

1 **SUSTAINABLE POWER PRODUCTION IN A MEMBRANE-LESS AND**  
2 **MEDIATOR-LESS WASTEWATER MICROBIAL FUEL CELL**

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## 1 **Abstract**

2 Microbial fuel cells (MFCs) fed with wastewater are currently considered a  
3 feasible strategy for production of renewable electricity at low cost.

4 A membrane-less MFC with biological cathode was built from a compact  
5 wastewater treatment reactor. When operated with an external resistance of 250 Ohm,  
6 the MFC produced a long-term power of approximately 70 mW/m<sup>2</sup> for ten months.  
7 Denaturing Gradient Gel Electrophoresis (DGGE) analysis of the cathode biomass  
8 when the MFC was closed on a 2100 Ohm external resistance showed that the  
9 sequenced bands were affiliated with *Firmicutes*, *α-Proteobacteria*, *β-Proteobacteria*,  
10 *γ-Proteobacteria*, and *Bacteroidetes* groups.

11 When the external resistance was varied between 250 and 2100 Ohm,  
12 sustainable resistance decreased from 900 to 750 Ohm, while sustainable power output  
13 decreased from 32 to 28 mW/m<sup>2</sup>. It is likely that these effects were caused by changes  
14 in the microbial ecology of anodic and cathodic biomass attached to the electrodes.  
15 Results suggest that cathodic biomass enrichment in “electroactive” bacteria may  
16 improve MFCs power output in a similar fashion to what has been already observed for  
17 anodic biomass.

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19 **Keywords:** microbial fuel cell, sustainable power, biocathode, PCR-DGGE.

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## 21 **1. Introduction**

22 In a Microbial Fuel Cell (MFC), microorganisms convert chemical energy to  
23 electrical energy, via microbial-catalyzed redox reactions. A typical MFC consists of  
24 anode and cathode compartments separated by a cationic membrane. Microbes in the

1 anode compartment oxidize a soluble electron donor (e.g., glucose, acetate) generating  
2 electrons and protons. Electrons are then transferred to the anode surface and from there  
3 to the cathodic compartment through the electrical circuit, while the protons migrate  
4 through the electrolyte and then through the cationic membrane. Electrons and protons  
5 are consumed in the cathode compartment reducing a soluble electron acceptor, such as  
6 oxygen or ferricyanide. Electrical power is harnessed by inserting a load between the  
7 two electrode compartments (Allen and Bennetto, 1993).

8         In early studies, exogenous electrochemicals mediators have been added into the  
9 MFCs to allow electron transfer from the microbial cells to the electrode, due to the  
10 non-conductive nature of the cell surface structures (Roller et al., 1984; Park and  
11 Zeikus, 2003; Logan and Regan, 2006). However, recent evidence (Kim et al., 2004;  
12 Jang et al., 2004; Gil et al., 2003) showed that complex microbial communities in  
13 wastewater-fed MFCs produce soluble redox mediators (e.g., pyocyanin; Rabaey et al.,  
14 2004). Furthermore, *Geobacter sulfurreducens* is known to transfer electrons beyond  
15 cell surfaces to electrodes through membrane proteins (Bond and Lovley, 2003;  
16 Chaudhury and Lovley, 2003) or nanowires (Reguera et al., 2005), *Shewanella*  
17 *oneidensis* MR1 was shown to produce both soluble redox mediators (Marsili et al.,  
18 2008) and nanowires (Gorby et al., 2006).

19         It has been shown that wastewaters of different origin can be fed to MFCs, thus  
20 allowing energy production from an abundant and inexpensive source. Most of the  
21 energy available from the oxidation of the organic load was converted to electricity  
22 (50÷90 % in term of Coulombic efficiency) while the remaining energy was used for  
23 microbial growth (Liu et al., 2007; Rabaey et al., 2005a). Integration of MFCs in  
24 wastewater treatment plants allowed energy recovery and reduction of excess sludge

1 production with little effect on the mineralization of organic load and the rest of the  
2 process (Rabaey and Verstraete, 2005). Wastewater MFCs are currently being assessed  
3 as a renewable energy strategy (Logan and Regan, 2006).

4 However, in order to make the process economically feasible, it is necessary to:  
5 a) eliminate the cationic membrane to reduce operating costs due to membrane  
6 maintenance; b) implement MFCs in existing wastewater treatment plants, to reduce  
7 capital investment; c) avoid an expensive cathodic catalyst in favour of aerobic biomass  
8 (He and Angenent, 2006).

