

Thermoelectric Properties of Bismuth and Silicon Nanowires

Thesis by

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*Dedicated in memory of my grandmother Neda, for her hard work,
generosity, and determination which represents the best of Arab peoples.*

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Abstract

Thermoelectric materials convert temperature differences into electricity and vice versa. Such materials utilize the Seebeck effect for power generation and the Peltier effect for refrigeration. In the Seebeck effect, a temperature gradient across a material causes the diffusion of charged carriers across that gradient, thus creating a voltage difference between the hot and cold ends of the material. Conversely, the Peltier effect explains the fact that when current flows through a material a temperature gradient arises because the charged carriers exchange thermal energy at the contacts. Thermoelectrics perform these functions without moving parts and they do not pollute. This makes them highly reliable and more importantly attractive as renewable energy sources, especially at a time when global warming is a growing concern. However, thermoelectrics find only limited use because of their poor efficiency.

The efficiency of a thermoelectric material is determined by the dimensionless figure of merit, $ZT = \frac{S^2 \sigma}{\kappa} T$, where S is the thermoelectric power, defined as the thermoelectric voltage, V , produced per degree temperature difference $S = \frac{dV}{dT}$, σ is the electrical conductivity, κ is the thermal conductivity, and T is the temperature. To maximize ZT , S must be large so that a small temperature difference can create a large voltage, σ must be large in order to minimize joule heating losses, and κ must be small to reduce heat leakage and maintain a temperature difference. Maximizing ZT is challenging because optimizing one physical parameter often adversely affects another. The best commercially available thermoelectric devices are alloys of Bi_2Te_3 and have a ZT of 1 which corresponds to a carnot efficiency of ~10%. My research has focused on

achieving efficient thermoelectric performance from the single component systems of bismuth and silicon nanowires.

Bismuth nanowires are predicted to undergo a semi-metal to semiconductor transition below a size of 50 nm which should increase the thermopower and thus ZT . Limited experimental evidence by other groups has been acquired to support this claim. Through electric field gating measurements and by tuning the nanowire size, we have shown that no such transition occurs. Instead, surface states dominate the electric transport at a size smaller than 50 nm and bismuth remains a semimetal.

Bulk silicon is a poor thermoelectric due to its large thermal conductivity. However, silicon nanowires may have a dramatically reduced thermal conductivity. By varying the nanowire size and impurity doping levels, ZT values representing an approximately 100-fold improvement over bulk silicon are achieved over a broad temperature range, including a $ZT \sim 1$ at 200K. Independent measurements of S , σ , and κ , combined with theory, indicate that the improved efficiency originates from phonon effects. The thermal conductivity is reduced and the thermopower is enhanced. These results are expected to apply to other classes of semiconductor nanomaterials.

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Chapter 1

Thermoelectrics: History and Physics

1.1 Introduction

In 1821 Thomas Johann Seebeck discovered that a magnetic compass would deflect in the presence of a material with ends at different temperatures¹. He attributed the effect to magnetism. Seebeck's interpretation was wrong. The correct reason was that the temperature difference created a current in the material that deflected the magnet. During seminars, he would vigorously defend his position in light of mounting evidence that suggested the effect was due to an electric current alone that was generated by the temperature difference. Seebeck's discovery, however, would later be named after him. In science, sometimes the interpretation of a discovery is not as important as the discovery itself.

Seebeck's discovery that a temperature gradient across a material creates a voltage was later followed by Peltier's discovery in 1834 of the reverse effect. Peltier showed that a current through a material can freeze water at one end and melt ice at the other². Peltier and Seebeck had discovered two physical effects that had the same underlying physics, and that could do useful work. The Seebeck effect can be used to generate electric power while the Peltier effect can be used to provide refrigeration. However, it wasn't until William Thompson's (Lord Kelvin) discovery of a third effect that the physics of thermoelectricity began to be understood. The Thompson effect

described a material evolving or absorbing heat under the presence of both a current and temperature gradient. Through an educated guess, Thompson correctly predicted that Seebeck's and Peltier's discoveries were actually different manifestations of the same underlying physics. In 1931, Onsager rigorously proved Thompson's educated guess and set the stage for a flurry of experimental studies that were focused on increasing the thermoelectric efficiency.

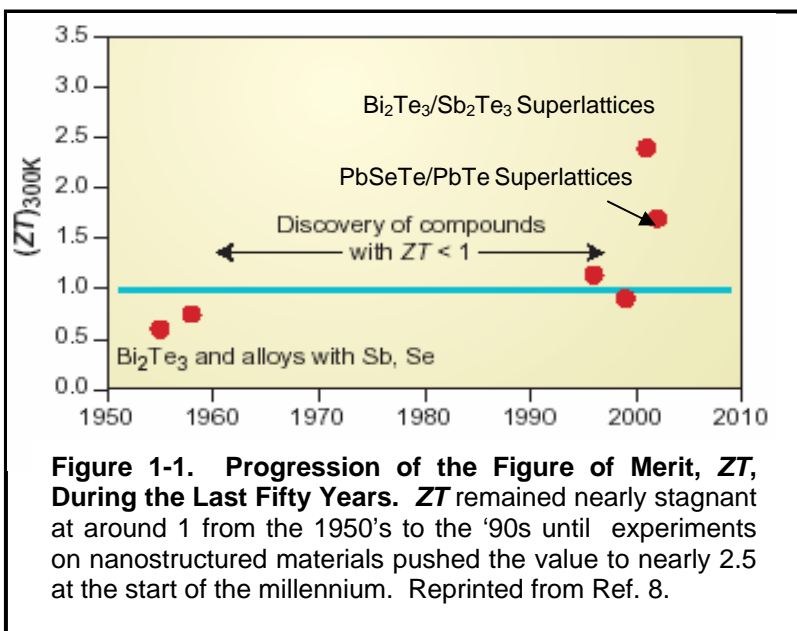
1.2 Thermoelectric Efficiency

Thermoelectric devices offer the promise of power generation and refrigeration with no moving parts and nearly maintenance free operation³⁻⁵. A temperature difference across any non-superconducting material will create a voltage that can be used to provide power. A current through that same material can be used to cool one end for refrigeration purposes. Thermoelectrics are essentially particle heat engines where the working fluid is composed of either electrons or holes. The outstanding challenge in the study of thermoelectrics is to find materials that can provide power and refrigeration at a high thermodynamic efficiency. Presently, thermoelectrics are thirty to twenty percent less efficient than present day fossil-fuel burning power plants and compressor-based refrigerators. The thermoelectric principles are well understood for bulk materials and the most efficient ones are based on alloys of Bi_2Te_3 with efficiencies⁶ hovering around 10%.

The efficiency of a thermoelectric material is determined by the dimensionless figure of merit, $ZT = \frac{S^2 \sigma}{\kappa} T$, where S is the thermoelectric power, defined as the

thermoelectric voltage (V) produced per degree temperature difference $S = \frac{\Delta V}{\Delta T}$, σ is the electrical conductivity, κ is the total thermal conductivity consisting of both phonon and electronic contributions, and T is the temperature. The efficiency is related to ZT by the following equation⁷ (see Appendix 1.1 for a full derivation):

$$\eta = \frac{\Delta T}{T_{Hot}} \frac{\sqrt{1 + ZT} - 1}{\sqrt{1 + ZT} + \frac{T_{Cold}}{T_{Hot}}} \dots\dots\dots\text{equation 1}$$



where T_{Hot} is the temperature of the hot junction and T_{cold} is the temperature of the cold junction. One immediately sees from equation 1 that the efficiency tends towards the Carnot limit when ZT

approaches infinity. To compete with modern-day compressor based refrigerators, a thermoelectric device must have a $ZT > 3$ (Figure 1-1). There is no theoretical limit to ZT . To maximize ZT , S must be large so that a small temperature difference can create a large voltage, σ must be large in order to minimize joule heating losses, and κ must be small to reduce heat leakage and maintain a temperature difference⁹. S , σ , and κ are not, however, mutually exclusive. For instance in a bulk material, the Weidmann-Franz law limits the ratio σ/κ_e , where κ_e is the electronic contribution to the total thermal

conductivity. Also, a sharply peaked density of states favors large \mathcal{S} , but the density of states is a smoothly varying function for bulk materials. Nanowires may offer the possibility to circumvent some of the materials limitations found in bulk. First, the thermal conductivity has been shown to decrease when the size of a material is reduced to the nano-scale¹⁰⁻¹³. Second, the thermopower is sensitive to the density of states and phonon-electron scattering, which may be very different in certain materials at the nano-scale¹⁴. To increase ZT , a better understanding of the interplay between the three materials parameters, \mathcal{S} , σ , and κ , must be developed.

1.3 Fundamental Principles—The Seebeck Effect for Power Generation

The Seebeck, thermoelectric power, or thermopower, effect describes the fact that a temperature gradient drives the diffusion of charged carriers which in turn creates a voltage³⁻⁵. The Seebeck coefficient of a material depends on the material's temperature and crystal structure. The terms thermoelectric power and thermopower are misnomers since they measure the voltage or electric field (not the electric power) induced in response to a temperature difference. Fundamentally, the thermopower is a measure of the amount of net entropy transported per carrier¹⁵. The major contributors to the transfer of entropy in the presence of a temperature gradient originate from diffusion and/or phonon drag effects. Both effects are seen in metals and semiconductors, however, one typically dominates over the other. For example, diffusion dominates the thermopower for most metals whereas phonon drag can be a hundred times larger than diffusion in semiconductors.

1.3.1 Diffusion Thermopower

Classically, gas molecules that are heated possess larger average velocities than when cold and thus diffuse more rapidly. In the solid state, a mobile electron gas diffusing to the cold side leaves behind the oppositely charged and immobile nuclei at the hot side which gives rise to a thermoelectric voltage. This separation of charges creates an electric field. At open-circuit equilibrium the buildup of electrons onto the cold side from diffusion eventually ceases at some maximum value because of the oppositely directed drift of charged carriers from the electric force-field. Only an increase in the temperature difference can resume the buildup of more charges on the cold side and thus lead to an increase in the thermoelectric voltage.

A classical explanation of the Seebeck effect only explains the thermoelectric voltage due to electrons and ignores holes. Also, classically, the statistics of the particles is ignored but electrons and holes are fermions and must obey Fermi-Dirac statistics. In reality, the sign of the thermoelectric voltage can take two values, positive or negative, depending on the dominant charge carriers—electrons or holes. By convention, if the dominant charge carriers are electrons then the Seebeck coefficient is negative and vice versa for holes.

1.3.2 Diffusion Thermopower in Metals

The analysis of the thermopower in a metal can be simplified if it is assumed that the density of states is that of a 3-D free electron system. Only electrons near the Fermi surface participate in the electronic transport. The electrons in such a material possess kT energy and there are kT/E_F electrons with that energy where k is Boltzmann's constant, T

is the temperature and E_F is the Fermi energy. The thermopower is the amount of entropy transported per electronic charge. kT/T is the entropy the electrons transfer where kT is the amount of heat they possess. Therefore the thermopower of a 3-D free electron system is proportional to $\frac{k^2T}{eE_F}$ where e is the electronic charge.

A more accurate quantum-mechanical explanation of the Seebeck effect was given by Sir Neville Mott derived from Boltzmann's transport equation¹⁶. The Mott equation, valid only for metals, is:

$$S = \frac{\pi^2 k^2 T}{3e} \left. \frac{\partial \ln \sigma(E)}{\partial E} \right|_{E_F} \dots\dots\dots \text{equation 2}$$

where T is the temperature, k is Boltzmann's constant, e is the electronic charge, and σ is the conductivity when the electron energy, E , equals to the Fermi energy, E_F . In a metal the electrical conductivity is a function of the density of states, scattering rate, and carrier velocity. Therefore equation 1 can be written:

$$S = \frac{\pi^2 k^2 T}{3e} \left[\left. \frac{\partial \ln N(E)}{\partial E} \right|_{E_F} + \left. \frac{\partial \ln \tau(E)}{\partial E} \right|_{E_F} + \left. \frac{\partial \ln v^2(E)}{\partial E} \right|_{E_F} \right] \dots\dots\dots \text{equation 3}$$

where $N(E)$ is the density of states (DOS), τ is the scattering rate and v is the carrier velocity. The Seebeck coefficient is therefore independent of the magnitude of these three terms and depends only on their rate of change. The diffusion thermopower is linearly dependent on T and due to the second law of thermodynamics goes to zero near 0K. A thermodynamic treatment of the change in chemical potential upon application of

a temperature gradient that ignores carrier scattering leads to a more intuitive explanation for the Seebeck coefficient.

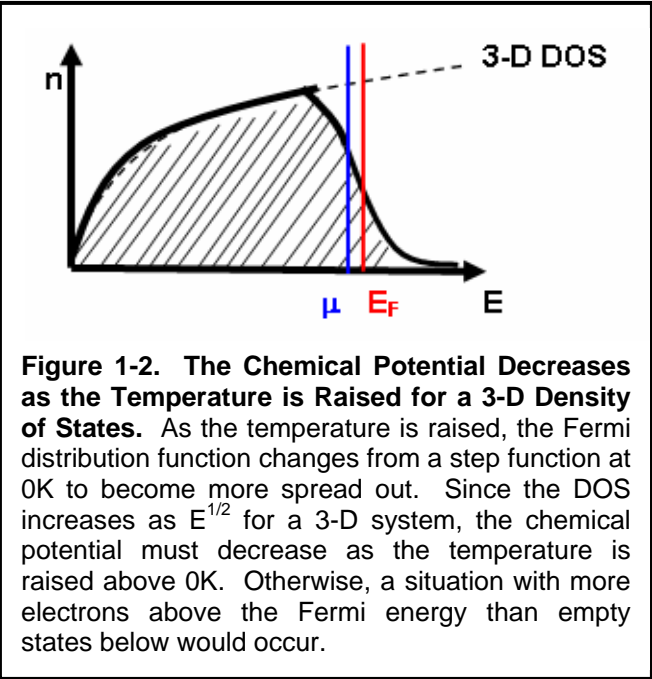
1.3.3 The (Electro-)Chemical Potential

The chemical potential is defined as the amount of energy needed to add one particle into a system while keeping the entropy and temperature constant. The chemical potential is a measure of the energy brought into and out of a system when particles are exchanged, akin to the temperature which measures the energy change of a system when entropy is exchanged¹⁷. Particles flow or diffuse when there are chemical potential differences. Chemical potential differences are responsible for the operation of most power generators such as batteries, solar cells, and thermoelectrics.

Batteries. Batteries provide power by employing anodes and cathodes that have different chemical potentials for electrons. Low lying energy states in the cathode cause electrons to flow from anode to cathode when the two are connected, for example, by a metallic wire. The flow of electrons from anode to cathode would cease if not for the electrolyte which contains chemicals that either give up electrons or accept them, thus replenishing the anode with electrons and removing them from the cathode. When the chemicals are used up, the battery can no longer provide power. The chemical potential difference between anode and cathode, therefore, is the cause of the electrical current flow. If the anode and cathode are the same material, then there would be no net chemical potential difference and the battery would provide no power.

Solar Cells A solar cell provides power upon illumination by photons. The photons create electron-hole pairs by promoting electrons into the conduction band from the

valence band. The electron-hole pairs are then separated into electrodes that have an affinity for either electrons or holes but not both. The affinity can be manifested by empty molecular orbitals in the electrode material that electrons and holes are drawn into, for example, in a polymer-inorganic photovoltaic cell. In typical p-n junction silicon solar cells, the photons create a chemical potential difference by altering the minority carrier concentration in the two junctions¹⁸. An often heard misconception is that the built-in electric field in a p-n junction solar cell is responsible for the separation which is not true. The separation is solely due to the chemical potential difference induced by the



photons.

Thermoelectrics A thermoelectric device provides power when a temperature difference is applied to its ends. The chemical potential is sensitive to the temperature and, neglecting scattering effects, depends on the derivative of the density of states through the Sommerfeld approximation⁴:

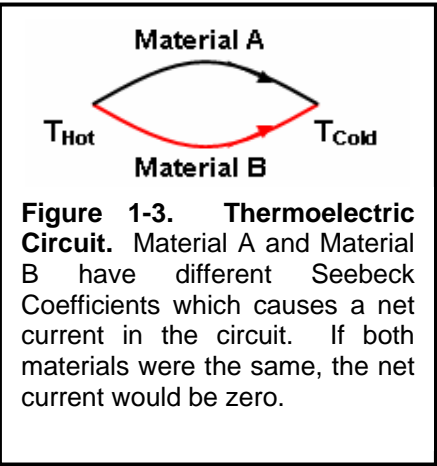
$$\mu = E_F - \frac{\pi^2}{6} (kT)^2 \left[\frac{\partial}{\partial E} \ln N(E) \right]_{E=E_F} + \dots \quad \text{equation 4}$$

The total number of electrons must always be the same regardless of the temperature.

The electron density is given by:

$$n = \int_0^\infty N(E) f(E) dE \dots\dots\dots \text{equation 5}$$

For 3-D free electron systems, the DOS is proportional to $E^{1/2}$. The Fermi function $f(E)$ becomes more spread out as T increases and since the electron density is a product of the DOS and Fermi function, the chemical potential must decrease (see Figure 1-2). Otherwise, one would encounter a situation with more electrons above the Fermi energy than empty states below¹⁹. Such a scenario would imply that electrons were added into the material as the temperature was increased. As long as the DOS is not constant near the Fermi energy, the temperature difference across a thermoelectric device will create a chemical potential difference that drives the diffusion of carriers (see Appendix 1.2).



Similar to the situation in batteries, a thermoelectric circuit constructed with the same material for both electrodes, (Figure 1-3), would provide no power. The chemical potential difference is the same across both electrodes and leads to opposing currents that cancel.

1.3.4 Diffusion Thermopower in Semiconductors

The expression for the thermopower must be modified for semiconductors since at the Fermi energy, the conductivity as expressed in equation 2 would be zero. Since, in general, the thermopower is the amount of net entropy transferred per charge carrier and since the entropy is just the heat carried by each charge carrier per unit temperature, we can write the thermopower as⁴:

$$S = \frac{Q}{T} \frac{1}{e} = \frac{E - \mu}{eT} \dots\dots\dots\text{equation 6}$$

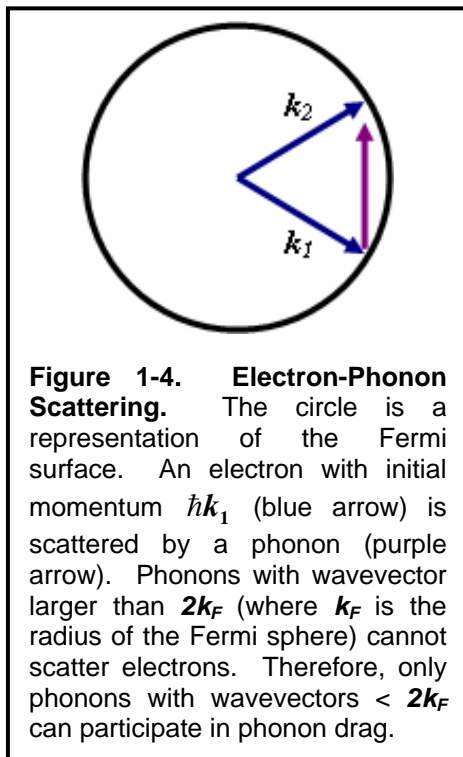
where Q is the heat transported by the charge carriers, T is the temperature, e is the electronic charge, E is the total energy, kinetic plus potential, that the carriers possess and μ is the chemical potential (Fermi energy). For lightly doped semiconductors, $E - \mu$ can be quite large so that semiconductors typically have larger thermopowers than metals²⁰. Thermopower values are typically on the order of hundreds of microvolts. The thermopower in semiconductors is highly sensitive to the doping concentration since this controls $E - \mu$.

