

THE STRUCTURAL BEHAVIOUR OF PRECAST LIGHTWEIGHT FOAMED
CONCRETE SANDWICH PANEL AS A LOAD BEARING WALL

NORIDAH BINTI MOHAMAD

A thesis submitted in fulfillment of the
requirements for the award of the degree of
Doctor of Philosophy (Civil Engineering)

Faculty of Civil Engineering
Universiti Teknologi Malaysia

JUNE 2010

ABSTRACT

Affordable quality housing is vital in developing countries to meet its growing population. Development of a new cost effective system is crucial to fulfill these demands. In view of this, a study is carried out to develop a Precast Lightweight Foamed Concrete Sandwich Panel (PLFP), as a new affordable building system. Experimental investigation and finite element analysis to study the structural behaviour of the PLFP panel under axial load is undertaken. The panel consists of two foamed concrete wythes and a polystyrene insulation layer in between the wythes. The wythes are reinforced with high tensile steel bars and tied up to each other through the polystyrene layer by steel shear connectors bent at an angle of 45°. The panels are loaded with axial load until failure. The ultimate load carrying capacity, load-lateral deflection profile, strain distributions, and the failure mode are recorded. Partial composite behaviour is observed in all specimens when the cracking load is achieved. Finite element analysis is also carried out to study the effect of slenderness ratio and shear connectors which are the major parameters that affect the strength and behaviour of the panels. An empirical equation to predict the maximum load carrying capacity of the panels is proposed. The PLFP system proposed in this research is able to achieve the intended strength for use in low rise building. Considering its lightweight and precast construction method, it is feasible to be developed further as a competitive IBS building system.

ABSTRAK

Perumahan yang berkualiti dan mampu dimiliki adalah perlu untuk negara yang sedang membangun bagi menampung jumlah penduduk yang kian bertambah. Penghasilan sistem baru yang lebih ekonomi adalah sangat diperlukan bagi memenuhi keperluan ini. Oleh itu, kajian telah dijalankan bagi menghasilkan panel pratuang sanwic yang diperbuat dari konkrit berbuisa foam (PLFP), sebagai sistem bangunan baru yang mampu dimiliki. Penyiasatan eksperimen dan analisis unsur terhingga bagi mengkaji kelakuan struktur panel PLFP yang dikenakan beban paksi telah dijalankan bagi tujuan ini. Panel ini terdiri daripada lapisan perangkap haba iaitu polisterin yang terletak diantara dua lapisan dinding konkrit berbuisa foam. Lapisan dinding dikuatkan dengan besi bertegangan tinggi yang diikat kepada besi penyambung ricih yang dibengkokkan 45° dan merentasi lapisan polisterin. Panel dibebankan dengan beban paksi sehingga gagal. Keupayaan maksima menanggung beban, profil hubungan beban dan pesongan sisi, penyebaran keterikan dan mod kegagalan telah direkodkan. Kelakuan komposit separa dapat dilihat dalam semua spesimen apabila ia mula mengalami retakan. Analisis unsur terhingga dijalankan bagi menentukan pengaruh nisbah kelangsingan dan penyambung ricih yang merupakan parameter utama yang mempengaruhi kekuatan dan kelakuan panel. Persamaan empirikal diterbitkan bagi menentukan keupayaan menanggung beban maksima panel. Sistem panel PLFP yang dicadangkan dalam kajian ini mampu mencapai kekuatan yang diinginkan bagi kegunaan di dalam bangunan rendah. Memandangkan panel ini ringan dan menggunakan kaedah pembinaan pratuang, ia boleh dibangunkan lagi kerana ia berpotensi sebagai sistem bangunan IBS yang berdaya saing.

TABLE OF CONTENTS

CHAPTER	TITLE	PAGE
	DECLARATION	ii
	ACKNOWLEDGEMENT	iii
	ABSTRACT	iv
	ABSTRAK	v
	TABLE OF CONTENTS	vi
	LIST OF TABLES	x
	LIST OF FIGURES	xiii
	LIST OF ABBREVIATIONS	xxii
	LIST OF SYMBOLS	xxiii
	LIST OF APPENDICES	xxvi
1	INTRODUCTION	
	1.1 Construction Industry in Malaysia	1
	1.2 Precast Concrete Building System	3
	1.3 Precast Sandwich Panel	6
	1.4 Lightweight Foamed Concrete	8
	1.4.1 Materials	9
	1.4.2 Characteristic properties of foamed concrete	9
	1.4.3 Advantages of Foam Concrete	10
	1.5 Precast Lightweight Foamed Concrete Sandwich Panel, PLFP	11
	1.6 Problem Statement	12
	1.7 Objectives	12
	1.8 Scope of Work	13
	1.9 Thesis Layout	14
2	LITERATURE REVIEW	
	2.1 Introduction	16
	2.2 Review of Past Studies on Sandwich Panel	19

2.2.1	Materials	20
2.2.2	Structural Behaviour of Sandwich Panel	27
2.2.3	Lightweight Sandwich Panel	37
2.4	Foamed Concrete Fabrication	46
2.5	Precast Concrete Sandwich Panel as Structural Wall Elements	55
2.6	Finite Element Analysis	61
2.7	Conclusion	66
3	EXPERIMENTAL PROGRAMME	
3.1	Introduction	68
3.2	Preliminary Experimental Investigation	69
3.2.1	Materials and Fabrication of Test Specimens	69
3.2.2	Test Set-up and Procedure	82
3.2.3	Preliminary Experimental Results	88
3.2.4	Observations and Further Enhancements	91
3.2.5	Discussion	94
3.3	Actual Experimental Programme	95
3.3.1	Materials and Fabrication of Test Specimens	97
3.3.2	Test Set-up and Procedure	107
3.4	Conclusion	110
4	EXPERIMENTAL RESULTS AND ANALYSIS	
4.1	Introduction	113
4.2	Objectives	114
4.3	Experimental Results	116
4.3.1	Ultimate Strength Capacity	116
4.3.2	Crack Pattern and Mode of Failure	119
4.3.3	Load-horizontal deflection Profile	124
4.3.4	Load-Strain Relationship	131
4.4	Conclusion	140
5	FINITE ELEMENT METHOD	
5.1	Introduction	142

5.2	Objective	142
5.3	FEM Modeling	143
5.3.1	Elements Used in FEM Modeling	143
5.3.2	Material Model	146
5.4	Validation of the Finite Element Model	151
5.5	Parameters of Study	154
5.6	FEM Results	
5.6.1	Crack Pattern	155
5.6.2	Load-lateral deflection Profiles	159
5.6.3	Load-strain relationship	163
5.6.4	Strain Distribution across Panel's Thickness	164
5.6.5	Optimum Diameters of Shear Truss Connectors	165
5.6.6	Effects of Symmetrical Orientation of Shear Truss Connectors	170
5.6.7	Effects of Various Heights and Overall Thickness of Panel	174
5.7	Conclusion	181
6	RESULTS AND DISCUSSION	
6.1	Introduction	182
6.2	Lightweight Foamed Concrete Mixture For PLFP Panel with Strength of 17 MPa	183
6.3	PLFP Panel for Testing Under Axial Load	185
6.4	The effects of Slenderness Ratio	185
6.5	The effectiveness of shear connector and the extent of composite behaviour achieved	192
6.6	Suitability of PLFP Panel as Load Bearing Wall in Low Rise Building	197
6.7	Mathematical Modeling	197
6.8	Conclusion	206
7	SUMMARY, CONCLUSION AND RECOMMENDATIONS	
7.1	Development of Precast Lightweight Foamed	

Concrete Sandwich Panel (PLFP)	209
7.1.1 Summary of the Development and construction of the sandwich PLFP panel using the lightweight foamed concrete	209
7.1.2 Conclusion	210
7.2 Development of Foamed Concrete Material	211
7.2.1 Summary of finding the right mixture for foamed concrete of sufficient strength	211
7.2.2 Conclusion	212
7.3 Structural Behavior of the PLFP	212
7.3.1 Summary of the experiment and FEM analysis	213
7.3.2 Conclusion	213
7.4 Semi empirical expression to estimate the load carrying capacity of the PLFP panel	214
7.4.1 Summary on the determination of the new empirical equation	214
7.4.2 Conclusion	215
7.5 Recommendations	215
REFERENCES	217
APPENDICES A-H	224

LIST OF TABLES

TABLE NO.	TITLE	PAGE
1.1	Housing Targets from the Public and Private Sector, 2006 to 2010 (Ministry of Housing and Local Government)	1
2.1	Measured Properties for FRC, PVC Foam and Balsa Core (Stoll F. et al., 2004)	23
2.2	Crack and Failure Loads for Panel Specimens (Benayoune et al., 2006)	31
2.3	Ultimate load and maximum deflection at mid-height in Panel Specimens (Mohammed and Nasim, 2009)	41
2.4	Typical mix details for foamed concrete (BCA, 1994)	53
2.5	Typical Properties of Foamed Concrete (BCA, 1994)	54
2.6	Comparison of ultimate loads (Sulaiman et al., 2008)	60
3.1	Dimension and Properties of Pilot Test Specimens	70
3.2	Ratio of material and characteristic properties for trial mix	74
3.3	Foamed Concrete Properties	78
3.4	Properties of Steel	78
3.5	Ultimate Strength Results of Pilot Test Specimens	89
3.6	Foamed Concrete Properties for Panels PLFP-5 and PLFP-6	93
3.7	Ultimate Strength Results of PLFP-5 and PLFP-6	94
3.8	Dimensions and details of specimens for actual experimental programme	96

3.9	Mixture Ratio for Casting of Foamed Concrete Panel	103
3.10	Foamed Concrete Properties	104
3.11	Mixture ratio for foamed concrete with strength 12 MPa to 17 MPa	110
4.1	Dimensions and Properties of PLFC Panel Specimens	115
4.2	Ultimate Failure Load for PLFC Panels	117
4.3	Crack Pattern and Mode of Failure for All Panels	121
4.4	Surface Strain Distribution	136
4.5	Maximum surface strain values from experiment	137
4.6	Maximum shear strain at mid-height of panel PA-7 to PA-14	140
5.1	Properties of Foamed Concrete used in the PLFP FE Model	147
5.2	Plastic Properties of Foamed Concrete Wythes	148
5.3	Properties of Steel used as Reinforcement and Shear Connectors in the PLFP Finite Element Model	149
5.4	Properties of Normal Concrete used in the PLFP FE Model	150
5.5	Ultimate Loads of PA-1 to PA-14 from experiment and FEM Analysis	153
5.6	First Crack Load and Failure Load of Panel PA-1 to PA-14 As Obtained From FEM	157
5.7	Crack Pattern for Various Slenderness Ratios	158
5.8	Ultimate strength, P_u , for panel PA-10 with various truss diameters	166
5.9	Comparison of ultimate load achieved for single and double shear truss connectors in panel PA-6	172
5.10	Effects of various height of panel on ultimate strength and	

	maximum lateral deflection	174
5.11	Ultimate load, deflection and strain distribution for various thicknesses of panel at mid-height	178
6.1	Ultimate Loads of PA-1 to PA-14 (Experimental, FEM and ACI318-89)	187
6.2	a) Ultimate Strength for Various Slenderness Ratio from Experiment	189
	b) Ultimate Strength for Various Slenderness Ratios from FEM Simulation	189

