

PERFORMANCE MODELLING OF REFRIGERANTS  
IN A VAPOR COMPRESSION REFRIGERATION CYCLE

SITI MARIAM BTE BASHARIE

UNIVERSITI TEKNOLOGI MALAYSIA

PERPUSTAKAAN UTHM



\*30000001866837\*

CU189169

## UNIVERSITI TEKNOLOGI MALAYSIA

## BORANG PENGESAHAN STATUS TESIS

JUDUL: PERFORMANCE MODELLING OF REFRIGERANTS  
IN A VAPOR COMPRESSION REFRIGERATION CYCLE

SESI PENGAJIAN: 2005/2006

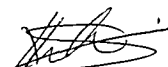
Saya SITI MARIAM BTE BASHARIE  
(HURUF BESAR)

mengaku membenarkan tesis (PSM/Sarjana/Doktor Falsafah)\* ini disimpan di perpustakaan Universiti Teknologi Malaysia dengan syarat-syarat kegunaan seperti berikut:

1. Tesis adalah hakmilik Universiti Teknologi Malaysia.
2. Perpustakaan Universiti Teknologi Malaysia dibenarkan membuat salinan untuk tujuan pengajian sahaja.
3. Perpustakaan dibenarkan membuat salinan tesis ini sebagai bahan pertukaran antara institusi pengajian tinggi.
4. \*\*Sila tandakan (✓)

- SULIT (Mengandungi maklumat yang berdarjah keselamatan atau kepentingan Malaysia sepertimana yang termaktub di dalam AKTA RAHSIA RASMI 1972)
- TERHAD (Mengandungi maklumat TERHAD yang telah ditentukan oleh organisasi/badan di mana penyelidikan dijalankan)
- TIDAK TERHAD

  
(TANDATANGAN PENULIS)

Disahkan oleh  
  
(TANDATANGAN PENYELIA)

Alamat Tetap:

428, Felda Air Tawar 5  
81920 Kota Tinggi  
Johor.

Dr. Normah bte Mohd Ghazali  
Nama Penyelia

Tarikh: 27 November, 2005

Tarikh: 27 November, 2005

- CATATAN:
- \* Potong yang tidak berkenaan.
  - \*\* Jika tesis ini SULIT atau TERHAD, sila lampirkan surat daripada pihak berkuasa/organisasi berkenaan dengan menyatakan sekali sebab dan tempoh tesis ini perlu dikelaskan sebagai SULIT atau TERHAD.
  - ♦ Tesis dimaksudkan sebagai tesis bagi Ijazah Doktor Falsafah dan Sarjana secara penyelidikan, atau disertasi bagi pengajian secara kerja kursus dan penyelidikan, atau Laporan Projek Sarjana Muda (PSM).

**Sekolah Pengajian Siswazah  
Universiti Teknologi Malaysia**

**PENGESAHAN PENYEDIAAN SALINAN E-THESIS**

**Judul tesis:** PERFORMANCE MODELLING OF REFRIGERANTS IN A  
VAPOR COMPRESSION REFRIGERATION CYCLE

**Ijazah:** SARJANA KEJ. MEKANIKAL (TULIN)

**Fakulti:** KEJURUTERAAN MEKANIKAL

**Sesi Pengajian:** 2005/2006

Saya, SITI MARIAM BTE BASHARIE  
(HURUF BESAR)

mengaku telah menyediakan salinan e-thesis sama seperti tesis asal yang telah diluluskan oleh panel pemeriksa dan mengikut panduan penyediaan Tesis dan Disertasi Elektronik (TDE), Sekolah Pengajian Siswazah, Universiti Teknologi Malaysia, Januari 2004.



(Tandatangan pelajar)

Alamat tetap:  
428 FELDA AIR TAWAR 5,  
81920 KOTA TINGGI,  
JOHOR.




(Tandatangan penyelia sebagai saksi)

**Nama penyelia:** DR. NORMAH MOHD GHAZALI

**Fakulti:** KEJURUTERAAN MEKANIKAL

**Nota:** Borang ini yang telah dilengkapi hendaklah dikemukakan kepada SPS bersama penyerahan CD.

“I hereby declare that I have read this thesis and in my opinion it has fulfilled the requirements in term of the scope and the quality for the purpose of awarding the Master Degree of Mechanical Engineering”

Signature :   
Name of Supervisor : DR. NORMAH BTE MOHD GHAZALI  
Date : 27 November, 2005

PERFORMANCE MODELLING OF REFRIGERANTS  
IN A VAPOR COMPRESSION REFRIGERATION CYCLE

SITI MARIAM BTE BASHARIE


This project report is submitted as a part of the  
fulfilment of the requirement for the award of the  
Master Degree in Mechanical Engineering

