Development of Endothelium-Denuded Human Umbilical Veins as Living Scaffolds for Tissue-Engineered Small Caliber Vascular Grafts

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Development of Endothelium-Denuded Human Umbilical Veins as Living Scaffolds for Tissue-Engineered Small Caliber Vascular Grafts

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Abstract

Tissue engineered small caliber vessel grafts may help to alleviate the lack of graft material for coronary and peripheral bypass grafting in an increasing number of patients. This study explored the use of endothelium-denuded human umbilical veins (HUV) as scaffolds for vascular tissue engineering in a perfusion bioreactor. Vessel diameter (1.2±0.4 mm), wall thickness (0.38±0.09 mm), uniaxial ultimate failure stress (8029±1714 kPa), and burst pressure (48.4±20.2 kPa, range 28.4 - 83.9 kPa) were determined in native samples. The effects of endothelium removal from HUV by enzymatic digestion, hypotonic lysis, and dehydration were assessed. Dehydration did not significantly affect contractile function, tetrazolium dye reduction, mechanical strength, and vessel structure, whereas the other methods failed in at least one of these parameters. Denudation by dehydration retained laminin, fibronectin, collagen, and elastic fibers. Denuded HUV were seeded in a perfusion bioreactor with either allogeneic HUV endothelial cells or with saphenous vein endothelial cells harvested from patients with coronary artery disease. Seeding in a perfusion bioreactor resulted in a confluent monolayer of endothelial cells of both sources as judged by histology and scanning electron microscopy. Seeded cells contained von Willebrand factor and CD31. In conclusion, denuded HUV should be considered an alternative to decellularized blood vessels as the process keeps the smooth muscle layer intact and functional, retains proteins relevant for biomechanic properties and for cell attachment, and provides a suitable scaffold for

1	Vascular grafts t
2 3 4	seeding an autologous and flow resistant endothelium.
5 6 7	Keywords: vascular tissue engineering, small caliber graft, endothelium,
8 9	biomechanics, human umbilical vein, bioreactor
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1. Introduction

Coronary artery disease and peripheral vascular disease are common maladies in elderly patients. Both are consequences of atherosclerosis and endothelial dysfunction. Risk factors are partly congenital and partly behavioural, which explains the high incidence of these conditions in western societies. Although symptoms of the diseases like angina pectoris can be treated successfully by pharmaceutical means, many patients eventually require surgical interventions. Coronary artery bypass grafting (CABG) and peripheral revascularization using autologous vessel grafts have turned into routine procedures with good longterm results. However, a considerable number of patients lack suitable autologous vessels due to varicosis, trauma, or prior removal, effectively precluding their optimal treatment. Also, surgical treatment of multi-vessel coronary artery disease usually requires the use of saphenous vein in addition to internal mammary artery. The former has patency rates of about 60% after 10 years due to vein graft disease <u>(Goldman et al. 2004)</u> and thus may require reoperations with a further limited supply of autologous grafts.

In contrast to the successful use of synthetic polymers like Dacron or ePTFE in the reconstruction of large diameter vessel defects, synthetic small-caliber vessel grafts are still considered inferior to autologous vessels in peripheral revascularization (Mamode and Scott 1999) and have only rarely been used in CABG (Hoenig et al. 2006). Synthetic graft failures have been attributed to infections, compliance mismatches, and thrombogenic surfaces (Bordenave et Page 5 of 50

al. 2005). Most synthetic polymers suitable as vessel replacements are less elastic and thus possess a far lower compliance compared to human vessels, and the lack of an endothelium promotes aggregation and adhesion of platelets. Consequently, research focused on tissue engineering by combining autologous cells with biocompatible scaffolds, thus addressing both the mechanical and thrombogenic issues of small-caliber synthetic grafts. Biocompatible polymers like collagens and fibrin, biodegradable polymers, and various preparations of extracellular matrix have been tested for their utility as scaffolds for vascular tissue engineering (Campbell and Campbell 2007). However, tissue-engineered vessels often suffer from one or more disadvantages which so far precluded their clinical use as bypass grafts. Among these are the absence of sufficient amounts of elastin, insufficient burst strengths, and culture times of up to one year.

Human umbilical cords contain one vein (human umbilical vein, HUV) and usually two arteries. These vessels are unbranched, have no valves with flaps, and can be obtained in lengths of up to 50 cm without ethical concerns. Glutaraldehyde-fixed HUV have been used as grafts for peripheral revascularizations for decades (Dardik et al. 2002). However, these grafts are entirely acellular, require an external Dacron stent, and merely act as passive conduits. Due to their lack of a functional endothelium, these grafts have never been considered for CABG. Decellularized HUV have been suggested as scaffolds for vascular tissue engineering (Daniel et al. 2005), whereas our group suggested to use denuded HUV (denHUV) as a semi-finished scaffold, to be

completed by the recipient's own endothelial cells <u>(Hoenicka et al. 2007)</u>. This approach is likely to decrease the time required to assemble and condition the graft, as the synthetic capabilities of the smooth muscle layer are preserved. More recently, decellularized human umbilical arteries have been tested as scaffolds as well <u>(Gui et al. 2009)</u>.

We have previously demonstrated that mechanically denuded HUV are suitable scaffolds for HUVEC seeding under static conditions. To further develop this material into vessel grafts, the current study explored methods to denude longer segments of vessels while retaining their mechanical integrity and function, and to develop seeding procedures in a perfusion system suitable for tissue-engineering vessel grafts of suitable lengths. Furthermore, the scaffolds were seeded with human saphenous vein endothelial cells (HSVEC) derived from CAD patients to demonstrate the feasibility of a recipient-derived endothelium.