LIST OF FIGURES

FIGURE NO.	TITLE	PAGE
1.1	Precast Structure Systems (Bohdan, 1966)	
	a) Bearing Wall Structure	4
	b) Frame and skeletal Structure	4
1.2	Various types of architectural load-bearing wall panels (Freedman, 1999)	5
1.3	Typical Precast Concrete Sandwich Panel with Its Components	7
1.4	Precast Concrete Sandwich Panel in 3-D (Benayoune et al., 2006)	7
2.1	Types of Compositeness of pre-cast concrete sandwich panel (Shutt, 1997)	18
2.2	Honeycomb-cored sandwich panel (Jeom et al., 1999)	20
2.3	Foam board strip wrapped by E-glass fabric (Stoll et al., 2004)	21
2.4	Core Preform (Stoll et al., 2004)	22
2.5	Molded panel with foam removed, showing composite webs and resin ridge (Stoll et al., 2004)	22
2.6	EPS Embedded With Trusses (Lee et al., 2006)	24
2.7	Cellulose Fiber Cement Board Panel (Lee et al., 2006)	25
2.8	Fiber-reinforced Composite Panel (Lee et al., 2006)	25

2.9	Floor and wall sandwich panels used in the panelized building model (Rizzo et al., 1979)	27
2.10	Half-scale sandwich panel building model (Rizzo et al., 1979)	28
2.11	Critical b/t ratios of profiled sandwich panel for local buckling (Pokharel and Mahendran, 2003)	29
2.12	Typical failure modes (a) local buckle (b) local plastic mechanism (Pokharel and Mahendran, 2003)	30
2.13	Influence of slenderness ratio on ultimate load (Benayoune et al., 2006)	32
2.14	Loading set up for walls (Pillai and Parthasarathy, 1977)	33
2.15	Comparison of load capacities of wall as obtained from experiment and theory (Pillai and Parthasarathy, 1977)	34
2.16	Details of truss girder connectors (Bush and Stine, 1994)	35
2.17	Diagonal Truss Connectors (Benayoune et al., 2006)	35
2.18	Front view and cross section of a multilayer wall specimen (Rosenthal, 1984)	38
2.19	Failure mode for Panel W1600 and W1400 (Sulaiman et al., 2009)	40
2.20	Applied Axial Load versus Displacement (Sulaiman et al., 2009)	40
2.21	Schematic diagram for Four-point bending test set-up (Mohammed and Nasim, 2009)	41
2.2.2	Schematic diagrams for the panels used in the experimental work (Mohammed and Nasim, 2009)	41
2.23	Comparison between AAC and FRP/AAC shear strength	

	(Mohammed and Nasim, 2009)	42
2.24	Shotcrete sandwich panel (Kabir, 2005)	42
2.25	Installed shotcrete sandwich panel (Rezaifar et al., 2008)	43
2.26	Dimensional view of the cross-section of the specimens (Memon et al., 2007)	45
2.27	Comparison of various properties of sandwich composite with control (Memon et al., 2007)	45
2.28	Failure mode of various specimens after tests (Memon et al., 2007)	46
2.29	Young Modulus versus Density (Tonyan and Gibson, 1992)	48
2.30	Compressive strength versus Density (Tonyan and Gibson, 1992)	48
2.31	Variation of flow of foam concrete with foam cement (Nambiar and Ramamurthy, 2006)	49
2.32	Strength density variation for mixes with sand of different fineness (Nambiar and Ramamurthy, 2006)	50
2.33	Strength density variation for mixes with different filler type (Nambiar and Ramamurthy, 2006)	50
2.34	Cross-sectional Dimensions of Test Specimens: (a) Concrete-filled CHS (b) Concrete-filled SH (Yasser, 1997)	51
2.35	Details of Loading System for Beam Specimens (Yasser, 1997)	52
2.36	Relationship between 7-day compressive strength and dry density for foamed concrete (BCA, 1999)	54
2.37	Schematic diagram for testing (Pokharel N. et al.)	62
2.38	(a) Half-length FEM model (b) Buckling shape of panel	

	(Pokharel N. et al.)	63
2.39	Load-deflection curves for horizontal slab bending test	
	(Kabir, 2005)	64
2.40	Influence of shear connector's diameter on flexural loading	
	(Kabir, 2005)	64
2.41	Specimen model by FEM (Rezaifar et al., 2008)	66
3.1	Mild steel BRC mesh and the truss connectors placed in the steel	
	Formwork	72
3.2	Fine sand sieved from no. 5 sieve	73
3.3	Foam generator	76
3.4	Foam right after being discharged from the generator	76
3.5	Specimen positioned in a testing machine for split tensile test	77
3.6	Specimen positioned in UTM machine with attachment of	
	compressometer to determine the Modulus Young, E	77
3.7	(a) BRC and Shear Connectors placed horizontally in the	
	formwork	79
	(b) The polystyrene was cut and placed on top of the	
	lower wythe	79
	(c) Foamed concrete poured on the top of polystyrene layer as	
	the upper wythe	80
	(d) Finish of the PLFP panel specimen	80
3.8	Details of PLFP specimens for Pilot Test	81
3.9	Set-up of specimen and test frame	83
3.10	Magnus Frame	84
3.11	(a) Bottom end condition of panel (Detail A)	85

	(b) Top end condition for panel (Detail B) and arrangement for applying pure axial load	85
3.12	Locations of LVDT at middle front and rear surface of all panels	87
3.13	(a) Crushing and cracking at top part of panel PLFP-3	88
	(b) Crushing and cracking at bottom part of panel PLFP-3	88
3.14	Load-deflection profile for panels PLFP-1 to PLFP-4	90
3.15	Fabrication of Panel PLFP-5 and PLFP-6	
	(a) (b) and (c) Bars and links for the end capping	92
	(d) and (e) BRC and shear truss were placed in the formwork before foamed concrete for the bottom layer is poured	92
	(f) polystyrene were cut and placed on the bottom layer	92
	(g) top BRC was placed before the top concrete layer is poured	92
	(h) top layer of foamed concrete is poured	92
3.16	Failure mode in panel PLFP-5 and PLFP-6	93
3.17	Load-deflection profile for panels PLFP-5 and PLFP-6	94
3.18	(a) and (b): High tensile steel of 9 mm diameter bars reinforcement	98
3.19	Continuous truss-shaped connectors running the full height of the panels used to tie the lower and upper wythes	99
3.20	(a) Shear connectors for 100 mm thick PLFP panel	100
	(b) Shear connectors for 125 mm thick PLFP panel	100

	(c) Shear connectors for 200 mm thick PLFP panels	101
3.21	Details of PLFP panel with capping at both ends	102
3.22	Fabrication of panel PA-1 to PA-14 for experimental Programme	
	(a) & (b): Reinforcement and Shear Connectors placed in the formwork of the specimen with capping at both ends	106
	(c) Normal concrete capping	106
	(d) Casting of lower wythe	106
	(e) Finish of PLFP with capping a both ends	106
3.23	Locations of Strain Gauges	108
3.24	Locations of LVDT at top front surface of panels PA-10, PA-11, PA-13, and PA-14	109
4.1	Ultimate Strength versus Slenderness Ratio for Panels PA-1 to PA-14 for 6 mm and 9 mm shear connectors	118
4.2	Curve fitting line which fall between the curves for 6 mm and 9 mm shear connectors	119
4.3	Crack and crush at the top and bottom half of panel of panel PA-10	122
4.4	Crushing at mid-height of panel PA-9 due to buckling in the middle zone of panel	123
4.5	Crack and crush at mid-height of panel PA-12	123
4.6	Load-horizontal deflection curves at mid-height of panels	124
4.7	Deflection along the height of panel PA-10	129
4.8	Deflection along the height of panel PA-13	130
4.9	(a) Load-strain curves for panel PA-6 under axial load	132

	(b) Load-strain curve for PLFP panel PA-4	133
	(c) Load-strain curve for PLFP panel PA-14	134
4.10	Shear strain distribution across the mid-height of panel PA-10	138
4.11	Load versus Strain at mid-height of panel PA-9	139
4.12	Load versus Strain at mid-height of panel PA-12	139
5.1	2-D plane stress element model of PLFP panel	145
5.2	2-D plane stress element model of PLFP in which nodes on steel shear truss connectors and wythe surface met	146
5.3	Load-lateral deflection curve for panel PA-10 measured at mid-height	154
5.4	Crack pattern of Panel PA-6 at failure load	156
5.5	FEM Result of Load versus Lateral Deflection for Panels PA-1 to PA-14 at mid-height	160
5.6	Deflection of wythe in PLFP panel PA-10	161
5.7	Deflection along the height of panel PA-10 at ultimate load	162
5.8	Deflection along the height of panel PA-10 as obtained from experiment and FEM at ultimate load	163
5.9	Load versus surface strain at mid-height of panels PA-2, PA-5 and PA-9	164
5.10	Strain distribution across thickness of panels PA-2, PA-5 and PA-10 at mid-height at ultimate load	165
5.11	Ultimate load versus bar diameter for panel PA-10 with reinforcement size of 9 mm	167
5.12	Strain across the thickness of panel PA-10 at ultimate load	

	measured at mid-height as obtained from FE analysis	168
5.13	(a) Strain across thickness of Panel PA-10 at mid-height with truss diameter 9 mm at ultimate load	168
	(b) Strain across thickness of Panel PA-10 at mid-height with truss diameter 10 mm at ultimate load	169
	(c) Strain across thickness of Panel PA-10 at mid-height with truss diameter 12 mm at ultimate load	169
5.14	Symmetrical orientation of shear truss connectors	171
5.15	Strain distribution across panel thickness with shear connector's diameter of 10 mm measured at mid-height	173
5.16	Strain distribution across panel thickness with shear connector's diameter of 12 mm measured at mid-height	173
5.17	Ultimate Load (P_u) for various Height of Panel (H)	175
5.18	Maximum lateral deflection values for different height of panel	176
5.19	Strain distribution across the panel's thickness for various heights	176
5.20	Ultimate Load versus Thickness for Panel 2800 mm	179
5.21	Deflection versus Overall Thickness	179
5.22	Strain distribution across the panel's thickness for various overall thicknesses of panels at mid-height	180
5.23	Strain distribution across the panel's thickness for 110 mm overall thickness of panel at mid-height	180
6.1	Percentage difference between ultimate strength from experiment and FEM	188

