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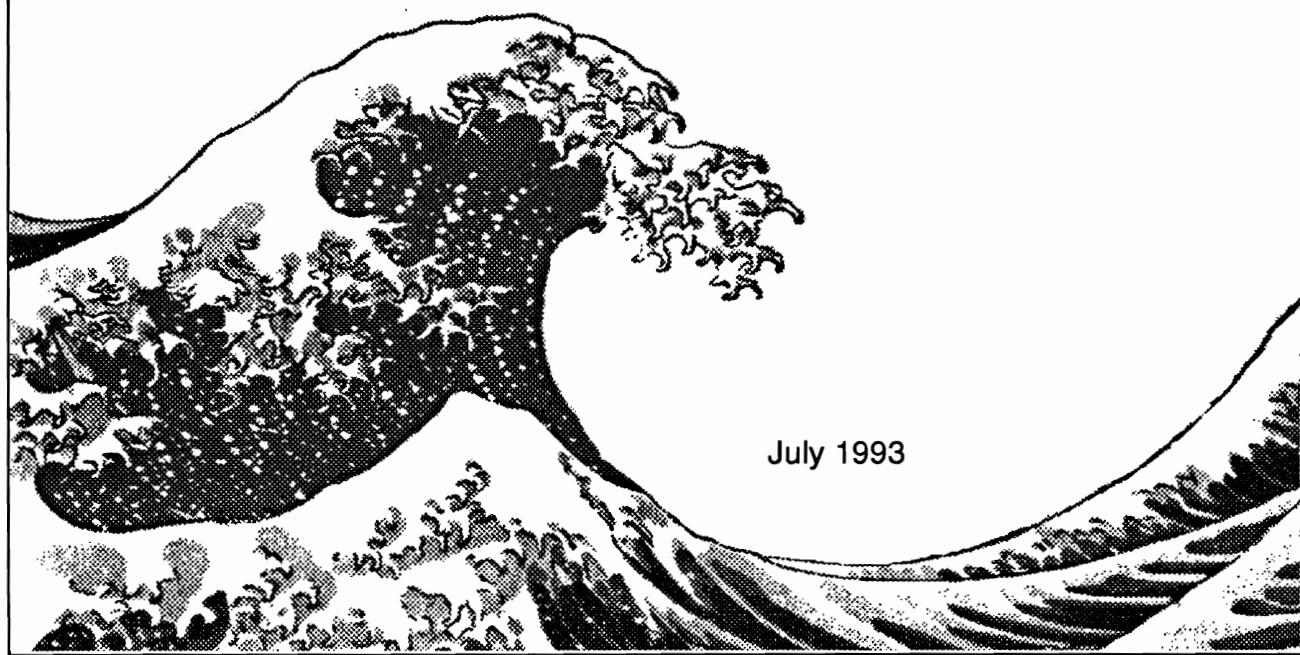
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NOAA/MLML Radiometric Data Acquisition and Processing

Michael E. Feinholz and William W. Broenkow

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Abstract

This report is a detailed description of data processing of NOAA/MLML spectroradiometry data. It introduces the MLML DBASE programs, describes the assembly of diverse data files, and describes general algorithms and how individual routines are used. Definitions of data structures are presented in Appendices.

Introduction

The purpose of this report is to document data processing of radiometric data obtained in support of the NOAA/MLML participation in the SeaWiFS project. This report presents details of program use, but a companion report (Broenkow, *et al.* 1993) presents a graphical, less-detailed summary of methods described here.

In 1978 the MLML oceanography group participated with the NOAA/NESDIS CZCS project by writing programs to acquire and process spectroradiometer data. Our current work provides similar support for the NOAA/NESDIS Marine Optical Characterization Experiment, MOCE, in preparation for the launch of the new ocean color satellite, SeaWiFS. During CZCS experiments, an 80-channel scanning radiometer measured in-water spectral upwelled radiance, $L_u(z, \lambda)$, and spectral downwelled irradiance, $E_d(z, \lambda)$, in the visible spectrum from 400 to 700 nm. A similar instrument onboard ship measured surface spectral irradiance, $E_s(\lambda)$. *In situ* observations of spectral L_u , E_d and E_s were required for calibration and validation of the spectral water-leaving radiance, $L_w(\lambda)$, as retrieved from the CZCS satellite sensor. These radiometric measurements were also used to develop and validate bio-optical algorithms and atmospheric correction algorithms.

The purpose of the data acquisition and reduction programs described here are similar to those of the CZCS program, and many of these programs directly parallel those used in the CZCS work. The purpose of the SeaWiFS project is to achieve remotely-sensed, water-leaving radiances within 5% accuracy, and chlorophyll *a* concentration within 35% over the range 0.05 to 50 mg m⁻³. New instruments were developed by Dennis Clark of NOAA/NESDIS to surface-truth the SeaWiFS sensor. The dual spectrograph (340 to

900 nm) Marine Optical System, MOS, measures in-water $L_u(z, \lambda)$ and $E_d(z, \lambda)$. The instrument can be used either in the Marine Optical Buoy (MOBY) or by deployment from a ship. Data from either mode are processed identically. A 38-channel Surface Irradiance Spectrometer, SIS, measures $E_s(\lambda)$ at the sea surface. An older 80-channel PMT spectroradiometer, Fastie (named after its optical designer), is also used from time to time. As part of the NOAA/NESDIS project MLML, has provided C and FORTRAN software to acquire data from these instruments. Unlike their earlier CZCS counterparts, the new instruments are controlled by a VAXStation 4000.

Measurements of L_u , E_d , and E_s are used to calculate normalized water-leaving radiance, $L_{WN}(\lambda)$. These near nanometer resolution spectra are weighted by the eight SeaWiFS response functions to simulate SeaWiFS-determined radiances. The SeaWiFS $L_{WN}(\lambda)$ will be used for "vicarious" satellite sensor calibrations. In addition, these data observations will be used for development of bio-optical and atmospheric correction algorithms.

Measurements of $L_u(z, \lambda)$ and $E_d(z, \lambda)$, made over the upper few optical depths, are required to compute the diffuse attenuation coefficients $K_E(z, \lambda)$ and $K_L(z, \lambda)$. Optical depth, $\tau(z, \lambda)$, in the context of this report is the reciprocal integral of $K(z, \lambda)$ (for either radiance or irradiance), from the surface to a given depth z . Profiles of $E_d(z, \lambda)$ and $L_u(z, \lambda)$ must be normalized to account for changes during a cast in solar zenith angle, cloud cover and aerosols, hence the need for measuring $E_s(z, \lambda)$. $K_L(\lambda)$ is used to extrapolate profiles of $L_u(z, \lambda)$ to an infinitesimal depth below the surface ($z = 0'$), $L_u(0', \lambda)$, which, when propagated through the sea surface leads to the estimated value of $L_w(\lambda)$. To standardize SeaWiFS in-water algorithms, it is necessary to normalize $L_w(\lambda)$ for sun zenith angle, earth-sun distance, and atmospheric transmittance, yielding $L_{WN}(\lambda)$.

In conjunction with oceanographic and atmospheric measurements, MOS and SIS spectroradiometers are operated shipboard at a bio-optics station. MOS is attached to a floating tetrahedron and lowered to typically three depths. The tetrahedron is floated away from the ship to avoid measuring a light field contaminated by the ship's shadow or reflection. Subsurface measurements are taken near local apparent noon, LAN, and require approximately two hours to complete. Typical sampling depths are 1, 6, and 11 m in eutrophic waters or 1, 11 and 21 m in oligotrophic waters. Simultaneous with underwater measurements, SIS measures $E_s(\lambda)$ to account for changing sky conditions. During the data acquisition session the workstation is used to control both instruments, to display the data in real-time and to save data in the MLML_DBASE format (Broenkow and Reaves, 1993).

MOS and SIS produce data sets, composed of several spectral scans and ancillary information. Each scan consists of two 500-channel spectra: the blue from about 340 to 640 nm; the red from about 600 to 900 nm. The spectral output from a diode array is measured as dark scans with the shutter closed and as radiance or irradiance scans when the shutter is open. MOS also contains light-emitting diodes for field calibration. The dark scans account for instrument background noise and are subtracted from radiance or irradiance measurements. Spectra are scanned in sets, typically composed of two dark scans followed by five radiance or irradiance scans, followed by another two dark scans. The number of scans is controlled by the operator depending on wave noise, sky variability and the achieved signal to noise ratio. MOS contains sensors to measure external water pressure and temperature, internal and array temperatures, instrument tilt and heading, heat exchanger cooler flow, and battery voltages. SIS measures internal temperature and reference voltages.

VAX FORTRAN and C software was developed at MLML to acquire and process large amounts of data gathered by the MOS and SIS spectroradiometers. Instrument control and acquisition software provides the interface between the person operating the instruments and the hardware. Control of MOS is done by sending FORTH commands to the instrument. MOS is controlled internally by a TattleTale 7 FORTH system described by Reaves and Broenkow (1993). The VAX MOS and SIS programs display menus, accept

commands from the operators terminal, send commands to, and receive data from the instruments, and display spectral scans and ancillary data to the operator. Acquisition programs save all data in MLML_DBASE or *PLOT* binary files. These scan-sets, are subsequently processed by converting raw data from digital counts to radiometric units, and by deriving required radiometric products. Broenkow and Reaves (1993), "Introduction to MLML_DBASE Programs", discusses *PLOT* terminology which will be used throughout this report. Broenkow, *et al.* (1993), "Processing NOAA Spectroradiometer Data", provides a terse, graphical outline of the NOAA/MLML data processing system.