Faculty of Mechanical Engineering  
Universiti Teknologi Malaysia

NOVEMBER, 2005

**DECLARATION**

“I declare that this thesis is the result of my own research except as cited in references.  
The thesis has not been accepted for any degree and is not concurrently submitted in  
candidature of any degree”

Signature :   
Name of Candidate : SITI MARIAM BTE BASHARIE  
Date : 27 November, 2005

*Istimewa Buat Suami Tersayang,  
Md Norrizam Mohd Jaat  
" terima kasih atas sokongan dan doronganmu"  
Buat Anak-anak Yang Dikasihi,  
Adam Haikal dan Aiman Syakirin  
Serta Untuk  
Keluarga Tercinta*



## ACKNOWLEDGEMENT

Alhamdulillah, great thanks to Allah for giving me strength and conveniences during this project. I would like to express my special thank to my supervisor, Dr. Normah Ghazali for her guidance, advice and help. Also special thanks to Prof. Amer Nordin Darus, Rahim and Mas Fawzi for their directly and indirectly contribution and helps during the preparation of this project. Also very thankful to my parents and family for their help and support during this course.

## ABSTRACT

The simulation model based on the actual vapor compression cycle is performed in order to evaluate the performance of 14 refrigerants in terms of first law and second law efficiency. A 10% pressure drop is modelled in both the condenser and evaporator. The refrigerants that have been evaluated include R12, R22, R502, and their alternatives R134A, R401A, R401B, R402A, R402B, R404A, R407C, R410A, R408A, R409A, and R507. Effects of evaporating and condensing temperature on the COP, second law efficiency and irreversibility have been studied. The evaluation results show that R401A, R401B, and R409A are predicted as the best replacements for R12. R410A is predicted as the best alternative for R22, while R402B, R407C, and R408A are the best alternatives for R502 in terms of COP and second law efficiency. The results of actual cycle model show better predictions than that obtained with the ideal cycle model.

## ABSTRAK

Model simulasi berdasarkan kitar pemampatan wap sebenar telah dihasilkan bagi tujuan menilai prestasi 14 bahan pendingin dari aspek kecekapan hukum pertama dan kedua. Kedua-dua pemeluwap dan penyejat telah dimodelkan dengan mempunyai kejatuhan tekanan sebanyak 10%. Bahan pendingin yang telah diuji termasuklah R12, R22, R502, dan bahan pendingin alternatif iaitu R134A, R401A, R401B, R402A, R402B, R404A, R407C, R410A, R408A, R409A, dan R507. Kajian kesan suhu penyejatan ke atas pekali prestasi, kecekapan hukum kedua dan ketidakbolehbalikan juga telah dijalankan. Hasil penilaian menunjukkan R401A, R401B, dan R409A sebagai alternatif terbaik menggantikan R12. R410A didapati alternatif terbaik bagi R22, manakala R402B, R407C, dan R408A untuk R502 dari aspek pekali prestasi dan kecekapan hukum kedua. Keputusan yang diperolehi menunjukkan model kitar sebenar dapat menghasilkan penilaian yang lebih baik berbanding model kitar unggul.

## TABLE OF CONTENTS

CHAPTER	CONTENTS	PAGE
	<b>TITLE</b>	i
	<b>DECLARATION</b>	ii
	<b>DEDICATION</b>	iii
	<b>ACKNOWLEDGEMENT</b>	iv
	<b>ABSTRACT</b>	v
	<b>ABSTRAK</b>	vi
	<b>TABLE OF CONTENTS</b>	vii
	<b>LIST OF TABLES</b>	x
	<b>LIST OF FIGURES</b>	xi
	<b>LIST OF SYMBOLS</b>	xiii
	<b>LIST OF APPENDICES</b>	xiv
 <b>CHAPTER I</b>	 <b>INTRODUCTION</b>	 1
	1.1 Introduction	1
	1.2 Refrigerants and Its Alternatives	2
	1.3 Performance Evaluation of Refrigerants in Refrigeration Cycle	3
	1.4 Simulation Model of Refrigerants Performance Evaluation	6
	1.5 Objectives	12
	1.6 Scopes of Project	12