6.2	Relationship between ultimate strength and slenderness ratio from experiment and FEM	190
6.3	Deflection of wythe in PLFP panels with different slenderness ratio	191
6.4	Strain distribution across the thickness of PLFP panel PA-5	194
6.5	Strain distribution across the thickness of panel PA-6	195
6.6	Stress-strain Curve for Steel	196
6.7	Ultimate strength vs slenderness ratio as obtained from experiment, FEM , Equation 6.2 and Equation 6.3	200
6.8	Comparison between ultimate strength from full-scaled test and using Equation 6.3	201
6.9	Comparison between ultimate strength from full-scaled test and using equation 6.4	202
6.10	Comparison between ultimate strength from experiment and using equation 6.5	204
6.11	Relationship between Ultimate Strength and Slenderness Ratio from Experiment, FEM, Equation 6.2, Equation 6.3 and Proposed Equation 6.5	205

LIST OF ABBREVIATION

CIDB	-	Construction Industry Development Board of Malaysia
IBS	-	Industrial Building System
PLFP	-	Precast Lightweight Foamed Concrete Sandwich Panel
FEM	-	Finite Element Method
PCSP	-	Precast Concrete Sandwich Panel
FRC	-	Fiber-Reinforced Composite
EPS	-	Expanded Polystyrene Panel System
PAC	-	Pumice Aggregate Concrete
HPC	-	High Performance Concrete
FRP	-	Fiber Reinforced Polymer
AAC	-	Autoclaved Aerated Concrete
BCA	-	British Cement Association
ASTM	-	American Standard Testing Method
BS	-	British Standard
UTM	-	Universal Testing Machine
E	-	Modulus Young
LVDT	-	Linear Voltage Displacement Transducer
ESG	-	Electrical Strain Gauge

LIST OF SYMBOLS

H	-	Height of panel
H/t	-	Slenderness ratio
EI	-	Stiffness
$E_c I_g$	-	Gross uncracked stiffness
P_u	-	Ultimate strength of panel
ϕ	-	Strength reduction factor
f_{cu}	-	Compressive strength of foamed concrete
A	-	Gross area of section
k	-	Slenderness Factor
t	-	Overall thickness of member
N	-	Ultimate axial load
N_{uz}	-	Design ultimate capacity
N_{bal}	-	Design axial load capacity for symmetrically reinforced rectangular section
k	-	Reduction Factor
A_{sc}	-	Area of steel
f_y	-	Tensile strength of steel
P_u	-	Ultimate axial load
A_c	-	Gross area of panel section
f_y	-	Yield strength of steel
L	-	Width of the panel

A_c	-	Gross area of the wall panel section (equal to the gross concrete area)
t_1	-	Thickness of wythe
t_2	-	Thickness of core layer
c	-	Concrete cover
f_t	-	Tensile Strength of foamed concrete
ε_c	-	Strain at peak uniaxial compression
ε_o	-	Strain at end of softening curve
G_f	-	Fracture energy per unit area
β_r	-	Biaxial to uniaxial stress ratio
Z_o	-	Initial relative position of yield surface
ψ	-	Dilatancy factor
m_g	-	Constant in interlock state function
m_{hi}	-	Contact multiplier on ε_o
m_{ful}	-	Final contact multiplier on ε_o
r_σ	-	Shear intercept on tensile strength
μ	-	Slope of friction asymptote for damage
σ_y	-	initial yield stress
Pt	-	Stress at ultimate
ε	-	Strain at Failure
E	-	Modulus Young of Steel
ρ_{wet}	-	Wet density of foamed concrete
ρ_{dry}	-	Dry density of foamed concrete
ν	-	Poisson's Ratio
α	-	Coefficient of thermal expansion

e - Eccentricity

LIST OF APPENDICES

APPENDIX	TITLE	PAGE
A	Foamed Concrete Properties	224
B	Steel Properties	232
C	Crack Pattern and Failure Mode for PLFP Panels	233
D	Load-Strain Graphs for PLFP Panels	242
E	Data for Deflection of PLFP Panels	256
F	Surface Strain Readings	265
G	Maximum Strain in Main Bar and Shear Connector	272
H	Calculation of Loading for 5-Storeys Residential Building	273

CHAPTER 1

INTRODUCTION

1.1 Construction Industry in Malaysia

Housing remains a major issue in Malaysia as in many other developing countries in the world. The problem is raised due to the increasing population, demands of affordable and quality houses, migration of rural masses into the city and industrial centers and also demands due to higher quality of life. The increase in housing demand during the Ninth Malaysia Plan (2006 to 2010) from the public and private sector is shown in Table 1.1. It is observed from this table that approximately 709,400 houses are targeted for different user-groups during the 5 years period.

Table 1.1: Housing Targets from the Public and Private Sector, 2006 to 2010
(Construction Industry Development Board, 2007)

<i>Programme</i>	<i>Number of houses</i>					<i>Total</i>	
	Housing for the poor (PPRT)	Low Cost	Medium Low Cost	Medium cost	High cost	Total units	%
Public sector	20,000	85,000	37,005	27,100	28,700	197,805	27.9
Private sector		80,400	48,500	183,600	199,095	511,595	72.1
Total	20,000	165,400	85,505	210,700	227,795	709,400	100.0
%	2.8	23.3	12.1	29.7	32.1	100.00	

It is difficult to provide solutions to this problem with the present traditional building construction systems because the traditional system is unable to meet the housing demand in a short time without sacrificing quality. Due to this inadequacy of traditional building construction systems, new technology is needed in the construction industries which can meet this requirement. Meeting the demands for higher performance, lower cost and faster projects requires transition from traditional building techniques to innovative construction methods.

Construction Industry Development Board of Malaysia, (CIDB), has produced a 10-year master plan for Malaysian construction industry for a period from 2006 to 2015. It is a comprehensive plan charting the strategic position and future direction of the Malaysian construction (CIDB, 2007). It is also aimed at supporting the nation's economic growth as well as increasing accessibility to adequate, affordable and quality houses for all income groups, particularly the lower ones.

The planning does not only focus on improving the living standard of Malaysians, but also on harvesting the development of caring society. There are seven strategic thrusts in the Master Plan which are inter-related and together serve to achieve the overall vision. The fifth strategic thrust in the Plan is innovation through research and development and adoption of new construction method. This thrust is aimed at addressing the polemic of the local construction industry which has been characterized as labour intensive and dependent on foreign unskilled workers. As such, the construction industry needs to progress towards one that is more focused in innovation.

Industrial Building Systems or IBS is one of the innovations and is seen as one solution in the development of new technology in the construction industries. IBS utilizes techniques, products, components, or building systems which involve prefabricated components and on-site installation. It has been in existence since the 1960's (Thanon *et al.*, 2003). However, according to the CIDB IBS Survey, less than one third of completed projects up to 2002 utilized IBS. IBS should be utilized more aggressively in the local industry because it helps to overcome problems imposed by the traditional labour intensive methods.

IBS promises numerous benefits compared to the conventional method. Its usage is usually more economical than the conventional construction system due to the following advantages (Junid, 1986, Esa and Nurudin, 1998, Lessing *et al.*, 2005):

- a) Standardization of sizes and materials allows faster and more accurate production with less waste.
- b) More accurate scheduling can be obtained because of more predictable production.
- c) The use of unskilled or semi skilled labour is possible by the simplicity and standardization of the construction technique.
- d) With the use of standardization of building components, the use of Information Technology (IT) in construction can further be enhanced. IT will speed up the networking between the consultants, architects, contractors and most importantly, the clients.

In general IBS construction method leads to increased efficiency and productivity. This chapter discusses precast lightweight sandwich technology as an IBS system that has great potential to be further studied and developed in Malaysian's construction industry.

1.2 Precast Concrete Building System

Precast building system is a system where parts, members and elements of structures are produced either on-site or at the factory, and transported to the site of construction. Using concrete material, the precast component may be cast in a formwork in a position other than the actual one. After the concrete has matured, the forms are removed and the component are installed and fixed in the actual position. The benefits of precast concrete as compared to conventional system include its better quality control and, fast delivery and installation. In most cases, precast panels are cast with high quality concrete and therefore results in smooth surface appearance.

The precast building systems are mainly categorized into load bearing wall structure system (Figure 1.1(a)), and frame and skeletal structure system (Figure 1.1(b)). The structural elements of load-bearing wall structure systems consist of load-bearing walls and floors while the structural elements of frame and skeletal structure systems consist of columns, beams and floors. The frame and skeletal structure systems are utilized mainly for industrial buildings, shopping malls, car parks, sporting facilities and office buildings, whereas the load-bearing wall structures are suitable for apartment buildings, nursing homes, dormitories, and hotels (Bohdan, 1966).

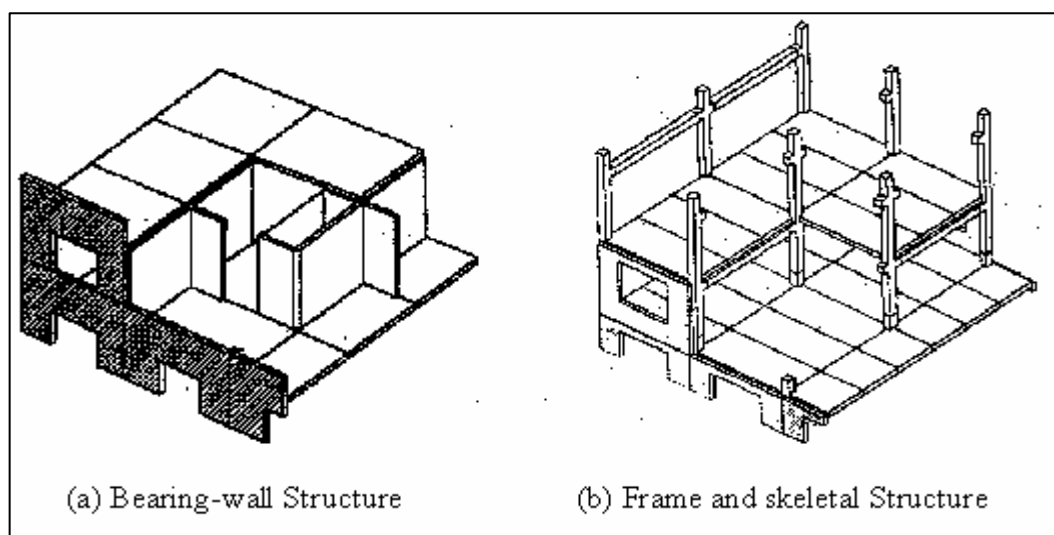
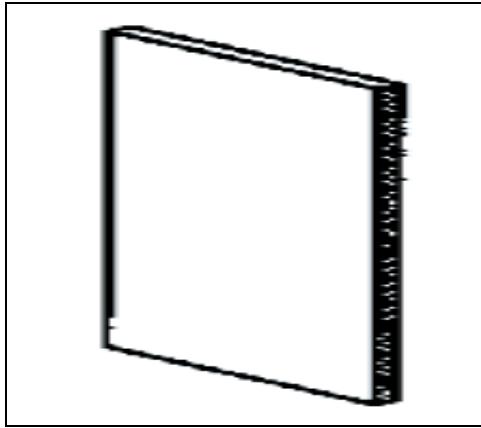
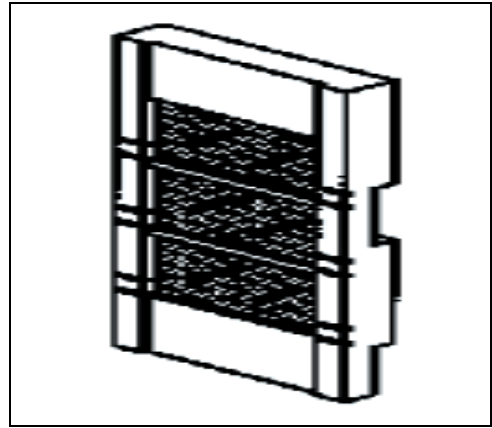