A completely processed optical profile from a MOCE bio-optics station is contained in a single file and consists of:

1. L_u , E_d , and E_s spectral scans at three depths with ancillary information.
2. Radiance and irradiance diffuse attenuation coefficients, K_L and K_E .
3. Water-leaving radiances, L_{WN} , normalized for time of day, location, atmospheric scattering functions, and L_{WN} weighted for the eight SeaWiFS bands.
4. Photosynthetically available radiation, PAR, solar zenith angle, airmass, and normalization factor, F_N .

Each file contains a header identifying: cruise and ship name; station name, GMT date and time, geographic location; cloud cover and type, sky conditions; wind direction and velocity, sea state; Secchi depth and Munsell color; instrument identification; calibration date and file identification; processing methods and algorithms; and observer names.

Data Acquisition Outline

Data acquisition programs control MOS, SIS and Fastie spectroradiometers via four X-Windows displays:

1. The control window displays a menu of commands to start and stop scans, setup

Table 1. The NOAA Main Menu for Processing Radiometric Data. Note that some program names are the same as those used in the main MLML_DBASE program *PLOT*.

#	Program	Description
1	CONVERT	Apply System Response, Immersion Factor
2	EDIT	Replace erroneous data with NaN
3	SMOOTH	Apply N-Point Running Mean Smoothing
4	ADJUST	Average Radiance & Dark; %Error; Rad-Drk; SNR
5	AVERAGE	Calculate Spectral Mean and %Error
6	MERGE	Combine E_d , L_u , E_s 's from <i>Archive</i> Files
7	CLIP	Replace Low SNR Data with NaN
8	DERIVE	Derive K_E , K_L , L_W , L_{WN} ; Apply SeaWiFS Weights
9	GRAPH	Plot 2-Page, 3-Panel X-Y Graphs
10	LIST	Print Data Report Listings
11	PROCESS	Execute Script Commands Files on <i>Archive</i> File List

operating parameters, and save data. Commands are selected via a mouse-driven menu bar and executed by "clicking" on the highlighted command.

2. Program prompts are displayed in a text window. All keyboard input is read from this window.
3. A third window displays instrument analog information and scan counters.
4. X-Y line graphs of spectral scan information are displayed in a graphics window.

MOS Data Acquisition

This section is in preparation.

SIS Data Acquisition

This section is in preparation.

Fastie Data Acquisition

This section is in preparation.

Data Processing Outline

The SeaWiFS Prelaunch Science Working Group

has recommended that $E_s(\lambda)$, $E_d(z,\lambda)$, and $L_u(z,\lambda)$ data should be recorded and archived at 4 levels:

- Level 0: Raw instrument digital output.
- Level 1: Instrument output in volts (or frequency) and depth.
- Level 2: Calibrated radiance/irradiance, ancillary measurements in appropriate geophysical or biological units, and depth, corrected for dark/zero offsets.
- Level 3: Smoothed profiles of $K(z,\lambda)$ and associated $L_u(z,\lambda)$ or $E_d(z,\lambda)$ normalized by measured $E_s(\lambda)$.
- Level 4: Level 3 data normalized to clear-sky, zenith sun at mean earth-sun distance, and spectrally adjusted to match SeaWiFS reference wavelengths and FWHM bandwidths.

NOAA/MLML radiometric data acquisition software (the SIS, MOS and Fastie programs) produces level 0 files in output units of raw digital counts. Before numerical processing begins, the various files taken at a single optics station must be assembled and inspected. This is done using a set of routines for "merging" file names into a file called MERGE.LIS. These files are then "grouped" time-

wise. Following that, spectral data from these files are inspected by the NOAA_LOOK program. After the files have been assembled into logical units constituting a single radiometer station, the programs described in Table 1 produce level 2 through level 4 files. The order in which those programs are applied to MOS and SIS data sets is usually top-down, i.e. Program 1 through Program 10, though this order can vary. Program 11 incorporates one or more of Programs 1 through 10 for batch-mode processing.

Data Description

A level 0 scan-set is acquired and saved to an *Archive* file, which consists typically of the following 10 *Variables* (the order of *Variables* 2 through 10 corresponds to the temporal sequence in which they were acquired):

Variable #

1. Nominal Wavelength (nm)
2. Dark Scan # 1 (counts)
3. Dark Scan # 2 (counts)
4. L_u or E_d or E_s Scan # 1 (counts)
5. L_u or E_d or E_s Scan # 2 (counts)
6. L_u or E_d or E_s Scan # 3 (counts)
7. L_u or E_d or E_s Scan # 4 (counts)
8. L_u or E_d or E_s Scan # 5 (counts)
9. Dark Scan # 3 (counts)
10. Dark Scan # 4 (counts)

Each of the above *Variables* contains 1000 *Elements* for a MOS $L_u(z,\lambda)$ or $E_d(z,\lambda)$ scan, or 48 *Elements* (38 spectral channels + 10 reference channels) for a SIS $E_s(z,\lambda)$ scan. Each *Element* contains the 16-bit (0-65535) intensity level of a single diode array pixel. All raw scan data units are counts, and wavelengths are un-calibrated nominal values in nm. The *Variable Header* for each scan contains an *Extension* which holds the following information collected at the time of the individual scan (see Appendix 5 for definitions of MLML_DBASE MOS, SIS and Fastie data structures):

Scan, Cruise, Station, Cast, Instrument Serial #, Instrument Configuration #, Multiplexer Serial # (MOS only), Scan Time, Navigation Type, Latitude, Longitude, Time of Last Satellite Overpass, Variable Type, Variable Subtype, Processing Code, Smoothing Code, Interpolation Code, Beginning Interpolation Wavelength, Interpolation Wavelength Interval, Number of Averages (SIS only), Multiplexer Position (MOS

only), Mirror Position (MOS only), Comments, Number of Points Edited, Number of Errors.

E_d and L_u *Variable Header Extensions* contain the following for each of the two (blue and red) MOS spectrographs:

Cooler Intensity, Intensifier Setting, LED Level, Data Length, Gain, Integration Time.

E_s *Variable Extensions* contain the following for the SIS spectrograph:

Shutter Setting, Number of Channels, Gain and Timeout for each channel.

Type, value, gain and average are saved for the following analog channels:

MOS

Internal Temperature, External Temperature, Pressure Transducer Temperature, External Pressure (depth), Battery Voltage, High and Low Voltage References, LED Temperature, Compass Direction, X-tilt, Y-tilt, Blue and Red Array Temperature, Heat Exchanger Cooler Flow, Compass Direction.

SIS

Internal Temperature, Battery Voltage, X-tilt, Y-tilt, Array temperature.

Appendix 5 provides the definition and ranges of values for data codes such as Variable Type, Processing Code, Cooler Intensity and Shutter Setting.

Level 1 files are not produced for the MOS and SIS instruments. This is because the diode array detectors with their integral analog to digital converters are calibrated as single units: their digital outputs are directly converted to radiometric units. This is also the case for all ancillary sensors, whose digital outputs are directly converted to physical units.

Assembling Data Files

The SIS, MOS and Fastie data acquisition programs produce independent files (one for each instrument) containing surface irradiances, upwelled radiance or downwelled irradiances at a number of depths. These instruments have different spectral resolution, and data acquisition from them is not done synchronously. This makes assembling and reducing

the diverse data sets difficult.

Perhaps the most difficult problem is to provide a flexible system to merge the various data sets with the goal of determining water-leaving radiances and diffuse attenuation coefficients. The data acquisition programs produce files with file names that uniquely determine their contents (Appendix 4). Data from a single cruise or calibration experiment are contained in a single directory. The data merging procedure is outlined as follows:

1. The first step is to create lists of file names which constitute data for a single optical profile or for a group of stations to be processed in one session. This is done with the command "ALIAS", which runs the DCL command file \$MLML\$DIR:ALIAS.COM. ALIAS is executed twice, first to assemble the MOS (and perhaps Fastie) files for a specific station and next to assemble the SIS files for that same station. The examples below result in two files: M.ALIAS and S.ALIAS, which are located in the user's logical directory ALIAS\$DIR. The use of VMS wild-cards (*) limits the search to selected files. Familiarity with the VMS file naming conventions is essential to accomplish this process. The syntax for this is \$ ALIAS input-files output-files, for example,

```
$ ALIAS [DATA.MOCE_2.MOS.RAW]STN2*.MLDAT M
$ ALIAS      [DATA.MOCE_2.SIS.RAW]*.MLDAT S
```

Examples of the ALIAS files are shown in Table 2.

2. The next step is to find the number of *PLOT Variables* and the time-span for each file. This is done by passing the M.ALIAS and S.ALIAS files to the NOAA_LIST_HEADERS program, which can be executed using the VMS symbol NLH, which is equivalent to \$ RUN NOAA_LIST_HEADERS, from the NOAA\$BIN directory. That program is invoked twice, once for MOS (or Fastie) files and again for SIS files. The syntax for this is \$ NLH input-alias-file output-list-file, for example,

```
$ NLH          ALIAS$DIR:M.ALIAS M.LIS
$ NLH          ALIAS$DIR:S.ALIAS S.LIS
```

Output from this procedure are the files, M.LIS and S.LIS, (Table 3) which contains header information from the selected MOS and SIS files.