2. Materials and Methods

2.1. Harvesting of vascular tissue

Human umbilical cords were procured in the OB/GYN departments of the participating universities as described previously (Hoenicka et al. 2008) and were used for experiments within 40 hours post partum. Written informed consent was obtained from the expectant mothers before birth commenced. The cords were stored immediately after birth at 4 °C in Krebs-Henseleit buffer (KHB; NaCl 118 mM, KCl 4.7 mM, MgSO₄ 1.2 mM, NaH₂PO₄ 1.2 mM, NaHCO₃ 16.7 mM, dextrose 5.5 mM, CaCl₂ 1.2 mM; chemicals were from Merck,

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Darmstadt, Germany, or from Sigma, Taufkirchen, Germany, unless noted otherwise) supplemented with HEPES (25 mM) and penicillin (100 U/ml) / streptomycin (100 μ g/ml, PAA, Pasching, Austria). HUV were dissected free from connective tissue in a sterile hood. All experiments were in accordance with the rules of the ethical review boards of the participating universities.

2.2. Denudation procedures

HUV segments of approx. 8 cm in length were subjected to several procedures designed to remove the endothelium without affecting the structure and function of the remainder of the vessel wall. The initial conditions described here were arrived at empirically, and all further optimizations are reported in the results section. Segments of the vessels were obtained before and after denudation for organ bath experiments, tetrazolium dye reduction, and histological analysis. In all methods, vessels were immersed in cell culture medium during the procedures to maintain the integrity of the vessel wall as far as possible. Also, vessels were thoroughly flushed with cell culture medium immediately after the procedures to remove any debris and to restore a conducive environment. Endothelial cells (EC) were removed enzymatically according to methods established to harvest EC from umbilical veins (Jaffe et al. 1973). In brief, vessels were filled with 0.1% (w/v) collagenase A solution (Roche, Mannheim, Germany) and incubated at 37 °C in a cell culture incubator. The vessels were then rinsed thoroughly with M199 (PAA) containing 10% fetal calf serum (FCS, PAA) to interrupt proteolysis.

The second method used hypotonic media to disrupt endothelial cells by osmotic lysis. The vessels were either slowly perfused with sterile distilled water at room temperature (for 1 min incubation time), or they were filled with distilled water and incubated at room temperature (for incubation times longer than 1 min).

Denudation method three used a gentle stream of gas to dehydrate EC. This method is based on earlier reports which investigated the role of endothelium in small-caliber animal vessels (Bjorling et al. 1992; Fishman et al. 1975). Carbogen (95% oxygen, 5% carbon dioxide, Linde, Pullach, Germany) flow was adjusted to 60 ml min⁻¹ by means of a needle valve. The gas stream was passed through a sterile filter into the vessels for 10 min.

2.3. Determination of contractile properties

Responses to vasoconstrictors were assayed in an organ bath as described previously (Hoenicka et al. 2007). In brief, vessel rings of 2 mm segment length were mounted between stainless steel hooks. The upper hook was attached to a transducer which allowed to read out isometric forces. The baths were filled with KH at 37 °C and bubbled with a mixture of 5% oxygen and 5% carbon dioxide (balance nitrogen, Linde). Vessel rings were equilibrated over a period of approx. 2 hours. Tensions were readjusted repeatedly until a stable baseline was established at approx. 20 mN. Then the response to 150 mM KCl was read. After allowing the rings to return to the baseline, dose-response curves to 5-hydroxytryptamine (5-HT, Sigma) were constructed. Four to eight rings per

sample were analyzed.

2.4. Determination of tetrazolium dye reduction

Cells and tissues reduce tetrazolium dyes to chromophores whose concentrations are proportional to the reductive capacities. The enzymatic conversion of the chromogenic substrate 3-(4,5-dimethylthiazol-2-yl)-5-(3carboxymethoxyphenyl)-2-(4-sulfophenyl)-2H-tetrazolium (MTS, Promega, Madison, WI, USA) on the luminal face of longitudinally opened vessels was determined as described previously (Hoenicka et al. 2007), using three to five wells per sample.

2.5. Determination of tensile strength

Mechanical properties of vessel segments were determined in a tensile testing rig (Inspekt Desk 50, Hegewald & Peschke, Nossen, Germany) equipped with a 20 N load cell (KAP-S, Peekel Instruments, Rotterdam, Netherlands). Vessel rings of 3 mm segment length were mounted between two cylindrical supports and strained uniaxially until they failed, using a constant speed of 10 mm min⁻¹. Force and displacement data were used to construct stress-strain relationships and to determine ultimate failure stresses. Four to five rings were analyzed per sample.

Representative vessel segments (n=15 with 4 sections per vessel) were used to determine internal diameters and wall thicknesses at physiological pressure near term. The segments were mounted on glass tubes, filled with phosphate-buffered formalin (4%), and sealed on on the opposite end. A hydrostatic

pressure equivalent to 15 mm Hg was applied for 10 min after which the samples were transferred to formalin and fixed overnight. Samples were then embedded in paraffin and stained using a standard H&E protocol. The area of the lumen, and the area of the smooth muscle layer were determined in each sample morphometrically. Idealized circular rings were computed from these data and provided internal diameters, median diameters, and wall thicknesses for further calculations.

2.6. Determination of burst pressure

Burst pressures of vessels were measured in a custom built instrument (Fig. 1). A 10 ml syringe was driven by a computer-controlled stepper motor and delivered a 5% (w/v) solution of methylcellulose in phosphate-buffered saline at a flow rate of 3.0 ml min⁻¹. Samples of 6 cm in length were mounted on glass tubes of 3 mm outer diameter. One glass tube was equipped with a stopcock, the other was attached to the syringe using silicone tubing. Luminal pressure between syringe and sample was read out by a pressure transducer with a precision of 0.1% (Wagner Meß- und Regeltechnik, Offenbach, Germany). Samples were monitored by two orthogonally mounted USB cameras (Webcam 9000, Logitech, Morges, Switzerland). Volume, pressure, and video data were saved in a synchronized fashion which facilitated correlating the sudden drop of luminal pressure with visual clues of bursting. As the measured burst pressures are likely to depend on the quality of vessel dissection (see discussion), samples were prepared independently by two skilled persons. One to four segments per subject were measured.