Figure 1.1: Precast Structure Systems (Bohdan, 1966)

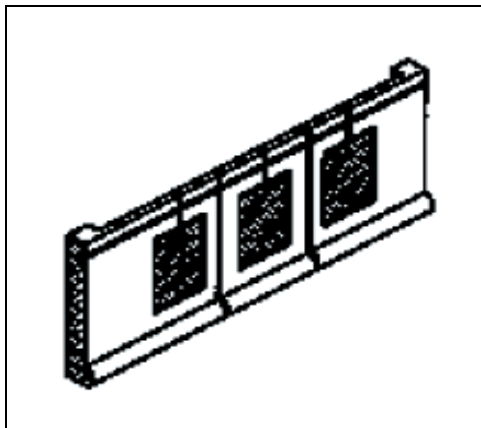
Wall element of a building can be constructed using precast system. A precast wall system can be comprised of flat or curved panels (solid, hollow-core, or insulated), window or mullion panels, ribbed panels, or a double-tee as shown in Figure 1.2. These precast elements are normally used as cladding material which is non-load bearing (Freeman, 1999). This is due to their structural capability as load bearing elements are often overlooked. For instance, in the case of low or medium rise buildings, the amount of reinforcements required in handling and erecting cladding panels such as wall and window panels are often more than necessary for carrying imposed loads. Thus, with relatively few modifications, these panels can function as load bearing members especially in the low to medium rise buildings.



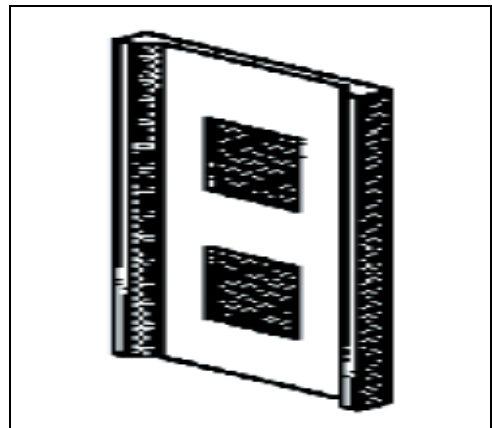
(a) Flat, hollow-core, or insulated panel



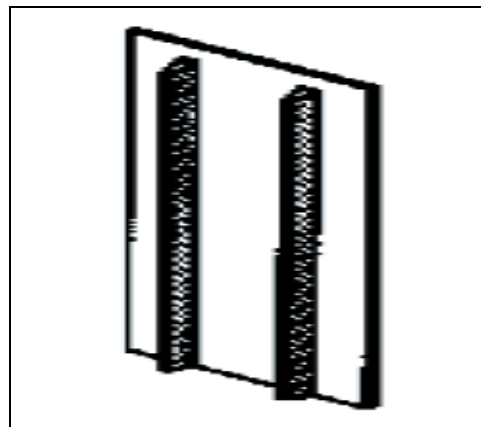
(b) Vertical window or mullion panel



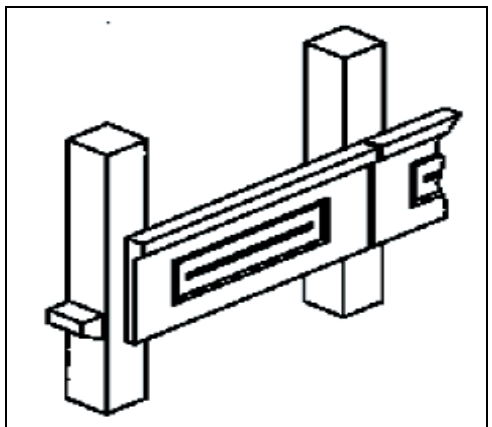
(c) Horizontal window or mullion panel



(d) Ribbed Panel



(e) Double-tee panel



(f) Spandrel

Figure 1.2: Various types of architectural load-bearing wall panels.

(Freeman, 1999)

1.3 Precast Sandwich Panel

Precast sandwich panel is a layered structural system composed of low density core material which acts integrally with the high strength facing material. Structures made of precast sandwich panels can be remarkably strong and lighter in weight. The trend for “stronger-lighter” product is becoming increasingly important in the construction industry.

Various forms of sandwich construction may be obtained by combining different wythe and core or insulation materials. The wythes may be constructed out of varieties of materials such as concrete, steel, aluminium, or carbon fiber material (Lee and Pessiki, 2006, Benayoune *et al.*, 2006, Liew and Sohel, 2009, Jeom *et al.*, 1999, Rice *et al.*, 2006). The core layers are often composed of lightweight concrete, fibre reinforced composite, balsa wood, foam, polymer foam and structural honeycomb material such a aluminium honeycomb concrete (Liew and Sohel, 2009, Jeom *et al.*, 1999, Stoll *et al.*, 2004, Scudamore and Cantwell, 2002). These materials can be combined to form composite panels which enable the optimum design to be produced for particular applications.

A typical concrete sandwich panel is shown in Figure 1.3. It consists of an insulation layer which is enclosed by inner and outer concrete wythes. The concrete wythes may be of a standard shape, such as a flat slab, hollow-core section or double tee. The wythes can be connected together using shear connectors through the insulation layer to promote composite action so that the system can be used as structural element. Figure 1.4 shows a typical 3-D view of sandwich panel with truss shaped shear connectors.

Structural sandwich panels provide the dual functions of transferring load and insulating the structure. They may be used solely for cladding, or they may act as beams, bearing walls, or shear walls. Interest in sandwich panels as load-bearing wall panels has been growing over the past few years because manufacturers are looking for more viable products and are pleased with their structural efficiency, insulation property, light weight and aesthetics values. Sandwich panels are similar to other precast concrete members with regard to design, detailing, manufacturing, handling,

shipping and erection; however, because of the presence of insulation layer, they do exhibit some unique characteristics and behavior.

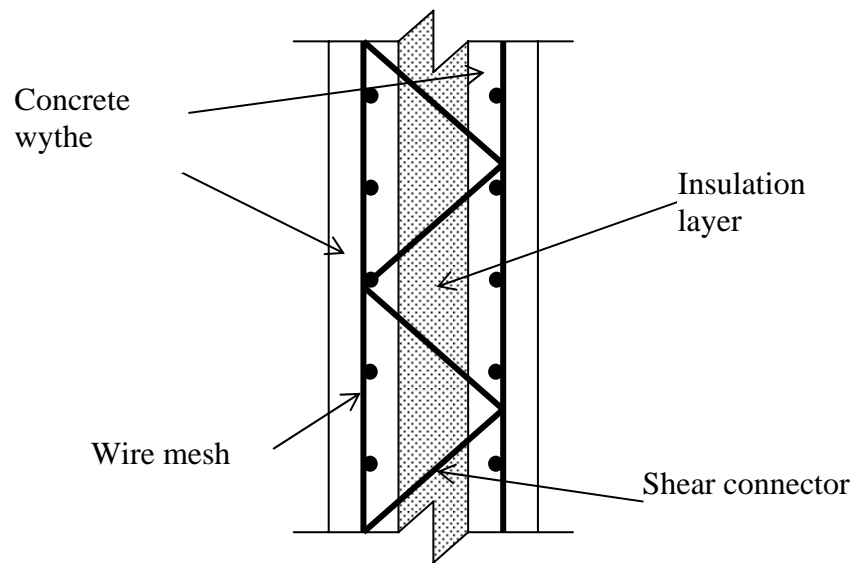


Figure 1.3: Typical Precast Concrete Sandwich Panel with Its Components

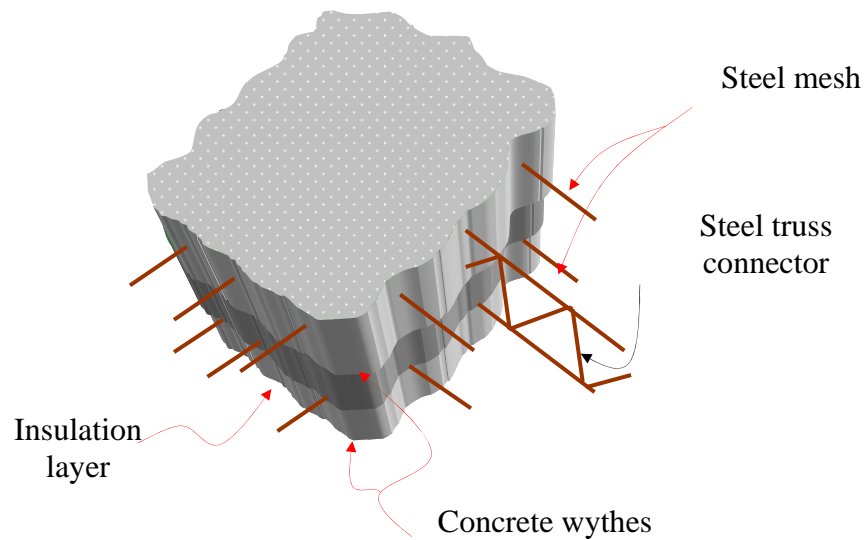


Figure 1.4: Precast Concrete Sandwich Panel in 3-D
(Benayoune *et al.*, 2006)

1.4 Lightweight Foamed Concrete

Foamed concrete has been widely used especially in the western countries. It is originated from Scandinavia some thirty years ago. Nowadays, foam concrete technology has been widely used in construction industries. It is considered as an attractive material for its lightweight, better thermal properties and ease of construction. In the United States for instance, foamed concrete are used in an increasing number of applications. Cast-in-place foamed concrete are used for insulating roof-deck systems and for engineered fills for geotechnical applications while precast auto-claved products are widely used as load-bearing blocks, reinforced wall, roof and floor units and as non load-bearing cladding panels over a primary structural frame (Tonyan and Gibson, 1992).