3. The third step in merging files is to "group" the surface irradiance files (SIS) by time with the contemporaneous MOS files containing downwelled irradiance and upwelled radiance. This is done by use of the program NOAA_GROUP_FILES which can be run using the VMS symbol, NGF, equivalent to

```
$ RUN $NOAA$BIN:NOAA_GROUP_FILES
```

The syntax to invoke the "grouping" program requires the ALIAS file names for the MOS and SIS file names followed by the name of the "merge" file, for example,

```
$ NGF          M.LIS S.LIS MERGE.LIS;1
```

Output from this procedure is shown in Table 4.

4. Up to this point, data reduction can be done more-or-less blindly, with the emphasis on "less blindly", because it is generally impossible to trap for all errors or exceptional circumstances that may occur aboard ship during data acquisition. Examples of exceptions might be erroneous latitude and longitude, erroneous system clock time or empty data files. Steps 1-3 are done outside of *PLOT*, from the VMS command line. The next step requires running *PLOT* and the NOAA programs to examine each E_d or L_u and E_s scan-set to determine which are suitable. This requires plotting each spectral scan and noting which are to be retained. The procedure is done inside *PLOT*. The syntax for doing this from the main *PLOT* prompt is to run the NOAA program and its subprogram *LOOK* followed by the merge listing file name, for example,

```
ML> NOAA LOOK          MERGE.LIS;1
```

While determining which files are to be combined, it is essential that a hardcopy of the MERGE.LIS;1 file is available on which to note the acceptable E_s, L_u, and E_d files. This procedure requires patience and practice.

After the *LOOK* program has been run, the MERGE.LIS;1 file is manually edited to produce the file, MERGE.LIS:2, which contains the file names of only those scans which have passed scrutiny. The others are deleted by a text editor. The MERGE.LIS:2 file should be kept as a permanent record of data processing procedure.

Table 2. Example of MOS and SIS ALIAS Files used to group all Station 2 files before numerical processing.

```
ALIAS$DIR:M.ALIAS
-----
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_11M_LU_05.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_ED_01.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_02.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_03.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_04.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_11M_08.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_11M_09.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_1M_18.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_6M_12.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_6M_13.MLDAT
.
.
.
```

```
ALIAS$DIR:S.ALIAS
-----
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]ONLY_A_TEST.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180202.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180302.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180402.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180502.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180602.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180702.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180802.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180902.MLDAT
_DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_181002.MLDAT
.
.
.
```

Table 3. Example of the M.LIS and S.LIS files formed by running the NOAA_LIST_HEADERS program.

M.LIS

```

M1 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_11M_LU_05.MLDAT #Var=10 31Mar93 19:45 to 31Mar93 19:50
M2 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_ED_01.MLDAT #Var=14 31Mar93 18:55 to 31Mar93 19:02
M3 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_02.MLDAT #Var=10 31Mar93 19:07 to 31Mar93 19:12
M4 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_03.MLDAT #Var=19 31Mar93 19:07 to 31Mar93 19:18
M5 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_04.MLDAT #Var=28 31Mar93 19:07 to 31Mar93 19:27
M6 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_11M_08.MLDAT #Var=10 31Mar93 20:35 to 31Mar93 20:39
M7 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_11M_09.MLDAT #Var=10 31Mar93 20:40 to 31Mar93 20:44
M8 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_1M_18.MLDAT #Var=10 31Mar93 22:11 to 31Mar93 22:14
M9 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_6M_12.MLDAT #Var=10 31Mar93 21:34 to 31Mar93 21:38
M10 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_6M_13.MLDAT #Var=10 31Mar93 21:39 to 31Mar93 21:42
.
.

```

S.LIS

```

S1 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]ONLY_A_TEST.MLDAT #Var=10 27Mar93 18:00 to 27Mar93 18:00
S2 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180202.MLDAT #Var=10 27Mar93 18:02 to 27Mar93 18:02
S3 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180302.MLDAT #Var=10 27Mar93 18:03 to 27Mar93 18:03
S4 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180402.MLDAT #Var=10 27Mar93 18:04 to 27Mar93 18:04
S5 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180502.MLDAT #Var=10 27Mar93 18:05 to 27Mar93 18:05
S6 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180602.MLDAT #Var=10 27Mar93 18:06 to 27Mar93 18:06
S7 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180702.MLDAT #Var=10 27Mar93 18:07 to 27Mar93 18:07
S8 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180802.MLDAT #Var=10 27Mar93 18:08 to 27Mar93 18:08
S9 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_180902.MLDAT #Var=10 27Mar93 18:09 to 27Mar93 18:09
S10 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930327_181002.MLDAT #Var=10 27Mar93 18:10 to 27Mar93 18:10
.
.

```

Table 4. Example of a MERGE.LIS:1 file produced by the NOAA_GROUP_FILES program before running NOAA_LOOK. Notice that the ALIAS file names (M20, S797) precede the complete file names.

MERGE.LIS:1

```

M1 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_11M_LU_05.MLDAT #Var=10 31Mar93 19:45 to 31Mar93 19:50
S819 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_195129.MLDAT #Var=10 31Mar93 19:51 to 31Mar93 19:51

M20 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_ED_01.MLDAT #Var=14 31Mar93 18:55 to 31Mar93 19:02
S797 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185546.MLDAT #Var=10 31Mar93 18:55 to 31Mar93 18:56
S798 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185646.MLDAT #Var=10 31Mar93 18:56 to 31Mar93 18:57
S799 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185747.MLDAT #Var=10 31Mar93 18:57 to 31Mar93 18:58
S800 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185846.MLDAT #Var=10 31Mar93 18:58 to 31Mar93 18:59
S801 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185946.MLDAT #Var=10 31Mar93 18:59 to 31Mar93 19:00

M2 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_02.MLDAT #Var=10 31Mar93 19:07 to 31Mar93 19:12
S801 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185946.MLDAT #Var=10 31Mar93 18:59 to 31Mar93 19:00

M22 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_03.MLDAT #Var=19 31Mar93 19:07 to 31Mar93 19:18
S801 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185946.MLDAT #Var=10 31Mar93 18:59 to 31Mar93 19:00

M3 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_04.MLDAT #Var=28 31Mar93 19:07 to 31Mar93 19:27
S801 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185946.MLDAT #Var=10 31Mar93 18:59 to 31Mar93 19:00

M4 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_ED_11M_08.MLDAT #Var=10 31Mar93 20:35 to 31Mar93 20:39
S863 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_203529.MLDAT #Var=10 31Mar93 20:35 to 31Mar93 20:35
S864 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_203629.MLDAT #Var=10 31Mar93 20:36 to 31Mar93 20:36
S865 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_203729.MLDAT #Var=10 31Mar93 20:37 to 31Mar93 20:37
S866 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_203829.MLDAT #Var=10 31Mar93 20:38 to 31Mar93 20:38
S867 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_203929.MLDAT #Var=10 31Mar93 20:39 to 31Mar93 20:39
.
.
```

Table 5. Example of the edited MERGE.LIS file containing those files that passed scrutiny in the NOAA_LOOK program.

```
MERGE.LIS;2
-----
!
! File: MOCE2_STN02_MERGE.LIS 22-Nov-1993 by M.Feinholtz
! MOS/SIS data files processed for MOCE2 Stn02 Isla Santa Cruz
!

! Ed surface

M20 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_ED_01.MLDAT      #Var=14 31Mar93 18:55 to 31Mar93 19:02
S797 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185546.MLDAT    #Var=10 31Mar93 18:55 to 31Mar93 18:56
S798 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185646.MLDAT    #Var=10 31Mar93 18:56 to 31Mar93 18:57
S799 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185747.MLDAT    #Var=10 31Mar93 18:57 to 31Mar93 18:58
S800 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185846.MLDAT    #Var=10 31Mar93 18:58 to 31Mar93 18:59

! Lu surface

M22 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_03.MLDAT      #Var=19 31Mar93 19:07 to 31Mar93 19:18
M3 _DUA1:[DATA.NOAA.MOCE_2.MOS.RAW]STN02_1M_LU_04.MLDAT        #Var=28 31Mar93 19:07 to 31Mar93 19:27
S801 _DUA1:[DATA.NOAA.MOCE_2.SIS.RAW]SIS_930331_185946.MLDAT    #Var=10 31Mar93 18:59 to 31Mar93 19:00
.
.
.
```

Table 6a. Schematic of MLML_DBASE Merged File Contents. Top, Mid and Bot refer to the sample depths.

MOCE2_STN02_MERGE.MLDAT

Var #	Symbol	Var #	Symbol	Var #	Symbol	Var #	Symbol
1	MOS lambda	3	Ed top	11	Ed mid	19	Ed bot
2	SIS lambda	4	SNR	12	SNR	20	SNR
		5	Es	13	Es	21	Es
		6	SNR	14	SNR	22	SNR
		7	Lu top	15	Lu mid	23	Lu bot
		8	SNR	16	SNR	24	SNR
		9	Es	17	Es	25	Es
		10	SNR	18	SNR	26	SNR

Table 6b. Schematic of MLML_DBASE Derived File Contents. Attenuation coefficients between top and mid are designated K_1, between top and bot as K_2, and between mid and bot as K_3. Water-leaving radiances are designated by the surface-most upwelled radiance and the attenuation coefficient (1,2,3) used in the extrapolation.