2.7. Cell culture

HUVEC were isolated enzymatically from human umbilical veins (Jaffe et al. 1973) and further cultured in M199 supplemented with 10% FCS (both from PAA) and endothelial cell culture supplement (Promocell, Heidelberg, Germany). HSVEC were prepared enzymatically from human saphenous veins and cultured in the same medium except that 20% serum were used. Both cell types were trypsinized (trypsin-EDTA, Sigma) at confluence and expanded to sufficient cell numbers. Cells of passages 1 and 2 for HUVEC and HSVEC, respectively, were harvested for seeding experiments. These cells were incubated with Calcein AM (1 μ g ml⁻¹, Molecular Probes, Eugene, OR, USA) for 60 min at 37 °C prior to seeding to facilitate easy identification of seeded cells in histological sections.

2.8. Perfusion System

Details of the perfusion system have been published previously (Hoenicka et al. 2010). In brief, mock circulations were set up consisting of media reservoirs, membrane oxygenators, separate peristaltic pumps for the perfusion and superfusion loops, compliance chambers, and vessel chambers. The oxygenators and the vessel chambers were kept at 37±0.05 °C. Each circulation was filled with M199 supplemented with 20% FCS at 37 °C. The oxygenators were perfused with a mixture of 20% oxygen and 5% carbon dioxide (balance nitrogen, Linde). Oxygen and carbon dioxide partial pressures as well as pH were monitored with a blood gas analyzer (ABL 800, Radiometer, Willich,

Germany). Vessel chambers were connected to computer-controlled stepper motors via timing belts to provide continuous or intermittent rotation during seeding procedures. Rotational speeds were adjustable between 0.06 and 60 rpm. Intermittent rotation included breaks of adjustable length after each 90° turn, providing some time of static incubation for cells to settle and adhere.

2.9. Seeding procedure

After mounting the scaffolds in the vessel chambers, perfusion and superfusion pumps were set to 20 ml/min and 40 ml/min, respectively. Scaffolds were equilibrated for 1 h under flow (Fig. 2). Prior to adding the cells, the perfusion was shut off, whereas the superfusion continued to run throughout the entire seeding procedure to maintain nutrient and oxygen delivery to the vessel walls. Cell suspensions were injected through ports in the perfusion loop at a concentration of approx. 5E6 cells ml⁻¹. Immediately after injecting the cells, automated rotation was started. After finishing the adhesion step (60 min), rotation was stopped, and the perfusion was turned on briefly to remove nonadhering cells and to replenish fresh medium inside the vessels. After an additional 60 min of static incubation, vessels were perfused continuously until the experiment was terminated. The constructs were then fixed in situ by slowly infusing phosphate-buffered formalin (4%). One half of each sample was used for histological analysis, the other half was further treated in phosphate-buffered paraformaldehyde (2%) supplemented with 2.5% glutardialdehyde for scanning electron microscopy (SEM).

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2.10. Histology and immunohistochemistry

Formaldehyde-fixed samples were embedded in paraffin. Thin sections were prepared in a microtome and mounted on glass slides. Fluorescently labelled cells were visualized under UV illumination using appropriate band-pass filters on a Leica DMRBE microscope (Leitz, Wetzlar, Germany). Histological staining was done using standard protocols. General morphology was analyzed in hematoxylin and eosin (Chroma, Münster, Germany) stained slides. Elastic laminae and collagen were visualized with resorcin-fuchsin (Chroma) and Sirius red (Sigma), respectively. Specific antibodies were used to label laminin (clone LAM-89, monoclonal from mouse, Sigma), fibronectin (A0245, polyclonal from rabbit, Dako, Glostrup, Denmark), CD31 (clone JC70A, monoclonal from mouse, Dako), von Willebrand factor (A0082, polyclonal from rabbit, Dako), and α -smooth muscle cell actin (clone 1A4, monoclonal from mouse, Sigma). Bound antibodies were visualized using biotinylated secondary antibodies (donkey anti rabbit and donkey anti mouse IgG [H+L], Jackson ImmunoResearch, Suffolk, UK) and the Vectastain Elite ABC kit (Vector, Burlingame, CA, USA) according to the manufacturer's protocol. Diaminobenzidine (Sigma) was used as chromogenic substrate.

2.11. Scanning Electron Microscopy

Formalin/glutardialdehyde-fixed vessel samples were dehydrated and sputtered with gold using standard protocols. Samples were analyzed in a Quanta-400F scanning electron microscope (FEI, Hillsboro, OR, USA) using an accelerating

voltage of 10 kV.

2.12. Data Analysis and Statistics

Numerical data are reported as means±standard deviation. The number of repeats n refers to the number of subjects. Treatments were compared using analysis of variance (ANOVA) followed by Holm-Sidak post-tests. Dose-response curves were analyzed by fitting a Hill function, which allowed to compute maximum responses and half maximal effective concentrations (EC₅₀). Dose-response curves were compared by two-way ANOVA. Differences were assumed to be statistically significant if the error probability p was less than 0.05.