Foam concrete is a low density hardened Portland cement paste, containing a large number of small bubbles. Cement foam can be manufactured either by a chemical or a mechanical foaming process. In the chemical process, a powdered metal (usually aluminum) is added to slurry composed of cement and lime. Most of the aerated concrete produce with this method have densities between 480 and 960 kg/m³ (Tonyan and Gibson, 1992).

In a mechanical foaming process, foaming agent is added into the cement slurry either directly or in a form of perform foam. The presence of cement causes the material to be cohesive after the hydration of the cement. The entrapped air bubbles increases the volume and thereby reduces the densities of a concrete. This volume between the slurry and the foam determine the density of the foam concrete. The preform foam provides better control of density and foam cell structure. The foamed concrete's materials and characteristic properties are described in the following sections. In both the chemical and mechanical processes described above, the cement foam is usually cured in a moist environment at ambient temperature.

1.4.1 Materials

Foam concrete is a mixture of cement, fine sand, water and special foam, which produces a strong, lightweight concrete containing millions of evenly distributed and consistently sized air bubbles or cells. The density of foam concrete is determined by the amount of foam added to the basic cement, sand and the water mixed together.

1.4.2 Characteristic properties of foamed concrete

The characteristic properties of foamed concrete includes its compressive strength, tensile strength, shear strength, shrinkage, coefficient of linear expansion, acoustic and thermal insulation, and fire resistance. The characteristic properties of foamed concrete will be presented in the following paragraphs according to the report on Foamed Concrete Composition and Properties (British Cement Association, 1994).

The compressive strength of foam concrete is influenced by many features like density, age, moisture content, and the physical and chemical characteristics of its component materials and mix proportions. A relationship exists between the density and the strength where it is found that the higher the density of the mixture, the greater the strength of the end product. For foamed concrete with densities ranging from 300 to 1600 kg/m³, the compressive strength at 28 days is from 0.2 to 12 N/mm². The compressive strength will continue to increase indefinitely due to the reaction with carbon dioxide, CO₂, present in the surrounding air.

Depending on the method of curing, the tensile strength of foam concrete can be as high as 0.25 of its compressive strength with a strain around 0.1% at the time of rupture. Meanwhile, the shear strength varies between 6% and 10% of the compressive strength.

Shrinkage property in foamed concrete is a phenomenon during the setting stage. The amount of shrinkage is dependent on the type of cement used, type of curing, the size and quality of the sand, the amount of cement in the mix, density of

the concrete, and the water cement ratio. The greater extent of shrinkage occurs during the first 28 days of the concrete's age.

The coefficient of linear thermal expansion for foam concrete is of the same order as that of normal concrete. Foam concrete has high sound absorption capacity and a very low transmission of heat. It is also extremely fire resistant where the level of resistance is greatly superior to normal concrete.

1.4.3 Advantages of Foamed Concrete

Foamed concrete has many advantages. However, the most important are its compressive strength and its low density. Foamed concrete in general has good mechanical strength combined with lightweight and low thermal conductivity. Good thermal insulation properties give energy conservation advantages which reduce the operating cost. Besides, it can be produced in a wide range of densities and properties that can suit any particular requirements. Like normal concrete, it can easily be mould to any desired shapes or sizes.

Foamed concrete is also an economical solution, particularly in large volume applications. It is self-compacting; as such, the casting process is much easier. Due to its lighter weight, lower crane capacity is required and lesser number in manpower is needed during the erection process. Its rapid installation contributes to the total cost saving. Placement of foamed concrete is a continuous operation from the mobile central plant where it pumps easily with relatively low pressure. The maintenance cost is also low because of its durability. It is also fire resistant and its surface texture makes it a good sound absorbent.

1.5 Precast Lightweight Foamed Concrete Sandwich Panel, PLFP

Lightweight foamed concrete can be produced by mixing sand, cement, water and stable foam using a mechanical air-entraining admixture. The product is a cementitious paste of cement and fine sand with micro discrete air cells uniformly distributed throughout the mixture to create a lightweight concrete. The density of the foamed concrete is controlled by the amount of tiny air pockets added into the mixture via foaming process. Lightweight foamed concrete has been used in construction for non-structural building wall panels or as partitions. It is considered as an attractive material because of its lightweight, better thermal properties and ease of construction.

Lightweight foamed concrete mixture can be designed to have higher strength which is close to the strength of the normal concrete. In order for lightweight concrete to be used as structural element, it must have the density of 1440 to 1840 kg/m³. Higher density results with higher strength of concrete. For structural application, the concrete strength should be 17 MPa or above (American Concrete Institute, 1989).

Precast Lightweight Foamed Concrete Sandwich Panel or PLFP is proposed in this study as an alternative structural sandwich component that can meet the rapid housing demand in this country. It consists of lightweight foamed concrete as the wythes which enclose the polystyrene which act as the insulation layer. Shear connectors are embedded across each layer to allow load shearing between wythes. The strength and stability of the PLFP rely a lot on the stiffness of these shear connectors and its ability to transfer load between wythes. The primary use of structural lightweight concrete is to reduce the dead load of a building. Structural lightweight concrete provides a most efficient strength-to-weight ratio in structural elements. Reduction of weight will result in easy construction, reduction of transportation cost and reduced of foundations, which eventually will reduce the overall cost.

1.6 Problem Statement

The demands from the growing population and migration of people to urban areas require this country to look for alternative construction method to provide fast and affordable quality housing to its citizens. Efforts have been taken to move from the traditional building construction technique to a more innovative construction method to meet these demands. As a part of this effort, an extensive investigation to develop a Precast Lightweight Foamed Concrete Sandwich Panel or PLFP as a load bearing wall system is undertaken.

1.7 Objectives

The aim of this study is to develop a load-bearing Precast Lightweight Foamed Concrete Sandwich Panel (PLFP) for use as structural component in low rise building construction. In order to achieve this aim, several objectives are set out:

1. To develop and construct the sandwich PLFP panel using the lightweight foamed concrete.
2. To propose the right mixture for lightweight foamed concrete of sufficient strength and density suitable for use as structural component.
3. To study the structural behaviour of the proposed sandwich PLFP panel by means of experimental work and finite element method, FEM.
4. To develop a semi-empirical expression to estimate the load carrying capacity of the PLFP panel.

1.8 Scope of Work

In order to develop and construct the sandwich PLFP panel using lightweight foamed concrete, an experimental programme which includes fourteen full-scaled specimens was conducted to study its behaviour and axial load carrying capacity. Finite element study was further conducted to examine the effect of various parameters which dictate the panel's strength and behaviour.

The experimental work started out with the pilot testing which includes trial mixing of lightweight foamed concrete to get the suitable density for the targeted compressive strength. The process of mixing was based on the typical mixture details for foamed concrete as given in British Cement Association. From the trial mixtures and the mixtures during the pilot testing and experimental programme, the right mixture for lightweight foamed concrete of sufficient strength and suitable density for use as a structural component is proposed.

The fourteen PLFP specimens in the experimental programme were tested under axial load to investigate its structural behaviour. The results were studied in term of its load carrying capacity, load-deflection profiles, strain distribution and efficiency of the shear connectors. Various height, thickness and diameters of shear connector were used in the FEM simulations to study the influence of slenderness ratio and to find the optimum shear connector's size which ensures the stability of the panel in term of its ultimate strength and degree of compositeness achieved. The strain distribution across the panel's thickness was used to study the efficiency and role of the shear connectors in transferring loads and to evaluate the extent of composite action achieved.

The results from the proposed FEM model and from the experimental work were analysed and compared. A semi-empirical expression was proposed to estimate the load carrying capacity of the PLFP panel. It was validated on the basis of the test data made available by previous research works.

1.9 Thesis Layout

The thesis consists of seven (7) chapters. The content of each chapter is described below:

Chapter I

This chapter presents an introduction of the Precast Lightweight Foamed Concrete Sandwich Panel, or PLFP, as an alternative building system which meets the challenge in the construction industry in Malaysia today. This chapter also discusses the objectives and the scope of work of the research.

Chapter II

This chapter presents the relevant literature review on the structural performance of the PLFP as sandwich wall panel. It also contains a review of the studies on lightweight foamed concrete and its properties. An overview of previous research works on sandwich wall panel of different material is also discussed with critical comments.

Chapter III

This chapter presents the methodology of the research, including the details on the actual and preliminary experimental work carried out to achieve the objectives as defined earlier. Fabrications and construction details of the test specimens and the materials used together with the test set up are described.

Chapter IV

This chapter contains presentation of results from the test data obtained from axial load tests on PLFP conducted experimentally in the present study. The observations are related to axial load bearing capacity, cracking patterns and mode of failure, load-deformation profiles, load-strain curves, and strain distribution across the panel's thickness. The observations were made to verify the FEM model and

facilitate interpretation of the theoretical results as described in Chapter V and Chapter VI.

Chapter V

This chapter describes the modeling and type of analysis used in the non-linear finite element study. It also presents the response of PLFP under axial load as determined by the FEM model. The applicability of the adopted FEM model was first validated on the basis of axial test data presented in Chapter IV. The results from the FE analysis are used in discussing the achievement of objectives and further drawing conclusions on the behaviour of PLFP panels as load-bearing wall element.

Chapter VI

This chapter presents the discussion of the results obtained from the experimental work and FEM. A semi-empirical expression is developed to estimate the strength capacity of PLFP panels using conventional approach based on reinforced concrete principles and data from previous research.

Chapter VII

A summary of the major findings of the study together with some recommendations for further work is given in this chapter.

CHAPTER II

LITERATURE REVIEW

2.1 Introduction

Precast concrete sandwich panel or PCSP technology has advanced gradually over the past four decades in North America. The first prefabricated panels were of non-composite type and consisted of a thick structural wythe, a layer of insulation and a non-structural wythe (Seeber *et al.*, 1997). PCSP have all of the desirable characteristics of a normal precast concrete panel such as durability, economy, fire resistance, large vertical spaces between supports, and potential usage as shear walls, bearing walls, and retaining walls. On top of that, PCSP can be relocated to accommodate building expansion. The hard surface on both the inside and outside of the panel provides resistance to damage and a finished product requiring no further treatment.

Many alternative forms of sandwich panels may be obtained by combining different facing and core materials as discussed previously in the second paragraph of Section 1.3 in Chapter 1. The combined materials can form composite panels which allow optimum design for various applications. The good properties of individual materials can be combined and the bad ones eliminated. It takes advantage of the shear strength of a lighter core material and the high compressive and tensile strength of high density wythes to obtain higher strength to weight ratios. The core material separates and stabilizes the outer facings against buckling under edgewise compression, torsion or bending. The wythes are usually made of high-strength material and they carry the primary loads. They resist tension and compression to prevent buckling under compression, tension failure and impact deformation.