<b>CHAPTER II</b>	<b>THEORY AND FORMULATION</b>	13
	2.1 Actual Vapor Compression Refrigeration Cycle	13
	2.2 Calculating Thermodynamic Properties	15
	2.3 Performance Analysis	17
<b>CHAPTER III</b>	<b>RESEARCH METHODOLOGY</b>	20
	3.1 Introduction	20
	3.2 Simulation Model	21
	3.2.1 Thermodynamics Model	23
	3.3 Computer Programming	25
	3.3.1 The REFTEST Simulation Program	26
	3.4 Performance Evaluation	32
	3.5 Performance Analysis	33
<b>CHAPTER IV</b>	<b>PERFORMANCE TEST AND ANALYSIS</b>	34
	4.1 COP Analysis of Refrigerants and Its Alternatives	34
	4.2 Second Law Efficiency of Refrigerants and Its Alternatives	37
	4.3 The effect of changes in evaporating temperature on the COP	39
	4.4 The effect of changes in condensing temperature on the COP	40
	4.5 Refrigerant with higher total irreversibility	41
	4.6 Locating the primary source of irreversibility	42
	4.7 The effect of changes in evaporating temperature on the irreversibility	43
	4.8 The effect of irreversibility on second law efficiency	44
	4.9 Comparison between the ideal and actual cycle with pressure drops	47

<b>CHAPTER V</b>	<b>CONCLUSION</b>	47
<b>REFERENCES</b>		49
<b>APPENDIX A</b>		51
<b>APPENDIX B</b>		72

**LIST OF TABLES**

<b>TABLE</b>	<b>DESCRIPTION</b>	<b>PAGE</b>
3.1	The key state point refer to Figure 3.2 and Figure 3.3	22
3.2	The set values of temperature ranges of input parameters	29
3.3	The default values of input parameters	29
3.4	The units of thermodynamic properties	30
3.5	The list of refrigerants that will be evaluated and their alternatives	33
4.1	Pressure ratio comparison between R12 and R134A	36
4.2	Component irreversibility of refrigerant R407C and R134A	42
4.3	Comparison between ideal and actual cycle of refrigerant R12	46

## LIST OF FIGURES

FIGURE	DESCRIPTION	PAGE
1.1	Impact of critical temperature of volumetric capacity and COP	4
1.2	Vapor compression cycle simulated by Cycle 11	8
1.3	Main graphic user interface (GUI) of Cycle D	9
1.4	Welcome interface of simulation program developed by Sia	10
1.5	Input interface of simulation program developed by Sia	11
1.6	One of the output interfaces of simulation program developed by Sia	11
2.1	T-s diagram for the ideal cycle	14
2.2	T-s diagram for the actual cycle	14
3.1	The general flow chart of methodology of the study	20
3.2	The schematic diagram of the simulation model cycle	21
3.3	The T-s diagram of the simulation model cycle	21
3.4	The general flow chart of the computer programming	26
3.5	Welcome interface of REFTEST	27
3.6	Input interface of REFTEST	28
3.7	The interface of thermodynamics property	30
3.8	Interface of first law analysis	31
3.9	Interface of second law analysis	32
4.1	COP of R12 and its alternatives	35
4.2	COP of R22 and its alternatives	36
4.3	COP of R502 and its alternatives	37
4.4	Second law efficiency of R12 and its alternatives	38
4.5	Second law efficiency of R22 and its alternatives	39
4.6	Second law efficiency of R502 and its alternatives	39
4.7	COP versus condensing temperature	40
4.8	Total irreversibility of refrigerant	41



4.9	The percentage of component irreversibility of R407C and R134A	42
4.10	Irreversibility versus evaporating temperature	43
4.11	Percentages of lost work for condenser and evaporator as a function of evaporating temperature predicted by Yumrutas et al. [19]	44
4.12	The effect of irreversibility on second law efficiency	45
4.13	Second law efficiency and total exergy loss in percentage predicted by Yumrutas et al. [19]	45

### LIST OF SYMBOLS

$COP$	Coefficient Of Performance
$COP_{carnot}$	Coefficient Of Performance of a carnot cycle
$COP_{ref}$	Coefficient Of Performance of a refrigeration cycle
$COP_{rev}$	Coefficient Of Performance of a reversible cycle
$h$	Specific enthalpy, $h=u+Pv$ , kJ/kg
$i$	Specific irreversibility, kJ/kg
$I$	Irreversibility, kJ
$\dot{m}$	Mass flow rate, kg/s
$P$	Pressure, kPa
$Q$	Total heat transfer, kJ
$\dot{Q}$	Heat transfer rate, kW
$Q_{evap}$	Useful refrigerating effect, kJ
$s$	Specific entropy, kJ/kgK
$S$	Total entropy, kJ/K
$T$	Temperature, °C or K
$T_O$	Ambient temperature, °C or K
$T_R$	Refrigerated space temperature, °C or K
$T_{surr}$	Surroundings temperature, °C or K
$u$	Specific internal energy, kJ/kg
$v$	Specific volume, m <sup>3</sup> /kg
$W_{net}$	Net work, kJ
$\dot{W}$	Power, kJ/kg
$\eta_{II}$	Second law efficiency