The data obtained from the tensile testing experiments were used to calculate ultimate failure stresses and extrapolated burst pressures. The undeformed cross section areas S_0 of the rings were calculated from the wall thickness t_0 and the segment length I_0 :

$$S_0 = 2 \times t_0 \times l_0 \tag{1}$$

The engineering (1. Piola-Kirchhoff) stress is calculated from the ultimate failure force F according to (2):

$$\sigma_{uPK} = \frac{F}{S_0}$$
(2)

The true (Cauchy) stress can be calculated from this quantity by multiplying it with the ultimate stretch ratio λ_t (3):

$$\sigma_{uC} = \sigma_{uPK} \times \lambda_t \tag{3}$$

Vascular grafts from umbilical veins

To compute the extrapolated burst pressures, the deformed radius R is calculated from the undeformed radius R_0 and the stretch ratio λ according to (4):

$$R = \lambda_t \times R_0 \tag{4}$$

The other deformed dimensions of the ring can be calculated from the incompressibility condition in the form $J = \lambda_r \times \lambda_r \times \lambda_a = 1$, where t, r, and a denote the circumferential, radial, and axial dimensions, respectively, of the rings in a cylindric coordinate system. As an initial approximation it was assumed that the material is isotropic. Then it holds $\lambda_r = \lambda_a$. Therefore,

$$\lambda_r = \sqrt{\frac{1}{\lambda_r}} \tag{5}$$

The deformed specimen thicknesses t and lengths I can be computed from these stretch ratios and the initial dimensions t_0 and I_0 . The resulting extrapolated burst pressure is then calculated using the Laplace law according to (6):

$$p_{burst} = \frac{\sigma_c \times t}{R} \tag{6}$$

The internal diameter d_i of the vessels during burst pressure measurements were computed according to (7) from the average outer diameter d_o along the entire sample using the histologically determined wall thickness at 15 mm Hg, assuming that the cross-sectional wall area A remains constant due to incompressibility of the wall.

$$d_i = 2 \times \sqrt{\frac{(0.5d_o)^2 \pi - A}{\pi}}$$

(7)

3. Results

3.1. Endothelium removal

If denuded HUV are to be seeded with autologous endothelial cells, the existing endothelium has to be removed entirely, not just inactivated. Starting from initial conditions taken from the literature, if available, all three denudation methods were optimized to effect complete removal of endothelial cells from the luminal surface of HUV as judged by histology. At least five vessels were evaluated per condition in this initial screening. Fig. 3A shows a native control with intact endothelial and smooth muscle layers. Collagenase treatments of 10, 20, and 30 min were tested. Essentially all EC were removed after 20 min (Fig. 3B). However, in many cases the structural integrity of the vessel wall was visibly affected and sometimes the smooth muscle layer appeared spongiform. Denudation by a gas stream was tested at 5, 10, and 20 min. Complete EC removal was accomplished after 10 min (Fig. 3C). Fig. 3D-F shows a time course (1, 3, and 5 min) of hypotonic treatment with distilled water. Incubation times of 5 min were required to destroy and remove virtually all endothelial cells.

3.2. Vessel dimensions and mechanical properties

Internal diameters of HUV under moderate pressure (15 mm Hg) were

determined as 1.2±0.4 mm. Wall thicknesses amounted to 0.38±0.09 mm. In order to assess the influence of denudation treatments on the mechanical stability of vessels, HUV were cut into four segments. One served as native control, whereas the others were subjected to the optimized denudation methods. Force-distension relationships of these specimens were determined (Fig. 4 A). The resulting stress and strain data were used in conjunction with the morphometric data to compute theoretical burst pressures. Denudation by dehydration and denudation by osmotic lysis did not affect tensile strength, whereas collagenase treatment significantly reduced the strength of the vessel rings (RM ANOVA, p=0.007, n=5, Table 1). All extrapolated burst pressures exceeded 1200 mm Hg.

Volume-pressure relationships and burst pressures of native vessel segments were determined experimentally (n=8). A representative burst experiment is shown in Fig. 4 B. The burst pressures were calculated as 362.7±151.7 mm Hg / 48.4±20.2 kPa (range 213.3 - 629.3 mm Hg / 28.4 - 83.9 kPa).

3.3. Influence of denudation on contractile function

The response to vasoconstrictors is a key feature and a sensitive marker of vessel wall integrity. Receptor-independent vasoconstriction was induced by adding 150 mM KCI to the baths. Responses of gas-denuded HUV did not differ from native controls. However, HUV treated by collagenase or by osmotic lysis showed significantly decreased contractions to KCI (RM ANOVA, p=0.005, n=7, Table 2).

5-HT is one of the most potent receptor-mediated vasoconstrictors in HUV_ (Hoenicka et al. 2007). Gas denudation did not affect 5-HT dose-response curves compared to native controls, whereas both collagenase treatment and osmotic lysis attenuated responses to this compound (RM ANOVA, p=0.001, n=7, Fig. 5). EC₅₀ values of collagenase-treated HUV were significantly higher compared to native controls and to gas-denuded vessels (RM ANOVA, p=0.006, n=7, Table 2).

3.4. Influence of denudation on reductive capacities

Tetrazolium dye reduction is a measure of the reductive capacities of cells and tissues and as such a useful marker to assess effects of treatments on energy metabolism. Denudation did not affect reductive capacities after any of the treatments, indicating that the contribution of the endothelium to dye reduction was small and that the metabolism of the remainder of the vessel wall was left intact (RM ANOVA, p=0.542, n=6, Table 2).