MOCE2_STN02_DERIVE.MLDAT

Var #	Symbol	Var #	Symbol	Var #	Symbol
27	Ke_1	33	Lw t1	37	Lwn
28	Kl_1	34	Lw t2	38	Lwn
29	Ke_2	35	Lw m1	39	Lwn
30	Kl_2	36	Lw b2	40	Lwn
31	Ke_3			41	Fn
32	Kl_3				

The liberal use of comments, which are denoted by a leading exclamation point (!), is essential. An example of the edited MERGE.LIS;2 file is shown in Table 5.

5. The last step required to assemble scans before numerical processing can begin is to form *PLOT* data files containing the E_s , L_u , and E_d , data for the Top, Mid and Bot sampling depths. That is done within *PLOT* using the *NOAA LOOK* program which requires the name of the merge listing file, for example,

```
ML> NOAA MERGE           MERGE.LIS;2
```

Notice that the second version number of the MERGE.LIS file is used.

Following preprocessing steps 1-5, the NOAA programs, *NOAA_CONVERT*, *NOAA_DERIVE*, *NOAA_CLIP*, *NOAA_GRAPH*, and *NOAA_LIST* can be run to produce calibrated radiances, attenuation coefficients and water-leaving radiances, as explained next. The second data processing phase involves numerical conversions and produces files containing a well-ordered set of radiometric values shown in Table 6.

1. Each raw MOS $L_u(z, \lambda)$, $E_d(z, \lambda)$ and SIS $E_s(z, \lambda)$ scan-set is converted from raw counts to radiometric units by applying the sensor's system response. Since E_d and L_u sensors are calibrated in air but are used to measure radiation underwater, an additional immersion correction factor, F_w , is applied.
2. For MOS data only, known "bad" pixels are replaced with a missing-data code, NaN.
3. For MOS data only, each scan is smoothed spectrally to reduce instrument noise.
4. Dark scans are averaged. Radiance or irradiance scans are averaged. Average dark count is subtracted from average radiance or irradiance. Percent errors are determined for each average, and Signal to Noise Ratio, SNR, is calculated.

These steps are repeated for each scan-set, with the resulting *Variables* recorded to *PLOT Archive* files in the following order (for example, using a SIS E_s scan-set):

Variable #

1. Corrected SIS Wavelength (nm)
2. Dark Scan # 1 ($\mu\text{W}/\text{cm}^2/\text{nm}$)
3. Dark Scan # 2 ($\mu\text{W}/\text{cm}^2/\text{nm}$)
4. E_s Scan # 1 ($\mu\text{W}/\text{cm}^2/\text{nm}$)
5. E_s Scan # 2 ($\mu\text{W}/\text{cm}^2/\text{nm}$)
6. E_s Scan # 3 ($\mu\text{W}/\text{cm}^2/\text{nm}$)
7. E_s Scan # 4 ($\mu\text{W}/\text{cm}^2/\text{nm}$)
8. E_s Scan # 5 ($\mu\text{W}/\text{cm}^2/\text{nm}$)
9. Dark Scan # 3 ($\mu\text{W}/\text{cm}^2/\text{nm}$)
10. Dark Scan # 4 ($\mu\text{W}/\text{cm}^2/\text{nm}$)
11. Mean Dark ($\mu\text{W}/\text{cm}^2/\text{nm}$)
12. Dark %RMSE
13. Mean E_s ($\mu\text{W}/\text{cm}^2/\text{nm}$)
14. E_s %RMSE
15. Mean E_s - Mean Dark ($\mu\text{W}/\text{cm}^2/\text{nm}$)
16. SNR

5. The dark-corrected radiance or irradiance and SNR (*Var# 15* and *16* above) of several sets which represent a single depth or a single time are averaged. For example, several E_s sets may span the time interval of one L_u scan, and hence must be averaged together.

At this point, each set has been processed to a corrected and dark-adjusted radiance or irradiance spectra with SNR. Multiple scan-sets have been averaged if necessary. Each (average) E_d and L_u at a depth has been associated with an (average) E_s .

The final step is to combine SIS and MOS files, trim the scans to wavelengths having acceptable signal to noise, derive attenuation coefficients and water-leaving radiances and produce hard-copy reports.

6. Processed data files are merged into a single optical profile, containing E_d and L_u spectra at three depths along with corresponding E_s and SNR's. We use the terminology "Top" for the surface-most data; "Mid" for data obtained at the middle depth; "Bot" for data taken at the deepest or bottom depth. A merged profile contains 26 *Variables* in the following order:

1. Corrected MOS Wavelength (nm)
2. Corrected SIS Wavelength (nm)
3. Top E_d ($\mu\text{W}/\text{cm}^2/\text{nm}$)
4. SNR of Top E_d
5. E_i for Top E_d ($\mu\text{W}/\text{cm}^2/\text{nm}$)
6. SNR of E_s for Top E_d

- 7. Surface L_u ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 8. SNR of Top L_u
 - 9. E_i for Top L_u ($\mu\text{W}/\text{cm}^2/\text{nm}$)
 - 10. SNR of E_s for Top L_u
 - 11. Mid E_d ($\mu\text{W}/\text{cm}^2/\text{nm}$)
 - 12. SNR of Mid E_d
 - 13. E_i for Mid E_d ($\mu\text{W}/\text{cm}^2/\text{nm}$)
 - 14. SNR of E_s for Mid E_d
 - 15. Mid L_u ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 16. SNR of Mid L_u
 - 17. E_i for Mid L_u ($\mu\text{W}/\text{cm}^2/\text{nm}$)
 - 18. SNR of E_s for Mid L_u
 - 19. Bot E_d ($\mu\text{W}/\text{cm}^2/\text{nm}$)
 - 20. SNR of Bot E_d
 - 21. E_i for deep E_d ($\mu\text{W}/\text{cm}^2/\text{nm}$)
 - 22. SNR of E_s for Bot E_d L_u ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 23. Bot L_u ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 24. SNR of Bot L_u
 - 25. E_i for Bot L_u ($\mu\text{W}/\text{cm}^2/\text{nm}$)
 - 26. SNR of E_s for Bot L_u
 - 7. The SeaWiFS project group identifies a SNR of 100:1 as the minimum quality assurance level. Individual data *Elements* below this level can be removed, or clipped, from the merged *Variables*.
 - 8. Diffuse attenuation coefficients and solar-normalized water-leaving radiances are calculated from *Variables* arranged in step 6 and clipped in step 7. SeaWiFS normalized responses are applied for the eight bands. PAR, FLH, solar altitude, and air mass are calculated and saved with processed spectral and analog data. This step derives the *Var#*'s 27 to 36. All 36 *Variables* are recorded in a single *Archive* file containing one optical profile. The file contents are summarized in Table 6.
 - 27. Top to Mid K_E (m^{-1})
 - 28. Top to Mid K_L (m^{-1})
 - 29. Top to Bot K_E (m^{-1})
 - 30. Top to Bot K_L (m^{-1})
 - 31. Mid to Bot K_E (m^{-1})
 - 32. Mid to Bot K_L (m^{-1})
 - 33. L_W Top/1 ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 34. L_W Top/2 ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 35. L_W Mid/1 ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 36. L_W Bot/2 ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 37. L_{WN} Top/1 ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 38. L_{WN} Top/2 ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 39. L_{WN} Mid/1 ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 40. L_{WN} Bot/2 ($\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$)
 - 41. F_N Solar normalizing factor
 - 9. Two pages of X-Y line graphs formatted with three plots per page are produced (Figs. 1 and 2). These can be displayed to a terminal, PostScript printer or PostScript file. Plots are available in color or in black-and-white.
 - 10. A data report listing is produced in tabular ASCII format and output to either a terminal, printer, or file (Figs 3 and 4). Graphical and tabular output are useful for archive and reference. The ASCII files generated here or more simple ASCII files generated by the *PLOT* program are used to distribute data to interested parties.
- The above processing is implemented in 10 steps to allow flexibility in program sequencing, to accommodate exceptions, and to allow use of partially processed profiles. This is necessary, for example, while processing calibration data to generate system response, $R(\lambda)$. In this situation, *CONVERT* is not applied and *DERIVED* parameters are not calculated. Instead, sets are *EDITed*, *SMOOTHed*, *ADJUSTed* and possibly *MERGED*. System response is computed as the ratio of the calibrated lamp spectra and the processed MOS or SIS spectral counts.
- The *CONVERT* step can be omitted if a valid system response is not available. This may be the case before post-cruise calibrations are performed. Scan-sets can be processed in raw units and later *CONVERTed* to radiometric units. Indeed, diffuse attenuation coefficients are identical if *DERIVED* from *CONVERTed* or unconverted scan-sets.
- ### Running Data Processing Programs
- What follows illustrates use of the NOAA programs, which run under the *MLML_DBASE* program, generally called *PLOT*. *PLOT* must be run from the VMS command line as
- ```
$ PLOT 100 1000 4 4 2000
```
- The four parameters passed to the *PLOT* program do the following: 100 indicates the number of *PLOT Variables*; 1000 indicates the number of data *Elements*;