**LIST OF APPENDICES**

<b>APPENDIX</b>	<b>DESCRIPTION</b>	<b>PAGE</b>
A	Programming codes	51
B	Test results	72

## CHAPTER I

### INTRODUCTION

#### 1.1 Introduction

Chlorofluorocarbon (CFC) issues like ozone layer depletion and global warming have brought many studies for alternative refrigerants with suitable properties to replace the CFC and hydrochlorofluorocarbon (HCFC) refrigerants. Now, more new refrigerants are appearing on the market. This is due to the effort that has been made to find suitable replacements for CFC and HCFC refrigerants. R22 for example, is widely used in refrigeration system and being the most popular replacement for R12 which has been totally phase out by January 1, 1996 (unless for the continued use from existing and for continued production for very limited essential uses) [1].

As the production of R22 is being totally phase out by January 1, 2030, the rush to find its alternative continues. The study of performance evaluation of the R22 and its possible replacement has become important especially by compressor manufacturers. Before an experimental test in an actual system is carried out, the test through simulation program becomes useful as a preliminary evaluation of a refrigerant performance.

Comparison and evaluation of the performance of a refrigerant and its possible replacement, is done through the theoretical testing or testing in actual application [2]. Theoretical testing and comparison are usually made using a simulation program. Tests enable the performance of refrigerant alternatives to be evaluated across a broad range of operating conditions.

Theoretical testing would depend on refrigerant properties while an actual test would depend more on detailed specification of the equipment. The way refrigerants behave and perform in theory or simulation differs from which it perform in an actual system. However, a theoretical test is very useful as a preliminary evaluation before an extreme experimental test which involved a high cost is carried out in a full size equipment.

## **1.2 Refrigerants and Its Alternatives.**

CFC and HCFC have taken the leading stand in refrigerating system since 1930s until early eighties. They became very popular and were found as the refrigerants with good performance compared with other refrigerants. However, by the eighties, CFC was considered as detrineutral to the environment, causing significant damage to the ozone layer. This resulted in the phasing out of the use and manufacture of CFCs, and later of HCFCs. It generates many studies as the search for alternative refrigerants with suitable properties to replace the CFCs and HCFCs. Continues now, many new refrigerants have been produced and commercialized by refrigerant manufacturers like DuPont, ICI, and Honeywell. Most of them are hydrofluorocarbons (HFC) which do not contain chlorine and have zero Ozone Depletion Potential (ODP).

The most common CFCs and HCFC that are being phased out are R12, R22 and R502. R12 is used in domestic refrigerators and freezers, and in automotive air conditioners. The most popular alternative for R12 when the CFCs phase out began is R22. It is pure fluid and has a very good efficiency characteristic on medium temperature range applications. But when the phase out of R22 began, the search for R12 alternatives continues. There are several alternative refrigerants that are potential substitutes for R12 and most of them are mixtures but some are pure fluids. They include R134A, R401A, R401B, R402B, and R409A.

R22 which is a HCFC is widely used in window air conditioners, heat pumps, air conditioners of commercial building and in large industrial refrigeration systems. It is considered as transitional or “interim” alternatives and has a high performance characteristic. Its contain chlorine and will eventually be phased out but can be

manufactured and used until 2030. The “long-term” alternatives for R22 that have been produced are mostly mixtures that do not contain any chlorine such as HFCs. They include R404A, R407C, R410A, and R507. R407C was the first to replace R22, but it was found out in recent research that new replacements R410A and R404A show better performance compared to R407C.

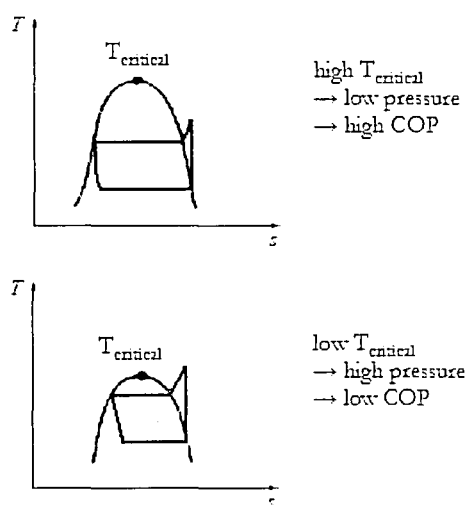
Other pure fluids alternatives for R22 are ammonia (R717) and propane (R290). Ammonia has been used for over 100 years. It is a low cost refrigerant with excellent thermodynamic properties and zero ODP. But it is toxic and flammable. Similar to ammonia, propane is no longer of interest because it is flammable even though it has similar thermophysical properties as R22 [2]. Other HCFC that has been considered is R134A which is widely used as substitute for R22 in large chillers, as well as in automotive air conditioners and refrigerators.