3.5. Histological Analysis of native and denuded HUV

The structures and compositions of native and denuded vessel walls were analyzed by histochemistry and immunohistochemistry (Fig. 6). H&E staining revealed the gross structure of the vessels including the endothelium. Native vessel sections contained an intact endothelial layer as well as a strong pink staining of the cytoplasm and a less intense staining of extracellular matrix. Denuded vessels were devoid of endothelial cells as desired. Collagenase treatment mostly affected the staining of the matrix, but it also caused a weaker

intracellular staining on the luminal side. There were no visible changes in the smooth muscle and subendothelial layer of gas-denuded and water/NaCldenuded vessels compared to the native controls. The α -smooth muscle actin antibody stained the entire smooth muscle layer homogenously. As expected, the stain was present only inside the cells. Denuded vessels did not stain differently from native vessels. Superficial differences in the staining intensity are due to different densities and orientations of individual smooth muscle cells. Extracellular matrix proteins are important for the remodelling and cell adhesion properties of scaffolds. Fibronectin is commonly associated with extracellular matrix in vessel walls. Native HUV showed an extracellular staining throughout the entire smooth muscle layer. There was a very intense staining in the subendothelial layer. Collagenase treatment caused a decrease of the staining intensity on the luminal side of the smooth muscle layer. There was no staining in the subendothelial layer. Denudation by dehydration or by osmotic lysis did not alter the fibronectin staining properties compared to the native controls. Laminin was also present throughout the smooth muscle layer. However, in contrast to fibronectin there was no intense staining of the subendothelial layer. Denudation by dehydration or by osmotic lysis did not affect laminin staining, whereas collagenase treatment caused a slightly weaker staining on the luminal side compared to native controls. Resorcin was used to visualize elastic fibers. Native vessels showed an intense staining of the subendothelial layer, with usually 2-4 slightly less intense layers underneath. In most samples, the entire smooth muscle layer contained weakly stained strands of elastic fibers.

Collagenase treatment strongly affected the staining of the subendothelial layer, leaving only a minor amount of the resorcin-stainable material in the vessel. In contrast, denudation by dehydration and by osmotic lysis did not affect elastic fibers. Finally, sirius red was used to stain collagen, a major component of the extracellular matrix. The entire smooth muscle layer was stained intensely red, with a weakly yellow stain inside the cells. As expected, collagenase treatment affected sirius red staining on the luminal side, whereas there was no such effect after applying the other denudation methods.

3.6. Seeding of denuded HUV

Based on the results described above, all vessels used in seeding experiments were denuded by dehydration. Translation of a static seeding model using longitudinally opened vessels to a perfusion system using tubular vessels necessitated the development of rotational patterns which optimized both homogenous distribution of the seeded cells and complete coverage. Optimization of cell distribution was done using HUVEC labelled with Calcein AM with at least 3 independent experiments per condition. First, continuous rotation was compared to intermittent rotation, using a total seeding time of 60 min. Rotational speeds were varied between 0.12 and 0.5 rpm. However, histological analysis revealed that none of the tested rotational speeds resulted in reasonable amounts of adherent cells (not shown). Second, intermittent rotation was optimized. This required the adjustment of two parameters, rotational speed and length of the static phases. Rotational speeds of 0.25, 0.5, and 1 rpm and static phases of 1 min to 5 min were evaluated. The results were

largely independent of rotational speed but sensitive to the duration of staticphases. 5 min tended to create alternating longitudinal strips of seeded andcell-free areas, whereas 1 min reduced the overall number of adhering cells.Based on these observations, rotation at 0.5 rpm interrupted by 3 min staticphases were used in all subsequent seeding experiments.

The initial endothelial cell coverage was supposed to be as complete as possible in order to avoid cell-free patches that might act as starting points of endothelium loss once shear forces were applied. Critical factors affecting coverage are seeding cell density and total incubation time. Based on our previous experience with static seeding models, cell suspensions ranging from 5E5 to 1E7 cells/ml were applied for one hour. Assuming an average diameter of the vessels of 3 mm during perfusion, these suspensions resulted in seeding densities of 6.6E4 to 1.3E6 cells per cm². In general, the lowest concentrations did not provide sufficient coverage, whereas the highest concentrations tended to acidify the medium in the lumen of the vessels visibly. Therefore concentrations of approx. 5E6 cells were used in all further experiments. Extending the incubation time beyond one hour did not further increase endothelial coverage. In order to obtain best possible results, the vessels were perfused briefly after the first hour of incubation, and a second batch of cells was injected, followed by another hour of intermittent rotation. The results obtained with a protocol based on the above mentioned optimizations are shown in figures 7 and 8. Both images are representative for 5 independent experiments per condition. All vessels were perfused for 24 h after

seeding at 20 ml/min. Figure 7 demonstrates that there were no differences in the appearance of cross sections of denuded HUV seeded with HUVEC and HSVEC. Both formed continuous monolayers. Figure 8 Panel A depicts the surface of native HUV as seen by SEM. Endothelial cells were densely packed and fairly small. After denuding HUV, the basal membrane on top of the smooth muscle layer was visible (Panel B). Seeding with HUVEC resulted in a completely covered surface. The cells appeared flattened, each one covering a larger area compared to native EC (Panel C). Seeding with HSVEC resulted in a similar endothelial coverage (Panel D), although the cells appeared slightly smaller compared to HUVEC.

The identity of seeded endothelial cells was verified using two markers. CD31 is a surface protein expressed on endothelial cells, whereas von Willebrand factor (vWF) is a protein synthesized in and secreted from endothelial cells. Cross sections of gas-denuded HUV and of EC-seeded HUV were stained with specific antibodies for each marker. Fig. 9 shows that the seeded cells express CD31 on their surfaces. vWF is also present, although a considerable level of staining is found in the subendothelial layer and was present before seeding.

4. Discussion

The necessity of artificial vessel grafts has long been recognized, either as an alternative to harvesting autologous vessels, or as a substitute if suitable autologous vessels are not available. In the past decades, a variety of scaffolds for vascular tissue engineering have been evaluated with mixed success.