## MODIS Marine Optical Characterization Experiment - I NOAA/MLML

CRUISE: MOCE-1 SHIP: De Steiguer  
STATION: 7-1 Mulligan Hill

Top = 1 m  
Mid = 5 m  
Bot = 10 m

POSITION: 36°44.4 N 121°51.2 W  
DATE: 22:13 (GMT) 08 Sep 1992

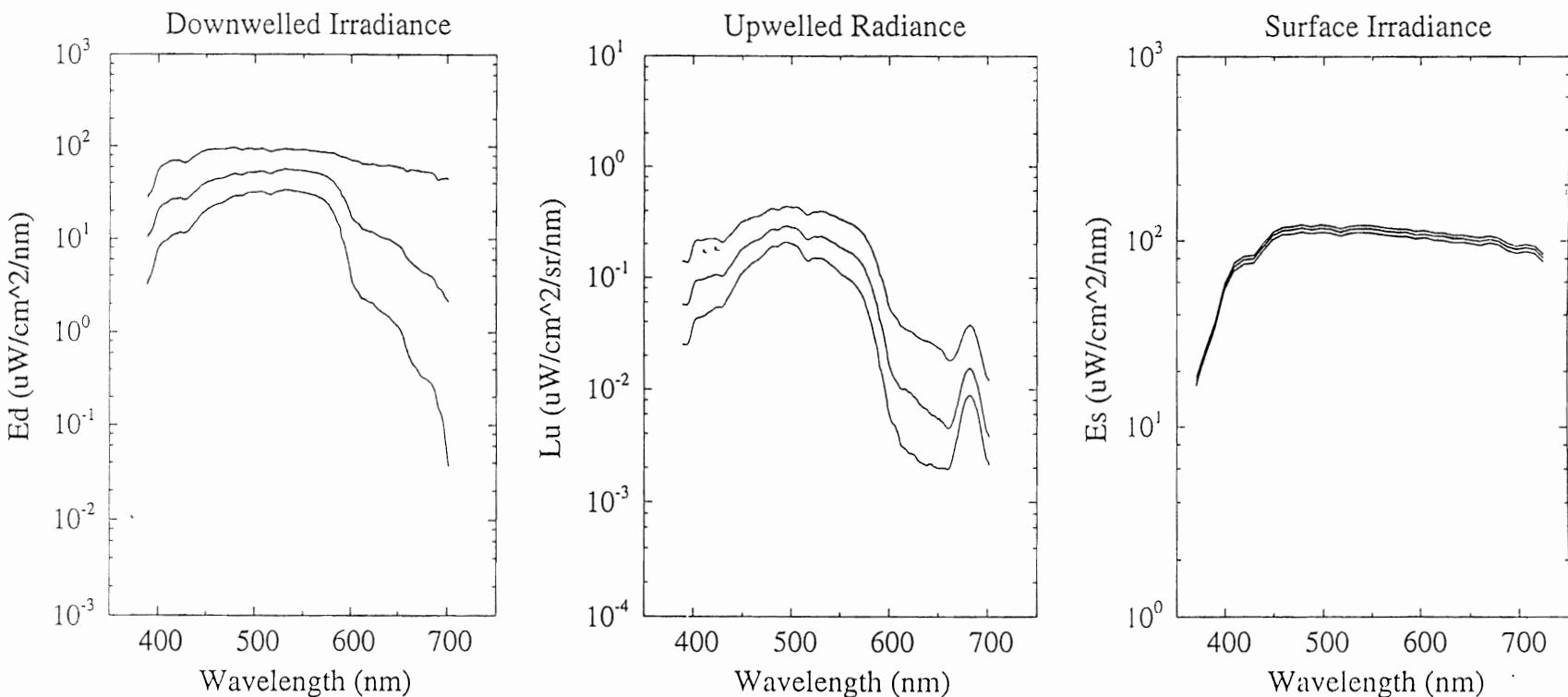


Figure 1. First page of figures, observed spectra, produced by NOAA\_GRAPH.

## MODIS Marine Optical Characterization Experiment - I NOAA/MLML

CRUISE: MOCE-1 SHIP: De Steiguer  
STATION: 7-1 Mulligan Hill

Top = 1 to 5 m  
Mid = 1 to 10 m  
Bot = 5 to 10 m

POSITION: 36°44.4 N 121°51.2 W  
DATE: 22:13 (GMT) 08 Sep 1992

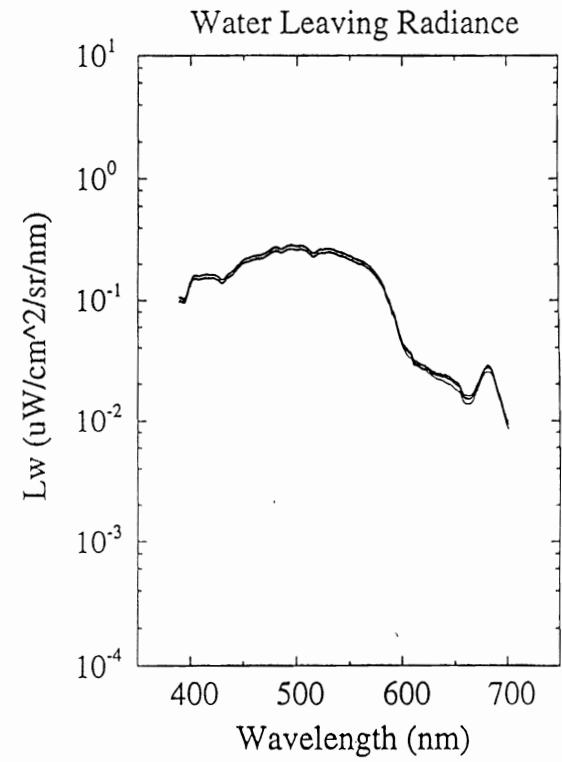
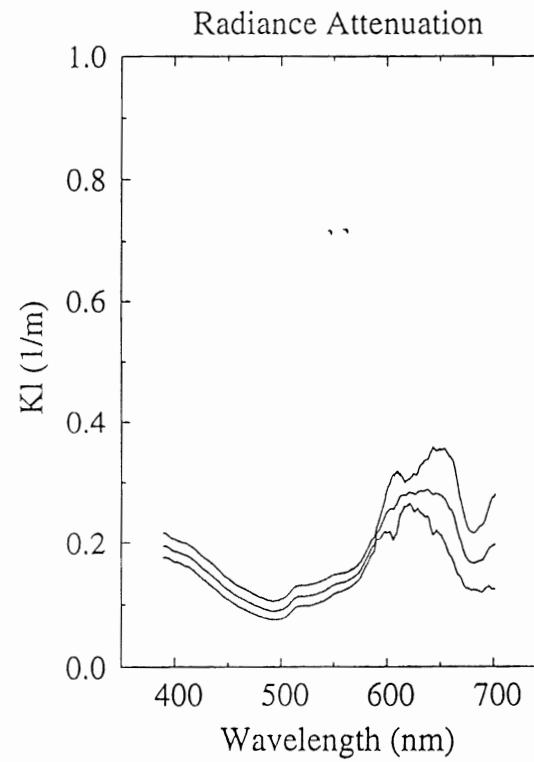
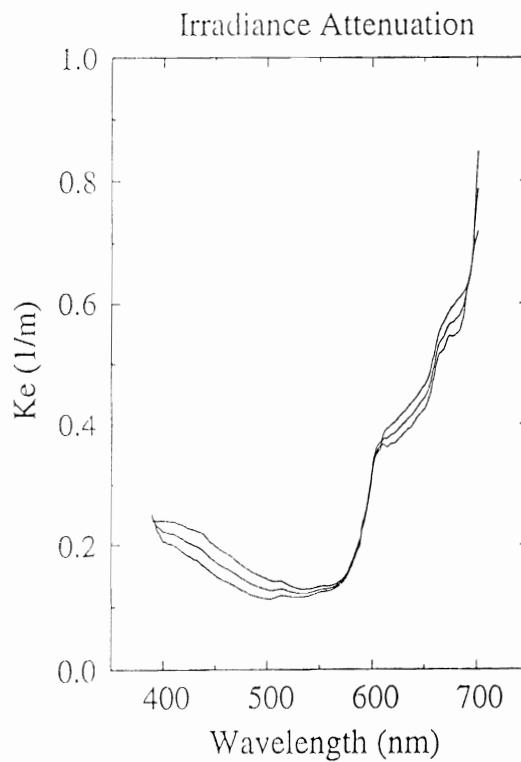


Figure 2. Second page of figures, attenuation coefficients and water-leaving radiances, produced by NOAA\_GRAPH.