Generally there are three types of pre-cast concrete sandwich panels or PCSP depending on the degree of composite action achieved (Shutt, 1997). A non-composite sandwich panel is one in which each concrete wythe acts independently to resist bending. Plane section behaviour is obtained in each wythe, but not through the entire panel depth. A fully composite sandwich panel is one in which the two concrete wythes act integrally to resist bending allowing the entire panel to perform as a single unit. In theory, a fully composite panel exhibits plane section behaviour throughout its entire depth at all locations along its span. Full composite behaviour is achieved by providing sufficient horizontal shear transfer between the wythes. Shear connectors were tied to the steel mesh in the concrete wythes. The connectors function to transfer load from the outer concrete wythe to the inner one.

A partially composite sandwich panel is one in which concrete wythes act atleast partly together to resist bending. Thus, a partially composite panel resists bending to a degree between that of a fully composite panel and a non-composite panel. The degree of composite action exhibit by a panel may change throughout the loading history of the panel. The distribution of stress and strain for the three types of sandwich wall panel is shown in Figure 2.1.

A fully composite panel fails either by concrete crushing or steel reinforcement yielding without failure of the connectors. The fully composite action is reflected in strains remaining essentially linear across the panel thickness, as shown in Figure 2.1(a). A PCSP is considered to be non-composite if its concrete wythes are tied with connectors that do not have the capacity for longitudinal shear transfer. In this case, the two wythes act independently. The variation of strains across the thickness, in case of non-composite panels is shown in Figure 2.1(c). A PCSP is considered partially composite if its connectors can transfer only a fraction of the longitudinal shear as required for the fully composite action. In this case, the connectors fail before concrete crushing or yielding of the reinforcement. Figure 2.1(b) describes the variation of strain across the panel thickness in such a case.

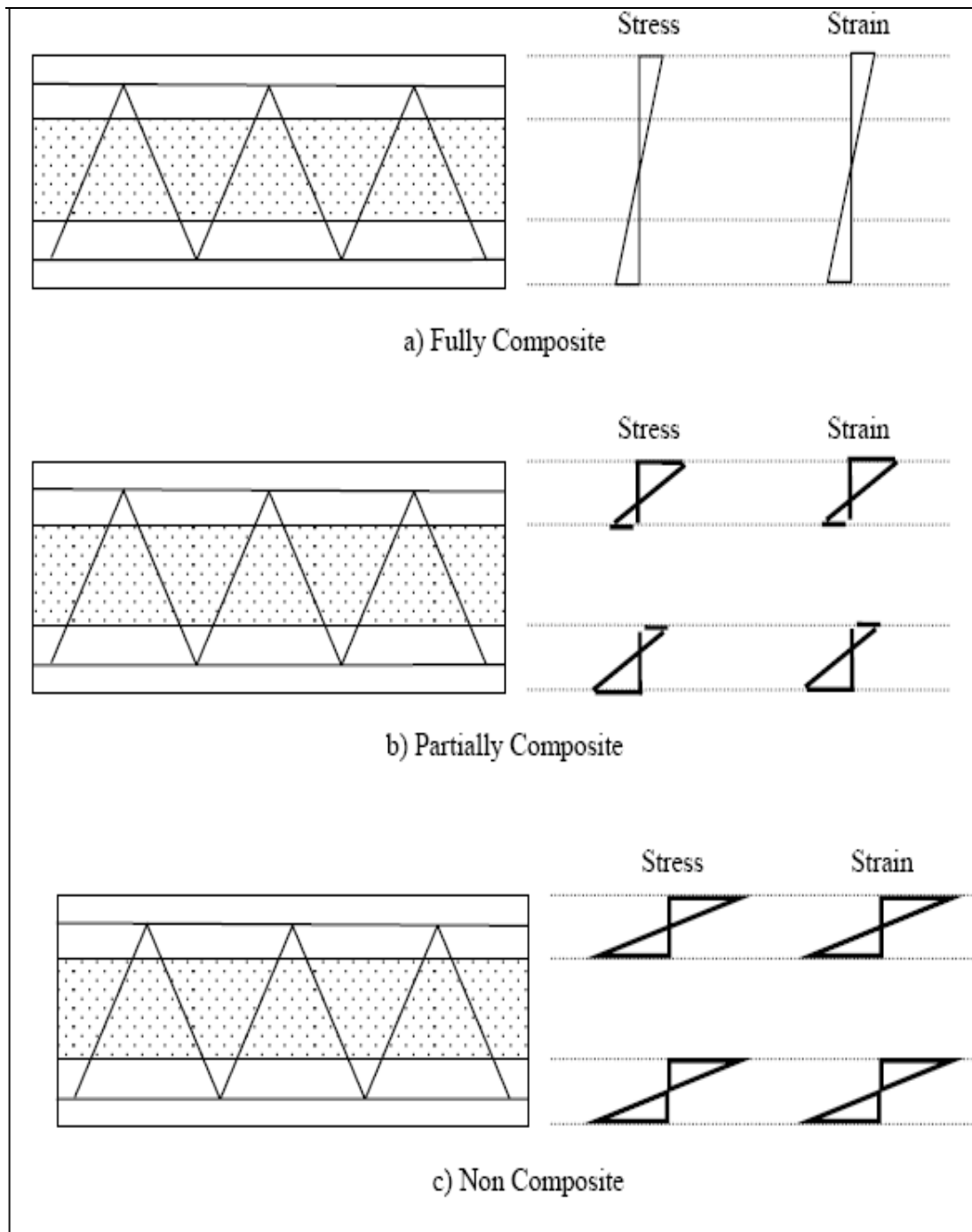


Figure 2.1: Types of Compositeness of pre-cast concrete sandwich panel.
(Shutt, 1997)

Sandwich panels have gained much attention as an effective structural element in engineering field. It has been used as load-bearing members in naval structures (Aicher and Hofflin, 1999). However, in the building and construction industry, most of the research published on sandwich panels are related to the study of the non-load bearing non-composite type of PCSP (Jokela *et al.*, 1981, Olin *et al.*, 1984, Hopp *et al.*, 1986 and Bush, 1998). Section 2.2 in this Chapter will discuss in details the previous research that has been carried out on sandwich panels. The section will be narrowed down to several sub-sections which will discuss the various material used as the wyhte and core, the shear connectors influences on the behaviour of panels and the structural behaviour of panels under various loading that have been done on this type of panel especially in the context of their applications as load bearing walls.

2.2 Review of Past Studies on Sandwich Panel

Previous research on sandwich panel have shown that various materials could be used as the core layer and skin faces. Therefore, a sandwich panel is unique in its own way because the materials it uses are different from any other sandwich panel. Sandwich panel development had started with normal weight material as both core and faces. However, the use of lightweight material as core layer has become more familiar in recent years as will be discussed in the next paragraphs. Review of the previous studies on the materials used, shear connector's effect on the structural behaviour, its structural behaviour, lightweight sandwich panel and the lightweight foamed concrete are presented in the sections below. All these sub-topics are actually interrelated. For instance, the materials and shear connectors used seem to have significant effects on the structural behaviour of the sandwich panel whilst the structural behaviour of the sandwich panel influences the types of materials chosen.

2.2.1 Materials

The wythes of sandwich panels are generally made of thin, high strength sheets material. The structural requirements for wythe materials are their abilities to resist local loads and resistance to corrosion and fire. The core materials are generally thicker and made of lower density materials. The core is low in density because the core usually does not take any load and function as an insulation material. As stated previously, many alternative forms of materials may be used either as the wythes or as a core layer of the sandwich panels. Various types of materials therefore provide various structural behaviours of the sandwich panels.

Jeom *et al.* (1999) investigated the strength characteristics of aluminum sandwich panels with aluminum honeycomb core theoretically and experimentally (Figure 2.2). They found out that the sandwich structure offers advantage in term of lighter weight for design of weight critical structures. It is also observed that aluminum honeycomb core has excellent properties with regard to weight savings and fabrication costs.

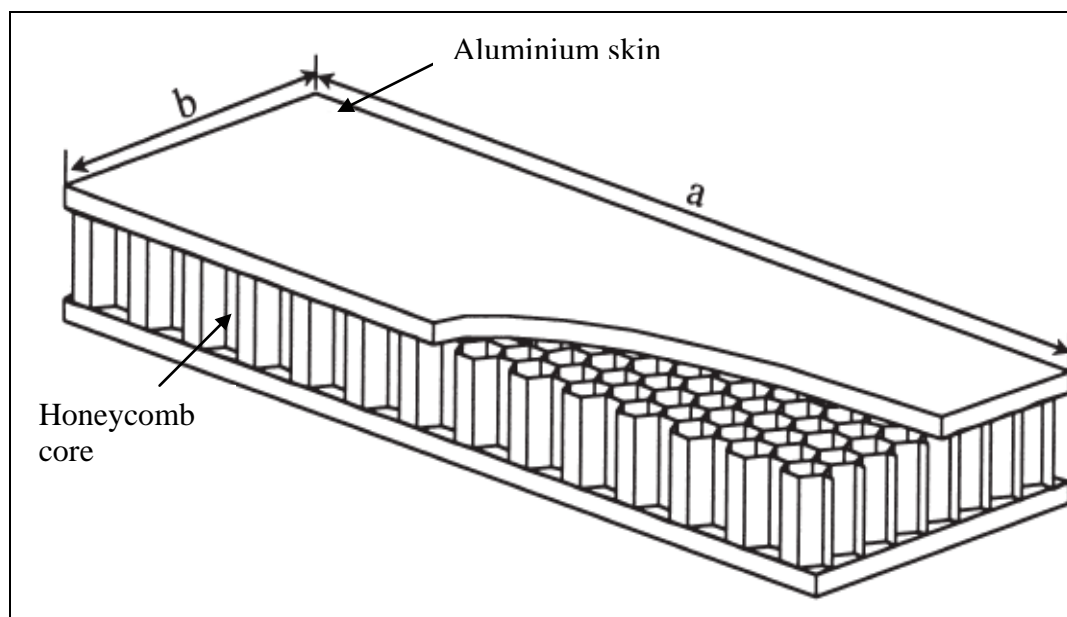


Figure 2.2: Honeycomb-cored sandwich panel (Jeom *et al.*, 1999)

Stoll *et al.*, (2004) investigated the effect of weight, strength, stiffness and failure mode of Fiber-Reinforced Composite (FRC) core in composite sandwich construction. In this study, dry fiber and preform foam are used in the molding processes to produce a fiber reinforced composite core panel. An FRC core pre-form was manufactured by cutting a foam board strip which was wrapped by fiber glass fabric around it as shown in Figure 2.3 and consolidating multiple wound strips into sheets as in Figure 2.4. Fiber glass fabric is added to the surfaces of the pre-form and the lay-up is infused with thermoset resin to produce a molded panel as shown in Figure 2.5. The fiberglass used in FRC test panel is E-glass fabric with G6 and G18 facing design. To enable comparisons of FRC cores with other core materials, test panels with 2.5 cm thick foam and balsa cores were molded. An 80 kg/m^3 PVC foam test panel was molded with the same facing design as the G6 test panels, and a nominal 150 kg/m^3 balsa was molded with the same facing design as the G18 test panels. The results of shear strength, stiffness and compressive strength on the FRC core were compared with the results taken from the tests on panels with PVC foam and balsa cores. It is found that the use of FRC cores increased the shear and compressive strength with only minor increase in core density (Table 2.1).



