolution ellipse, respectively (Fig. 1) and  $\mu$  is the projection of the scattering angle to the surface. The angles  $\beta$  and  $\epsilon$  are explained in Fig. 1. The Lorentz factor given by Eq. (2) is composed of two terms, the first representing the intensity correction assuming  $\delta$ -function like lattice rods and strictly parallel incident radiation, the second (under the square root) takes account for the domain size,  $\zeta$ , and the primary beam divergence  $\Delta\tau$ . In the low exit angle regime ( $\ell \leq 1$ ) the correction calculated from Eq. (1) agrees with the published formula [1,2], provided that the domain size  $\zeta$  is large and the primary beam is parallel ( $\Delta\tau=0$ ).

### 3. Results and Discussion

In order to elucidate the different factors contributing to the intensity corrections we have calculated  $L(\ell)$  for the (1/2 1/2) and (3/2 5/2) superlattice reflection rod of the Ge(001)(2x1) structure assuming a wavelength of  $\lambda=1.54 \text{\AA}$ . The results are shown in Fig. 2. In order to maximize the intensity at low  $\ell$  it is evident that the detector has to be aligned with a high acceptance parallel to the rods. However, the situation changes at intermediate and high  $\ell$ , where the intersection of the lattice rod with the Ewald sphere crosses the detector transmission increasingly oblique to the long axis. Under these conditions it is preferable to rotate the detector by  $90^\circ$ , as displayed in Fig.1. Additionally, the dependence on  $Q_{0\parallel}$  results in an about four times larger intensity of the (1/2 1/2  $\ell$ ) as compared with the (3/2 5/2  $\ell$ ) reflections for  $\ell \leq 1$ .

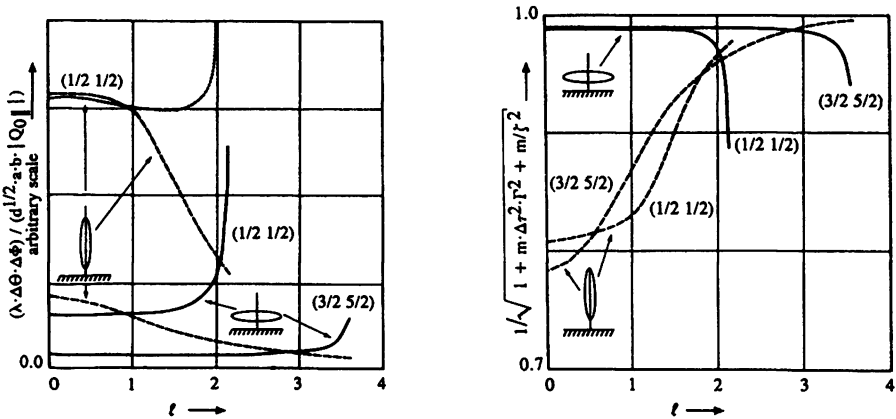


Fig. 2: Lorentz factor as a function of  $\ell$  for both detector settings (solid and dashed line) assuming parallel primary beam and  $\delta$ -like rods (left panel). The detector acceptance angles are  $0.4^\circ$  and  $2.0^\circ$ . The dotted line indicates the resolution correction for the (1/2 1/2) rod as given by ref. [2]. The right panel shows the  $\ell$ -dependence of the correction term in Eq. 2 for a domain size  $\zeta$  of  $500 \text{\AA}$  and a beam divergence  $\Delta\tau$  of  $0.23^\circ$ .