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Synthetic polymers often do not achieve suitable mechanical and antithrombotic properties. Therefore, tubular organs of animal or human origin have attracted attention because of their wall structures, mechanical properties, and lack of foreign body reactions after suitable treatments. Decellularized blood vessels (reviewed in (Hoenig et al. 2005)) and ureters (Narita et al. 2008; Derham et al. 2008; Clarke et al. 2001) of various species have been investigated for their utility as biological conduits, requiring recellularization in vivo, or as scaffolds for vascular tissue engineering. Recellularization can be readily achieved in various species, including dog and sheep, which usually also manage to grow a confluent autologous endothelium on grafts. These results are enticing, but usually reflect a transanastomotic growth of endothelial cells on the often short grafts. In humans, this type of endothelial growth rarely exceeds 2 cm in length and is clearly insufficient for both coronary and peripheral bypass grafts which usually require ten times this length (Zilla et al. 2007). Endothelialization is of utmost importance for graft patency as it suppresses thrombogenesis and graft rejection. Therefore, tissue engineering is currently the most promising approach, as it allows to grow an autologous endothelium from patient-derived endothelial cells in vitro.

Human umbilical vessels have been evaluated for their utility as bypass grafts previously. HUV is an unbranched vessel which can be harvested in lengths suitable for one or two coronary bypasses. The diameter of vessel cross sections was determined in the present study as approx. 1.2 mm under moderate pressure (15 mm Hg). This was less than the value of 2.4 mm reported for term pregnancies in a recent study <u>(Li et al. 2008)</u>. The lower values may be attributed to a gentler method of sample preparation in the present study (dissection vs. "stripping"). It should also be noted that the diameter is up to 5 mm in utero as measured by ultrasound <u>(Rigano et al.</u> <u>2008)</u>, which is also roughly the diameter of the umbilical vein-based UVg graft_ (Dardik et al. 2002). Our burst pressure measurements indicated that umbilical veins distend to almost this diameter under arterial pressure. Therefore HUV are properly sized for small-diameter bypass grafts.

HUV have been tanned and wrapped in dacron sheets to use them as peripheral bypass grafts with good results (Dardik et al. 2002). However, these grafts have never been considered for coronary bypass grafting. Using decellularized umbilical vessels was suggested both for veins (Daniel et al. 2005) and for arteries (Gui et al. 2009). Unfortunately, procedures based on decellularized tissues face several problems. First, the chemicals or enzymes used to remove the cells may require tedious post-processing to remove or inactivate them. Second, the generation of a layered wall structure is difficult to achieve in vivo, as there is usually only minor cell ingrowth from the surfaces_ (Gui et al. 2009). Third, the time to engineer a fully repopulated and endothelialized graft in vitro is usually too long for on-demand production. We have suggested to overcome these limitations by using endothelium-denuded HUV and seed these with autologous cells derived from the recipient (Hoenicka et al. 2007). This way, there is a layered wall structure with vital cells from the start, and matrix synthesis by smooth muscle cells present in denuded vessel

walls is likely to reduce the time of the tissue-engineering procedure considerably. Also, it was shown previously that allogeneic vessel transplantations succeed without immunosuppression if the denuded vessels are seeded with autologous endothelial cells before implantation (Lamm et al. 2001).

In our previous study, patches of HUV were denuded mechanically and seeded under static conditions, providing a first proof of concept that a confluent allogeneic endothelium can be generated on this type of scaffold. The present study attempted to create endothelium-seeded grafts under perfusion conditions. Therefore methods to denude longer segments of HUV had to be developed. Based on reports in the literature and on our own preliminary experiments, three methods were evaluated in detail with respect to their simplicity, reproducibility, and effect on vessel wall structure and function. The first method is a slight modification of a well-established procedure to harvest endothelial cells from umbilical veins (Jaffe et al. 1973). Usually the incubation time is optimized to ensure purity of the harvested cells at the expense of yield. In order to create an endothelium-denuded scaffold, the incubation time had to be optimized to ensure complete removal of endothelial cells. This required longer incubations (20 min vs. 10 min for cell harvesting). However, this method had a noticeable impact on the structure of the vessel as well as on its function. Although there was no decrease in reductive capacity, indicating an unaltered energy metabolism, contractions induced by KCI or by 5-HT were significantly weaker. The failure stresses were significantly reduced as well. Histology

revealed that smooth muscle actin was largely unaffected, whereas collagen, elastin, fibronectin, and to a smaller degree also laminin stained weaker on the luminal side. This is easily explained by the loss of anchoring sites due to the digestion of parts of the collagen framework. Many vessels also showed structural defects as a consequence of collagen loss. These resulted in significantly lower failure stresses compared to the native controls.

Hypotonic media have been used to lyse cells in various contexts <u>(Kong et al.</u> <u>2008; Crowston et al. 2004)</u>. Preliminary experiments have shown that this method is also suitable to lyse cells on the luminal face of blood vessels if the vessels are flushed or filled with distilled water. Time courses demonstrated that it took 5 min to completely destroy and remove endothelial cells. However, contractile responses to KCI and 5-HT were attenuated after incubations as short as 3 min, and were significantly lower after 5 min incubations. Histological evaluation confirmed that this treatment specifically removed endothelial cells without affecting any of the investigated components. Failure stresses were not affected.

Dehydration of endothelial cells by a stream of gas has originally been used to investigate the role of endothelium in microvessels too small for mechanical denudation (Bjorling et al. 1992; Fishman et al. 1975). However, we found this method useful for denuding HUV as well. The residence time, i.e. the time it took to replace the gas volume in our samples, can be estimated as 0.1 s. It seems quite unlikely that the gas gets saturated with humidity in this short amount of time. Therefore the method is likely to work also for segments longer Page 27 of 50

than those used in this study. At the flow rate and incubation time which were found to remove the endothelium reproducibly, none of the functional and mechanical parameters was affected. Histological analysis also confirmed that the treatment solely affected the endothelium.