9 Recently, membrane-less wastewater MFCs have been designed and tested (Jang  
10 et al., 2004; Moon et al., 2006; Ghangrekar and Shinde, 2007). While many studies  
11 have dealt with anodic compartment (Min and Logan, 2004; You et al., 2006; Liu et al.,  
12 2004), a few studies have been performed both to develop a biocathode capable of  
13 directly reducing oxygen and to characterize the microbial community responsible for  
14 the cathode catalysis (Bergel et al., 2005; Chen et al., 2008; Clauwaert et al., 2007;  
15 Kang et al., 2003, Rabaey et al., 2008).

16 In this study, a membrane-less, mediator-less MFC was implemented on a  
17 compact lab-scale wastewater treatment plant (WWTP), with a simple and economic  
18 design, to couple wastewater treatment (removal of organic compounds and ammonia  
19 oxidation) with sustainable electrical power production to avoid the use of expensive  
20 catalysts for the cathode. The effect of the external load on sustainable power  
21 production was investigated. Furthermore, the microbial composition of cathodic  
22 biomass was characterized in order to determine whether the long-term operation of the  
23 MFC cause an enrichment in electroactive bacteria at the cathode. The results indicate

1 that the electroactivity of cathodic biomass affect the power production in completely  
2 biological MFCs.

## 3 **2. Material and Methods**

### 4 *2.1 Process and reactor design*

5 The two-stage process shown in Fig. 1 was adopted for organic substrate  
6 removal and ammonia nitrification of high strength wastewaters (Malina and Pohland,  
7 1992; Tchobanoglous et al., 2003). Sedimentation and fermentation of easily degradable  
8 organic substrate took place in the first anaerobic stage of the process, and the following  
9 aerobic stage nitrified ammonia and further oxidized organic compounds.

10 The bench-scale WWTP was built in PVC, composed of two anaerobic  
11 compartments arranged in series (ABR, Anaerobic Baffled Reactor), and an aerobic  
12 chamber and a sludge settler (implementing an activated sludge process), as shown in  
13 Fig. 1. The volumes of the four compartments were 18 L, 18 L, 22 L, and 5 L,  
14 respectively. The anaerobic compartments #1 and #2 were connected through an  
15 overfall. A recycle pump (Watson Marlow 503 S, Wilmington MA, USA) was placed  
16 between the two anaerobic compartments to evenly distribute the liquid below the  
17 sludge blanket. Constant temperature in the ABR (35°C) was maintained with a heating  
18 element (Rena, France) located in compartment #1 and controlled by a temperature  
19 probe (Tersid, Milano, Italy) in compartment #2. The return activated sludge was  
20 recycled from the settler #4 to the oxidation chamber #3 (Recycle ratio  $R_r=2$ ). The  
21 aerobic compartment #3 was aerated and stirred with an aquarium air pump (Schego,  
22 Germany), with an air flow rate of approximately 6 L/min.

### 23 *2.2 Inoculation and medium*

1 Anaerobic compartments #1 and #2 were inoculated with 15.2 L of granular  
2 sludge from a full-scale Up-flow Anaerobic Sludge Blanket (UASB) reactor treating  
3 paper factory wastewater (Castelfranco Emilia, Italy). The aerobic compartment #3 was  
4 inoculated with 6 L of activated sludge from a full-scale domestic wastewater treatment  
5 plant (Trebbo di Reno, Italy).

6 The plant was fed with synthetic wastewater with the following composition (per  
7 liter of tap water): 168 mg  $(\text{NH}_4)_2\text{SO}_4$ , 60 mg  $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$ , 6 mg  $\text{MnSO}_4 \cdot \text{H}_2\text{O}$ ,  
8 126 mg  $\text{NaHCO}_3$ , 0.3 mg  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ , and 6 mg  $\text{CaCl}_2 \cdot 2\text{H}_2\text{O}$ . Anhydrous glucose was  
9 used as the organic substrate, at different concentrations as shown in Table 1. The  
10 synthetic wastewater was buffered at pH 7.3 with 0.7 M  $\text{K}_2\text{HPO}_4$  and 0.3 M  $\text{KH}_2\text{PO}_4$ .  
11 All chemicals were of reagent grade. Synthetic wastewater was stored and fed to the  
12 reactor at 4°C and replaced every 3-4 days.