1.3.5 Phonon Drag Thermopower

A temperature gradient across a thermoelectric material causes the phonon system to be placed out of thermodynamic equilibrium. This is manifested in the form of a heat current where the phonon energy is propagated down the temperature gradient. If the phonon-carrier interaction is strong, the phonons may impart some of their energy to the diffusing carriers via momentum transfer³. At open circuit, the phonons effectively “drag” the carriers along the temperature gradient which causes an increase in the buildup of charge above that from diffusion of the carriers alone. The phonon drag and diffusion components can be treated independently and therefore the total thermopower can be written as $S = S_{diffusion} + S_{phonon-drag}$.

A classical treatment similar to that for the diffusion thermopower applies to the phonon system. The phonons can be treated as an isotropic gas that expands due to the temperature gradient. The expanding phonon gas exerts a pressure on the carriers that is biased towards the cold end due to the temperature gradient. The magnitude of the phonon drag thermopower depends on the strength of the interaction between the carriers

and phonons. Also, the phonon-carrier relaxation time should be shorter than the phonon-phonon relaxation time. That is because to enhance the thermoelectric voltage, the phonons should preferentially lose their energy to the carriers rather than to other phonon scattering events that arise from anharmonic coupling³. The fact that phonons may scatter with other phonons is the main reason why phonon drag in metals is only observed at low temperatures. At high temperatures phonons in metals lose most of their energy by scattering with other phonons. At very low temperatures, there are not enough populated phonon modes to significantly contribute to the thermopower. The thermopower due to phonon drag can be expressed as: $S_{\text{ph}} \approx \left(\frac{\tau_{\text{ph}}}{\mu T} \right)$ where τ_{ph} is the phonon-phonon relaxation time, μ is the carrier mobility and T is the temperature³. Metals exhibit a thermopower that peaks between 4-50K due to phonon drag.



Phonons participating in phonon drag are typically low frequency because they scatter less often with other phonons than their high frequency counterparts. Only phonons with wave-vectors smaller than $2k_F$ can participate in phonon-carrier scattering (Figure 1-4). The Fermi surface in semiconductors is considerably smaller than metals since the carrier concentration is lower by ~3-4 orders of magnitude. Therefore, phonon drag dominates the thermopower in low doped semiconductors such as silicon since the low

frequency phonons are the dominant heat carriers²¹.

1.4 Other Entropic Contributions to the Thermopower

In general any net transfer of entropy due to a temperature gradient will give rise to a thermoelectric voltage. The thermopower can generally be expressed as:

$$S = \frac{S_{entropy}}{e} \dots\dots\dots\text{equation 7}$$

where $S_{entropy}$ is the net entropy transferred in the presence of a temperature gradient and e is the electronic charge. Magnetic systems such as $Na_xCo_2O_4$ can transfer spin entropy which gives rise to a thermopower²². According to equation 7, such systems exhibit a contribution from the spins given by:

$$S = \frac{\ln \Omega}{e} \dots\dots\dots\text{equation 8}$$

where $\ln \Omega$ is the entropy from the spin degeneracy, Ω .

1.5 Fundamental Principles—The Peltier Effect for Refrigeration

The Peltier effect describes the fact that a current through a thermoelectric material will

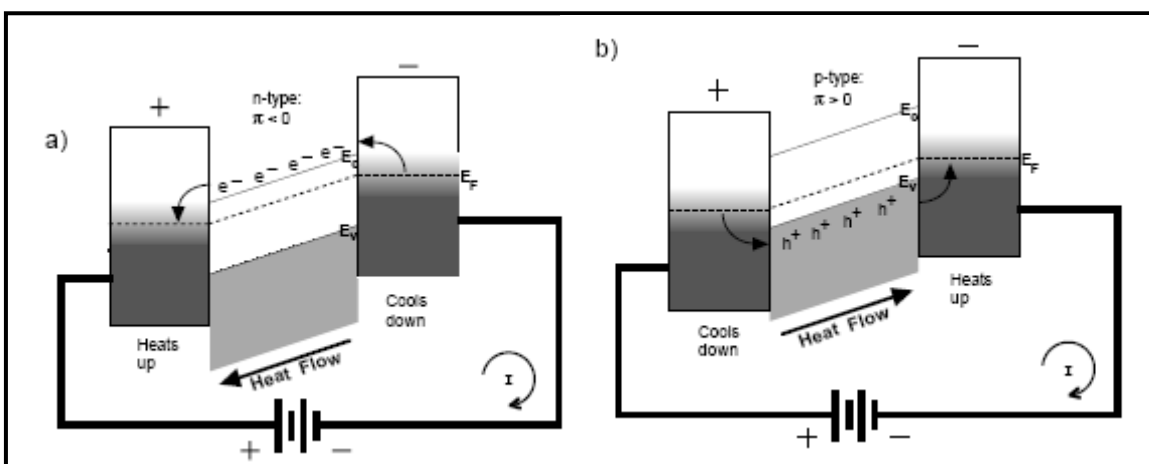


Figure 1-5. Peltier Effect for a Semiconductor/Metal Circuit. a) Only hot electrons at the right junction are able to enter the semiconductor’s conduction band. These electrons remove heat from the junction and subsequently cool it down. Electrons from the semiconductor enter the metal at the left junction and thermalize near the metal’s Fermi energy. This causes the left junction to become hot. b) The current direction is reversed which causes the left junction to become cold and the right junction to become hot. Reprinted from Ref. 23.

generate a temperature difference across its ends. The Peltier effect is the reverse of the Seebeck effect. The current, supplied by a power generator, exchanges heat at the junctions with the electrodes²³ (Figure 1-5). There the heat is either absorbed or released. This causes one junction to become cold and the other hot. The cold junction can be used as a refrigerator. The Peltier effect is reversible meaning that the cold and hot junctions can change polarity if the current direction is reversed.

The magnitude of the Peltier effect is given by the Peltier coefficient, Π , which is the ratio between the heat current and electric current. The Peltier coefficient is related to the Seebeck coefficient by the following relation: $\Pi = ST$.

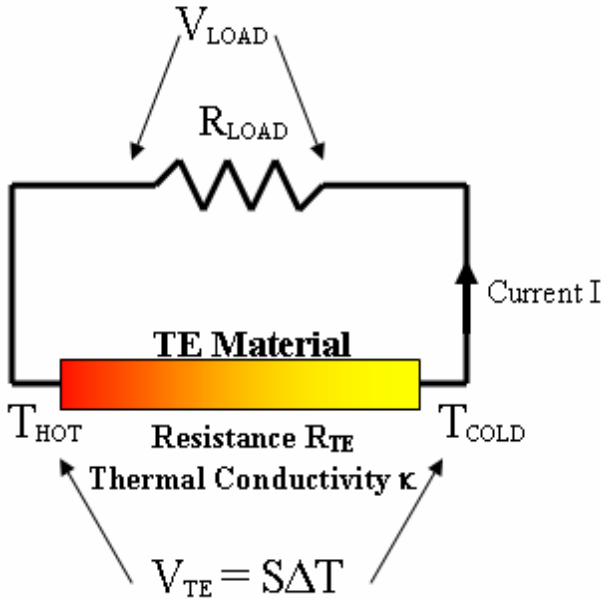
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Appendix 1.1

Derivation of the Efficiency for a Thermoelectric Device



1. The efficiency η is given by: $\eta = \frac{W}{Q}$ where W is the work output of the TE generator and Q is the heat input into the hot reservoir.
2. The useful work that can be extracted from the TE generator is equal to the power dissipated in the load resistor. $W = IV_{LOAD}$.
3. From voltage division: $V_{LOAD} = V_{TE} \left(\frac{R_{LOAD}}{R_{LOAD} + R_{TE}} \right) = S\Delta T \left(\frac{R_{LOAD}}{R_{LOAD} + R_{TE}} \right)$.
4. The current is: $I = \frac{S\Delta T}{R_{LOAD} + R_{TE}}$.
5. Therefore: $W = S^2 \Delta T^2 \left[\frac{R_{LOAD}}{(R_{LOAD} + R_{TE})^2} \right]$.
6. The heat input into the TE generator can be broken up into three terms: a) the heat that originates at the hot junction via standard thermal conduction (phonons and carriers) $Q_1 = \kappa\Delta T$, this heat is transferred to the cold junction, b) the heat that

originates at the hot junction by the Peltier effect due to the current

$$Q_2 = IST_{HOT} = \frac{S^2 \Delta T T_{HOT}}{(R_{LOAD} + R_{TE})}, \text{ this heat is also transferred to the cold junction,}$$

and c) the heat that originates via joule heating in the material half of which continues to the cold junction and half of which is transferred back to the hot junction; the latter is what we are concerned about since Q is the heat input at the

$$\text{hot junction } Q_3 = -\frac{1}{2} I^2 R_{TE} = -\frac{1}{2} \frac{S^2 \Delta T^2 R_{TE}}{(R_{LOAD} + R_{TE})^2}.$$

7. Therefore combining the terms:

$$Q = \kappa \Delta T + \frac{S^2 \Delta T T_{HOT}}{(R_{LOAD} + R_{TE})} - \frac{1}{2} \frac{S^2 \Delta T^2 R_{TE}}{(R_{LOAD} + R_{TE})^2}.$$

8. So the efficiency becomes: $\eta = \frac{S^2 \Delta T^2 \left[\frac{R_{LOAD}}{(R_{LOAD} + R_{TE})^2} \right]}{\kappa \Delta T + \frac{S^2 \Delta T T_{HOT}}{(R_{LOAD} + R_{TE})} - \frac{1}{2} \frac{S^2 \Delta T^2 R_{TE}}{(R_{LOAD} + R_{TE})^2}}.$

9. We now want to know how to maximize the efficiency. This will depend on the ratio of the load resistance to the TE resistance. We will define this ratio as

$$m = \frac{R_{LOAD}}{R_{TE}}. \text{ We know from standard electronics that maximum power transfer}$$

occurs when $R_{LOAD} = R_{TE}$ so that $m = 1$. But what value will m take for maximum efficiency?

10. We can rewrite the efficiency as: $\eta = \frac{S^2 \Delta T^2 \frac{m}{R_{TE} (m+1)^2}}{\kappa \Delta T + \frac{S^2 \Delta T T_{HOT}}{R_{TE} (m+1)} - \frac{1}{2} \frac{S^2 \Delta T^2}{R_{TE} (m+1)^2}}.$

11. Reducing this equation further by pulling out the term: $\frac{S^2 \Delta T T_{HOT}}{R_{TE} (m+1)}$ out of the

denominator, we have:
$$\eta = \frac{\Delta T}{T_{HOT}} \left[\frac{\frac{m}{(m+1)}}{1 + \frac{\kappa R_{TE} (m+1)}{S^2 T_{HOT}} - \frac{1}{2} \frac{\Delta T}{T_{HOT}} \frac{1}{(m+1)}} \right]$$

12. Now we are in the position to maximize η .

13.
$$\frac{\partial \eta}{\partial m} = 0 =$$

$$\frac{\Delta T}{T_{HOT}} \left\{ \frac{\left[\frac{1}{(m+1)} - \frac{m}{(m+1)^2} \right] \left[1 + \frac{\kappa R_{TE} (m+1)}{S^2 T_{HOT}} - \frac{1}{2} \frac{\Delta T}{T_{HOT}} \frac{1}{(m+1)} \right] - \left(\frac{m}{m+1} \right) \left[\frac{\kappa R_{TE}}{S^2 T_{HOT}} + \frac{1}{2} \frac{\Delta T}{T_{HOT} (m+1)^2} \right]}{\left[1 + \frac{\kappa R_{TE} (m+1)}{S^2 T_{HOT}} - \frac{1}{2} \frac{\Delta T}{T_{HOT}} \frac{1}{(m+1)} \right]^2} \right\}$$

14. Defining $Z = \frac{S^2}{\kappa R_{TE}}$, we have:

$$0 = \frac{1}{(m+1)} - \frac{m}{(m+1)^2} + \frac{1}{Z T_{HOT}} - \frac{1}{2} \frac{\Delta T}{T_{HOT} (m+1)^2} - \frac{1}{Z T_{HOT}} \frac{m}{(m+1)} + \frac{1}{2} \frac{\Delta T}{T_{HOT}} \frac{m}{(m+1)^3} - \frac{m}{(m+1)} \frac{1}{Z T_{HOT}} - \frac{1}{2} \frac{\Delta T}{T_{HOT}} \frac{m}{(m+1)}$$

15.
$$0 = \frac{1}{(m+1)} - \frac{m}{(m+1)^2} + \frac{1}{Z T_{HOT}} - \frac{2m}{Z T_{HOT} (m+1)} - \frac{1}{2} \frac{\Delta T}{T_{HOT} (m+1)^2}$$

16. Multiplying through by $(m+1)^2$, we have:

$$m+1 - m + \frac{(m+1)^2}{Z T_{HOT}} - \frac{2m(m+1)}{Z T_{HOT}} - \frac{1}{2} \frac{\Delta T}{T_{HOT}} \frac{1}{(m+1)^2} = 0$$

17.
$$\frac{(m+1)^2}{Z T_{HOT}} - \frac{2m(m+1)}{Z T_{HOT}} = \frac{1}{2} \frac{\Delta T}{T_{HOT}} - 1$$

18. Multiplying through by ZT_{HOT} , we have:

$$m^2 + 2m + 1 - 2m^2 - 2m = \frac{1}{2}Z\Delta T - ZT_{HOT}$$

19. $m^2 = 1 + \frac{Z}{2}(2T_{HOT} - T_{HOT} + T_{COLD})$

20. Finally: $m = \sqrt{1 + \frac{Z}{2}(T_{HOT} + T_{COLD})} = \sqrt{1 + Z\bar{T}}$ where $\frac{T_{HOT} + T_{COLD}}{2} = \bar{T}$

21. Substituting back into the equation for the efficiency, we have:

$$\eta_{\max} = \frac{\Delta T}{T_{HOT}} \frac{\sqrt{1 + Z\bar{T}} - 1}{\sqrt{1 + Z\bar{T}} + \frac{T_{COLD}}{T_{HOT}}}$$

22. We can see that as $Z\bar{T} \rightarrow \infty$, $\eta_{\max} = \frac{\Delta T}{T_{HOT}}$ (the Carnot efficiency)

Appendix 1.2

Derivation of the Thermopower Dependence on the Density of States

Consider a thermoelectric material with density of states $N(E)$ and temperature difference $\Delta T = T_{Hot} - T_{Cold}$ across its ends. Using the first two terms of the Sommerfeld expansion, the chemical potential can be approximated by:

$$\mu = E_F - \frac{\pi^2}{6} (kT)^2 \left[\frac{\partial}{\partial E} \ln N(E) \right]_{E=E_F}$$

The chemical potential at the cold end of the thermoelectric is given by:

$$\mu = E_F - \frac{\pi^2}{6} (kT_{Cold})^2 \left[\frac{\partial}{\partial E} \ln N(E) \right]_{E=E_F}$$

The chemical potential at the hot end of the thermoelectric is given by:

$$\mu = E_F - \frac{\pi^2}{6} [k(T_{Cold} + \delta T)]^2 \left[\frac{\partial}{\partial E} \ln N(E) \right]_{E=E_F}$$

where δT is $\ll 1$. Therefore, there is a chemical potential difference between the hot and cold ends of the thermoelectric material:

$$\Delta\mu = \frac{\pi^2}{6} k^2 (2T_{Cold} \delta T) \left[\frac{\partial}{\partial E} \ln N(E) \right]_{E=E_F}$$

The carriers diffuse because the temperature difference creates a chemical potential difference. The diffusion of the charged carriers creates an electric field that opposes further diffusion. Eventually, a dynamic equilibrium exists and the chemical potential difference equals the voltage difference that opposes further diffusion:

$$\Delta\mu = e\Delta V = \frac{\pi^2}{6} k^2 (2T_{Cold} \delta T) \left[\frac{\partial}{\partial E} \ln N(E) \right]_{E=E_F}$$

Therefore, the thermopower is:

$$S = \frac{\Delta V}{\delta T} = \frac{\pi^2}{3} \frac{k^2}{e} T_{Cold} \left[\frac{\partial}{\partial E} \ln N(E) \right]_{E=E_F}$$

This is identical to the Mott formula derived using Boltzmann's transport equation except that the dependence of scattering has not been taken into account.

Chapter 2

Fabrication and Measurements of Bismuth and Silicon Thermoelectric Devices

The results presented in this chapter and chapters 3 and 4 are largely extracted from A. Boukai, *et al.* *Advanced Materials* 18, 864–869 (2006) and A.I. Boukai *et al.* *Nature* 451, 168–171 (2008).

2.1 Bismuth and Silicon Nanowires for Use as Thermoelectrics

Bismuth has a small effective mass ($0.001m_0$ along the trigonal direction), large thermoelectric power ($50 \mu\text{V/K}$ to $100 \mu\text{V/K}$), and small thermal conductivity ($8 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$), all of which help increase ZT^1 . For bulk Bi, ZT is limited because the conduction and valence bands indirectly overlap ($\sim 38 \text{ meV}$), which causes Bi to be a compensated semimetal,² meaning that the contributions of holes and electrons to S cancel each other. However, a semimetal-to-semiconductor transition has been predicted for Bi nanowires below a critical size ($\sim 50 \text{ nm}$ depending on the crystal orientation) due to the quantum confinement effect^{1,3}. Below this size, Bi nanowires can be doped either n- or p-type which causes S to be significantly enhanced for Bi nanowires (NWs) with optimized position of the Fermi energy. 1-D semiconductors are also characterized by a sharply peaked density of states^{4,5}. Experimental evidence of the enhancement of S has been reported in Bi nanocomposites⁶. A Bi nanowire will also have a reduced κ due to phonon scattering off the sidewalls which helps increase $ZT^{1,7}$.

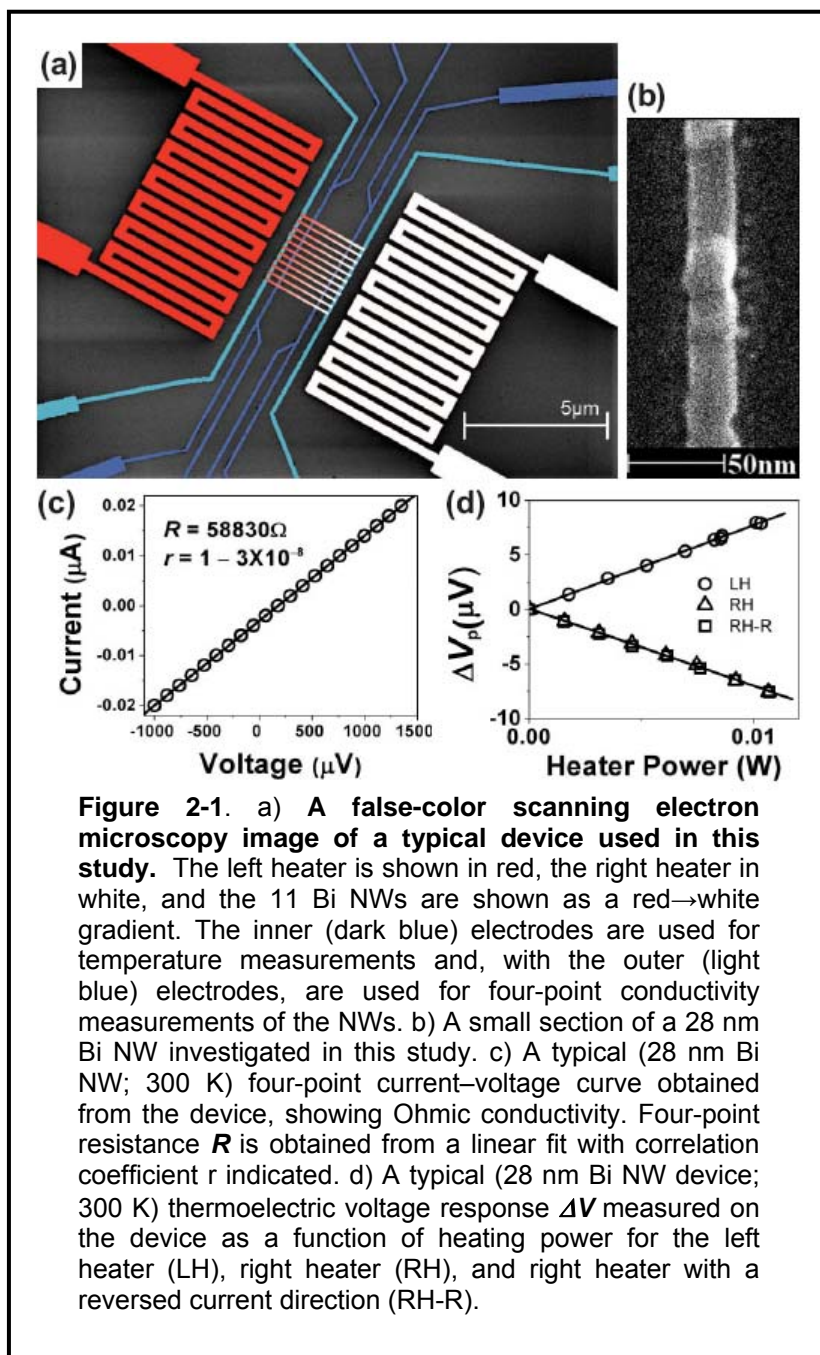
Bulk Si is a poor thermoelectric due to its large thermal conductivity, $150 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$, at room temperature. Si nanowires have been shown to have dramatically reduced thermal conductivities. Therefore, if the electrical conductivity and thermopower of a Si nanowire can be maintained similar to the bulk, the Si nanowires have the potential to be efficient thermoelectrics.