Two key results from the histological analysis should be pointed out: first, while HUV lack an external elastic lamina, they contain copious amounts of elastin in the subendothelial layer as well as throughout the smooth muscle layer, which positively affects their elastic properties. Second, denudation retains proteins, especially fibronectin and laminin, which are considered important for endothelial cell attachment and growth, whereas decellularized vessels usually require precoating with one of these proteins to facilitate endothelial cell adhesion (Gui et al. 2009).

The mechanical properties of HUV were investigated by determining the stressstrain relationships of HUV rings in an uniaxial tensile testing rig and by measuring the burst pressure of HUV segments directly. The stress-strain curves of HUV displayed a biphasic behaviour which is commonly found in blood vessels. This was not altered by any of the denudation procedures. The corresponding pressure-volume relationships of intact vessels display a slightly different behaviour which can be best described as triphasic. A fairly steep initial phase was followed by a rather flat intermediate phase at physiological arterial pressures. Additional pressure resulted in a second steep phase until the vessel failed. The mechanism and the structural base of this behaviour require further biomechanical analyses which are currently under way. The burst pressures

varied between 213.3 and 629.3 mm Hg. This may indicate a problem of dissecting the vessels cleanly without injuring the vessel wall. This also resulted in a marked deviation of the burst pressures extrapolated from the stress-strain curves and the experimentally determined values. The latter were found to be considerably lower. Several factors contribute to this deviation. First, vessels measured in the burst pressure apparatus fail at their weakest point by design, whereas the failure stresses of the replicates of each sample in the tensile testing experiments were averaged. Second, experimental determination of burst pressures exerted biaxial stress whereas tensile testing was uniaxial. Biaxial ultimate stresses are substantially lower than uniaxial ones even in isotropic elastomers, and the stress-strain curves differ also in these materials. Moreover, the data suggest that HUV are less resistant to axial stress compared to circumferential stress and thus appear to be anisotropic. When comparing these burst pressures with those of autologous bypass vessels or artificial vessel grafts, it should be taken into consideration that the parameters of vessel conditioning in a perfusion bioreactor, which was not done in this initial study, are usually optimized to increase extracellular matrix formation and thus to increase mechanical stability.

With these results at hand, dehydration of the endothelium by a stream of gas appeared to be the most appropriate technique to denude HUV and was used in all subsequent seeding experiments. Most importantly, neither contractile responses as an indicator of general smooth muscle cell function nor tetrazolium dye reduction were affected by the procedure. Therefore it is Page 29 of 50

reasonable to expect that biosynthetic functions remain intact as well and allow vessel wall remodeling during a conditioning step.

The seeding experiments in this study had two main goals: first, to show that seeding denuded HUV works in a perfusion bioreactor. Second, to show that HSVEC from CAD patients, in addition to the commonly used HUVEC, are suitable for regenerating a confluent endothelium on denuded HUV. The seeding concentration of 5E6 cells ml⁻¹ resulted in a seeding density of approx. 1.5E6 cells cm⁻² and was arrived at empirically. This value is considerably higher compared to the one applied during static seeding (3E4 cells cm⁻²) in our previous study (Hoenicka et al. 2007). Apparently the curvature of the scaffold makes it more difficult for cells to attach, requiring higher local concentrations to succeed. The perfusion system used in the present study allowed to employ continuous or intermittent rotation of the denuded vessel samples after applying the endothelial cells. Interestingly, continuous rotation even at extremely slow angular velocities did not allow endothelial cells to attach to the denuded surface in reasonable numbers. EC seem to require a minimum of one to three minutes of entirely static conditions to attach successfully. On the other hand, too long a static phase during intermittent rotation caused longitudinal "strips" of endothelium to form, as the cells apparently move towards the lowest point in the curvature of the scaffold fairly rapidly due to gravity. This was avoided by limiting the static phases to three minutes, and by repeating the seeding step with a second batch of cells.

Our experiments also showed that there were only minor differences between

HUVEC-seeded and HSVEC-seeded scaffolds based on histology, immunohistology, and scanning electron microscopy. Both types of cells were equally able to restore a confluent monolayer of cells. However, regenerated endothelia with either cell type differed greatly in appearance from their native counterparts. Native endothelial cells usually appeared tightly packed in a palisade-like fashion in vessel cross sections. Seeded cells appeared flattened instead. Also, native endothelium consisted of fairly small and slightly irregular cells when viewed en face under a scanning electron microscope. In contrast, seeding resulted in homogenous layers of fairly large cells. At this preliminary stage it is yet unclear whether this morphology changes if the constructs are conditioned with elevated shear forces or luminal pressure.

5. Conclusions

This study explored the utility of endothelium-denuded HUV for vascular tissue engineering. Longer segments of HUV can be effectively endothelium-denuded by passing a stream of carbogen through the lumen. As both contractile function and reductive capacities are unaltered and proteins relevant for endothelial cell attachment are unaffected by this procedure, the procedure appears to be an interesting alternative to completely decellularizing vessels als scaffolds. The biomechanical properties are suitable, although both burst pressure and Young's modulus need to be improved by conditioning the vessels in order to obtain vessel grafts suitable for arterial conditions. Denuded HUV can be reendothelialized in a perfusion bioreactor. The resulting neoendothelium is Page 31 of 50

confluent and flow-resistant at venous flow rates.

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Figure Legends

Figure 1: Measurement of burst pressure. The stepper motor (1) drives the plunger of the syringe (2) at a constant rate. The luminal pressure is recorded via a pressure gauge (3). Two USB cameras (4, only one is shown for the sake of clarity) record the dimensions of the sample which is mounted in the vessel chamber (5). After filling the vessel with medium at the beginning of the experiment, the stopcock (6) is closed to allow buildup of pressure.