### 13 *2.3 Chemical analyses*

14 A pH electrode (Mettler Toledo, OH, USA) was placed in the anaerobic  
15 compartment #2. Biogas production rate from the two anaerobic compartments was  
16 monitored through a custom prepared wet tip gas flow meter. Methane content in biogas  
17 was analyzed with an Ultramat 23 infrared spectrophotometer (Siemens, NY, USA).  
18 Oxidation-reduction potential (ORP) was measured in both anaerobic (#2) and aerobic  
19 compartments (#3) with metallic electrodes (Crison model 52-61, Alella, Spain).  
20 Dissolved oxygen (DO) concentration in compartment #3 was measured with a Cell OX  
21 325 oxymetric sensor (WTW OXI 340, Weilheim, Germany). Chemical Oxygen  
22 Demand (COD) and ammonia nitrogen were determined in samples collected from  
23 compartment #2 and #4, according to the Standard Methods (APHA, 1999).

### 24 *2.4 Microbial fuel cell*

1 Untreated glassy carbon anode and cathode, with geometrical surface of 160 cm<sup>2</sup>  
2 each, were cleaned overnight in 1 M HCl and rinsed with deionized water prior to use,  
3 then placed in compartment #2 and #3, respectively (Fig. 1). Electrodes were connected  
4 via an external electric circuit on a load variable between 150 and 2000 Ohm. A  
5 saturated calomel electrode (SCE, Hanna Instruments, RI, USA), was placed in  
6 compartment #3 and used as reference to measure anodic and cathodic electrochemical  
7 potentials.

8 Cell and half cell potentials were measured every hour with a milli-voltmeter  
9 (Datataker, UK). Current was calculated from the potential through a shunt resistance of  
10 100 Ohm. Temperature, pH, redox potentials, biogas production and electric measures  
11 were stored in a Datataker 605 (Datataker, UK). The total applied resistance is referred  
12 as the sum of external variable load and shunt resistance (100 Ohm), since the shunt  
13 was in series with the load on the external circuit.

14 Sustainable power measure was performed daily with an in-house built  
15 programmable variable resistance, as described by Menicucci et al., (2006). In a typical  
16 experiment, total applied resistance varied between 1800 and 110 Ohm, with a rate of  
17 400 Ohm/min. This procedure returned the maximum sustainable power (MSP), which  
18 is the highest electrical power produced at steady state conditions. In addition to  
19 maximum sustainable power, the minimum sustainable external resistance and the  
20 maximum sustainable cell potential were determined.

### 21 *2.5 MFC Operating conditions*

22 Following inoculation, the reactor was continuously fed for 14 months. Changes  
23 in operating conditions during this time period are shown in Table 1. The synthetic  
24 wastewater was fed to the anaerobic compartment #1 of the MFC, with an organic load

1 (OL) variable between 0 and 16 g<sub>COD</sub>/day, maintaining an anaerobic hydraulic residence  
2 time of 12 days. The anode was never changed during the experiment, while a clean  
3 cathode was inserted on day 238.

#### 4 2.6 Microbiological analyses

##### 5 2.6.1 Sample collection and DNA extraction

6 During step #8 suspended activated sludge (about 50 ml) was collected from the  
7 aerobic chamber and sludge attached on the cathode was removed using a sterile razor  
8 blade and re-suspended in a sterile phosphate buffer saline solution. Samples were  
9 stored at - 80°C until use.

10 Sludge samples (5 ml) were dispersed overnight with a cation-exchange resin  
11 (Chelex 100, Biorad, CA, USA) as described by Frølund et al. (1996). Lysis of the cells  
12 was performed by the lysozyme + SDS technique described by Bourrain et al., (1999).  
13 Total DNA from microbial cells was obtained by phenol/chloroform extraction and  
14 isopropanol precipitation methods as previously described (Zhou et al., 1996).  
15 Purification of crude DNA extracts was performed by the Wizard DNA clean-up system  
16 (Promega, WI, USA). DNA concentration was determined spectrophotometrically with  
17 NanoDrop instrument ND-1000 (NanoDrop Technologies Inc., Wilmington, DE, USA).