2.2 Fabrication of Bismuth Nanowires

Owing to its chemical instability and low melting point ($\sim 271^\circ\text{C}$), fabrication and electric measurements of Bi nanowires are challenging. Embedded nanowire arrays have been prepared in porous templates by various methods⁸⁻¹⁰. Transport properties of such embedded NWs are limited to two-point resistance measurements,^{9,10,11-16} with the numbers of wires measured being indeterminate^{17,18}. Fewer measurements on the thermoelectric power of Bi nanowire arrays have been reported^{15,16}. In addition, the very small thicknesses of the embedded NW samples leads to an underestimate of S because the thermocouples used to measure the temperature are comparable to the sample thickness¹⁷.

We have overcome several of these limitations by coupling a device architecture used by Small *et. al.*¹⁹ and Llaguno *et. al.*²⁰ for nanotube studies with nanofabrication steps that are compatible with the material limitations of bismuth. This resulting device provides a reliable four-point electrical conductivity measurement, allows for accurate measurements of thermoelectric power, and permits quantitation of electric and magnetic field effects on the transport of individual Bi NW.

Figure 2-1(a) shows one of our devices. Thin Pt/Ti (7 nm/3 nm) electrodes and



Pt/Ti (50 nm/10 nm) heaters are fabricated onto a thermal SiO₂ coated (500 nm thick) degenerately doped Si substrate by electron beam lithography (EBL). As the last step, ~2 μm long NWs are defined across the Pt electrodes by EBL. 15 nm of bismuth (99.999%, Puratronic, Alfa Aesar) is e-beam evaporated at room temperature at 0.5 Å/s with a base pressure of $< 5 \times 10^{-7}$ Torr. A 28 nm wide Bi NW is

shown in Figure 2-1(b). The NWs are polycrystalline with an in-plane grain size comparable to the wire width. XRD results on a 15 nm thick film show the (003) and (006) peaks of rhombohedral Bi, with grains aligning to the (001) trigonal orientation

normal to the substrate, but likely with arbitrary in-plane orientations²¹. Dimensions are measured with a scanning electron microscope (SEM) and atomic force microscopy (AFM).

The Bi NWs are extremely fragile due to their small size, low melting point, and chemical instability. They are easily broken by ambient static charges and oxidation typically causes a 1% increase of the measured four-point resistance for every hour of air exposure. Thus, the NWs are fabricated just prior to wire bonding and chip mounting. During these last steps, the device contacts are shorted through a guard ring that is disconnected right before the device is loaded into a helium-sealed thermostat. With this approach, the NWs remain intact and no discernible increase of resistance is found during the course of the few-week measurement period.

2.3 Thermoelectric Measurements on Bismuth Nanowires

The outer electrodes pass a current through the NWs, while the inner two sets serve as voltage probes for the four-point measurements and the thermoelectric voltage measurements. A current passed through a heater locally heats the SiO₂, resulting in a temperature gradient (and thermoelectric voltage) along the Bi NWs. The thermoelectric voltage is detected from the inner two sets of electrodes with a Keithley 2182 nanovoltmeter (impedance >10GΩ), as a function of the heater power [Figure 2-1(d)]. The temperature difference between these inner electrodes is calibrated to the heater power by monitoring the respective changes in their four-point resistance when changing the heater power or system temperature (within 4K). The calibration is done on every

device for each temperature point that the thermoelectric power is measured. The highly doped Si substrate underneath SiO₂ serves as a gate electrode for electric field effect measurements.

Care was taken to eliminate possible experimental artifacts. For four-point resistance measurements, I - V curves [Figure 2-1(c)] are always obtained with good linearity, confirming ohmic conductivity of the NWs. The resistance is obtained from the slope rather than from a single-point I - V calculation to avoid possible influences from offset voltages. For thermoelectric measurements, either of the heaters is turned on right after re-zeroing the nanovoltmeter, and the voltage change ΔV is recorded as the thermoelectric voltage after the system has reached thermal equilibrium. ΔV originates from the temperature gradient caused by local heating based on the observations that ΔV increases linearly with the increase of heater power (square of the current), and that a reversed direction of current in the heater (which produces the same joule heat) doesn't change ΔV . Finally, passing a current through the heater on the other side of the NWs produces a comparable ΔV , but with opposite sign [Figure 2-1(d)]. The measured thermopower contains the thermopower contribution from the electrical leads (Appendix 2.1).

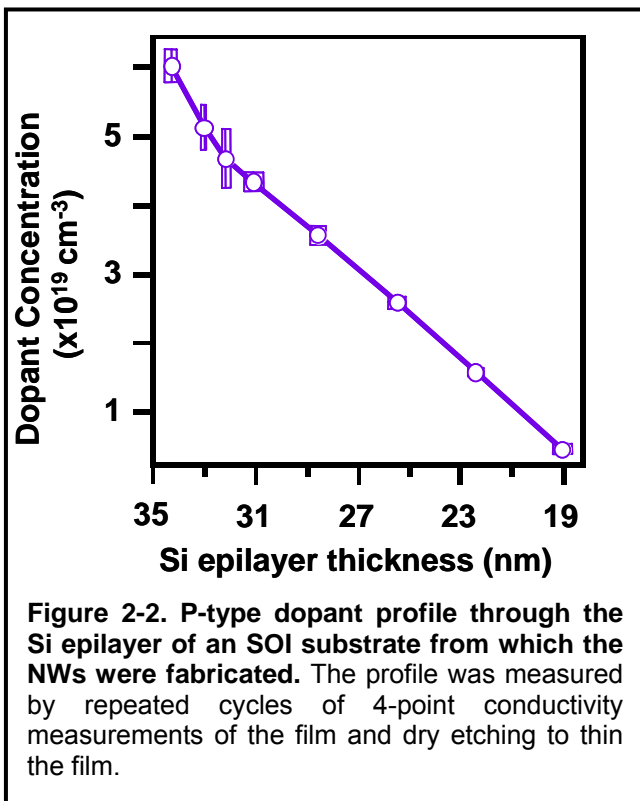
2.4 Fabrication of Silicon Nanowires

The devices used were fabricated from intrinsic silicon-on-insulator (SOI) substrates (Ibis Technology) with a buried oxide thickness of 150nm. The top Si(100) epilayer began with a thickness of 400nm and was thinned through repeated thermal oxidations and wet

chemical etching steps until the desired Si layer thickness (20nm or 35nm) was obtained. AFM analysis revealed a smooth surface with an rms roughness of ~ 3.6 Å. Next, the Si epilayer was doped using a boron containing spin-on dopant (Filmtronics Boron-A) (21). After spin coating, the substrates were baked (250 °C; 5 min) and annealed under flowing N₂ using a rapid thermal processor at temperatures corresponding to the desired doping concentration by allowing the boron to diffuse into the silicon. Four-point probe conductivity measurements determined the p-type doping concentration. We have previously reported that the doping profile through the thickness of the epilayer drops rapidly from the top surface (Figure 2-2)²².

There are multiple ways to prepare Si NWs, including materials methods for bulk production. We wanted Si NWs in which the dimensions, impurity doping levels, crystallographic nature, etc., were all quantifiable and precisely controlled. Thus we utilized the Superlattice Nanowire Pattern transfer (SNAP) method²³ that translates the atomic control over the layer thickness of a superlattice into control over the width and spacing of NWs. Si NWs made via SNAP inherit their impurity dopant concentrations directly from the single-crystal Si epilayers of the silicon-on-insulator (SOI) substrates from which they are fabricated. These epilayers were 20 or 35 nm thick Si(100) films on 150 nm of SiO₂, and were p-type impurity (Boron) doped using diffusion based doping²². Four-point probe conductivity measurements of the SOI films were utilized to extract dopant concentrations. We prepared NW arrays several micrometers long, with lateral dimensions of 10×20, 20×20, and 520×35 (width×thickness in nm). This last one approximates the bulk and, in fact, measurements on the sample obtained bulk values for S , σ , and κ .

After the diffusion doping process, the substrates were used to fabricate Si NWs using the SNAP process²³. The PMMA/epoxy used to hold the superlattice onto the SOI consisted of .37g of 6% by weight PMMA dissolved in 20 mL of chlorobenzene with the



addition of 20 drops part A epoxide and 2 drops part B hardener (Epoxy Bond 110, Allied High Tech, Rancho Dominguez, CA). The depth of the NWs was nominally 20nm (the SOI substrate thickness). However, the “electrical” depth, the distance at which the doping concentration decreased by an order of magnitude or more, was 10-15 nm (Figure 2-2). SEM and AFM were used to

determine the dimensions of our Si NWs. Devices contained from 10 to 400 NWs connected in parallel. For all measurements on the 10 nm wide wires other than thermal conductivity, monolithic contacts were used in order to minimize the contact resistance (Figure 2-3.). The use of monolithic contacts means that the NWs constitute a bridge between two micrometer-sized pads, with the NWs and pads all part of the same single crystal silicon structure. This method effectively removes contact resistance.

Measurement of the three thermoelectric parameters, S , σ , and κ was accomplished using a device architecture similar to those of other published reports^{19,24-25} (Figure 2-4). Heaters and electrodes were fabricated using e-beam lithography (EBL)

and e-beam evaporation of metal. The heaters and electrodes were both composed of titanium/platinum and were 20nm/100nm thick and 20nm/160nm thick respectively. Prior to metallization of the electrodes, the Si NWs were dipped in a buffered HF solution

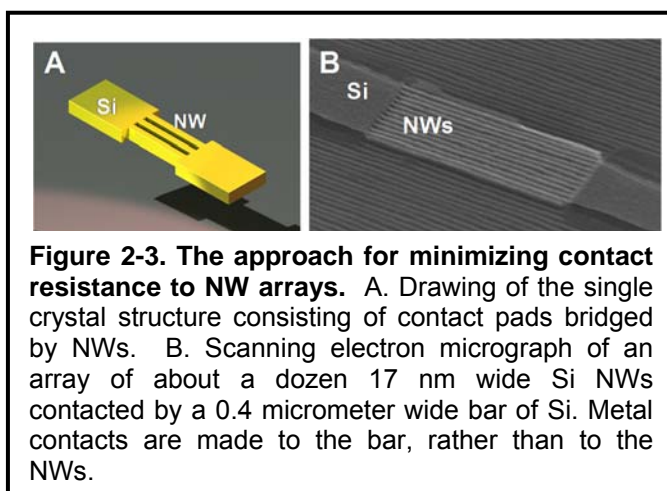


Figure 2-3. The approach for minimizing contact resistance to NW arrays. A. Drawing of the single crystal structure consisting of contact pads bridged by NWs. B. Scanning electron micrograph of an array of about a dozen 17 nm wide Si NWs contacted by a 0.4 micrometer wide bar of Si. Metal contacts are made to the bar, rather than to the NWs.

for 3 seconds to remove any native oxide. After electrode metallization, the device was annealed in forming gas inside the RTP (475°C; 5 min). The electrodes were then contacted by large gold pads (10nm/220nm

Ti/Au) that were defined by photolithography.

We used EBL and several etching steps to suspend the Si NWs. Polymethyl methacrylate (PMMA), an EBL resist material, is spun coated onto the surface of a chip containing a fully fabricated device. EBL is used to define an opening in PMMA around the active area of the device. A small rectangular island of PMMA remains on top of the NWs, electrodes and heaters to protect them during subsequent etching steps. Next, we used a CF_4 plasma etch, 20 minutes at 40W and 20 mTorr, to remove the SiO_2 around the active region. A 1.5 minute XeF_2 etch removes the exposed silicon and undercuts the silicon handle layer underneath the active region. During this step, the NWs are protected by the thick rectangular island of PMMA on top and the 150nm thick oxide underneath. The PMMA is then removed using an O_2 plasma (5 min; 40W; 20 mTorr). At the end, the Si NWs remain anchored on top of a thin rectangular island of 150nm thick SiO_2 .

Removal of the oxide island would cause the NWs to collapse, and so, as described below, measurements of κ were carried out as a differential measurement – i.e. a measurement of the NWs + oxide island followed by a measurement of the oxide island. Since this is a measurement of the heat flow only through the NWs, the oxide acts as a parasitic path for this heat flow that must be experimentally quantified.

Electrodes contacting the Si NWs were initially shorted together to minimize device damage through static charge. When the measurement begins, the shorts were disconnected. The Si substrate is mounted onto a thermally conductive chip carrier with

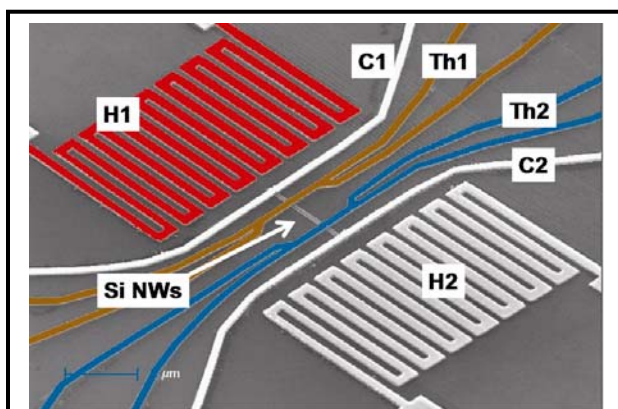


Figure 2-4. False color SEM image of a (non-suspended) thermoelectric device platform used in this study. The heaters (H1 and H2) are shown, one in red to indicate that Joule heating is done using just one of the heaters. C1, C2, Th1 and Th2 comprise the 4-point electrical contacts to the Si NWs, with C1 and C2 utilized as the current source and drain for those electrical conductivity measurements. Th1 and Th2 also serve as resistive thermometers (note that these two electrodes are themselves 4-point devices).

the gold pads wire-bonded to that same chip carrier. The chip carrier is then mounted onto the cold finger of a vacuum sealed liquid nitrogen cryostat (Janis Research VPF-475), which is evacuated to $\leq 10^{-6}$ Torr for the measurements. A temperature controller (Lakeshore Model 331) allows global control of the cryostat temperature from 350K to 77K with a precision of .01K.

2.5 Thermoelectric Measurements on Silicon Nanowires

Determining the thermopower, $\frac{\Delta V}{\Delta T}$, requires measurements of the thermoelectric voltage ΔV and the temperature difference ΔT along the Si NWs. A switching matrix (Keithley 707A) allows reconfigurable electrical connections from device to instrumentation for the various thermoelectric measurements.

We first create a temperature gradient along the Si NWs using a DC current through one heater (Joule heating) (Figure 2-4). We then measure the resultant thermoelectric voltage, ΔV (TEV). A Keithley 2182A nano-voltmeter measures the TEV between the inner electrodes (Th1 and Th2). In order to verify that the measured voltage is truly a result of the temperature gradient, the measurement is repeated using the second heater situated on the opposite side of the NW circuit. This should yield a voltage with similar magnitude but opposite polarity. A second check is to reverse the current polarity in the heater – this should not alter the magnitude or the polarity of the thermoelectric voltage. Figure 2-5A verifies that the measured voltage is indeed due to the temperature gradient.

Two separate measurements yield ΔT by using the inner electrodes as resistive thermometers. A resistive thermometer responds to temperature changes with a proportionate change in resistance. In the first measurement, the resistance of the Ti/Pt electrodes is continuously recorded by a four-point probe measurement as a function of heater power with one heater on. As the power dissipated in the heater slowly ramps stepwise, four lock-in amplifiers (Stanford Research Systems SR-830) simultaneously monitor the resistance of both thermometers. The first pair of lock-in units measures the

AC current and voltage at 913 Hz for one thermometer. Another pair of lock-in units performs the same functions for the other thermometer at 921 Hz. We obtain the resistances, R , of each thermometer as a function of heater power, Q (Figure 2-5B).

In the second measurement, we ramp the cryostat temperature stepwise by 1K increments while simultaneously measuring the thermometer's resistance. We obtain a linear relationship between the change in resistance and the cryostat temperature (Figure 2-5C). This relates our thermometer's resistance change to a temperature difference, ΔT , through the relation:

$$\Delta T = W \cdot \left(\frac{dR_{Left}/dQ}{dR_{Left}/dT} - \frac{dR_{Right}/dQ}{dR_{Right}/dT} \right)$$

where R_{Left} and R_{Right} are the resistances of the left and right thermometers respectively.

The slope of a linear fit to the TEV vs ΔT data provides the value of the thermopower.

This process is repeated to calculate the thermopower from 300K down to 100K.