File: MOCE1:[MOS.PRC]STN07\_1\_PRC.MLDAT;1

MODIS Marine Optical Characterization Experiment - 1 NOAA/MLML

CRUISE: MOCE-1 SHIP: De Steiguer  
DATE: 22:13 (GMT) 08 Sep 1992

STATION: 7-1 Mulligan Hill  
POSITION: 36°44.4' N 121°51.2' W

SeaWiFS-weighted normalized water-leaving radiance:

|                   |         |         |         |         |         |         |         |     |
|-------------------|---------|---------|---------|---------|---------|---------|---------|-----|
| Wavelength (nm):  | 412     | 443     | 490     | 510     | 555     | 670     | 765     | 865 |
| Lwn (μW/cm^2/sr): | 2.69E-1 | 3.08E-1 | 4.20E-1 | 4.04E-1 | 3.37E-1 | 2.82E-2 | 2.99E-3 | nil |

| Depth (m)  | Top   | Top   | Mid   | Mid   | Bot   | Bot   |
|------------|-------|-------|-------|-------|-------|-------|
|            | 0.6   |       | 5.0   |       | 5.6   |       |
| Time (GMT) | 22:29 | 22:22 | 22:15 | 22:09 | 22:01 | 21:55 |

| $\lambda$ (nm) | Ed_1    | Es_1    | Lu_1    | Es_1    | Ed_2    | Es_2    | Lu_2    | Es_2    | Ed_3    | Es_3    | Lu_3    | Es_3    |
|----------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 400            | 5.52E+1 | 5.34E+1 | 1.97E-1 | 5.40E+1 | 2.05E+1 | 5.63E+1 | 8.57E-2 | 5.70E+1 | 7.91E+0 | 5.90E+1 | 3.90E-2 | 5.97E+1 |
| 410            | 6.60E+1 | 6.84E+1 | 2.15E-1 | 6.91E+1 | 2.47E+1 | 7.19E+1 | 9.56E-2 | 7.27E+1 | 9.78E+0 | 7.54E+1 | 4.49E-2 | 7.59E+1 |
| 420            | 7.00E+1 | 7.43E+1 | 2.21E-1 | 7.51E+1 | 2.69E+1 | 7.81E+1 | 1.04E-1 | 7.91E+1 | 1.13E+1 | 8.18E+1 | 5.13E-2 | 8.23E+1 |
| 430            | 6.69E+1 | 7.55E+1 | 2.06E-1 | 7.61E+1 | 2.66E+1 | 7.93E+1 | 1.03E-1 | 8.05E+1 | 1.18E+1 | 8.31E+1 | 5.48E-2 | 8.37E+1 |
| 440            | 7.95E+1 | 8.77E+1 | 2.50E-1 | 8.86E+1 | 3.29E+1 | 9.22E+1 | 1.33E-1 | 9.33E+1 | 1.55E+1 | 9.65E+1 | 7.60E-2 | 9.71E+1 |
| 450            | 9.05E+1 | 1.01E+2 | 3.15E-1 | 1.02E+2 | 4.04E+1 | 1.06E+2 | 1.80E-1 | 1.07E+2 | 2.04E+1 | 1.11E+2 | 1.10E-1 | 1.11E+2 |
| 460            | 9.39E+1 | 1.07E+2 | 3.43E-1 | 1.08E+2 | 4.39E+1 | 1.12E+2 | 2.06E-1 | 1.14E+2 | 2.32E+1 | 1.17E+2 | 1.33E-1 | 1.18E+2 |
| 470            | 9.38E+1 | 1.08E+2 | 3.63E-1 | 1.09E+2 | 4.62E+1 | 1.13E+2 | 2.26E-1 | 1.15E+2 | 2.53E+1 | 1.18E+2 | 1.52E-1 | 1.20E+2 |
| 480            | 9.61E+1 | 1.11E+2 | 4.14E-1 | 1.12E+2 | 5.03E+1 | 1.16E+2 | 2.69E-1 | 1.18E+2 | 2.90E+1 | 1.21E+2 | 1.88E-1 | 1.22E+2 |
| 490            | 9.38E+1 | 1.08E+2 | 4.20E-1 | 1.10E+2 | 5.11E+1 | 1.14E+2 | 2.80E-1 | 1.15E+2 | 3.04E+1 | 1.19E+2 | 2.00E-1 | 1.19E+2 |
| 500            | 9.35E+1 | 1.11E+2 | 4.26E-1 | 1.11E+2 | 5.26E+1 | 1.16E+2 | 2.81E-1 | 1.17E+2 | 3.18E+1 | 1.21E+2 | 2.00E-1 | 1.22E+2 |
| 510            | 9.32E+1 | 1.10E+2 | 4.03E-1 | 1.10E+2 | 5.31E+1 | 1.15E+2 | 2.49E-1 | 1.16E+2 | 3.16E+1 | 1.20E+2 | 1.67E-1 | 1.21E+2 |
| 520            | 9.01E+1 | 1.06E+2 | 3.76E-1 | 1.07E+2 | 5.27E+1 | 1.11E+2 | 2.25E-1 | 1.12E+2 | 3.12E+1 | 1.16E+2 | 1.45E-1 | 1.16E+2 |
| 530            | 9.43E+1 | 1.09E+2 | 3.93E-1 | 1.10E+2 | 5.66E+1 | 1.14E+2 | 2.33E-1 | 1.16E+2 | 3.38E+1 | 1.19E+2 | 1.49E-1 | 1.20E+2 |
| 540            | 9.23E+1 | 1.10E+2 | 3.65E-1 | 1.12E+2 | 5.56E+1 | 1.15E+2 | 2.11E-1 | 1.17E+2 | 3.29E+1 | 1.21E+2 | 1.31E-1 | 1.21E+2 |
| 550            | 9.26E+1 | 1.10E+2 | 3.35E-1 | 1.11E+2 | 5.48E+1 | 1.15E+2 | 1.87E-1 | 1.17E+2 | 3.16E+1 | 1.20E+2 | 1.10E-1 | 1.21E+2 |
| 560            | 8.92E+1 | 1.08E+2 | 3.06E-1 | 1.09E+2 | 5.25E+1 | 1.13E+2 | 1.68E-1 | 1.15E+2 | 2.98E+1 | 1.19E+2 | 9.56E-2 | 1.19E+2 |
| 570            | 8.70E+1 | 1.06E+2 | 2.66E-1 | 1.08E+2 | 4.95E+1 | 1.11E+2 | 1.41E-1 | 1.13E+2 | 2.70E+1 | 1.17E+2 | 7.61E-2 | 1.17E+2 |
| 580            | 8.55E+1 | 1.05E+2 | 1.97E-1 | 1.06E+2 | 4.28E+1 | 1.10E+2 | 9.35E-2 | 1.12E+2 | 2.04E+1 | 1.15E+2 | 4.42E-2 | 1.16E+2 |
| 590            | 7.77E+1 | 1.05E+2 | 1.12E-1 | 1.06E+2 | 3.00E+1 | 1.10E+2 | 4.53E-2 | 1.12E+2 | 1.09E+1 | 1.15E+2 | 1.77E-2 | 1.16E+2 |
| 600            | 7.16E+1 | 1.02E+2 | 5.52E-2 | 1.03E+2 | 1.75E+1 | 1.07E+2 | 1.67E-2 | 1.08E+2 | 3.87E+0 | 1.12E+2 | 6.01E-3 | 1.13E+2 |
| 610            | 6.68E+1 | 1.01E+2 | 4.03E-2 | 1.01E+2 | 1.37E+1 | 1.05E+2 | 1.08E-2 | 1.06E+2 | 2.43E+0 | 1.10E+2 | 3.75E-3 | 1.11E+2 |
| 620            | 6.43E+1 | 9.98E+1 | 3.37E-2 | 1.01E+2 | 1.20E+1 | 1.05E+2 | 9.48E-3 | 1.06E+2 | 2.10E+0 | 1.09E+2 | 2.75E-3 | 1.10E+2 |
| 630            | 6.23E+1 | 9.74E+1 | 2.93E-2 | 9.81E+1 | 1.07E+1 | 1.02E+2 | 7.65E-3 | 1.04E+2 | 1.74E+0 | 1.07E+2 | 2.32E-3 | 1.07E+2 |
| 640            | 6.28E+1 | 9.77E+1 | 2.69E-2 | 9.85E+1 | 9.92E+0 | 1.02E+2 | 6.46E-3 | 1.04E+2 | 1.47E+0 | 1.07E+2 | 2.15E-3 | 1.07E+2 |
| 650            | 5.97E+1 | 9.58E+1 | 2.37E-2 | 9.66E+1 | 8.49E+0 | 1.00E+2 | 5.46E-3 | 1.01E+2 | 1.13E+0 | 1.05E+2 | 1.99E-3 | 1.05E+2 |
| 660            | 5.44E+1 | 9.44E+1 | 1.84E-2 | 9.50E+1 | 6.02E+0 | 9.87E+1 | 4.48E-3 | 9.96E+1 | 5.94E-1 | 1.03E+2 | 1.96E-3 | 1.04E+2 |
| 670            | 5.50E+1 | 9.66E+1 | 2.26E-2 | 9.72E+1 | 4.89E+0 | 1.01E+2 | 7.71E-3 | 1.02E+2 | 3.94E-1 | 1.06E+2 | 4.03E-3 | 1.06E+2 |
| 680            | 5.30E+1 | 9.45E+1 | 3.68E-2 | 9.51E+1 | 4.18E+0 | 9.89E+1 | 1.52E-2 | 9.97E+1 | 3.06E-1 | 1.03E+2 | 8.68E-3 | 1.04E+2 |
| 690            | 4.41E+1 | 8.82E+1 | 2.70E-2 | 8.87E+1 | 3.13E+0 | 9.23E+1 | 1.05E-2 | 9.34E+1 | 1.74E-1 | 9.65E+1 | 6.07E-3 | 9.67E+1 |
| 700            | 4.51E+1 | 8.54E+1 | 1.26E-2 | 8.57E+1 | 2.22E+0 | 8.93E+1 | 4.05E-3 | 9.05E+1 | 4.57E-2 | 9.35E+1 | 2.29E-3 | 9.35E+1 |

Figure 3. First page of the data report, observed spectra, produced by NOAA\_LIST.