Figure 2.3: Foam board strip wrapped by fiber glass fabric (Stoll *et al.*, 2004)

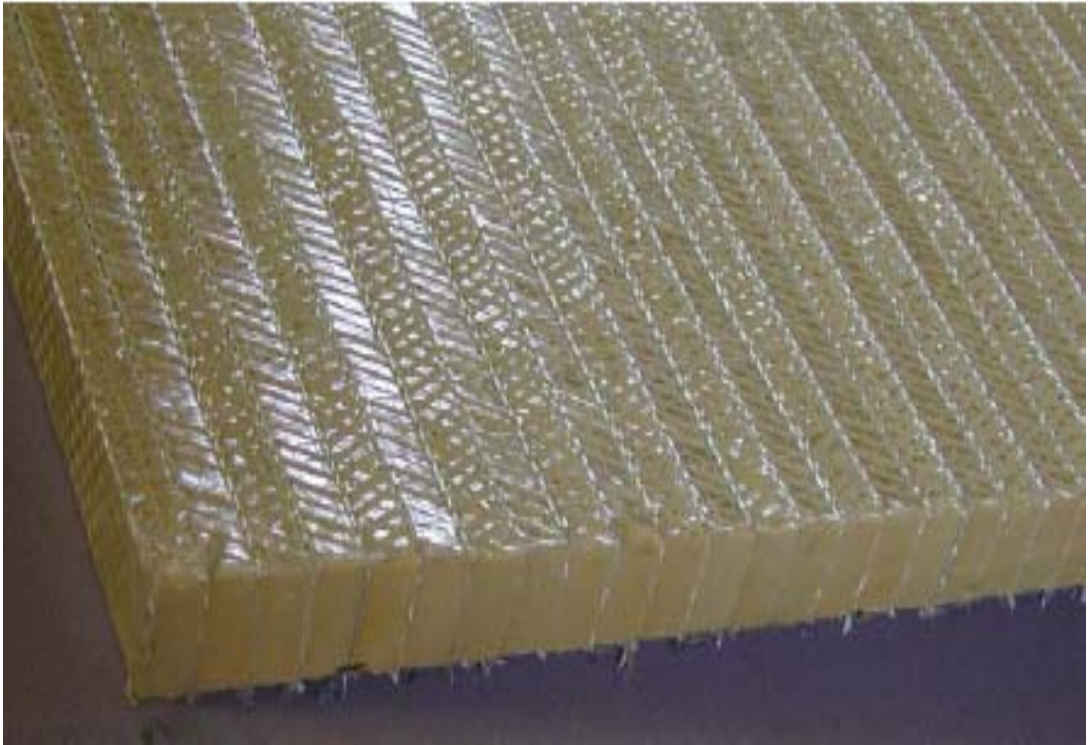


Figure 2.4: Core Preform (Stoll *et al.*, 2004)

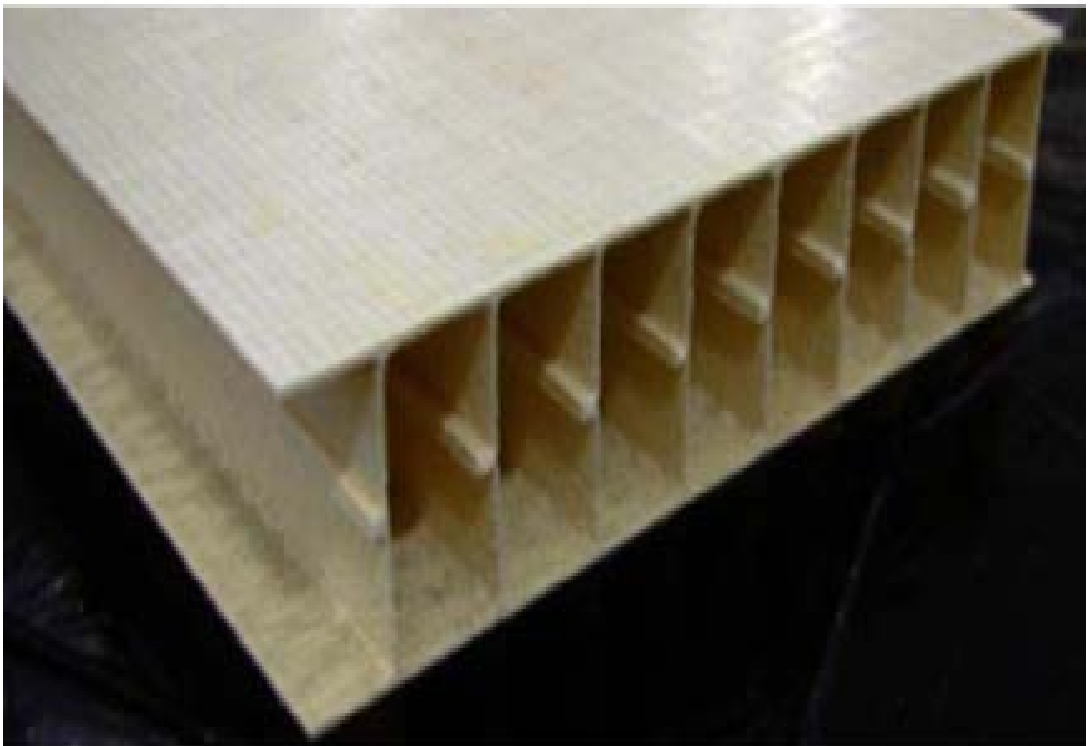


Figure 2.5: Molded panel with foam removed, showing composite webs and resin ridge (Stoll *et al.*, 2004)

Table 2.1: Measured Properties for FRC, PVC foam and Balsa Cores.

(Stoll *et al.*, 2004)

Core design	Infused core density kg/m ³ (lb/ft ³)	Shear strength, short-beam bending		Shear strength, plate shear		Shear modulus		Compressive strength MPa (psi)	Tensile strength MPa (psi)
		MPa (psi)		MPa (psi)		MPa (ksi)			
		L	W	L	W	L	W		
G6	97 (6.0)	1.52 (221)	0.11 (16)	1.80 (261)	0.18 (26)	134 (19.4)	5.5 (0.8)	2.83 (410)	0.82 (119)
G18	103 (6.4)	3.79 (549)	0.20 (28.5)	3.09 (448)	0.23 (34)	257 (37.5)	6.2 (0.9)	7.55 (1095)	2.17 (314)
PVC foam	76 (4.8)	1.08 (157)		0.87 (126)		28 (4)		1.14 (166)	2.15 (312)
Balsa	348 (21.7)	2.35 (341)		2.57 (373)		276 (40)		11.64 (1690)	9.50 (1380)

Lee *et al.* (2006) in their paper described an ongoing project to demonstrate an affordable, safe, and energy-efficient housing technology based on expanded polystyrene (EPS) foam panels with a cementitious coating. In this system, the EPS was acting as the core while the cellulose fiber cement board panel was acting as the facings of the panel. The EPS core layer was embedded with the wire trusses which were connected to the wire mesh that enclosed the EPS layer. The cement board facings were screwed to the surface of the EPS layer. The concepts being described are as shown in Figure 2.6, Figure 2.7 and Figure 2.8. Preliminary tests were conducted to analyze the costs, to simulate seismic forces, to conduct the test against environmental conditions, and to build pilot houses.

The test results indicate that houses constructed from EPS structural insulated panels with a cementitious coating meet the defined needs of populations in many parts of the developing world. The structural and fire safety test, energy use and cost analysis showed that panel homes met the necessary criteria of safety and affordability. Structural simulations demonstrated that the technology was highly resistant to ordinary and extreme forces such as high wind, snow load, and earthquakes. The panel homes were also shown to be safe in fire and damages was

easy and inexpensive to repair. Affordable concerns in this research were addressed through the cost analysis and energy modeling, which demonstrated that the panel design is inexpensive to build and maintain.

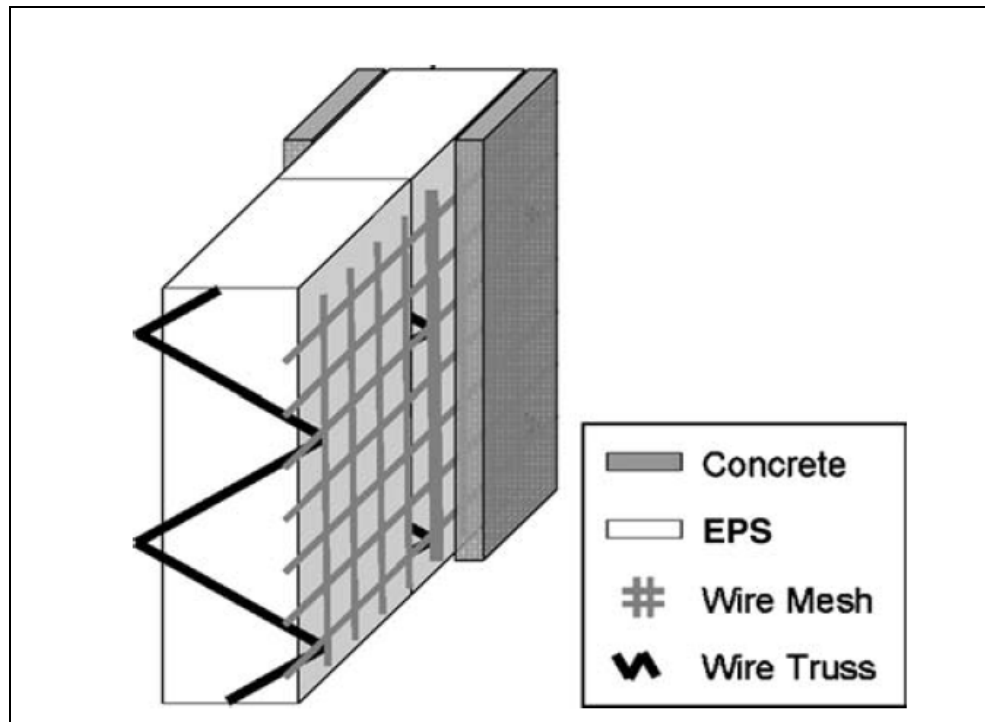


Figure 2.6: EPS Embedded With Trusses (Lee *et al.*, 2006)

LIST OF REFERENCES

- Aicher S. and Hofflin L. (1999). Long-term Performance Test of Eccentrically Loaded Sandwich Wall Elements With Wood-Based Skins. *Otto-Graf-Journal*, 10, 128-142.
- American Concrete Institute (1989). *ACI 213R. Guide For Structural Lightweight Aggregate Concrete*. Farmington Hills, MI. American Concrete Institute.
- Attard M. M., Minh N. G. and Foster S. J. (1996). Finite Element Analysis of Out-Of-Plane Buckling of Reinforced Concrete Walls. *Journal of Computers and Structures*, 61(6) 1037-1042.
- Benayoune A. et al. (2006a). Response of Precast Reinforced Composite Sandwich Panels to Axial Loading. *Journal of Construction and Building Materials*, 21, 677-685. Elsevier.
- Benayoune A. et al. (2006b). Structural Behaviour of Eccentrically Loaded Precast Sandwich Panels. *Journal Of Construction And Building Material*, 20, 713-724. Elsevier.
- Bohdan L. (1966). Building With Large Prefabrication. *Journal of Construction and Building Material*. Elsevier, London.
- Bush T. D. and Stine G. L. (1994). Flexural Behaviour of Composite Precast Concrete Sandwich Panels With Continuos Truss Connectors. *PCI Journal of Precast/ Prestressed Concrete*, 112-121.
- Bush T. D. and Wu Z. (1998). Flexural Analysis of Prestressed Concrete Sandwich Panels with Truss Connectors. *PCI Journal*, 76-86.
- British Cement Association (1994). *Foamed Concrete Composition and Properties*. 165-168. British Cement Association.
- British Standard Association (1985). *BS 8110: Part 2. Additional Considerations in the Use of Lightweight Aggregate Concrete*. British Standard Institution.