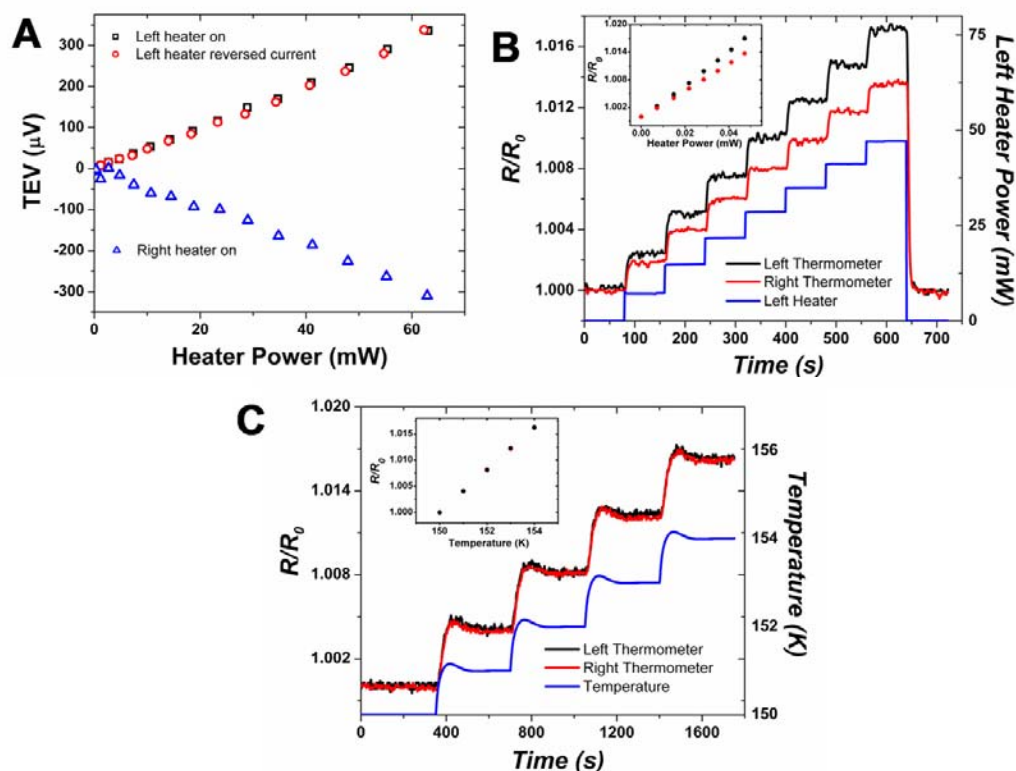
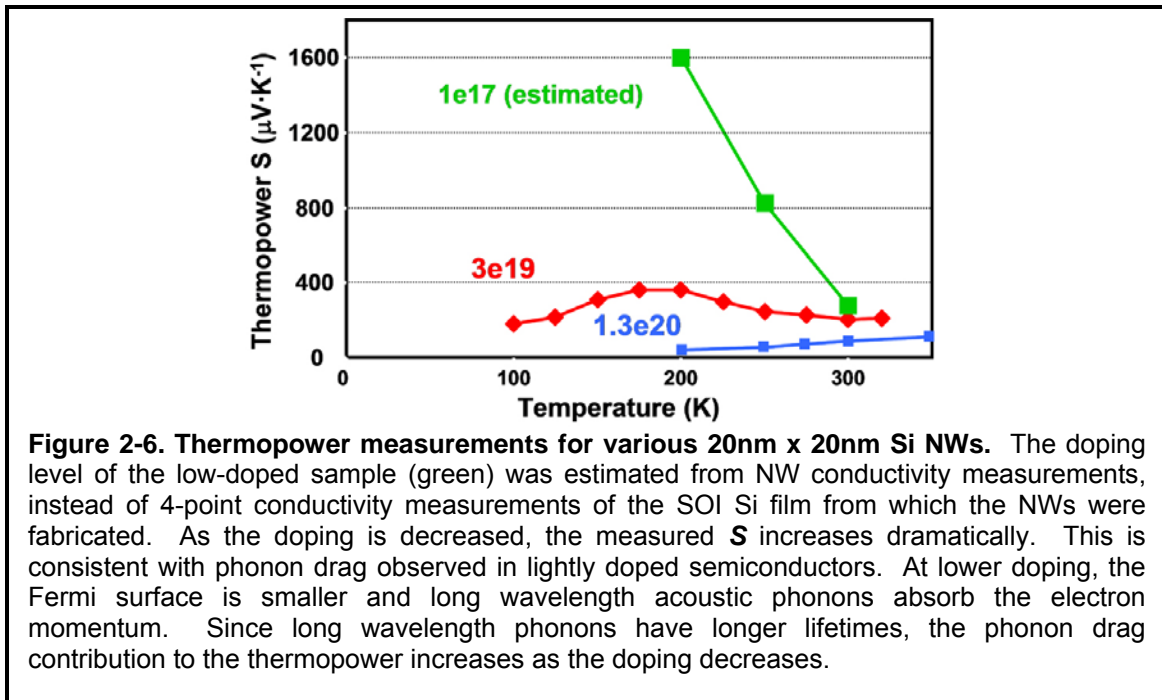


Figure 2-5. Measurement of the thermoelectric power of Si NWs. **A.** Plot of the thermoelectric voltage (TEV), which is a linear function of heater power at 150K. Each point represents the average of 6 measurements. With the left heater on, the TEV has no dependence on the heating current direction. With the right heater on, the TEV has the opposite polarity. **B.** Thermometer calibration. The graph shows the simultaneously measured resistance of both left and right thermometers (black and red trace, left y-axis) in response to the stepwise increase in heater power (blue trace, right y-axis) at 150K. The inset shows the linear relationship of the normalized thermometer resistance as a function of heater power. The slope of the linear fit to these two lines provides dR_{Left}/dQ and dR_{Right}/dQ . Each point in the inset corresponds to an average of 20 points collected from the time plot at each plateau. **C.** Graph of the simultaneously measured resistance of both thermometers (black and red trace, left y-axis) as a function of global temperature in the cryostat (blue trace right y-axis). Inset shows a linear relationship of the normalized thermometer's resistance to the cryostat temperature. The slope of the linear fit to these two lines provides dR_{Left}/dT and dR_{Right}/dT . Each point in the inset represents an average of 150 points collected in the time plot at each plateau.



2.5.1 Thermal Conductivity: Measurement and Data

Techniques utilized to measure the thermal conductivity, κ , were developed by Majumdar's group^{26,27}. The general expression for the thermal conductance of any system is given by the expression: $Q=K\Delta T$, where Q is the heat transferred across the NWs, ΔT is the temperature difference and K is the thermal conductance (K is related to κ through geometrical factors). Measurement of κ is not as straightforward since parasitic pathways for the heat flow, Q , must be accounted for. Therefore, we determine the parasitic heat flow through the beams that support the suspended structure. A direct measurement of the power dissipated in the heater, Q_{Heater} , is possible by using the 4-point probe electrodes attached to the heater's windings since the power dissipated in the heater is equal to the product of its current and voltage drop. A lock-in measurement similar to that described for measurement of the thermopower allows us to measure ΔT .

Also, the thermometers are in intimate contact with the ends of the NWs, eliminating any contributions from contact thermal resistances. The resistance of the thermometers is typically two orders of magnitude smaller than the resistance of the NWs. Taking into account the thermal conductance of the beams, K_b , the thermal conductance of the sample, K_s , is given by (17):

$$K_s = K_b \frac{T_C}{\Delta T} \dots\dots\dots \text{eq. 1}$$

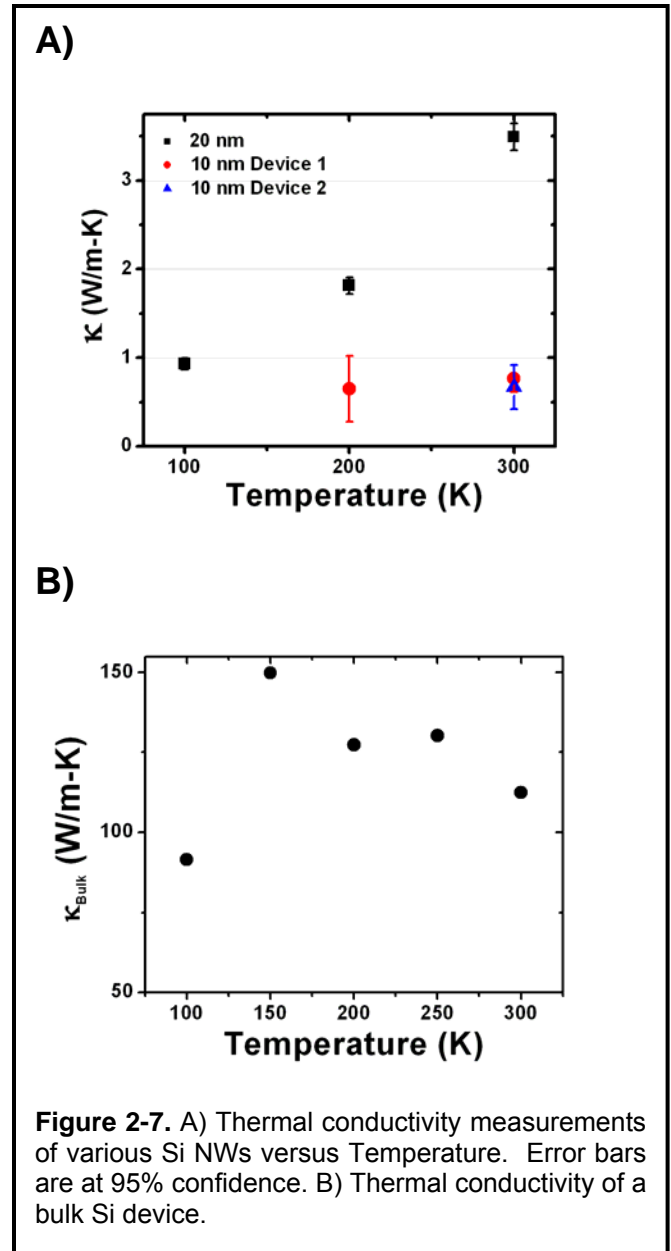
where T_C is the temperature increase at the cold junction and ΔT is the temperature difference between the hot and cold junctions. The thermal conductance of the beams is given by:

$$K_b = \frac{Q}{T_H + T_C} \dots\dots\dots \text{eq. 2}$$

where Q is the power dissipated in the heater and T_H is the temperature increase of the hot junction.

Our suspended structure is a combination of the SiO_2 island that supported the NWs and electrodes, and the Si NWs. To estimate the contribution of the SiO_2 to the measured K_{total} , we selectively

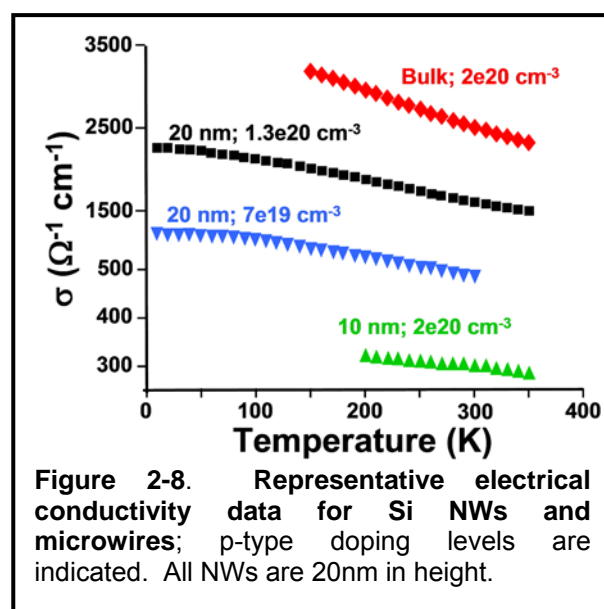
remove the NWs with a XeF_2 etc²⁸ and then measure K_{SiO_2} . The thermometers were



separately calibrated during each thermal conductance measurement – both before and after the Si NWs were removed. K_{SiO_2} is subtracted from K_{total} , giving K_{NWs} . Finally, K_{NWs} is converted to the κ from dimensions and number of NWs (Figure 2-7). The $\kappa_{bulkSi} \sim 150 \text{ W m}^{-1}\text{K}^{-1}$ at 300K. κ of thin films of Si has been found to be reduced by 50-70% over the bulk, depending upon the thickness, doping, and roughness of the film²⁹. Our measured value of $\sim 100 \text{ W m}^{-1}\text{K}^{-1}$ at 300K is somewhat higher than other reported values. This may arise from factors such as the smoothness of our epilayers or the doping profile through the thickness of our films. Our measured values are consistent with published reports from Majumdar's and Yang's groups²⁷. Also, the change in the thermal conductance of the metallic beams before and after XeF_2 is much less than 1%. This indicates that the difference between the two values of the thermal conductance arises solely from removal of the NWs.

2.5.2 Electrical Conductivity: Measurement and Data

The electrical conductivity of our NWs was measured using a four-point probe technique that removes any contribution from the contacts. A Keithley 2400 provides a current source through the outer electrodes and the nanovoltmeter measures the voltage drop between the two inner electrodes. The conductance value is calculated from the slope of a linear fit



of the I-V data. The conductance is then converted to an electrical conductivity using the dimensions & numbers of the NWs (Figure 2-8).

The measured thermopower includes the contribution from the oxide substrates. We show that the contribution from the oxide thermopower S_{oxide} is negligible because the oxide resistance is much larger than the NWs resistance.

Since our measured $S_{total} = 200 \mu\text{V/K}$ and $S_{oxide} = 400 \mu\text{V/K}$ at 300K,³⁰ the oxide contribution to the measured thermopower is negligible when the resistance of the oxide

$$S_{Total} = \frac{G_{oxide}S_{oxide} + G_{NW}S_{NW}}{G_{oxide} + G_{NW}}$$

is much larger than the resistance of the NWs. This can be seen by the equation below for S_{total} where G_{oxide} and G_{NW} are the conductances of the oxide and NWs respectively. The resistance of our NWs is $\sim 10^4 \Omega$ at 300K.

To determine the resistance of our oxide substrate, we performed a current-voltage measurement on the substrate. Since we did not obtain a linear fit to the data (due to the tiny currents $<100\text{pA}$ at $\sim 1 \text{ V}$), we estimated the order of magnitude of the resistance by dividing each individual current-voltage point. This gave us a resistance order of magnitude of $\sim 10^{10} \Omega$. Since the substrate resistance is $\sim 10^6$ times larger than the NWs resistance and the orders of magnitude of their respective thermopowers is the same, the total thermopower, S_{total} , is completely dominated by the NW contribution.

2.5.3 Error Analysis- Thermal Conductivity

A measurement of the thermal conductivity of our Si NWs requires knowing the power dissipated in the heater and the temperature difference across the NWs. In addition, we

must determine the parasitic heat flow through the beams that support the suspended structure. Heat also flows through the thin oxide film underneath the NWs. The measured thermal conductivity value is then a contribution from the NWs + oxide. To eliminate the contribution from the oxide, we remove the NWs using a highly selective XeF₂ etch and determine the thermal conductivity of the oxide in a second measurement. The difference between the two measured values is the thermal conductivity of the NWs.

The thermal conductance of the sample, K_s , is given by (17):

$$K_s = K_b \frac{T_C}{\Delta T} \dots\dots\dots \text{Equation 1}$$

where K_b is the thermal conductance of the beams, T_C is the temperature increase at the cold junction after the heater is turned on and ΔT is the temperature difference between the hot and cold junctions. The thermal conductance of the beams, K_b , is given by:

$$K_b = \frac{Q}{T_H + T_C} \dots\dots\dots \text{Equation 2}$$

where Q is the power dissipated in the heater and T_H is the temperature increase of the hot junction after the heater is turned on. Using error propagation, the error of K_s , δK_s , is give by:

$$\delta K_s = K_s \sqrt{\frac{\delta K_b^2}{K_b^2} + \frac{\delta T_C^2}{T_C^2} + \frac{[\delta(T_H - T_C)]^2}{(T_H - T_C)^2}} \dots\dots\dots \text{Equation 3}$$

Further simplifying this expression, we substitute for the error of K_b and ΔT :

$$\frac{\delta K_b^2}{K_b^2} = \frac{\delta Q^2}{Q^2} + \frac{\delta T_H^2 + \delta T_C^2}{(T_H + T_C)^2}, \dots\dots\dots \text{Equation 4}$$

$$[\delta(T_H - T_C)]^2 = \delta T_H^2 + \delta T_C^2 \dots\dots\dots \text{Equation 5}$$

$$\delta K_s = K_s \sqrt{\frac{\delta Q^2}{Q^2} + \frac{\delta T_c^2}{T_c^2} + 2 \frac{(\delta T_H^2 + \delta T_c^2)(T_H^2 + T_c^2)}{(T_H^2 - T_c^2)^2}} \dots\dots\dots \text{Equation 6}$$

The error in Q can be ignored because its uncertainty, $\frac{\delta Q}{Q}$, is 1 part in 1000000 or .001%. The errors in the temperature measurement for both hot and cold junctions are therefore the dominant terms in equation 6. Determining the error of the temperature measurement requires using error propagation on the formula used to find the temperature. The thermopower measurement section describes how we measured the temperature of each junction. The temperatures of the hot and cold junction are given by:

$$T_H = Q \cdot \left(\frac{dR_H/dQ}{dR_H/dT} \right) \qquad T_C = Q \cdot \left(\frac{dR_C/dQ}{dR_C/dT} \right)$$

where R_H and R_C are the resistances of the hot and cold thermometers. The term,

$\left(\frac{dR/dQ}{dR/dT} \right)$ is called the conversion factor and is calculated for each thermometer. The

terms, dR/dQ and dR/dT , are the slopes of the best linear fits to the data points in the resistance vs. heater power and resistance vs. temperature plots respectively (see thermopower measurement section).

For example, each data point on the resistance vs. heater power plot is determined by selecting a point from each plateau in the resistance vs. time plot for the heater power calibration. Figure 2-9 shows how this is accomplished. Since there are 55 plateaus and 100 useable points/plateau after temperature equilibration, we generate a series of 100 lines, with each line defined by 55 points. The slopes of all 100 lines are calculated and

averaged giving dR/dQ . The error of the average slope is calculated by finding the standard deviation of all 100 slopes and dividing by $\sqrt{100}$. This value is:

$$\delta\left(\frac{dR}{dQ}\right) = \frac{\sigma}{\sqrt{100}}$$

where σ is the standard deviation of the 100 slope values. Similarly, $\delta\left(\frac{dR}{dT}\right)$ is calculated by generating 800 linear fits, each with 40 data points (since there are 800 useable points/plateau after equilibration in the resistance vs. time plot and 40 plateaus for the temperature calibration). The value of dR/dT is found by taking the average of all 800 slopes and the error is $\delta\left(\frac{dR}{dT}\right) = \frac{\sigma}{\sqrt{800}}$.

We now find the error for our temperature measurement by first calculating the error of the conversion factor. The error in the conversion factor is:

$$\delta\left(\frac{\frac{dR}{dQ}}{\frac{dR}{dT}}\right) = \left(\frac{dR}{dQ}\right) \sqrt{\left[\frac{\delta\left(\frac{dR}{dQ}\right)}{\frac{dR}{dQ}}\right]^2 + \left[\frac{\delta\left(\frac{dR}{dT}\right)}{\frac{dR}{dT}}\right]^2}$$

Therefore, the error in the measured temperature for both thermometers is:

$$\delta T = T \sqrt{\left[\frac{\delta\left(\frac{dR}{dQ}\right)}{\frac{dR}{dT}}\right]^2 + \left[\frac{\delta\left(\frac{dR}{dT}\right)}{\frac{dR}{dT}}\right]^2}$$

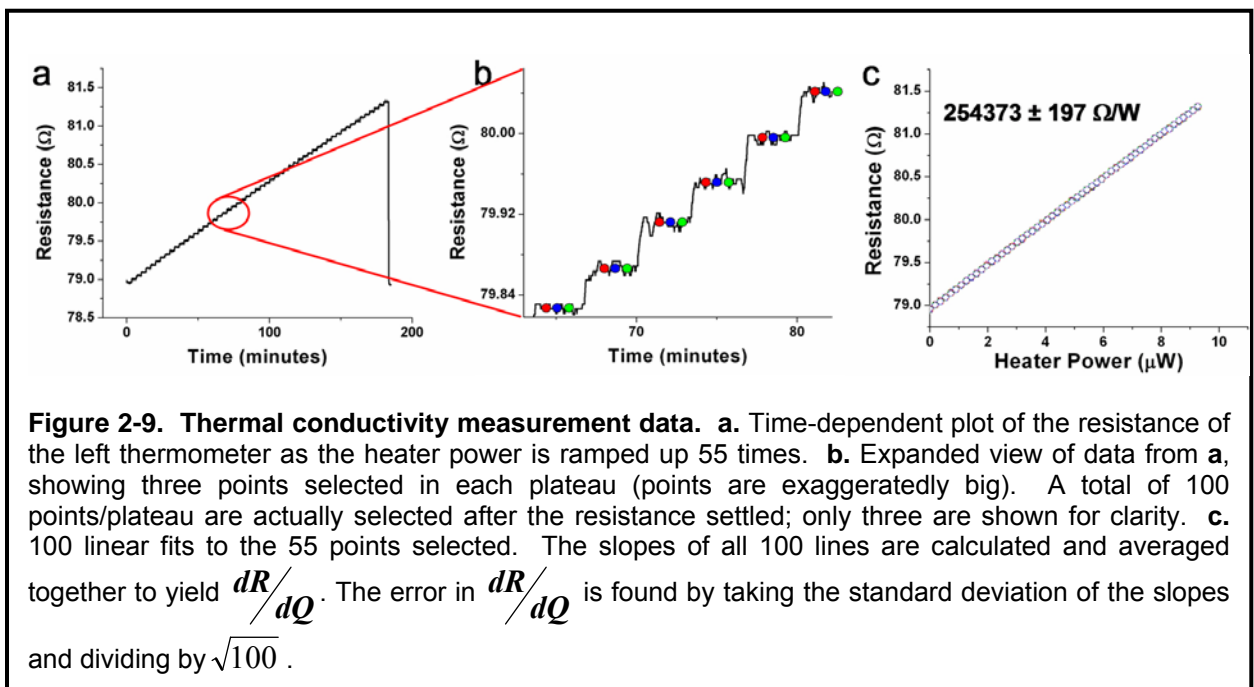
where we have ignored the error in Q because it is small. Based on the data collected, our uncertainty in the temperature is .01% at 300K. This sets the uncertainty in K_s to .068%. We obtain two values for K_s , before etching the NWs and after etching, and then subtract these to value to obtain K_{NW} . The error in K_{NW} is:

$$\delta K_{NW} = \sqrt{\delta K_{s \text{ Before Etch}}^2 + \delta K_{s \text{ After Etch}}^2}$$

We have a total error of .47 nW/K (or 9.7%) at 300K for the thermal conductance of our 10nm NWs. Finally, we determine the thermal conductivity, $\kappa = K_s L/A$ where L and A are the length and cross-sectional area of our NWs respectively. The uncertainty of the thermal conductivity is:

$$\delta \kappa = \kappa \sqrt{\left(\frac{\delta K_s}{K_s}\right)^2 + \left(\frac{\delta L}{L}\right)^2 + \left(\frac{\delta A}{A}\right)^2} \dots \dots \dots \text{equation 7}$$

The length, L , is measured by scanning electron microscopy (SEM) and its error is $\sim 5\text{nm}$, while A is measured by AFM and its error is $.1\text{nm}$. Therefore the dominant term in the right-hand side of equation 7 is the uncertainty of K_s . The percent uncertainty of our thermal conductivity value at 95% confidence for our 10nm NWs is $2(\delta \kappa / \kappa) = 19.5\%$ at 300K.