File: MOCE1:[MOS.PRC]STN07\_1\_PRC.MLDAT;1

MODIS Marine Optical Characterization Experiment - 1 NOAA/MLML

CRUISE: MOCE-1 SHIP: De Steiguer  
DATE: 22:13 (GMT) 08 Sep 1992

STATION: 7-1 Mulligan Hill  
POSITION: 36°44.4' N 121°51.2' W

SeaWiFS-weighted normalized water-leaving radiance:

| Wavelength (nm):  | 412     | 443     | 490     | 510     | 555     | 670     | 765     | 865 |
|-------------------|---------|---------|---------|---------|---------|---------|---------|-----|
| Lwn (uW/cm^2/sr): | 2.69E-1 | 3.08E-1 | 4.20E-1 | 4.04E-1 | 3.37E-1 | 2.82E-2 | 2.99E-3 | nil |

| Depth(m) | 1-5     | 1-5     | 1-10    | 1-10    | 5-10    | 5-10    | Top<br>KL_1 | Top<br>KL_2 | Mid<br>KL_1 | Bot<br>KL_2 | Lw_1    |
|----------|---------|---------|---------|---------|---------|---------|-------------|-------------|-------------|-------------|---------|
| Res      | 0.954   | 0.951   | 0.912   | 0.916   | 0.956   | 0.963   |             |             |             |             |         |
| λ (nm)   | Ke_1    | KL_1    | Ke_2    | KL_2    | Ke_3    | KL_3    | Lw_1        | Lw_1        | Lw_2        | Lw_3        | Lwn     |
| 400      | 2.40E-1 | 2.05E-1 | 2.22E-1 | 1.86E-1 | 2.06E-1 | 1.68E-1 | 1.40E-1     | 1.37E-1     | 1.48E-1     | 1.50E-1     | 2.56E-1 |
| 410      | 2.39E-1 | 2.00E-1 | 2.19E-1 | 1.80E-1 | 2.00E-1 | 1.62E-1 | 1.52E-1     | 1.48E-1     | 1.60E-1     | 1.62E-1     | 2.71E-1 |
| 420      | 2.33E-1 | 1.88E-1 | 2.09E-1 | 1.68E-1 | 1.88E-1 | 1.51E-1 | 1.54E-1     | 1.50E-1     | 1.62E-1     | 1.64E-1     | 2.68E-1 |
| 430      | 2.25E-1 | 1.73E-1 | 2.00E-1 | 1.53E-1 | 1.77E-1 | 1.36E-1 | 1.40E-1     | 1.37E-1     | 1.47E-1     | 1.49E-1     | 2.40E-1 |
| 440      | 2.15E-1 | 1.58E-1 | 1.89E-1 | 1.39E-1 | 1.65E-1 | 1.22E-1 | 1.67E-1     | 1.63E-1     | 1.75E-1     | 1.78E-1     | 2.81E-1 |
| 450      | 1.98E-1 | 1.42E-1 | 1.73E-1 | 1.24E-1 | 1.50E-1 | 1.08E-1 | 2.06E-1     | 2.01E-1     | 2.17E-1     | 2.20E-1     | 3.42E-1 |
| 460      | 1.87E-1 | 1.30E-1 | 1.63E-1 | 1.12E-1 | 1.41E-1 | 9.68E-2 | 2.21E-1     | 2.16E-1     | 2.33E-1     | 2.36E-1     | 3.64E-1 |
| 470      | 1.75E-1 | 1.22E-1 | 1.53E-1 | 1.04E-1 | 1.33E-1 | 8.88E-2 | 2.32E-1     | 2.26E-1     | 2.43E-1     | 2.47E-1     | 3.76E-1 |
| 480      | 1.61E-1 | 1.12E-1 | 1.41E-1 | 9.56E-2 | 1.23E-1 | 8.12E-2 | 2.61E-1     | 2.55E-1     | 2.74E-1     | 2.79E-1     | 4.21E-1 |
| 490      | 1.52E-1 | 1.06E-1 | 1.33E-1 | 9.00E-2 | 1.17E-1 | 7.59E-2 | 2.62E-1     | 2.57E-1     | 2.76E-1     | 2.80E-1     | 4.19E-1 |
| 500      | 1.44E-1 | 1.08E-1 | 1.28E-1 | 9.17E-2 | 1.13E-1 | 7.68E-2 | 2.67E-1     | 2.61E-1     | 2.81E-1     | 2.85E-1     | 4.25E-1 |
| 510      | 1.41E-1 | 1.23E-1 | 1.28E-1 | 1.05E-1 | 1.17E-1 | 8.98E-2 | 2.57E-1     | 2.51E-1     | 2.70E-1     | 2.74E-1     | 4.09E-1 |
| 520      | 1.35E-1 | 1.31E-1 | 1.26E-1 | 1.13E-1 | 1.17E-1 | 9.77E-2 | 2.42E-1     | 2.37E-1     | 2.55E-1     | 2.59E-1     | 3.84E-1 |
| 530      | 1.29E-1 | 1.33E-1 | 1.22E-1 | 1.15E-1 | 1.16E-1 | 9.94E-2 | 2.54E-1     | 2.48E-1     | 2.67E-1     | 2.71E-1     | 4.04E-1 |
| 540      | 1.28E-1 | 1.39E-1 | 1.23E-1 | 1.21E-1 | 1.18E-1 | 1.05E-1 | 2.38E-1     | 2.33E-1     | 2.50E-1     | 2.54E-1     | 3.77E-1 |
| 550      | 1.32E-1 | 1.48E-1 | 1.28E-1 | 1.31E-1 | 1.23E-1 | 1.16E-1 | 2.21E-1     | 2.16E-1     | 2.32E-1     | 2.36E-1     | 3.51E-1 |
| 560      | 1.34E-1 | 1.51E-1 | 1.30E-1 | 1.36E-1 | 1.26E-1 | 1.23E-1 | 2.03E-1     | 1.99E-1     | 2.13E-1     | 2.17E-1     | 3.22E-1 |
| 570      | 1.42E-1 | 1.59E-1 | 1.38E-1 | 1.46E-1 | 1.34E-1 | 1.34E-1 | 1.78E-1     | 1.75E-1     | 1.88E-1     | 1.91E-1     | 2.85E-1 |
| 580      | 1.72E-1 | 1.84E-1 | 1.67E-1 | 1.72E-1 | 1.62E-1 | 1.61E-1 | 1.36E-1     | 1.34E-1     | 1.43E-1     | 1.46E-1     | 2.16E-1 |
| 590      | 2.32E-1 | 2.23E-1 | 2.25E-1 | 2.11E-1 | 2.19E-1 | 2.01E-1 | 8.18E-2     | 8.06E-2     | 8.60E-2     | 8.80E-2     | 1.29E-1 |
| 600      | 3.38E-1 | 2.89E-1 | 3.29E-1 | 2.50E-1 | 3.21E-1 | 2.17E-1 | 4.38E-2     | 4.16E-2     | 4.60E-2     | 4.55E-2     | 6.94E-2 |
| 610      | 3.79E-1 | 3.17E-1 | 3.72E-1 | 2.68E-1 | 3.66E-1 | 2.25E-1 | 3.33E-2     | 3.12E-2     | 3.50E-2     | 3.40E-2     | 5.24E-2 |
| 620      | 4.00E-1 | 3.06E-1 | 3.83E-1 | 2.82E-1 | 3.68E-1 | 2.61E-1 | 2.74E-2     | 2.65E-2     | 2.88E-2     | 2.90E-2     | 4.27E-2 |
| 630      | 4.19E-1 | 3.23E-1 | 4.01E-1 | 2.85E-1 | 3.84E-1 | 2.51E-1 | 2.44E-2     | 2.31E-2     | 2.56E-2     | 2.53E-2     | 3.76E-2 |
| 640      | 4.39E-1 | 3.43E-1 | 4.20E-1 | 2.84E-1 | 4.02E-1 | 2.33E-1 | 2.30E-2     | 2.13E-2     | 2.41E-2     | 2.32E-2     | 3.52E-2 |
| 650      | 4.64E-1 | 3.52E-1 | 4.43E-1 | 2.78E-1 | 4.25E-1 | 2.13E-1 | 2.04E-2     | 1.85E-2     | 2.15E-2     | 2.02E-2     | 3.10E-2 |
| 660      | 5.22E-1 | 3.39E-1 | 5.03E-1 | 2.52E-1 | 4.87E-1 | 1.76E-1 | 1.56E-2     | 1.39E-2     | 1.64E-2     | 1.52E-2     | 2.36E-2 |
| 670      | 5.73E-1 | 2.61E-1 | 5.49E-1 | 1.97E-1 | 5.28E-1 | 1.41E-1 | 1.73E-2     | 1.59E-2     | 1.82E-2     | 1.74E-2     | 2.59E-2 |
| 680      | 6.01E-1 | 2.16E-1 | 5.73E-1 | 1.67E-1 | 5.48E-1 | 1.23E-1 | 2.66E-2     | 2.49E-2     | 2.80E-2     | 2.72E-2     | 3.97E-2 |
| 690      | 6.25E-1 | 2.30E-1 | 6.15E-1 | 1.72E-1 | 6.06E-1 | 1.20E-1 | 1.98E-2     | 1.84E-2     | 2.08E-2     | 2.00E-2     | 2.94E-2 |
| 700      | 7.10E-1 | 2.75E-1 | 7.64E-1 | 1.95E-1 | 8.13E-1 | 1.24E-1 | 9.85E-3     | 8.86E-3     | 1.04E-2     | 9.68E-3     | 1.45E-2 |

Figure 4. Second page of the data report, attenuation coefficients and water-leaving radiances, produced by NOAA\_LIST.

which is sufficient for NOAA MOS or SIS spectra; 4 indicates use of `MLML_DBASE DATA_TYPE 4`, being `REAL*4` values having about 7 significant digits; the second 4 indicates the `DATA_ELEMENT_SIZE` as 4 bytes; and 2000 sets the File Header Extension size to be 2000 bytes. The File Header Extension holds derived products, and Appendix 5 shows the details of the extension variables.