##### 18 2.6.2 DGGE analysis of the V3 region of the 16S rRNA gene

19 Two µl (10 to 30ng of DNA) of each sample were subjected to PCR  
20 amplification of the 16S rRNA gene using Bacteria-specific primers 27F (5'-  
21 GAGAGTTTGATCCTGGCTCAG-3') and 1495R (5'-CTACGGCTACCTTGTTACG  
22 A-3') as described by Di Cello et al., (1997) to produce a 1.450-bp fragment, which was  
23 then used as a template for nested PCR with two different sets of primers. The first set,  
24 composed of primers 357F-GC-clamp (5'-



1 CGCCCGCCGCGCCCCGCGCCCGGCCCGCCGCCCCCGCCCCCTACGGGAGG  
2 CAGCAG-3') and 518R (5'-ATTACCGCGGCTGCTGG-3'), amplified a fragment of  
3 161 bp (small fragment). The second set, consisted of primer 63F-GC-clamp (5'-  
4 CGCCCGCCGCGCGCGGGCGGGGCGGGGGCACGGGGGGCAGGCCTAAC  
5 ACATGCAAGTC-3') and the reverse primer 518R described above, was used to  
6 produce a 495 bp fragment (large fragment). Nested PCRs to obtain the small and the  
7 large fragments were carried out according to the procedures described by Van der  
8 Gucht et al., (2005) and by El Fantroussi et al., (1999), respectively, with Taq DNA  
9 polymerase (Quiagen, Milano, Italy). Fragments were resolved by double gradient  
10 denaturing gradient gel electrophoresis (DG-DGGE) as described by Cremonesi et al.,  
11 (1997), in a DCode universal mutation detection system (Bio-Rad, CA, USA). A 6 %-  
12 12 % polyacrylamide (acrylamide: N,N-methylenebisacrylamide, 37.5:1) gel with  
13 denaturing gradient ranging from 30 % to 60 % was used to resolve small fragments,  
14 whereas a 6 %-12 % polyacrylamide (acrylamide: N,N-methylenebisacrylamide, 37.5:1)  
15 gel with denaturing gradient ranging from 40 % to 70 % was used to resolve large  
16 fragments. A 100 % denaturing solution contained 7 M urea and 40 % deionized  
17 formamide. Approximately 700 ng of purified PCR products were loaded in each well.  
18 The gels were run for 16 h at 75 mV in 1X TAE buffer at 60°C, stained with 50 µg/ml  
19 ethidium bromide for 30 min, destained in water and photographed with the UVIpro  
20 Platinum Gel Documentation System (GAS7500/7510).

### 21 2.6.3 Sequencing of DGGE fragments and phylogenetic analysis

22 DGGE-separated fragments were excised with a razor blade and allowed to passively  
23 diffuse into the water at 4°C overnight. The eluted DNA was reamplified with the same  
24 primers and PCR conditions described for DGGE analysis. The PCR products were

1 tested by DGGE for purity and identity with the original bands in the community  
2 profiles and then sequenced. Sequencing reactions were prepared using Applied  
3 Biosystem Big Dye® Terminator sequencing kit version 3.1, according to the  
4 manufacturer's instructions and analyzed using a 3730 DNA Analyzer Applied  
5 Biosystem apparatus. Each sequence was submitted to the CHECK\_CHIMERA  
6 program of the Ribosomal Database Project (RDP)  
7 (<http://rdp.cme.msu.edu/cgis/chimera.cgi?su=SSU>) to detect the presence of possible  
8 chimeric artifacts. Sequence similarity searches were performed using the BLAST  
9 network service of the NCBI database and Seqmatch tool of the RDP  
10 (<http://www.ncbi.nlm.nih.gov/BLAST/> and <http://rdp.cme.msu.edu/>, respectively). For  
11 phylogenetic analysis, identification of 16S rRNA gene sequences was performed with  
12 RDP Classification Algorithm (<http://rdp.cme.msu.edu/classifier/classifier.jsp>).

13 Partial 16S rRNA gene sequences obtained in this study have been deposited in  
14 the NCBI nucleotide database under accession numbers EU492873-76 (small fragment  
15 bands A-D) and EU597325-31 (large fragment bands F-N).

### 16 **3. Results**

#### 17 *3.1 COD and ammonia removal*

18 The influent and effluent organic load during phase I to III (see Table 1) are  
19 shown in Fig. 2, while Table 2 shows the COD removal in anaerobic and aerobic stages  
20 of the process, as well as methane production in anaerobic stage. During phase I, the  
21 influent glucose concentration was increased from 1.5 to 5 g/L (steps #1 to #4),  
22 corresponding to a measured feeding OL of 3.4 to 16.0 g<sub>COD</sub>/day. The average COD  
23 removal in the anaerobic compartment varied between 66 and 91 % (Table 2). The

1 lowest value of COD removal was observed during the initial adaptation of anaerobic  
2 biomass.