2.5.4 Error Analysis- Thermopower and Electrical Conductivity

The measured S ($= \frac{\Delta V}{\Delta T}$) is the slope of a best fit line to ΔV as a function of ΔT . The error of each ΔV point was found by calculating the standard deviation of each of the six voltage measurements taken for that point (Figure 2-5A). The relative error was found to be $\sim 1\%$ whereas for lower doped NW's, the relative error was $\sim 5\%$.

Next, the error of the temperature difference, δT , was determined using the same method as stated above for the thermal conductivity error analysis. Since we need to determine the temperature difference, ΔT , the error is:

$$\delta T \approx \sqrt{\left[\frac{dR_H/dQ}{dR_H/dT} \cdot \sqrt{\left(\frac{\delta(dR_H/dQ)}{dR_H/dQ} \right)^2 + \left(\frac{\delta(dR_H/dT)}{dR_H/dT} \right)^2} \right]^2 + \left[\frac{dR_C/dQ}{dR_C/dT} \cdot \sqrt{\left(\frac{\delta(dR_C/dQ)}{dR_C/dQ} \right)^2 + \left(\frac{\delta(dR_C/dT)}{dR_C/dT} \right)^2} \right]^2}$$

where we have neglected the error in Q since it is less than 1%. The relative error for ΔT is found to be 2-3% for most devices measured throughout the full temperature range (300K to 100K).

Finally, the uncertainty in S is calculated from the standard error of the slope of the best fit lines to the ΔV vs. ΔT plot at the 95% confidence level. We find that our relative error for S is between 1 and 6%.

The error of the electrical conductivity is less than 1% and the current-voltage traces are highly linear with $R^2 \sim .999$.

2.5.5 Error Analysis– ZT

The uncertainty in ZT is calculated using the following formula:

$$\delta ZT = ZT \sqrt{\left[4 \left(\frac{\delta S}{S} \right)^2 + \left(\frac{\delta \kappa}{\kappa} \right)^2 + \left(\frac{\delta \sigma}{\sigma} \right)^2 \right]}.$$

The factor of four appears in the above equation because $ZT \propto S^2$. The relative error in σ can be ignored since it is less than 1%. The uncertainty in ZT at the 95% confidence level, $2 \times \delta ZT$.

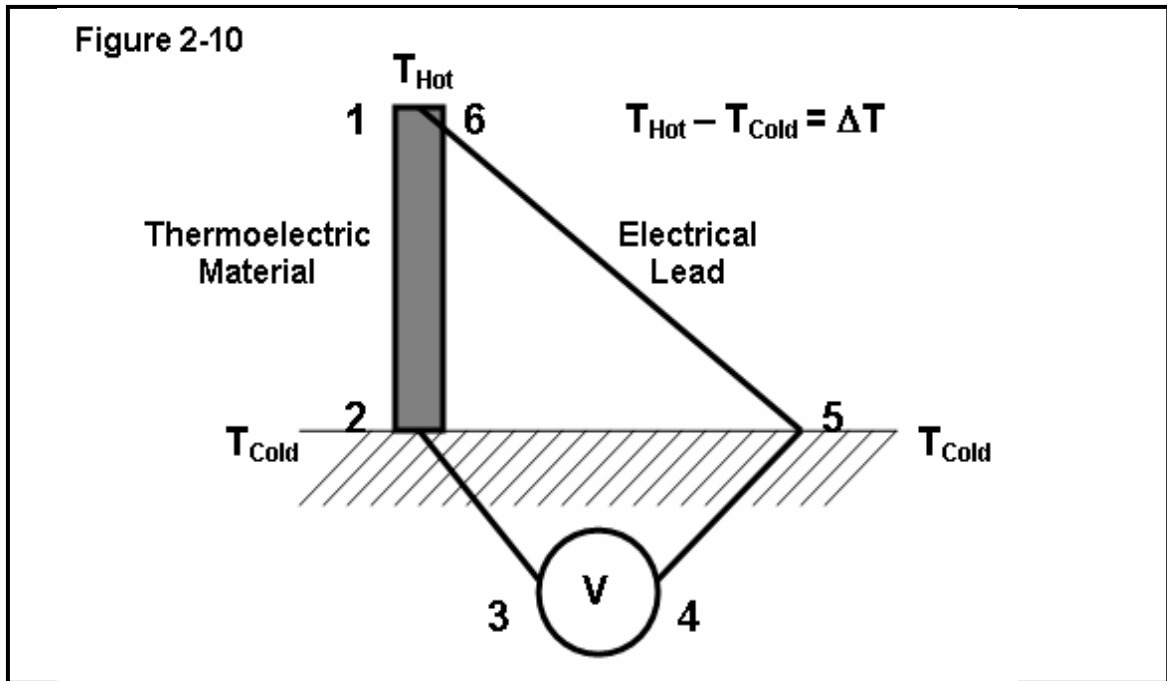
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Appendix 2.1 Thermopower Measurement

A thermoelectric measurement can be setup in such a way that there are only two regions that have temperature gradients (Figure 2-10). Applying Kirchoff's voltage law to the circuit in Figure 2-10 yields the following:



$$1. \quad V = \int_1^2 E \cdot dx + \int_2^3 E \cdot dx + \int_4^5 E \cdot dx + \int_5^6 E \cdot dx$$

Substituting for the electric field $E = S\nabla T$

$$2. \quad V = \int_1^2 S \frac{dT}{dx} \cdot dx + \int_2^3 S \frac{dT}{dx} \cdot dx + \int_4^5 S \frac{dT}{dx} \cdot dx + \int_5^6 S \frac{dT}{dx} \cdot dx$$

$$3. \quad \text{Simplifying: } V = \int_1^2 SdT + \int_2^3 SdT + \int_4^5 SdT + \int_5^6 SdT$$

4. The only temperature gradients exist between points 1 and 2 and 5 and 6. Therefore:

$$V = S_{\text{thermoelectric}} \Delta T - S_{\text{lead}} \Delta T$$

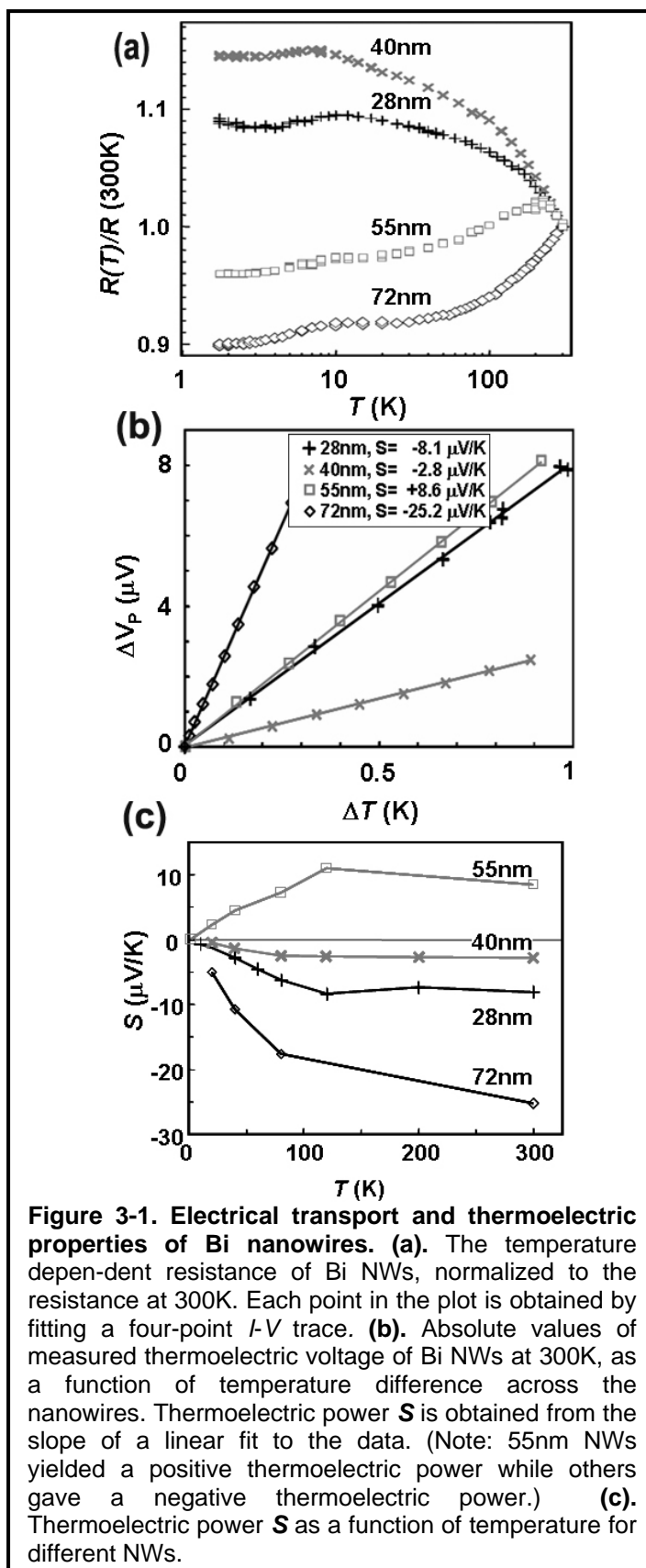
Chapter 3

Thermoelectric Results on Bismuth Nanowires

3.1 4-Point Resistance Results and Discussion

Resistivity of the NWs can be calculated from the four-point resistance since the NW dimensions and numbers of NWs measured are both known. The resistivity at 300K is 13, 9.5, 55, and $66 \mu\Omega \cdot \text{m}$ for cross sections of 15 nm by 72, 55, 40 and 28 nm, respectively, which corresponds to 10, 7, 42, and 50 times of that of bulk Bi. The increase of resistivity for thinner Bi wires reflects greater contributions from boundary and surface scatterings. Previously reported four-point measurement on a 70 nm diameter NW prepared from template assisted growth yielded a resistivity 6 times greater than that of bulk Bi¹.

The temperature dependent resistance is given in Figure 3-1(a). The observed trends generally agree with two-point measurements on vapor-deposited Bi nanowire arrays:² The widest wires yield bulk-like semimetal behavior, while the resistance for the thinnest two sets of NWs increases monotonically with decreasing temperature. The 55 nm wires exhibit an intermediate behavior. These trends have been cited as evidence that a quantum confinement-induced semimetal-to-semiconductor transition occurs when the wire width decreases below about 50 nm,^{3,4} consistent with theoretical predictions⁵. However, separating changes in carrier density and carrier mobility is inherently



difficult⁶. Our electric field effect measurements (see below) suggest the 40 nm wide NWs are still semimetallic. Consequently, the observed trends may reflect a decreased mobility through surface and grain-boundary scattering³.

A resistance drop is observed below 10K in all devices. This is reminiscent of the reported superconducting transition of amorphous Bi films around 6K,^{7,8} and may imply the existence of amorphous regions within the polycrystalline structure. We found that the drop disappears when a strong magnetic field is applied, which presumably quenches the superconducting transition.

3.2 Thermopower Results and Discussion

The thermopower measurements on the Bi NWs are shown in Figure 3-1(b) and 3-1(c). Figure 3-1(b) demonstrates the linearity of the thermoelectric voltage measured with respect to the applied temperature difference, indicating $S = \frac{dV}{dT}$ is a constant. The measured S is really that of the NW/electrode couple since it contains a contribution from the thermoelectric power of the metal electrodes, S_m . However, the S of Pt and Ti tend to cancel each other and are both within $\pm 5 \mu\text{V/K}$ at all temperatures studied here⁹.

The 72 nm wide NWs show the largest (room temperature) S of $-25.2 \mu\text{V/K}$. This value is about one half of that of bulk Bi in the same direction (perpendicular to the trigonal axis)¹⁰, but agrees with both earlier measurements of S ($-28 \mu\text{V/K}$) of thin (33 nm) Bi film¹⁰ and recent results ($-22 \mu\text{V/K}$ and $-28 \mu\text{V/K}$) on two NW arrays¹¹. S is reduced dramatically for the smaller NWs. Both theory¹² and experiment¹⁰ have concluded that surface and grain-boundary scattering will reduce S in polycrystalline thin films. This may also apply to the width for the NWs. The magnitude of S for all NWs tends to zero as the temperature is decreased. S is also the entropy per electric charge, and so must go to zero at 0 K.

For bulk Bi, and for the 72, 40, and 28 nm NWs S is negative valued, because electrons have a much higher mobility than holes and dominate the transport^{13,14}. The 55 nm NW, on the other hand, shows a positive S [Fig. 3-1(c)] indicating p-type carrier dominated transport, which has been reported in two Bi NW composites and a 200 ± 50 nm Bi wire¹⁵ before. Calculations based on the gating response of our NWs (see

below) suggest that an impurity level of 10 ppm could be sufficient to change S from negative to positive.

3.3 Gating Response of Bismuth Nanowires

Controlling the position of the Fermi energy (E_F) in order to enhance the thermoelectric power⁴ may be achieved through doping or the electric field effect (EFE)^{16,17}. Controlling the doping level to a precision of 10^{17} cm^{-3} (or 4 ppm of dopants) is desirable, but hard to achieve experimentally⁵. For example, 99.999% purity Bi has an impurity level of 10 ppm. However, our Bi NWs are thinner than the screening length,¹⁷ thus enabling EFE measurements. The effective doping level can be estimated based on the Si-SiO₂-Bi capacitance structure as a function of the gating voltage V_g :

$$N_d = \frac{Q_d}{eV_{Bi}} = \frac{CV_g}{eAh_{Bi}} = \frac{\epsilon_0 \epsilon_{r, SiO_2} \frac{A}{d_{SiO_2}} V_g}{eAh_{Bi}} = \frac{\epsilon_0 \epsilon_{r, SiO_2}}{ed_{SiO_2} h_{Bi}} V_g \quad (1)$$

where $\epsilon_0 \epsilon_{r, SiO_2}$ is the permittivity of the SiO₂ layer, which serves as the dielectric medium, and $d_{SiO_2} = 500 \text{ nm}$ and $h_{Bi} = 15 \text{ nm}$ are the thickness of the SiO₂ layer and the height of the Bi NWs, respectively. From Eq.(1) we obtain $N_d = 2.8 \times 10^{16} \text{ cm}^{-3} / V \cdot V_g$. Thus, the effective dopant concentration can be controlled to 10^{16} cm^{-3} or lower with appropriate V_g . Our devices functioned properly up to $V_g = \pm 150 \text{ V}$, or an effective dopant concentration of $4 \times 10^{18} \text{ cm}^{-3}$. This is sufficient for the thermoelectric optimization predicted by theory⁵. The EFE results of the 40 nm Bi NW device at 20 K are given in Fig 3-2. Ohmic conductivity was observed for all gating voltages, and the

conductance (G) values were obtained from a linear fit to the I - V curves. Similar behavior has been observed in thin carbon films¹⁷.

The conductance and thermoelectric power trends in Fig 3-2, which were collected separately during several different scans to avoid possible drift, are found to be well correlated by the Mott formula, which relates the diffusive thermoelectric power, S_d , to the conductance G ¹⁸:

$$S_d = \frac{-\pi^2 k_B^2 T}{3|e|} \frac{1}{G} \left. \frac{dG}{dE} \right|_{E=E_F} \quad (2)$$

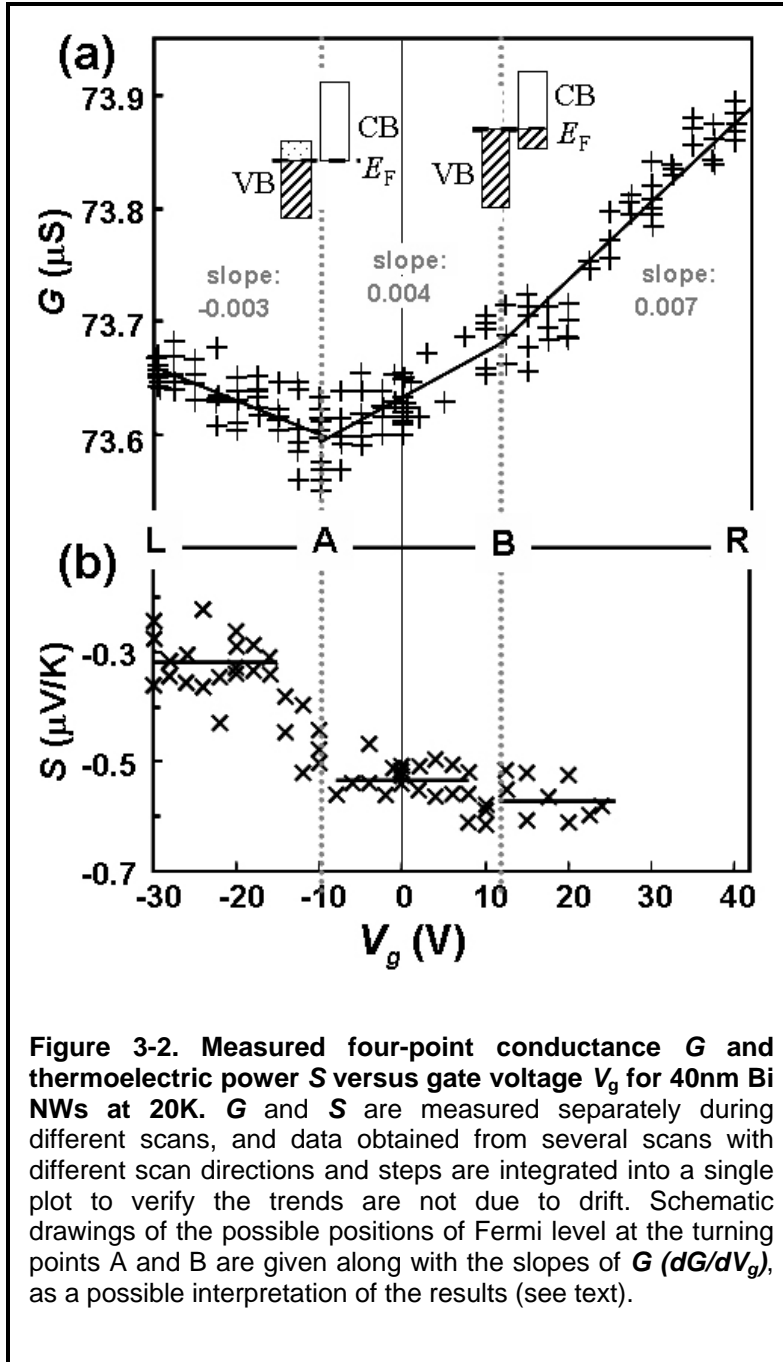
An increase in V_g would put more electrons into the Bi nanowires and elevate E_F , *i.e.*

$\left. \frac{dE_F}{dV_g} \right|_{E=E_F}$ is positive. Consequently, $\left. \frac{dG}{dV_g} = \frac{dE_F}{dV_g} \frac{dG}{dE} \right|_{E=E_F}$ is expected to be of the same sign

as $\left. \frac{dG}{dE} \right|_{E=E_F}$, and thus from Eq. (2) S_d should have the opposite sign of $\left. \frac{dG}{dV_g} \right|_{E=E_F}$. The

measured S clearly shows this trend: a sudden drop in the measured S is observed when the slope of G with respect to V_g changes from negative to positive at point A. This correlates to a change of positive S_d to negative S_d . Another decrease in S (and an increase in the slope of G) is observed around point B. It naturally follows that somewhere around point A (~ -10 V), with a measured S of between -0.5 to -0.4 $\mu\text{V/K}$, should correspond to an S_d value of 0. The observed non-zero value of S is reflective of two facts: 1) S_g , the phonon-drag component of S has not been taken into account, which could be significant at this temperature¹⁹, and 2) S_m , the thermoelectric power of Pt/Ti electrodes used to establish the thermocouple with Bi nanowires has not been considered.