R502 which is a blend of R115 and R22 is the dominant refrigerant used in commercial refrigeration systems such as those in supermarkets because it allows low evaporating temperatures while operating in a single-stage compressor. One of the replacements that have been produced for R502 is R404A. As discussed by David Wylie and Davenport [2], the data of Alternative Refrigerants Evaluation Program (AREP) indicates that R404A has about the same capacity as R502 at lower condensing temperatures, but rapidly decreasing at higher condensing temperatures. For a fixed evaporating temperature, R404A has a lower efficiency when condensing temperature increase compared to R502. It has less efficiency when compared to R502 at high condensing temperature. Other mixtures that have replaced R502 include R402A, R402B, R407C, R408A and R507.

### **1.3 Performance Evaluation of Refrigerants in Refrigeration Cycle.**

The study of refrigerant performance is very important because the behaviour of refrigerants or refrigerant mixtures strongly influence the design of the refrigeration system. Different refrigerants have performed differently based on their thermodynamic properties and behavior. According to Vaisman [3], different refrigerants shows different heat transfer ratios and pressure drops in condensers and evaporators.

Yana Motta and Domanski [4], reported on how the refrigerant's critical temperature affects the refrigerant performance in the vapor compression cycle. As shown conceptually in **Figure 1.1**, differences in refrigerant's critical temperature and the shape of the two-phase dome on T-s diagram explain the different performance trends of the refrigerants.



**Figure 1.1 : Impact of critical temperature of volumetric capacity and COP [4].**

For the same condensing and evaporating temperature, a fluid with a lower critical temperature will tend to have a higher volumetric capacity and a lower Coefficient of Performance (COP) while a fluid with a higher critical temperature will tend to have a lower volumetric capacity and a higher COP. The difference in COPs is related to the different levels of irreversibility on the superheated-horn side and at the throttling process. These levels of irreversibility vary with operating temperatures because the slopes of the saturated liquid and vapor lines change, particularly when approaching the critical point [4]. These are important issues besides considerations like safety, availability, and cost.

The performance comparison which was carried out by simulation had been done by many researchers in terms of first law and second law analysis. Yana Motta and Domanski [4] studied the performance of refrigerant R22 and its possible replacements which are R134a, R290, R410A and R407C in an air-cooled air conditioner system. All

these refrigerants have been evaluated using the NIST's simulation program Cycle 11. The study focuses on the COP and the effect of outdoor temperature on system capacity. It includes performance results for the basic cycle and for the cycle with a liquid line and suction line heat exchanger. The result shows a decreasing in system performance with increasing outdoor temperature. It also shows that the fluids with a low critical temperature experience a larger degradation of cooling capacity.

Vaisman [3] has presented the performance evaluation of R22 and R407C in an air conditioner system with a rotary vane compressor. The exergy approach is applied and performance evaluation is produced taking into account the actual system configuration including compressor data, coil's design, suction line, discharge line and liquid line design, and the data from the fan and blower. The result shows that R407C is compatible with R22 in terms of air conditioner performance.

Spatz and Yana Motta [5] evaluated the performance of R22 but in medium temperature refrigeration systems with its potential alternatives of R410A, R404A, and R290. The studies include thermodynamic analysis, comparison of heat transfer and pressure drop characteristics, system performance comparisons using a validated detailed system model, safety issues, and determination of the environmental impact of refrigerant selection. The result shows that the R410A is an efficient and environmentally acceptable option to replace R22 in medium temperature applications.

Stegou-Sagia and Paignigiannis [6] have focused on exergy analysis of 10 working fluids including R401B, R401C, R402A, R404A, R406A, R408A, R409A, R410A, R410B, R410B and R507. The performances of these mixtures have been compared with the old refrigerants they replace which are R12, R22 and R502. When comparing the exergy efficiencies at constant evaporating temperature, the exergy losses of old refrigerants are found lower. The compression process has been predicted as the process which involved higher exergy losses followed by condensation process. R406A shows the highest value of exergy efficiency, while the lowest value is belongs to the mixture R409A.

C.K Sia [7] has developed a simulation program based on an ideal cycle to evaluate the performance of R12 and its possible replacements R134A and R401A, R22