3 During phase II (step #5, see Table 2), glucose was removed from the influent  
4 and the reactor was operated in absence of carbon and energy source. During this phase,  
5 the COD values in the outlet were lower than 70 mg<sub>COD</sub>/L.

6 During phase III (step #6 and #7), glucose was added again to the influent, at a  
7 concentration of 3 g/L, corresponding to a measured OL of approximately 9.1 g<sub>COD</sub>/day.  
8 COD removal in anaerobic compartment rapidly stabilized at 94 % (Table 2). The  
9 anaerobic COD removal measured in step #3, step #6 and #7 increased, although the  
10 feeding OL was the same. This was due to the anaerobic biomass growth, consequent to  
11 the absence of sludge withdrawal during the experimental period.

12 Daily methane production (Table 2) increased with OL and the organic substrate  
13 removed in the ABR chamber (#1 and #2) was almost completely converted into  
14 methane. The average pH value in the second ABR chamber was 6.9.

15 Dissolved oxygen in the aerobic compartment was 6.5±0.3 mgO<sub>2</sub>/L through all  
16 the experiment, while ammonia nitrogen in the effluent was always below than  
17 1 mg NH<sub>4</sub>-N/L, corresponding to 98 % nitrogen removal.

### 18 *3.2 Electrical power production*

19 Immediately after inoculation, the cell was closed on a total applied resistance of  
20 250 Ohm for a period of 270 days. The cell potential grew from 50±3 mV at the end of  
21 the starting phase (step #1), to 411±10 mV at the end of step #3 (Table 3),  
22 corresponding to an OL of 9.6 g<sub>COD</sub>/day (and a substrate concentration in the second  
23 anaerobic chamber of 420 g<sub>COD</sub>/m<sup>3</sup>, Table 2). Further OL increase from 9.6 to  
24 16 g<sub>COD</sub>/day (815 g<sub>COD</sub>/m<sup>3</sup> in the second anaerobic chamber, Table 2 step #4) did not

1 change the cell potential. Current and power output showed a similar pattern, reaching a  
2 plateau of  $163 \pm 5 \text{ mA/m}^2$  and  $65.1 \pm 3.5 \text{ mW/m}^2$  of geometric electrode surface at  
3 substrate concentration higher than  $420 \text{ g}_{\text{COD}}/\text{m}^3$ , indicating that organic substrate  
4 concentration was not limiting power output.

5 When glucose was removed from medium for two weeks (step #5), power  
6 production dropped rapidly reaching  $1.2 \pm 0.3 \text{ mW/m}^2$ , indicating that electricity was  
7 produced mainly by the catalytic oxidation of organic substrate. During step #6, the  
8 reactor was operated with an OL of  $9.5 \text{ g}_{\text{COD}}/\text{day}$  and the electrical power production  
9 reached in 14 days a plateau value of  $72.7 \pm 1.6 \text{ mW/m}^2$ . Specific current, cell potential  
10 specific power, anodic and cathodic potential throughout the experiment are shown in  
11 Fig. 3 a, Fig. 3 b, Fig. 3 c and Table 3.

### 12 *3.3 Anodic and cathodic potential*

13 At OL higher than  $6.4 \text{ g}_{\text{COD}}/\text{day}$  (step #2), anode and cathode potential reached a  
14 plateau of  $-176 \pm 5$  and  $+234 \pm 5 \text{ mV vs. SCE}$ , respectively (Fig. 3 c and Table 3). In the  
15 absence of organic substrate (step #5), anodic potential increased to  $+237 \pm 28 \text{ mV vs.}$   
16  $\text{SCE}$ , while cathode potential was less affected, indicating that the cathode was not the  
17 current-limiting electrode in the cell (i.e. the one of the two electrodes that exhibits the  
18 slower charge-transfer kinetics). Both specific power output and anode potential were  
19 restored at nearly 100 % of their maximum values upon reintroduction of substrate in  
20 the medium (step #6, Fig. 3 b and Fig. 3 c), suggesting that the anodic attached biomass  
21 maintained its substrate oxidation capability.