The Pt/Ti electrodes are not expected to contribute to the EFE due to their extremely small screening lengths¹⁷, but they might cause a uniform shift $-S_m$ in S at all V_g .



40 nm Bi NWs have been predicted to be semiconductors at 20 K for any growth direction⁵, and results similar to Figure 3-1(a) has been cited as evidence of the semimetal-to-semiconductor transition around 55 nm^{3,20}. Our EFE result, however, is found to be more readily explained with a semimetal model¹⁷. The two turning points A and B around ± 10 V correspond to an effective dopant concentration of about

$N_d = 3 \times 10^{17} \text{ cm}^{-3}$, which is close to the carrier concentrations measured in bulk (semimetal) Bi, $N_e \approx N_h = 2.5 \sim 4 \times 10^{17} \text{ cm}^{-3}$, obtained from various methods^{21,22}.

These two turning points are thus assigned to be when the Fermi level is at the bottom of the conduction band (A) and at the top of the valence band (B). If the bottom of conduction band is lower than the valence band as in a semimetal [see drawings in Fig 3-2(a)], the observed results can be rationalized. According to the assignment, holes are the only carrier when $V_g < -10$ V, which results in positive S_d , and a decrease in G with an increase in V_g , as the concentration of holes would decrease when putting more electrons in the nanowires. Similarly, electrons are the only carrier for $V_g > 12$ V, which results in negative S_d and an increase in G with increase of V_g . For -12 V $< V_g < 12$ V, both electrons and holes carriers are present and contribute to the conductivity σ and thermoelectric power S :

$$\sigma = \sigma_e + \sigma_h = e(N_e \mu_e + N_h \mu_h) \quad (3)$$

$$S = \frac{\sigma_e S_e + \sigma_h S_h}{\sigma_e + \sigma_h} = \frac{N_e \mu_e S_e + N_h \mu_h S_h}{N_e \mu_e + N_h \mu_h} \quad (4)$$

An increase in V_g in this region would cause an increase in N_e , the concentration of electrons, but a decrease in N_h , the concentration of holes.

Consider the value of dG/dV_g [the slope of Fig. 3-2(a)] in the three regions L-A, A-B, and B-R. Note that $|\text{slope}|_{\text{B-R}} > |\text{slope}|_{\text{L-A}}$. This is consistent with the higher mobility^{13,14} electrons dominating the region B-R and holes dominating L-A. Also note that $\text{slope}_{\text{A-B}} \approx \text{slope}_{\text{L-A}} + \text{slope}_{\text{B-R}}$. This indicates that both electrons and holes participate in the charge transport in the region A-B. A more quantitative analysis of the results would require knowledge of the density of states (DOS), but the near-linear dependence of G over V_g in the different regions suggests a near-constant DOS characteristic of a 2D

system¹⁷. This is reasonable for a 15nm×40nm cross section wire as the electronic de Broglie wavelength is 30~40 nm in Bi²³.

Our EFE results suggest semimetal behavior for 40nm Bi NWs, with electron and hole carrier concentrations comparable to bulk values, contradicting theoretical predictions that Bi nanowires thinner than 50 nm would become semiconductor at this temperature⁵, and that as a consequence the total carrier density for 40 nm NW at 20 K would decrease significantly to smaller than 10^{16} cm^{-3} , about 100 times smaller than the bulk value⁵. This could stem from the polycrystalline nature of our NWs, since interface states would be expected to contribute to the total density of states near E_F . Similar conclusions have been drawn from recent Shubnikov-de Haas oscillation measurements on 30 nm Bi wires in terms of surface-induced charge carriers⁶. Our 28 nm NW device was found to give similar trends as the 40 nm NW device, but the data set was less complete.

3.4 Conclusion

In conclusion, nanofabrication methods and a device architecture have been combined to allow for four-point electric, thermoelectric, and electric field effect measurements on individual Bi nanowires. No clear semimetal-to-semiconductor transition or enhancement in thermoelectric power has been observed, probably due to the polycrystalline nature of our NWs and the presence of surface states. Therefore, the passivation of such surface states and single-crystalline material are necessary to improve the thermoelectric performance of Bi nanowires.

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Chapter 4

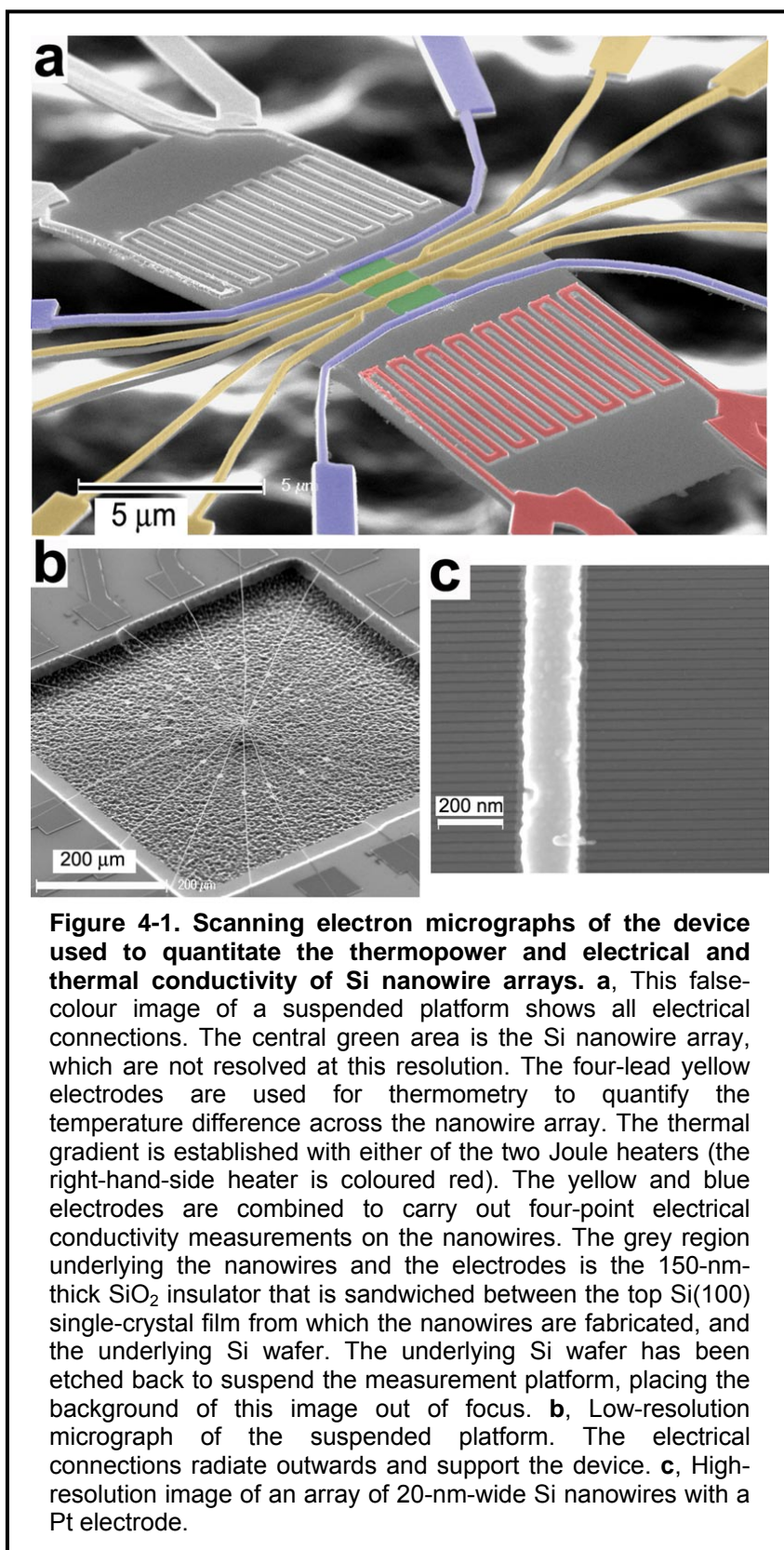
Thermoelectric Results on Silicon Nanowires¹

4.1 Introduction

The most efficient TEs have historically been heavily doped semiconductors because the Pauli principle restricts the heat carrying electrons to within kT of the Fermi level² for metals. The Wiedemann-Franz law, $(\kappa_e/\sigma T) = (\pi^2/3)(k/e)^2 = (156 \mu\text{V/K})^2$, where κ_e is the electronic contribution to κ , constrains ZT . Semiconductors have a lower density of carriers, leading to larger S and κ that is dominated by phonons (κ_{ph}) implying that the electrical and thermal conductivities are somewhat decoupled². κ can be reduced by using bulk semiconductors of high atomic weight, which decreases the speed of sound. However this strategy has not yet produced materials with $ZT > 1$.

For a metal or highly doped semiconductor, S is proportional to the energy derivative of the density of electronic states (DOS). In low-dimensional (nanostructured) systems the DOS has sharp peaks⁶⁻⁸ and, theoretically, a high thermopower. Harnessing this electronic effect to produce high ZT materials has only had limited success^{9,10}. However, optimization of the phonon dynamics and heat transport physics in nanostructured systems has yielded results³⁻⁵. Nanostructures may be prepared with one or more dimensions smaller than the mean free path of the phonons and yet larger than that of electrons and holes. This potentially reduces κ without decreasing σ ¹¹. Bulk Si is

a poor thermoelectric ($ZT_{300K} \sim 0.01$)²³, and this phonon physics is important for our SiNWs where the electronic structure remains bulk-like.

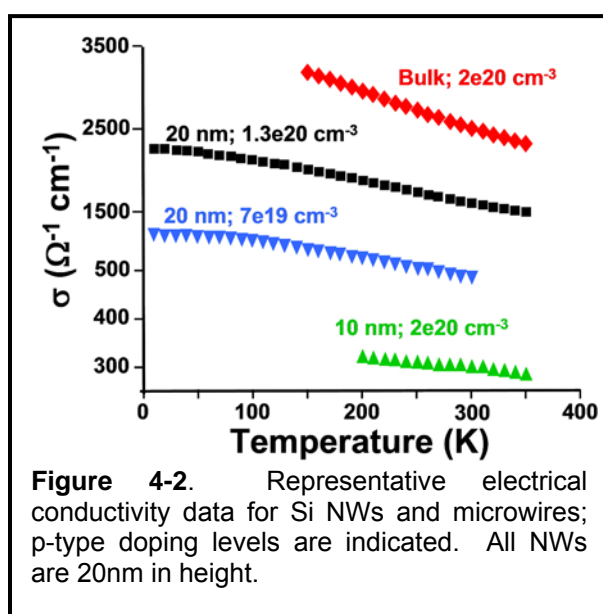


4.2 Results of S , σ , and κ

Figure 4-1 shows images of the devices and the Si NWs we utilized for these experiments. The platform permits 4-point measurements of the electrical conductivity of the NWs, Joule heating to establish a thermal gradient across the NWs, and 4-point thermometry to quantify that gradient^{9,12}. The resistance of the 4-point thermometry

electrodes is typically 2 orders of magnitude smaller than the resistance of the NWs. The measurement platform is suspended in vacuum to allow measurement of NW thermal conductivity^{13,14}. For all measurements, the SiNWs could be selectively removed using a XeF₂ etch, thus allowing for measurements of the contributions to σ , S , and κ from the platform and oxide substrate.

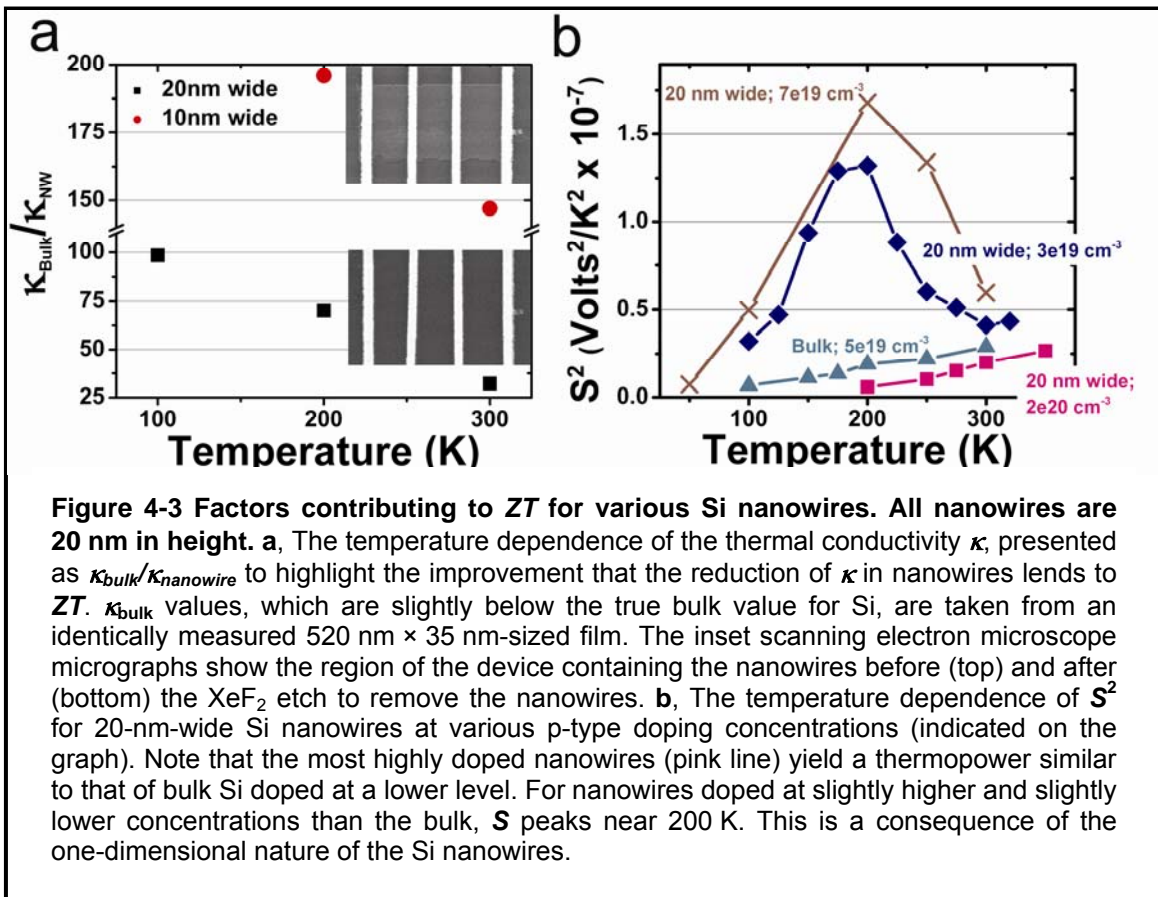
All values of S , σ , and κ reported here are normalized to individual NWs, although each experiment utilized a known number of NWs ranging from 10 and 400. The Si microwires and NWs were prepared using the same substrates, doping methods, etc., but different patterning methods (electron-beam lithography versus SNAP). Measurements of σ , κ and S^2 for Si NWs (and microwires) for different NW sizes and/or doping levels are presented in Figures 4-2 and 4-3. The NW electrical conductivity is



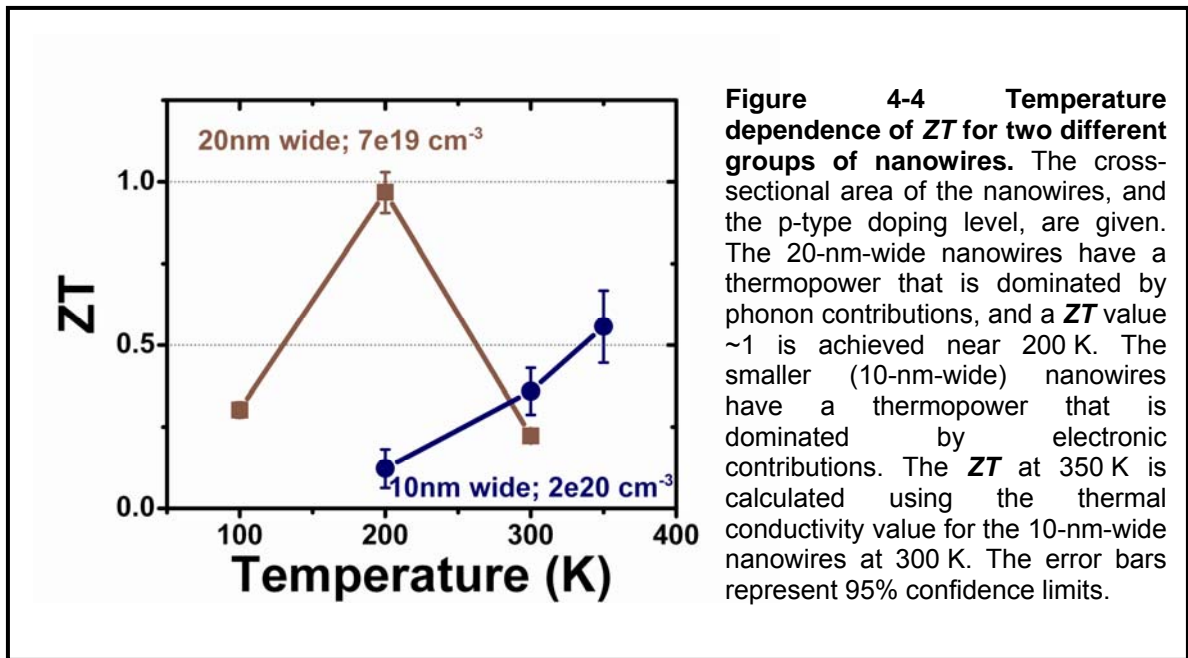
between 10 and 90% of the bulk, depending on NW dimensions. A reduced σ likely arises from surface scattering of charge carriers¹⁵. Nevertheless, all NWs are highly doped and most exhibit metallic-like conductivity (increasing σ with decreasing T).

The temperature dependence of κ for a microwire and 10 and 20 nm wide NWs were recorded at modest statistical resolution in order to establish trends. This data indicated that κ drops sharply with shrinking NW cross section (Figure 4-3a) and that the 10 nm wide NWs exhibited a κ

($0.76 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1} \pm 0.15 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$) that was below the theoretical limit of $0.99 \text{ W}\cdot\text{m}^{-1}\cdot\text{K}^{-1}$



for bulk Si. Thus, very large data sets were collected for 10 and 20 nm wide NWs to allow for a more precise determination of κ . Our observed high ZT for Si NWs (Figure 4-4) occurs because κ is sharply reduced and the phonon drag component of the thermopower, S_{ph} , becomes large. Below, we show that S_{ph} increases due to a 3D to 1D dimensional crossover of the phonons participating in phonon drag, and to decreasing κ . However, we first address the issue that our measured κ at 300K for 10 nm wide Si NWs is $< \kappa_{\text{min}}^{16}$.