Figure 2: Seeding procedure. Cultured endothelial cells (1) are labelled (2), harvested, and transferred into a sterile syringe (3). Perfusion is stopped, whereas superfusion continues to run. The upstream perfusion stopcock (4) is closed, and the syringe is attached to the upstream port. After infusing the cell suspension into the sample, the downstream stopcock (5) is closed as well. Rotation (6) is then started to facilitate even distribution of the cells. The arrow (7) indicates the direction of medium flow during perfusion.

Figure 3: H&E stained thin sections of native and denuded HUV. (A) native HUV. (B) HUV denuded by luminal dehydration. (C) HUV denuded by collagenase treatment. (D-F) HUV denuded by osmotic lysis after 1, 3, and 5 min, respectively. Bar indicates 100 μm.

Figure 4: Representative uniaxial tensile testing experiments (Panel A) and burst pressure experiments (Panel B). Both samples were native HUV and are representative for 5-8 subjects.

Figure 5: Serotonin (5-HT) dose-response curves of native and denuded HUV. Filled circles: native HUV; open circles: collagenase-denuded HUV; filled triangles: gas-denuded HUV; open triangles: water-denuded HUV. * significantly different from native controls (RM ANOVA, p=0.006, n=7).

Figure 6: Histological analysis of native and denuded HUV. aSMA, α-smooth muscle actin stained with a specific antibody; Fibronectin, specific antibody; H&E, hematoxylin & eosin; Laminin, specific antibody; Resorcin, histochemical stain for elastic fibers; Sirius Red, histochemical stain for collagen. The images are representative for 9 independent experiments. Bar indicates 100 μm.

Figure 7: Fluorescence microscopy images of cross sections of denuded HUV seeded with endothelial cells. (A) HUVEC. (B) HSVEC. Images are representative for five independent experiments each. Bar indicates 100 µm.

Figure 8: Scanning electron microscopy images of the luminal surfaces of (A) native HUV. (B) HUV denuded by dehydration. (C) denuded HUV seeded with allogeneic HUVEC, and (D) denuded HUV seeded with allogeneic HSVEC. Images are representative for three to five independent experiments.

Figure 9: CD31 and von Willebrand factor immunohistology. Gas-denuded HUV were devoid of any CD31 staining (A) whereas there was a confluent monolayer of CD31 positive cells (arrows) after seeding with HSVEC (B). Gas-denuded HUV showed a weak staining of von Willebrand factor in the subendothelial layer (arrow, C). After seeding with HSVEC, both the cells and the subendothelial layer stained positively for von Willebrand factor (arrows, D). Images are representative for 8 independent experiments. Bar indicates 100 μ m.

Vascular grafts	from	umbilical	veins
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treatment	failure force	ultimate failure	extrapolated burst
	(N)	stress (kPa)	pressure (kPa (mm Hg))
native	2.53±0.54	8029±1714	268.8 (2016)
collagenase	1.58±0.36 *	5014±1142 *	167.9 (1259) *
gas	2.35±0.28	7458±889	249.7 (1873)
water	2.61±0.52	8283±1650	277.3 (2080)

Table 1: Tensile testing data of native and denuded HUV. * significantly different from native HUV (RM ANOVA, p=0.007, n=5).

treatment	contractile force 150 mM KCI (mN)	maximum contractile force 5-HT (mN)	log(EC₅₀) 5-HT (M)	reductive capacity (OD490)
native	45.05±26.27	62.60±29.36	-8.44±0.63	0.76±0.33
collagenase	16.89±12.90*	30.00±21.09 ^{\$}	-7.84±1.00 [†]	0.64±0.18
gas	37.55±18.75	58.39±27.17	-8.55±0.60	0.66±0.16
water	18.61±20.61*	32.87±30.31 ^{\$}	-8.03±0.58	0.66±0.14

Table 2: Organ bath and tetrazolium dye reduction data of native and denuded

HUV. * significantly different from native HUV (RM ANOVA, p=0.005, n=7).

^{\$} significantly different from native HUV (RM ANOVA, p=0.001, n=7).

[†] significantly different from native HUV (RM ANOVA, p=0.006, n=7).



Figure 1: Measurement of burst pressure. The stepper motor (1) drives the plunger of the syringe (2) at a constant rate. The luminal pressure is recorded via a pressure gauge (3). Two USB cameras (4, only one is shown for the sake of clarity) record the dimensions of the sample which is mounted in the vessel chamber (5). After filling the vessel with medium at the beginning of the experiment, the stopcock (6) is closed to allow buildup of pressure.

297x210mm (300 x 300 DPI)

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Figure 2: Seeding procedure. Cultured endothelial cells (1) are labelled (2), harvested, and transferred into a sterile syringe (3). Perfusion is stopped, whereas superfusion continues to run. The upstream perfusion stopcock (4) is closed, and the syringe is attached to the upstream port. After infusing the cell suspension into the sample, the downstream stopcock (5) is closed as well. Rotation (6) is then started to facilitate even distribution of the cells. The arrow (7) indicates the direction of medium flow during perfusion.

150x97mm (300 x 300 DPI)

С

E



Figure 3: H&E stained thin sections of native and denuded HUV. (A) native HUV. (B) HUV denuded by luminal dehydration. (C) HUV denuded by collagenase treatment. (D-F) HUV denuded by osmotic lysis after 1, 3, and 5 min, respectively. Bar indicates 100 μ m. 1058x702mm (72 x 72 DPI)

2,5

2,0

1,5

1,0

0,5

0,0

50

40

30

20

10

0

0

pressure (kPa)

0

В

2

4

1

6

8

path (mm)

10

12

3

4

14

force (N)

А



59 60



2

volume (ml)

Figure 4: Representative uniaxial tensile testing experiments (Panel A) and burst pressure

experiments (Panel B). Both samples were native HUV and are representative for 5-8 subjects.

601x932mm (150 x 150 DPI)









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