### 22 *3.4 Role of cathodic biomass*

23 Cathodic potential dropped rapidly to  $-214 \pm 1.4 \text{ mV vs. SCE}$  when a clean  
24 glassy carbon cathode was inserted in the aerobic compartment (step #7). However,

1 residual electrical power was  $10.5 \pm 0.1 \text{ mW/m}^2$ , suggesting that suspended biomass and  
2 soluble redox mediators had a role in the cathodic process (Fig. 3 c and Fig. 3 b).  
3 Although thermodynamically feasible, direct oxygen reduction at the glassy carbon  
4 electrode is not possible at the measured potential, as it was also shown during the  
5 acclimation of cathodic biomass (step #1) The clean cathode was quickly colonized by  
6 aerobic biomass, and after 5 days cell potential and power production resumed to  $100$   
7  $\pm 10\%$  and  $100 \pm 3.3\%$  of their values measured at the end of step #4, respectively  
8 (Table 3 and Fig. 3 b).  
9 To investigate the composition of the microbial community suspended in the aerobic  
10 chamber and attached on the cathode, a partial domains profile of eubacterial 16S rRNA  
11 gene was performed by DGGE. This was done after PCR amplification of the 16S  
12 rDNA genes from total DNA of the two samples with the two sets of primers described  
13 in Materials and Methods. Fig. 4 a and Fig. 4 b shows the DGGE patterns of the small  
14 and large 16S rDNA fragments. There are fewer bands in the DGGE profiles of the  
15 small fragment than in the DGGE patterns of the large fragment. However, suspended  
16 aerobic biomass and the cathode attached biomass showed high fingerprint similarity as  
17 most of the bands obtained were present in both samples (Fig. 4 a and Fig. 4 b).  
18 Separated DGGE bands were excised from the gels, purified to determine the sequence,  
19 and assigned to a specific group on the basis of a combination of Blast searches and  
20 phylogenetic analysis. Table 4 shows the percentage of similarity between sequences of  
21 excised bands and the closest relatives (NCBI Database). The nucleotide sequences of  
22 the small fragment bands were referred to uncultured bacteria or DGGE clones of the  
23 *Firmicutes*,  *$\beta$ -Proteobacteria*, and *Bacteroidetes* groups (Table 5), whereas most of the  
24 sequences of the large fragment bands were affiliated with  *$\alpha$ -Proteobacteria* and  *$\gamma$ -*

1 *Proteobacteria* groups. A band (E) was identified as a putative chimeric artefact based  
2 on result from CHECK\_CHIMERA analyses. Moreover, two large fragment bands (G  
3 and H) were distantly affiliated with unclassified bacterial sequences retrieved from a  
4 river sediment sample (EF667579), from a commercial nitrifying inoculum  
5 (AJ786605.1) and from a biocathode chamber in a microbial fuel cell (EU 426928.1),  
6 (Table 4).

### 7 *3.5 Sustainable resistance measure*

8 Sustainable resistance was measured at four different values of total applied  
9 resistance, 250, 430, 1100, and 2100 Ohm, for at least 30 days. When the total applied  
10 resistance was changed, the average value of sustainable resistance changed as shown in  
11 Fig. 5 a. Specifically, at low total applied resistance (250 Ohm), the sustainable  
12 resistance decrease rapidly with time, while at high total applied resistance (2100 Ohm),  
13 the sustainable resistance value did not change appreciably with time (data not shown).  
14 Sustainable power slightly increased when total resistance decreased (Fig. 5 a).

### 15 *3.6 Factor limiting power production*

#### 16 *3.6.1 Current-limiting electrode*

17 The sustainable resistance was determined through an external resistance scan.  
18 Anode and cathode potentials were measured at each external resistance value. The  
19 electrode whose potential changes more during the scan is the current-limiting electrode  
20 (Menicucci et al., 2006; Fuel cells handbook, 2004). Fig. 5 b and Fig. 5 c show a typical  
21 external resistance scan between 110 and 1800 Ohm. The cathodic potential was nearly  
22 constant at each external resistance value, showing that the current production was  
23 limited by the anode.

#### 24 *3.6.2 Limiting step in electron transfer*

1 Current did not show a maximum during the resistance scan, while power  
2 reached a maximum at low value of external resistance (Fig. 5 c). A recent model  
3 proved that these trends are typical of a MFC in which diffusion processes limits power  
4 output (Shimotori et al., 2007). Because of these limitations, the sustainable power is  
5 less than half the maximum power (Fig. 5 a). Diffusion limitations to electron transfer  
6 are predominant in the range of total applied resistance explored in this study, which is  
7 between 250 and 2100 Ohms.