4.2.1 Discussion of κ_{min}

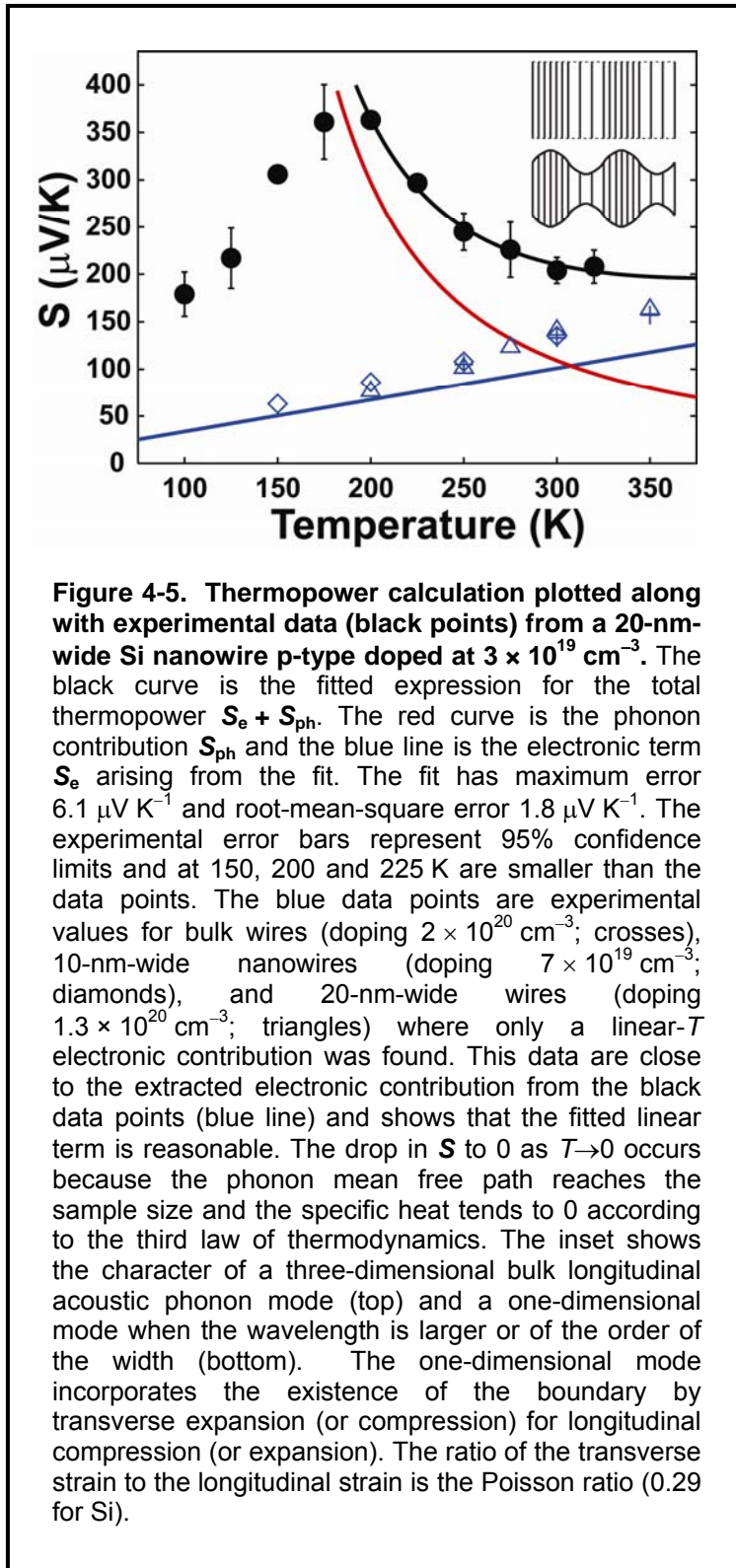
The derivation of κ_{min} assumes that the minimum path length of wavelength λ phonons is $(1/2)\lambda$ and that the phonons are described by the Debye model using bulk sound speeds with no optical modes. The $(1/2)\lambda$ value is an order of magnitude estimate and is difficult to determine precisely in analogy to the minimum electron mean free path used to calculate the Mott-Ioffe-Regel σ_{min} . Also, κ_{min} is proportional to the transverse and longitudinal acoustic speeds of sound¹⁶. These are reduced in our NWs at long wavelengths because the modes become 1D. The ratio of the 1D to 3D longitudinal speeds of sound is $[(1+\nu)(1-2\nu)/(1-\nu)]^{1/2} = 0.87$ where $\nu = 0.29$ is the Poisson ratio of Si. The transverse acoustic speed goes to zero at long wavelength since $\omega \sim k^2 d$ where d is the NW width¹⁷. Thus the bulk κ_{min} estimate above is invalid for our NWs and values smaller than κ_{min} are attainable.

4.2.2 Phonon Drag

For all but the most highly doped NWs, S peaks near 200K (Figure 4-3b). This peak is unexpected: similarly doped bulk Si exhibits a gradual decrease in S as T is reduced (green trace). For $T < 100K$ a peaked $S(T)$ is observed for metals and lightly doped semiconductors and is due to phonon drag¹⁸⁻²⁰.

Phonon drag is generally assumed to vanish with decreasing sample dimensions because the phonon path-length is limited by the sample size²¹⁻²³. This appears to eliminate phonon drag as the reason for the peak in our NWs. We show below that the phonon wavelengths participating in drag are on the order of or larger than the wire width. This leads to a 3D to 1D dimensional crossover of these modes and removes the cross-sectional wire dimensions from limiting the phonon mean path (see Figure 4-5 inset). The NW boundaries are incorporated into the 1D mode and are not an obstacle to phonon propagation. Therefore, the limiting size becomes the wire length ($\sim 1 \mu\text{m}$) and phonon drag “reappears” at very small dimensions. In addition, classical elasticity theory¹⁷ is valid for the phonon wavelengths considered here²⁴, leading to thermoelastic damping^{17,25,26} of sound waves proportional to κ . Thus S_{ph} is further enhanced due to the observed reduced thermal conductivity κ .

It might appear that elasticity theory leads to a contradiction because κ is proportional to the mean phonon lifetime. If the phonon lifetimes increase as stated above, then κ should also increase. The resolution is that the elasticity expression is only valid for long wavelength modes. We now consider separately the electronic and phonon contributions, $S = S_e + S_{ph}$ to the thermopower for the NW data at $T > 200K$.



Charge carriers dissipate heat to the lattice through a process that first involves momentum conserving (non-dissipative) electron-phonon collisions. The phonons that contribute to phonon drag cannot have a wavelength shorter than λ_{min} , which is determined by the size of the Fermi surface. Phonon drag is observed in metals only at low T because the Fermi surface is large and the heat carrying short wavelength phonons have short lifetimes. At low T ($< 20\text{K}$), $S_{ph} \sim T^3$ from the phonon specific heat ($\sim T^3$). For $kT \gg \Theta_{Debye}$, the specific heat becomes

constant and the number of phonons available for phonon-phonon scattering is $\sim T$ leading to $S_{ph} \sim 1/T$ (1).

For p-type Si, the holes are near the valence band maximum. The phonon drag modes are acoustic with largest wavevector, $k_{ph} = 2k_{fermi} = 0.2 \text{ \AA}^{-1}$ (for impurity doping $3 \times 10^{19} \text{ cm}^{-3}$). The shortest wavelength is $\lambda_{ph} = 2\pi/k = 31 \text{ \AA}$. Umklapp (non-momentum conserving) phonon-phonon scattering processes determine the rate of phonon heat dissipation. The Debye energy (Θ_D) sets the energy scale for Umklapp scattering. The number of Umklapp phonons available to dissipate the long wavelength phonons is given by the Bose-Einstein function

$$N_U = \frac{1}{e^{\Theta_D/T} - 1}$$

leading to a scattering rate $1/\tau_{ph} \sim N_U$. When $T \gg \Theta_D$, $1/\tau_{ph} \sim T$. Since $\Theta_{Debye} = 640\text{K}$ for Si, the full Bose-Einstein expression must be applied for $T \leq 350\text{K}$.

The electronic contribution (S_e) is estimated from the Mott formula (1)

$$S_e(T) = \frac{\pi^2 k^2 T}{3e} \left(\frac{\partial \ln \sigma(\epsilon)}{\partial \epsilon} \right) \approx (283 \mu\text{V} / \text{K})(kT / E_f),$$

where the conductivity derivative equals the reciprocal of the energy scale over which it varies (the Fermi energy E_f). Assuming hole doping occurs in the heavier Si valence band (mass 0.49), this leads to $E_f = 0.072 \text{ eV} = 833\text{K}$ and $k_f = 0.1 \text{ \AA}^{-1}$ for $n = 3 \times 10^{19} \text{ cm}^{-3}$. Thus $S_e(T) = aT$ where $a = 0.34 \mu\text{V}/\text{K}^2$.

The $T > 200\text{K}$ thermopower data of the 20 nm wire (doping $n=3 \times 10^{19} \text{ cm}^{-3}$) fits

$$S = S_e + S_{ph} = aT + b[\exp(\Theta_D / T) - 1]$$

where a , b and Θ_D are varied to obtain the best fit (Figure 4-5). The coefficients are $a = 0.337 \mu\text{V}/\text{K}^2$, $b = 22.1 \mu\text{V}/\text{K}$, and $\Theta_{Debye} = 534 \text{ K}$. The coefficient a is almost identical to our estimate of $0.34 \mu\text{V}/\text{K}^2$. Thus phonon drag explains the observed thermopower. Consistent with measurements of phonon drag in bulk Si²¹, S in our NWs increases significantly at lighter doping. This data, plus a fit of the Figure 4-5 data with Θ_{Debye} fixed to experiment at 640K, is presented in section 4.3.4.

The phonon drag contribution to S is of the form^{20,27}

$$S_{ph} \sim \left(\frac{\tau_{ph}}{\mu T} \right).$$

τ_{ph} , the phonon lifetime, is $\sim 1/\kappa$ from elasticity theory. μ is the electron mobility. ZT scales as (neglecting S_e)

$$S_{ph} \sim \frac{1}{\mu T \kappa}, \quad \sigma \sim n \mu, \quad ZT \sim \frac{n}{\mu T \kappa^3},$$

leading to increased ZT with *decreasing* mobility. This is opposite the conclusion reached when considering only S_e ⁶.

4.3 Theoretical Analysis

4.3.1 1D versus 3D electronic structure.

The first question to consider in understanding the unexpectedly large Seebeck effect observed for the relatively lightly doped NWs is whether the electronic structure in the 10-

20 nm wires is 1D or 3D above 100K. This can be estimated from the magnitude of the zero-point energy due to the finite cross-section of the wire. The effective masses for the two bands at the Valence Band Maximum of Si are 0.49 and 0.16 electron masses. Hole doping will occur predominantly in the heavier band. The zero-point energy is

$$\varepsilon = \frac{\hbar^2 k^2}{2m^*}, \quad k = \frac{\pi}{d},$$

where d is the wire diameter. For $m^* = 0.49$, $\varepsilon = 89\text{K}$ for $d = 10$ nm and $\varepsilon = 22\text{K}$ for $d = 20$ nm. Thus for temperatures above 100K thermal smearing is larger than the zero-point energies, suggesting that the electronic properties should be 3D. Furthermore, the thermopower data in Figure 4-5 (green and pink data points) and 4-3 (blue data points) shows that the 10 and 20nm wires and bulk samples with similar impurity doping levels have an almost identical magnitude and linear temperature dependence. Since these 10 nm, 20 nm, and bulk wires have similar thermopowers, the different zero-point energies are not leading to a large change in S and we may conclude the electronic structure in all the wires remains 3D for temperatures $> 100\text{K}$.

4.3.2 Is there a Boron impurity band?

For Boron doping levels within the range of 10^{19} - 10^{20} cm^{-3} , the electron gas becomes degenerate and it is possible that a B impurity band forms containing the charge carriers. By comparing an estimate of the thermopower due to holes in the Si valence bands of the NW with measured values, we conclude that this is unlikely.

If the holes are primarily in the Si valence bands, then the holes are predominantly in the heavier valence band with mass 0.49. For doping n , the Fermi momentum satisfies

$$n = \frac{k_f^3}{3\pi^2}.$$

For $n = 3 \times 10^{19} \text{ cm}^{-3}$, $k_f = 0.1 \text{ \AA}^{-1}$ leading to Fermi energy $E_f = 0.072 \text{ eV} = 833\text{K}$.

From the Mott formula for the electronic contribution \mathcal{S} :

$$\mathcal{S}_e(T) = \frac{\pi^2 k^2 T}{3e} \left(\frac{\partial \ln \sigma(\varepsilon)}{\partial \varepsilon} \right) \approx (283 \mu\text{V/K})(kT/E_f),$$

we estimate that $\mathcal{S}_e = 102 \mu\text{V/K}$ at $T = 300\text{K}$. We assumed that the derivative of the logarithm of the conductivity is the reciprocal of the energy scale over which $\sigma(\varepsilon)$ changes $\sim 1/E_f$ in computing \mathcal{S}_e . This estimate for \mathcal{S}_e is compatible with $\mathcal{S}_e = 130\text{-}170 \mu\text{V/K}$ from experiments for bulk samples at 300K for wires that only have a linear T electronic contribution to \mathcal{S} . A Boron impurity band would likely lead to much heavier masses and hence to \mathcal{S}_e larger than observed.

4.3.3 Derivation of the results from elasticity theory for the phonon lifetime

For doping $n = 3 \times 10^{19} \text{ cm}^{-3}$, the longitudinal acoustic (LA) phonons that can receive momentum from the electrons are characterized by wavelengths of $> 31 \text{ \AA}$, corresponding to > 5.5 unit cells of Si. Classical elasticity theory models the system by an elastic continuum. Indeed, recent molecular dynamics simulations show classical elasticity is a good approximation for these wavelengths²⁴. Since the wavelengths of the phonons

involved in phonon drag are larger than several unit cells, classical elasticity theory is expected to give a good approximation to their dynamics. When a sound wave propagates through an elastic medium it generates local temperature gradients from the local volume changes in the wave. Thermal conduction acts to remove these gradients by heat flow with a corresponding increase in entropy. This irreversible heat flow leads to damping of the sound wave²³.

Consider a volume element $\delta x \delta y \delta z = \delta x \delta A$ with a temperature gradient along the x-direction. The temperature at x is T and $T + \delta T$ at $x + \delta x$. Over a time interval δt an amount of heat δQ

$$\delta Q = (+\kappa \nabla T) \delta A \delta t$$

flows to T . κ is the thermal conductivity. The change in entropy (S) is

$$\delta S = \frac{\delta Q}{T} - \frac{\delta Q}{T + \delta T}.$$

The irreversible energy lost due to the increasing entropy is

$$T \delta S = \frac{\delta T}{T} \delta Q,$$

leading to the rate of energy lost by thermal conduction

$$\begin{aligned} \frac{dE}{dt} &= -\frac{\delta T}{T} \frac{\delta Q}{\delta t} = -\frac{\delta T}{T} \kappa \frac{\delta T}{\delta x} \delta y \delta z = -\frac{\kappa}{T} \left(\frac{\delta T}{\delta x} \right)^2 dV, \\ \frac{dE}{dT} &= -\kappa \int \frac{1}{T} (\nabla T)^2 dV. \end{aligned}$$

A 3D longitudinal wave given by $u_x = u_0 \cos(kx - \omega t)$ where $\omega = c_L k$ and c_L is the longitudinal speed of sound leads to local temperature gradients due to local volume changes as the wave propagates. The volume deformations of the longitudinal wave are separated by one-half the wavelength λ . For low ω , the separation between the high and low temperature regions is too large to be equalized during the period of the wave. Thus for low ω , the volume changes are adiabatic²⁸. At high frequencies, the wavelength is small and thermal gradients are rapidly equalized leading to isothermal volume changes for large ω ²⁸.

A 3D longitudinal acoustic (LA) phonon with momentum (q_x, q_y, q_z) that makes an angle θ with the long axis of the 1D wire (z-direction) is a linear combination of a longitudinal phonon of momentum q_z with amplitude $\cos\theta$ and a transverse acoustic (TA) phonon with momentum q_z with amplitude $\sin\theta$. Thus electron-phonon scattering around the Fermi surface leads to a 1D LA mode with probability $\cos^2\theta$ and a TA mode with probability $\sin^2\theta$. TA modes have temperature gradients perpendicular to the wire axis. LA modes have temperature gradients along the wire axis.

The largest momentum (shortest wavelength) phonon modes participating in phonon drag by being excited due to the holes scattering with phonons are 3D longitudinal acoustic with wavevector, $k_{LA} = 2k_f = 0.2 \text{ \AA}^{-1}$ for an impurity doping level of $3 \times 10^{19} \text{ cm}^{-3}$. The wavelength is $\lambda_{sh} = 2\pi/k = 31 \text{ \AA}$. The speed of sound in the (100) direction for Si is $c_L = 8.43 \times 10^5 \text{ cm/s}$, leading to $\omega_{LA} = c_L k = 1.7 \times 10^{13} \text{ sec}^{-1}$. Phonon drag thermopower is an average over all the phonon modes that are scattered by the electrons at the Fermi surface. Thus ω_{LA} is an upper bound on the phonon frequencies participating in phonon drag.

The crossover frequency from adiabatic volume deformations to isothermal deformations for LA modes occurs at $\omega_0(\text{LA}) = c_L^2/\chi$ where χ is the thermal diffusivity. $\chi = 0.8 \text{ cm}^2/\text{s}$ for bulk Si at 300K leading to $\omega_0(\text{LA}) = 8.9 \times 10^{11} \text{ sec}^{-1}$. 3D LA modes with frequency ω_{LA} are isothermal.

For TA modes, the crossover frequency is determined by the width of the wire, d , and the thermal diffusivity, $\omega_0(\text{TA}) = \pi^2\chi/d^2$. In this case, frequencies *below* $\omega_0(\text{TA})$ are isothermal and frequencies *above* $\omega_0(\text{TA})$ are adiabatic^{25,26}. For $d = 20\text{nm}$, $\omega_0(\text{TA}) = 2 \times 10^{12} \text{ s}^{-1}$ using the bulk value of the thermal diffusivity.

For the NW, the thermal diffusivity is ~ 100 times smaller than bulk since the diffusivity is proportional to the thermal conductivity. Thus the LA crossover frequency is ~ 100 times larger than the bulk $\omega_0(\text{LA})$ leading to adiabatic damping for LA modes. The TA mode crossover frequency decreases by a factor of ~ 100 . TA modes are also adiabatic in the NW at 300K.

The damping rate for an LA sound wave of momentum k is^{28,29}

$$\frac{1}{\tau_{LA}(k)} = \frac{1}{\tau_0} \cdot \frac{(\omega_k \tau_0)^2}{1 + (\omega_k \tau_0)^2} \cdot \varepsilon,$$

where the terms in the expression are defined as

$$\omega_k = c_L k, \quad \tau_0 = \frac{\chi}{c_L^2}, \quad \chi = \frac{\kappa}{\rho C_p}, \quad \varepsilon = \frac{v_{th}^2}{c_L^2}, \quad v_{th}^2 = \left[\frac{\alpha^2 K_{ad} T}{\rho C_p} \right].$$

ρ is the density, χ is the thermal diffusivity, κ is the thermal conductivity, α is the volume thermal expansion coefficient ($\alpha = 3\alpha_{linear}$ where α_{linear} is the linear expansion

coefficient) , K_{ad} is the adiabatic bulk modulus, c_L is the speed of sound, and C_p is the constant pressure specific heat per volume. For $\omega_k \gg 1/\tau_\theta$, the damping saturates to ε/τ_θ . This occurs for 3D LA modes relevant to phonon drag.