- British Standard Institution (1997). *BS 8110: Part 1. Design Objective and General Recommendations*. British Standard Institution.
- Case D. M. and Lake R. S. (1997) Glass Fiber-Based Honeycomb Core Sandwich Panels. *Journal of Composite materials*, 31, 2249.
- Construction Industry Development Board (CIDB) (2007). *Construction Industry Master Plan Malaysia 2006-2015*. Malaysian Construction Industry Development Board.
- Davies J. M. (1987). Design criteria for structural sandwich panels. *Journal of Structural Engineering*. 12, 435–441.
- Davies J. M. (1993). Sandwich Panels. *Journal of Thin-Walled Structures*, 16, 179–198.
- Einea, Amin, Salmon, David C., Tadros, Maher K., and Todd. (1994). A New Structurally and Thermally Efficient Precast Sandwich Panel System. *PCI Journal*, 38(4), 90-101.
- Esa H. and Nurudin M. M. (1998). Policy on Industrialised Building Systems. *Colloquium on Industrialised Construction Systems*. Kuala Lumpur.
- Freeman S. (1999). Loadbearing Architectural Precast Concrete Wall Panels. *PCI Journal*, 92-115.
- Heng C. C. (1998). The Structural Response of Precast Sandwich Panel Under Axial and Lateral Load. *Research Report*. Universiti Putra Malaysia.
- Hoigard K. R., Kritzler R. W. and Mulholland G. R. (1993). Structural Analysis of Stone Clad Precast Concrete Building Panels. *International Journal of Rock Mechanics, Mineral Science, and Geomechanical*, 30(7), 1567-1573.
- Hopp J. and Hemerstad A. (1986). Sandwich Elements - Construction Handbook of Concrete Elements. Norwegian Industries Association, Oslo, Norway.

- Huang J. S. and Huang Z. H. (2000). Fatigue of Cement Foams in Axial Compression. *Journal of Materials Science*, 35, 4385-4391.
- Ishai O. et al. (1995). Sandwich Structures Based on Syntactic Foam. *Journal of Composite Material*, 26, 47.
- Jeom K. P., Thayamballi A. K., and Kim G. S. (1999). The Strength Characteristics of Aluminum Honeycomb Sandwich Panels. *Journal of Thin-Walled Structures*, 35, 205-231. Elsevier.
- Jokela J. and Sarja, A. (1981). Development of Reinforcement for Sandwich Facade Element. *Research Note No. 19*, VIT-Technical Research Center of Finland, Finland.
- Junid S. M. S. (1986). Industrialised Building Systems. *Proceedings of UNESCO/FEISEAP Regional Workshop*, University Putra Malaysia (UPM). Serdang, Selangor.
- Kabir M. Z. (2005). Structural Performance of 3-D Sandwich Panels Under Shear and Flexural Loading. *Journal of Scientia Iranica*, Vol 12(4), 402-408. Sharif University of Technology.
- Leabu V.F. (1959). Problems and Performance of Precast Concrete Walls. *ACI Journal Proceeding*, 56, 287-298.
- Lee A. J., Kelly H., Jagoda R., Rosenfeld A., Stubee E., Colaco J., Gadgil A. Akbari H., Norford L. and Van Burik H. (2006). Affordable, Safe Housing Based On Expanded Polystyrene (EPS) Foam and a Cementitious Coating. *Journal of Material Science*, 41, 6908-6916.
- Lee B. J. and Pessiki S. (2006). Thermal Performance Evaluation of Precast Concrete Three-Wyhte Sandwich Wall Panels. *Journal of Energy and Buildings*, 38, 1006-1014. Elsevier.
- Lessing J., Ekholm A. and Stehn L. (2005). Industrialised Housing-Definition and Categorisation of the Concept. *13th International Group for Lean Construction*. Sydney, Australia.

- Liew J. Y. and Soheli K. M. A. (2009). Lightweight Steel-Concrete-Steel Sandwich System With J-hook Connectors. *Journal of Engineering Structures*, 31, 1166-1178. Elsevier.
- Memon N. A. et.al (2007). Ferrocement encased lightweight aerated concrete: A novel approach to produce sandwich composite. *Journal of Materials*. 61, 4035-4038. Elsevier.
- Mohammed A. M. and Nasim U. (2009). Experimental and analytical study of carbon fiber-reinforced polymer (FRP) / autoclaved aerated concrete (AAC) sandwich panels. *Journal of Engineering Structures*, 31,2337-2344, Elsevier.
- Nambiar E. K. and Ramamurthy K. (2005). Influence of Filler Type on the Properties of Foam Concrete. *Journal of Cement and Concrete Composite*, (28), 475-480. Elsevier.
- Obelender G. D. and Everard N. J. (1977). Investigation of Reinforced Concrete Wall Panels. *ACI Journal Proceedings*, 74(6), 256- 263.
- Olin J., Ravio J., and Jokela J. (1984). Development of Heat Economy and Construction Façade Elements. *Research Report No. 28*, VIT-Technical Research Center of Finland, Espoo, Finland.
- Papanicolaou C. G. and Triantafillou T.C. (2004). Analysis and Minimum Cost Design of Concrete Sandwich Panels under Out-of-plane Loading. *Journal of Structural Concrete*, 5(1), 1464-4177.
- PCI Committee. (1977). State of the Art of Precast/Prestresses Sandwich Wall Panels. *PCI Journal*, 42(2), 92-133.
- Pessiki S. and Mlynarczyk A. (2003). Experimental Evaluation of the Composite Behaviour of Precast Concrete Sandwich Wall Panels. *PCI Journal*, 54-68.

- Pfeifer D.W. and Hanson J.A. (1964). Precast Concrete Wall Panels: Flexural Stiffness of Sandwich Panels. *Special Publication SP11*, 67-86. American Concrete Institute, Farmington Hills, MI.
- Pillai S. U., and Parthasarathy C. V. (1977). Ultimate Strength and Design Of Concrete Walls. *Journal of Building and Environment*, 12, 25-29. London.
- Pokharel N. and Mahendran M. (2003). Experimental Investigation and Design of Sandwich Panels Subject To Local Buckling Effects. *Journal of Constructional Steel Research* . 59, 1533–1552. Elsevier.
- Pokharel N. and Mahendran M. (2004). Finite Element Analysis and Design of Sandwich Panels Subject to Local Buckling Effects. *Journal of Thin Wall Structures*. 42, 589–611. Elsevier.
- Ramli M. (2008). Flexural Strength of Ferrocement Sandwich Panel for Industrialised Building Systems. *Malaysian Construction Research Journal*, 2(1), 57-75.
- Rezaifar O., Kabir M. Z., Taribakhsh M. and Tehranian A. (2007). Dynamic behaviour of 3-D panel single-storey system using shaking table testing. *Journal of Engineering Structures*, Vol 30, 318-337. Elsevier.
- Rice M. C., Fleischer C. A., and Zupan M. (2006). Study on the Collapse Of Pin-Reinforced Foam Sandwich Panel Cores. *Journal of Experimental Mechanics*, 46, 197-204. Proquest.
- Rizzo S. and Fazio P. (1979). Lateral Deflection of a Sandwich Panel Building Model under Combined Loading. *Journal of Experimental Mechanics*. 193-199.
- Rosenthal I. (1984). Structural Behaviour Of Loaded Multilayer Wall Panels. *Journal of Materials and Structures*, Volume 17(4), pp. 329-332.
- Saheb S. M. and Desayi P. (1989). Ultimate Strength of RC Wall Panels in One-Way In-Plane Action. *Journal of Structural Engineering, ASCE*, 115(10), 2617- 2630.

- Saheb S. M. and Desayi P. (1990). Ultimate Strength of RC Wall Panels in Two-Way In-Plane Action. *Journal of Structural engineering, ASCE*, 116(5), 138-1402.
- Scudamore R. J. and Cantwell W. J. (2002). The Effect of Moisture and Loading Rate on the Interfacial Fracture Properties of Sandwich Structures. *Journal of Polymer Composites*, 23(3), 406. ProQuest.
- Seeber K. E. et al. (1997). State-of-the-Art of Precast/Prestressed Sandwich Wall Panels. *Journal of Precast Sandwich Wall Panels*. PCI Committee.
- Short A. and Kinniburgh W. (1978). Lightweight Concrete. *Journal of Applied Science*, 3rd edition.
- Shutt C. A. (1997). Report Codifies, Details Sandwich Wall Panels. *Ascent Journal*, 28-33. Springer.
- Stoll F. et al. (2004). High-Performance, Low-Cost Infusion Cores for Structural Sandwich Panels. *Proceedings of SAMPE*. Long Beach, California.
- Sulaiman M.A. et al. (2008). Development And Behaviour Of Lightweight Foamed Concrete Wall Panel. *IEM Journal*, 70(1), 14-20. The Institution of Engineers, Malaysia
- Thanoon W.A.M., Peng L.W., Abdul Kadir M.R., Jaafar M.S. and Salit M.S. (2003). The Experiences of Malaysia and Other Countries in Industrialised Building System in Malaysia. *Proceeding on IBS Seminar*. UPM, Malaysia.
- Tonyan T. D. and Gibson L. J. (1992). Structure and Mechanics of Cement Foams. *Journal of Materials Science*, 27, 6371-6378. Chapman & Hall.
- Triantafillou T. C. and Gibson L.J (1989). Debonding In Foam-core Sandwich Panels. *Journal of Materials and Structures*, 22, 64-69.
- Yang M. and Qia P. (2005). Higher-order Impact Modeling of Sandwich Structures with Flexible Core. *Journal of Solid and Structures*, 42, 5460-5490. Elsevier.