#### 8 **4. Discussion**

##### 9 *4.1 Power production*

10 The cell was initially operated with a total applied resistance of 250 Ohm. After  
11 58 days of biomass growth and with non-limiting OL, cathode and anode potential  
12 reached a stable plateau of  $234 \pm 5$  mV and  $-176 \pm 5$  mV vs. SCE, respectively (Fig. 3 c).

13 Both anodic and cathodic biomass established slowly and a plateau in current  
14 and power production was reached only after 70 days (i.e. after about 3.3 times the total  
15 Hydraulic Retention Time, HRT). Anodic attached biomass maintained its catalytic  
16 activity over two weeks of feeding without glucose (step #5). When a new cathode was  
17 inserted in the cell (step #7) suspended biomass adhered to the electrode in 5 days fully  
18 restoring the catalytic reducing activity and the half cell potentials.

19 The potential of the biocathode, about 230 mV vs. SCE (474 mV vs. SHE), was  
20 closed to that ( $\sim 463$  mV vs. SHE) observed for oxygen abiotic reduction at  
21 conventional Pt-coated electrodes in cathode chamber (Oh et al., 2004). Therefore,  
22 biocathode proved to be an efficient catalyst for oxygen reduction, and a feasible  
23 alternative to abiotic systems in wastewater-fed MFCs.

1           Concerns arose in the past over non-catalytic power production in wastewater  
2 fed MFC. Several media used for bacterial growth contained significant amount of  
3 redox mediators, such as cysteine, and high strength wastewater contained reduced  
4 sulfur species, which can work as abiotic electron donor and increase power production  
5 in short term experiments. In this study, minimal salt media was used, therefore electron  
6 donors other than glucose or redox mediators could be only by products of glucose  
7 anaerobic degradation or microbially produced electron shuttles (Rabaey et al., 2004,  
8 pyocyanine). In fact, when glucose was removed from the artificial wastewater fed to  
9 the MFC (step#5), the power dropped, indicating a discharge to the anode of the  
10 electrons stored in the attached biomass (e.g., in the protein membranes) and the  
11 reoxidation of most of the reduced species in solution.

12           The MFC was initially run under demanding conditions for current production  
13 (low external resistance). During this phase, glucose concentration in the wastewater  
14 and OL were increased until non-limiting conditions were achieved. Since further  
15 experiments were run using higher external resistance, it is assumed that non-limiting  
16 conditions with respect to glucose concentration were maintained. With a non limiting  
17 organic substrate concentration of  $434 \pm 77 \text{ g}_{\text{COD}}/\text{m}^3$  in the second ABR chamber, the  
18 specific current increased in an exponential fashion and then stabilized at  
19  $159 \pm 1 \text{ mA}/\text{m}^2$ , while power reached a plateau at  $60.6 \pm 1 \text{ mW}/\text{m}^2$  (Fig. 3 a and Fig.  
20 3 b).

21           Organic substrate removed in the ABR was converted almost completely into  
22 methane, as shown in Table 2. This results was expected due to the low ratio of  
23 electrode surface to the volume of anodic compartment  
24 ( $S_{\text{electrode}}/V_{\text{anode compartment}} = 0.4 \text{ m}^2/\text{m}^3$ ). In other studies, different electrode material



1 configurations were adopted in order to maximize power output such as, granular  
2 graphite (Rabaey et al., 2005b), or high specific surface electrodes (Logan et al., 2006;  
3 Gil et al., 2003; Chaudhury and Lovley, 2003). In such systems (Rabaey et al., 2005c),  
4 an average COD to current efficiency of  $59 \pm 4$  % was obtained and no methane  
5 production was observed.

#### 6 *4.2 Electron transfer mechanism*

7         When attached cathodic biomass was removed (step #7), power production  
8 dropped to 13 % of the maximum power formerly measured. As discussed above, this  
9 observation suggested that microbially produced redox mediators facilitated electron  
10 transfer from the suspended and attached biomass to the anode. Microbially produced  
11 redox mediators were identified in at least two cases (Rabaey et al., 2004; Marsili et al.,  
12 2008). It is not clear from our results whether the increase in cathodic potential and  
13 power production following electrode colonization is due to the concentration of such  
14 microbial redox mediators in the attached biomass, or if direct electron transfer modes  
15 are possible, as shown for dissimilatory metal-reducing bacteria (Reguera et al., 2005;  
16 Gorby et al., 2006). However, the residual power measured seems to indicate the co-  
17 presence of mediated and direct electron transfer mechanisms.