The ratio of the 1D and 3D LA scattering times for a mode with momentum k is

$$\frac{\tau_{3D}(k)}{\tau_{1D}(k)} = (kc_L)^2 \left(\frac{\chi}{c_L^2} \right)^2 \left[\frac{(1-\nu)}{(1+\nu)(1-2\nu)} \right] \left[\frac{\kappa(1D)}{\kappa(3D)} \right],$$

where ν is the Poisson ratio ($\nu = 0.29$ for Si). For the largest momentum $k = 2k_f$, the 3D LA mode lifetime is 3.3 times larger than the 1D LA mode. We take the ratio of the thermal conductivities to be 1/100. For the shortest wavelength LA modes, phonon drag is not enhanced in the wire. For long wavelength LA modes (small k), the lifetime of the 1D mode rapidly increases relative to the bulk due to the k^2 term and phonon drag is enhanced. In addition, the 3D scattering rate for long wavelength LA modes becomes adiabatic rather than isothermal leading to a further increase in the 1D LA mode lifetime relative to 3D. In this regime, the lifetime is increased by the ratio of the 3D to 1D thermal conductivities or ~ 100 .

The scattering rate of the 1D TA modes is smaller than the corresponding LA modes in bulk. The scattering rate of the 1D TA mode is²⁸

$$\frac{1}{\tau_{TA}(k)} = \omega_0(TA) \cdot \frac{(\omega_k / \omega_0(TA))^2}{1 + (\omega_k / \omega_0(TA))^2} \cdot \Delta, \quad \Delta = \left[\frac{\alpha_{linear}^2 K_{ad} T}{C_p} \right]$$

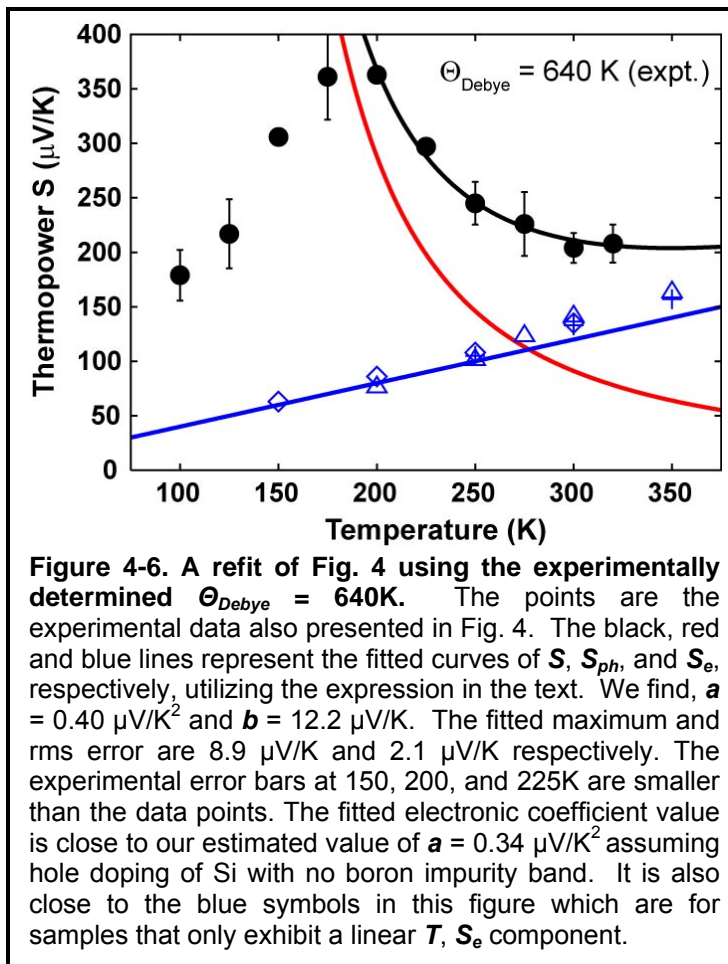
Since $\omega \gg \omega_0(TA)$, the TA modes are adiabatic and the scattering rate saturates to $\Delta\omega_0$. Using experimental values $K_{ad} = 9.8 \times 10^{11}$ dyne/cm, $\alpha_{linear} = 2.6 \times 10^{-6}$ K⁻¹, and $\rho = 2.3$ g/cm³ leads to $\tau_{3D}/\tau_{TA} \sim 1/2$. The phonon drag contribution from the TA modes is

increased due to the decreased thermal conductivity in the NW. Thus we have shown that the decreased thermal conductivity leads to increased phonon drag due to TA modes and long wavelength LA modes.

4.3.4 Theoretical Fit to the Phonon Drag Data

In Figure 4-6 we show how well the high temperature data (>200K) in Figure 4-3b is explained by:

$$S = S_e + S_{ph} = aT + b[\exp(\Theta_D / T) - 1]$$



where we set the Debye energy parameter to its experimental value of $\Theta_{Debye} = 640K$. As shown in Figures 4-5 and 4-6, phonon drag explains the observed monotonic increase in S as T decreases.

Ultimately, we must have $S \rightarrow 0$ as $T \rightarrow 0$ (by the 3rd law of thermodynamics) and this is observed experimentally. One factor

that we have not included is that at sufficiently low temperature, the mean free path approaches the dimensions of the system leading to scattering that eventually reduces S toward zero. It is also possible that for the doping levels used here the energy dependence of the electron-phonon scattering reduces the momentum transfer to LA phonons leading to a further reduction in S_{ph} at low T .

4.4 Conclusion

We have combined experiment and theory to demonstrate that semiconductor NWs can be designed to achieve extremely large enhancements in thermoelectric efficiency, and we have shown that the temperature of maximum efficiency may be tuned by changing the doping and the NW size. Theory indicates that similar improvements should be achievable for other semiconductor NW systems because of phonon effects. These nanowire thermoelectrics may find applications related to on-chip heat recovery, cooling, and power generation. Additional improvements through further optimization of NW size, doping, composition, etc., should be possible.

4.5 References

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Chapter 5

Future Directions

5.1 Reversible Thermoelectrics

The figure of merit, ZT , must be large to obtain a high efficiency. Principally, the thermopower and electrical conductivity must be large, and the thermal conductivity must be small. This general approach requires testing many different types of binary and even ternary materials. Until recently, there has been no known materials independent approach to reach the Carnot limit. A paper, published by T.E. Humphrey and H. Linke explains how to engineer a nanostructured material that would potentially provide an infinite ZT and thus, a route towards the Carnot efficiency¹.

The Carnot limit of any heat engine is achieved only when the heat engine operates under reversible equilibrium conditions². For a particle heat engine, such as a thermoelectric device where the working fluid consists of charged carriers, the equilibrium condition is satisfied when the Fermi-Dirac function is spatially invariant across the entire thermoelectric material¹. The Fermi function, $f = \frac{1}{e^{(E-\mu/kT)} + 1}$, describes the probability that an electronic state is occupied. If the temperature, T , and chemical potential, μ , are constant across the material, the f will be invariant. There is no preferred direction for particle flow or energy and therefore the electronic system is under equilibrium. Under such reversible equilibrium conditions, no additional entropy,

stemming from frictional or resistive losses is produced and the heat engine operates at the Carnot limit. The challenge, therefore, is to engineer a thermoelectric material in a way that provides for the spatial invariance of f under the imposed conditions of a temperature and chemical potential difference across that material³.

A thermoelectric device operates under the conditions of a temperature and chemical potential difference. In addition, bulk materials possess a continuum of electronic states with energies, E , that the charged carriers are allowed to occupy. Under a temperature gradient, the charged carriers will occupy a different distribution of those states that is appropriate at each temperature along the gradient. Therefore, f in a thermoelectric material is not spatially invariant. However, a nanostructured material composed of a superlattice nanowire (SLNW) has the ability to allow f to be constant across the material even under the influence of temperature and chemical potential differences.

A SLNW is a material composed of a series of quantum dots connected together,

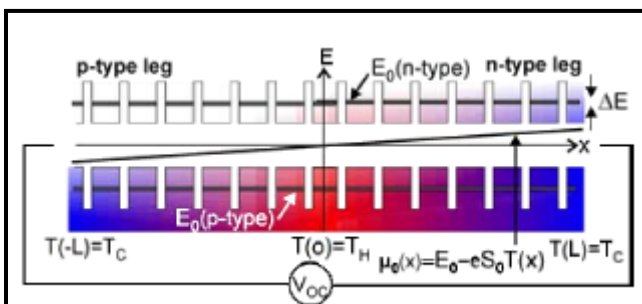


Figure 5-1. A superlattice nanowire (SLNW) consists of a series of quantum dots each with its own miniband ΔE . The entire material is under equilibrium when ΔE approaches a single energy state and the chemical potential and temperature differences offset each other exactly. These conditions make f spatially invariant. Figure is from Reference 1.

each with its own miniband ΔE for electrons or holes. ΔE represents a continuum of electronic states that the electrons or holes occupy within the quantum well. The chemical potential is tuned, either by doping or a gate voltage, across the SLNW to counteract the temperature difference so that the term, $(E -$

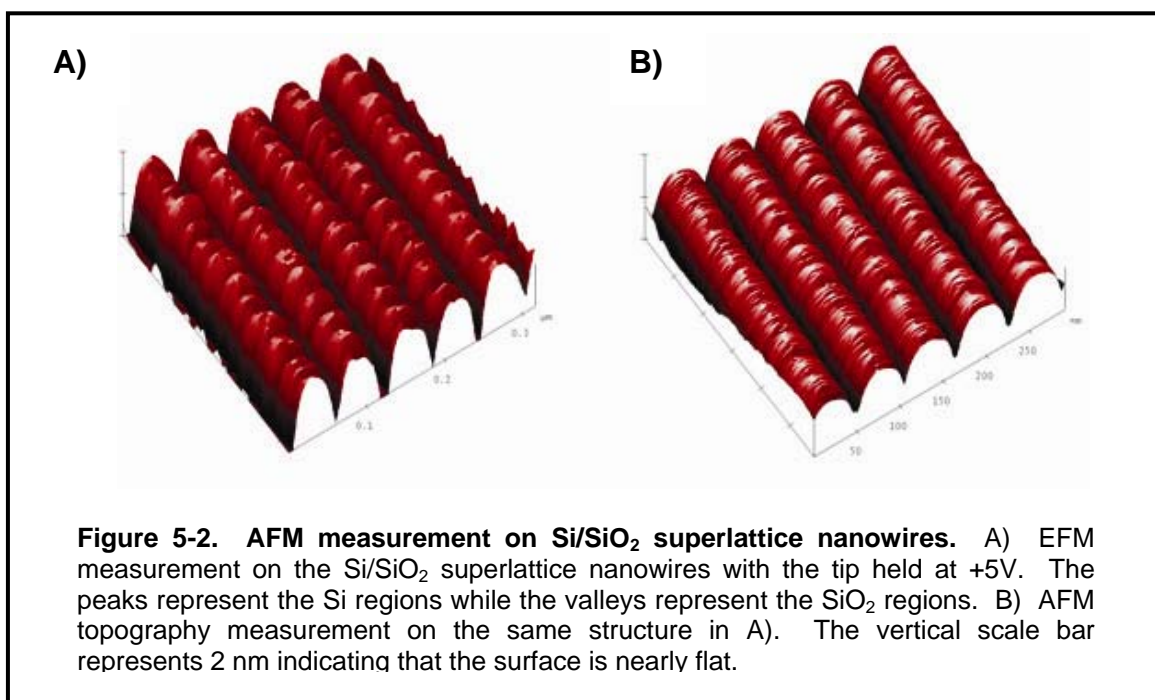
$\mu)/T$, is constant across the entire length of the SLNW when E represents only one electric energy level (Figure 5-1). If the quantum dots are made small so that the electronic states are separated by an energy larger than kT , then the electrons or holes occupy a single energy level $\Delta E = E_0$. The density of states is essentially composed of delta functions separated by an energy larger than kT so that only one state is occupied for each quantum dot in the SLNW. These conditions place the thermoelectric material under equilibrium and allow the efficiency to approach the Carnot limit.

5.1.1 Silicon Nanowire Based Quantum Dot Superlattices

A SLNW can be fabricated from a Si NW using the SNAP process. First, SNAP is used to create an array of degenerately doped Si NWs 20 nm in width and 20 nm tall. Next, a closely spaced array of Pt NWs fabricated by SNAP with a pitch of 10 nm and NW width of 20 nm is placed atop the Si NWs. Next, the entire structure is subjected to an O₂ plasma using a reactive ion etcher operating at 100W and 20 sccm for 5 minutes. Finally the Pt NWs are removed by placing the structure in a boiling solution of aqua regia for 20 minutes. The result is an array of Si NWs that have been periodically oxidized every 20 nm. This effectively creates a series of Si quantum dots 20 x 20 x 20 nm separated by a 10 nm thick tunneling barrier composed of SiO₂.

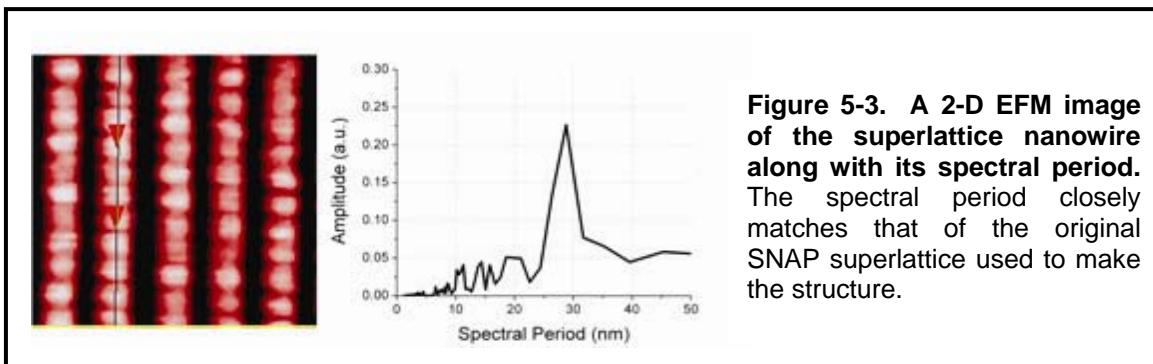
Atomic force microscopy (AFM) was used to characterize the Si quantum dot superlattice. Specifically, an AFM was operated in non-contact mode using electric force microscopy (EFM) whereby a +5V voltage is applied to a conductive Si tip. The tip hovers 50 nm above the surface of the sample as it is scanned. The grounded sample deflects the tip by either a repulsive or attractive force which depends on the sample's

conductance. When the tip is over the conductive Si quantum dots, there is an attractive force between it and the sample. When the tip is over the insulating SiO₂ tunneling barrier, the attractive force is diminished. This can be seen in the EFM image in Figure 5-2.



The image in 5-2A is an EFM scan with the tip held at +5V. The peaks are Si and the valleys are the oxidized Si surfaces. The image in Figure 5-2B was taken in tapping mode and shows the topography of the surface. The vertical scale bar in Figure 5-2B is 2 nm which clearly indicates that the surface is effectively flat. Therefore, the peaks in Figure 5-2A originate from the conductance difference of the Si and oxide and are not artifacts from topographic Van der Waals forces. Figure 5-3 shows a two dimensional EFM image along with the periodicity of the Si quantum dots. The periodicity of the Si dots closely follows the periodicity of the original SNAP lattice that was used to fabricate

the device, which was ~ 30 nm. The device was not tested electrically due to time constraints.



5.2 Enhanced Thermoelectric Properties of Thin Silicon Films With Nanostructured Holes

Bulk Si would exhibit a large figure of merit if its thermal conductivity was not so high. One strategy to increase ZT would be to alloy Si with germanium to decrease the thermal conductivity. This has already been tried and Si/Ge alloys find use as thermoelectrics at high temperatures where the thermopower is higher⁴. Another strategy to make bulk Si a useful thermoelectric material at room temperature would be to introduce defects that scatter phonons yet do not deleteriously affect the electrical transport properties.

Phonons in bulk Si have a mean free path on the order of ~ 100 nm while the electron's mean free path is much shorter, on the order of ~ 1 nm⁵. Defects can be introduced so that phonons are scattered preferentially over electrons and holes. This could be accomplished by periodically removing parts of the Si material, so that there exists a Si/air interface. These defects are essentially an array of holes etched into the Si that have a diameter of > 10 nm and periodicity > 10 nm (Figure 5-4). The size of the holes will scatter phonons but should not significantly interfere with the electronic

transport. This will allow a reduced thermal conductivity from bulk Si while maintaining bulk electrical conductivity.

The structure in Figure 5-4 is constructed using SNAP and reactive ion etching (RIE)⁶. First, the SNAP process is performed on a degenerately doped SOI substrate with a top Si layer thickness ~20 nm. Next, another round of SNAP is performed orthogonally on top of the first set of SNAP nanowires. The nanowires in both SNAP rounds are made from Pt. Next, the RIE is used to etch into the top Si layer through the SNAP on SNAP pattern using a plasma of CF₄. Finally, the structure is placed in aqua regia to remove the Pt. The resulting structure is an array of holes etched into a thin Si film (Figure 5-4). The holes have a diameter and periodicity determined by the SNAP superlattice. The structure in Figure 5-4 will soon be electrically tested.

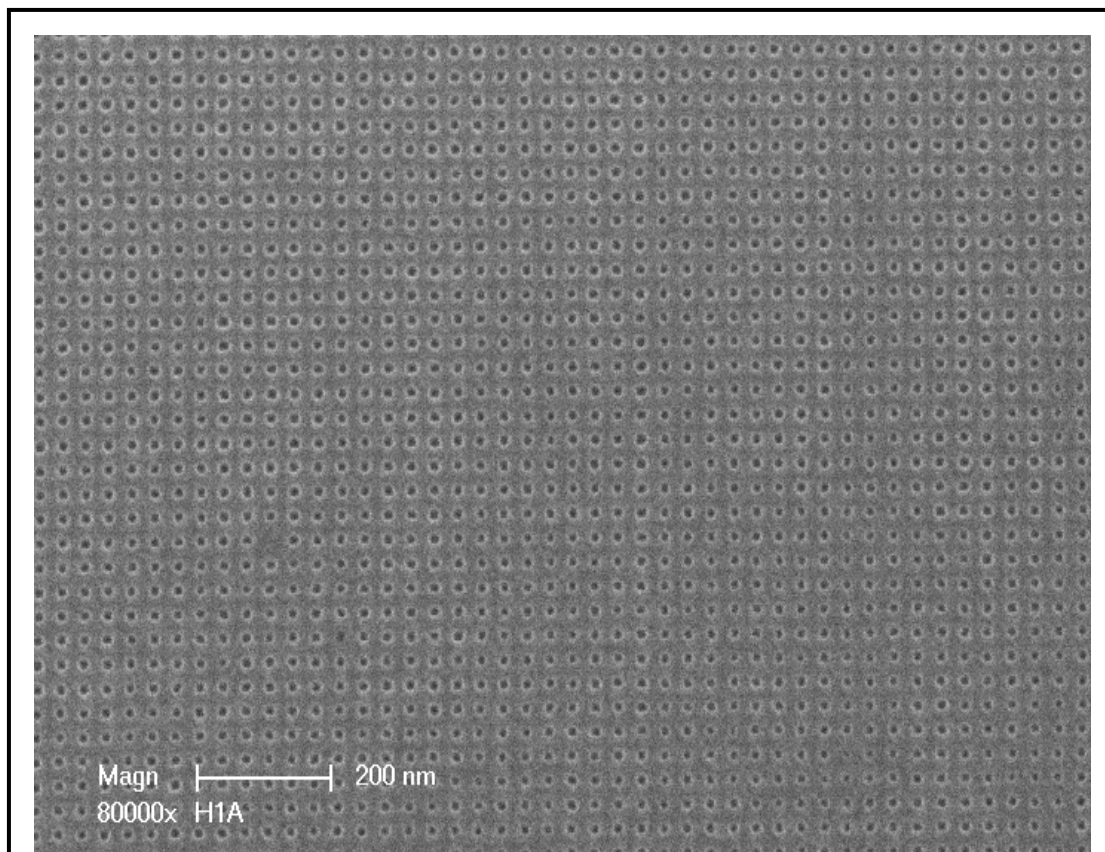


Figure 5-4. A 20 nm thick degenerately doped Si film with 20 nm diameter holes etched into its surface. This structure may provide the ability to scatter phonons while keeping the electrical transport properties bulk-like. Improvements in the figure of merit, **ZT**, should be possible.

5.3 References

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