#### 18 *4.3 Factors limiting power production*

19         The current-limiting electrode was determined through the sustainable power  
20 measures. In a typical external resistance scan, between 1800 and 110 Ohm, cathodic  
21 potential decrease by 20 % while the anodic potential increase by 70 % (Fig. 5 b). Once  
22 the cathodic biomass had developed, the anode was the current-limiting electrode.  
23 Sustainable power determination also provided insight over the processes which limit  
24 long-term power. When an MFC is limited by diffusion, the current measured during a

1 sustainable resistance scan always increases as external resistance decreases, although  
2 with a rate lower than that calculated from Ohm's law, since the cell potential is not  
3 constant (Menicucci et al., 2006). However, in MFCs with membrane electrode  
4 assembly (MEA) (Liang et al., 2007), power production is less affected by diffusion,  
5 and is rather limited by the amount of the immobilized biomass and its catalytic activity  
6 (Marsili et al., 2008; Shimotori et al., 2007). Sustainable power increases as long-term  
7 external resistance decreases, and sustainable resistance decreases as long-term external  
8 resistance decreases. Since decreased external resistance corresponds to higher electron  
9 flow at the attached biomass/electrode interfaces, it is likely that such conditions favor  
10 species with faster electron transfer rate. At higher external resistance, electroactive  
11 bacteria are no longer favored and biomass nor efficient in substrate utilization is likely  
12 selected.

13         DGGE of cathodic biomass using two different set of primers provided an  
14 analytical tool to study the diversity of the microbial community suspended and  
15 attached on the cathode. Use of the primers set P357F-GC clamp and 518R revealed a  
16 high fingerprint similarity between the two samples. However, it is often not easy to  
17 assign short partial sequences accurately, especially if the sequences lack close relatives  
18 in the database (Kuske et al., 1997). Because of this reason and to overcome PCR bias  
19 that often has been reported in DGGE experiments, (Hansen et al., 1998), we used the  
20 second set of primer (p63F-GC clamp-518R). The DGGE profiles obtained by this  
21 different set, that generated a larger 495-bp fragment, again revealed that the genomic  
22 fingerprintings of the two samples are very similar. Moreover, the use of both primer  
23 sets allowed a more accurate discrimination of different taxonomic groups inside the  
24 samples. In related studies that examined the microbial community present at the

1 biocathode, a similar breadth of phylogenetic diversity was detected ( $\alpha$ ,  $\beta$ ,  $\gamma$   
2 *Proteobacteria*, *Bacteroidetes*) (Clauwert et al., 2007; Chen et al., 2008; Rabaey et al.,  
3 2008), whereas members of the *Firmicutes* group were detected for the first time. The  
4 presence of this bacterial taxon in the cathodic compartment could be related to the fact  
5 that the system was fed with glucose.

## 6 **Conclusions**

7 Further studies are needed to better understand the effect of external resistance  
8 on microbial composition. It is possible that increased power production corresponds to  
9 increased organization in electron transfer network in attached biomass. Also shift in  
10 electron transfer strategies (e.g., from mediated to direct electron transfer) may play a  
11 role in the change of sustainable resistance and sustainable power with time.

12 Based on the results from this study, we can conclude that with simple  
13 modifications, a common wastewater treatment plant can produce electrical power,  
14 without changes in COD removal and ammonia nitrification. The power produced was  
15 limited by diffusion phenomena, rather than from catalytic activity of electrode  
16 biomass. Sustainable power measures indicated that at lower external resistance  
17 electroactive bacteria are favored.

18 Biocathode is proved to be an efficient catalyst for oxygen reduction, and a  
19 feasible alternative to expensive Pt-based catalysts in wastewater-fed MFCs. A  
20 taxonomic characterization performed on both suspended and attached cathodic  
21 biomass showed that the sequenced DGGE bands were affiliated with *Firmicutes*,  $\alpha$ -  
22 *Proteobacteria*,  $\beta$ -*Proteobacteria*,  $\gamma$ -*Proteobacteria*, and *Bacteroidetes* groups.

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