Two methods access the above programs from `PLOT`:

1. At the `ML>` prompt type "NOAA" to print a menu and display the `NOAA>` prompt.
2. At the `ML>` prompt type "NOAA" followed by the program name or number.

Typing `EXIT` or 0 at the `NOAA>` command line exits back to `PLOT` prompt, `ML>`, and entering an empty `RETURN` at `NOAA>` redisplays the menu shown below. As with the `PLOT` program, DCL commands can be run from the `NOAA>` prompt by preceding them with a \$, or a DCL "shell" can be run by typing \$ `RETURN`.

To display the main NOAA processing menu:

```
ML> NOAA
```

Notice that the prompt changes to NOAA, and that NOAA program names or numbers rather than the PLOT program names are in use.

```
NOAA: NOAA/MLML Radiometric Data Processing
rev. 24-May-1993
```

| #  | Command | Description                       |
|----|---------|-----------------------------------|
| 1  | CONVERT | Apply Sys Resp, Immr Factor       |
| 2  | EDIT    | Replace Erroneous Data with NaN   |
| 3  | SMOOTH  | Apply N Point Running Mean Smooth |
| 4  | ADJUST  | Ave Rad & Drk,%Err,rad-drk,SNR    |
| 5  | AVERAGE | Average Spectral Mean & %Err      |
| 6  | MERGE   | Collect Es, Ed, Lu's in one place |
| 7  | CLIP    | Replace SNR < 100:1 Data with NaN |
| 8  | DERIVE  | Ke,KI,Lw,Lwn,SeaWiFS Weights,PAR  |
| 9  | GRAPH   | Plot 2-Page, 3-Panel Graphs       |
| 10 | LIST    | Radiometric Data Report Listing   |
| 0  | EXIT    |                                   |
|    | NOAA>   |                                   |

To exit from `NOAA>`:

```
NOAA> EXIT
```

or

```
NOAA> 0
ML>
```

To start the `SMOOTH` program, for example:

```
ML> NOAA SMOOTH
```

or

```
ML> NOAA 3
```

...

NOAA programs will prompt the user for necessary input. Typing `CTRL Z` in response to a prompt exits that program without processing data. Many prompts provide default values which can be accepted, modified or re-entered. Program input requests can be satisfied by passing parameters to the program when it is started. When passing parameters to a program, default inputs can be accepted by typing the wildcard \* in place of the specific *Variable* or *Element* ranges. It is best to run a program through the interactive mode the first time to understand what input needs are required and what default values are provided. For example, `SMOOTH` prompts for the *Variable* list to be smoothed and the number of points to use for the smoothing window. `SMOOTH` provides 5 as the default window size. Input requests from `SMOOTH` can be answered in several ways:

1. Starting `SMOOTH` from the main `NOAA>` command line:

```
ML> NOAA
(--- NOAA main menu printed here ---)
NOAA> SMOOTH
NOAA_SMOOTH Enter Range of Variable # to Smooth:
2-10
NOAA_SMOOTH Enter # of Elmts/Window (odd):
5
Working...
Done.
```

2. Starting `SMOOTH` from the `ML>` command line:

```
ML> NOAA SMOOTH
NOAA_SMOOTH Enter Range of Variable # to Smooth:
2-10
NOAA_SMOOTH Enter # of Elmts/Window (odd):
5
Working...
Done.
```

3. Passing input to `SMOOTH`:

```
ML> NOAA
(--- NOAA main menu printed here ---)
NOAA> SMOOTH
2-10 7
```

Working...  
Done.

or

ML> NOAA SMOOTH 2-10 7  
Working...  
Done.

#### 4. To use the default *SMOOTH* window size (5):

ML> NOAA SMOOTH 2-10 \*  
Working...  
Done.

The following paragraphs define the user interface and some details of processing algorithms and data handling for each of the *NOAA* programs.

### MLML\_NOAA

The main *NOAA* program provides an interface to the ten radiometric data processing programs. The tasks of *NOAA* are four:

1. *NOAA* displays the processing menu and the *NOAA>* prompt (see example above), reads and parses user commands.
2. *NOAA* handles any parameters passed from *PLOT*.
3. *NOAA* handles any parameters passed to subprograms.
4. *NOAA* runs its subprograms.

The menu contents and physical location of subprogram code is known to *NOAA* via the ASCII file *NOAA\_MAIN\_MENU.DAT* (see Appendix 4). This file contains three lines for each subprogram: line 1 = program name; line 2 = program description; line 3 = complete VMS filename of program. *NOAA* reads this file, prints the name and description information to the user's terminal in a menu format, and uses the VMS filename to run subprograms. *NOAA\_MAIN\_MENU.DAT* can be updated to add, delete, or change the name, description, or location of a *NOAA* subprogram.

### Programming Details

A temporary disk file is used to pass parameters between separate programs because FORTRAN does

not allow directly for passing arguments to a main program. The existence of the temporary parameter file is known to separate program units via the VMS logical *MLML\_DBASE\_PARAMETER* in a VMS logical table (Appendix 3). Managing parameter files constitutes most of *NOAA*'s work. If input is passed from *PLOT*, this information is extracted from the parameter file for interpretation by a subroutine. The name of the parameter file is retrieved from the VMS logical and saved, freeing the logical to be used, if necessary, to pass parameters to subprograms. Before exiting back to *PLOT*, the original parameter filename is replaced in the logical and returned to *PLOT*. If it is necessary for *NOAA* to pass parameters to a subprogram, it creates a temporary parameter file, writes information to the file, calls the subprogram, then deletes the file after the subprogram is finished.

If all the *NOAA* programs were coded as subroutines, *NOAA* would not have to pass parameters via external files. As separate programs, however, command line mode is enabled from both the *ML>* and *NOAA>* levels. This is convenient for an advanced user who may write batch mode command files from *ML>*, and for the novice user who runs the *NOAA* programs by passing parameters within the *NOAA* processing environment. As individual programs, the processing routines are also accessible to future high-level application programs, and the increased modularity facilitates program modification and maintenance.

### NOAA\_CONVERT

*CONVERT* applies a system response and/or immersion correction factor to SIS and MOS data. *CONVERT* has three prompts:

*NOAA> CONVERT*

*NOAA\_CONVERT:* Apply System Response  
rev. 22-Jul-1993

*NOAA\_CONVERT:* Enter Response Filename:  
[DATA:NOAA:MOCE\_2]PRECAL

*NOAA\_CONVERT:* Enter Response Var # to Use: 2

*NOAA\_CONVERT:* Enter Range of Var #'s to Convert: 4-8

Working...  
Done.

The system response,  $h(\lambda)$ , is a spectral multiplier used to convert raw units of MOS or SIS radiance

scans  $C(\lambda)$  and dark scans  $D(\lambda)$  (both in counts) to radiometric units of radiance  $L(\lambda)$  ( $\mu\text{W}/\text{cm}^2/\text{sr}/\text{nm}$ ) or irradiance  $E(\lambda)$  ( $\mu\text{W}/\text{cm}^2/\text{nm}$ ) for integration times,  $\Delta t$ . Multipliers are

$$L(\lambda) = \frac{C(\lambda) - D(\lambda)}{\Delta t} F_w(\lambda) h(\lambda) \quad (1)$$

determined via laboratory calibration of  $L_u$ ,  $E_d$  and  $E_s$  sensors. The immersion factor,  $F_w(\lambda)$ , is a spectral multiplier necessary when the calibration situation is different from that of the field-measurement. When measuring  $L_u$  and  $E_d$  underwater, the difference between the indices of refraction for air and water is accounted for by  $F_w(\lambda)$ . Immersion factors are only applied to MOS data. The air-water  $F_w(\lambda)$  for radiance is calculated from values for indices of refraction for fused quartz (MOS radiance port), with seawater salinity of 35 PSU and temperature of 16°C (Austin, 1976). The immersion factor for irradiance must be empirically determined; we use data from Tyler and Smith (1970) for the Scripps Spectroradiometer. The radiance immersion factors are listed in Appendix 4.

## NOAA\_EDIT

Erroneous data generated by "bad" pixels in a silicon diode array detector must be removed and replaced with a missing-data code, i.e. NaN "Not a Number". All other processing routines check for the presence of NaN and skip processing of such *Elements*. *EDIT* prompts the user for *Variable* and *Element* ranges to be replaced.

NOAA> EDIT

NOAA\_EDIT: Replace Bad Data  
rev: 22-Jul-1993

NOAA\_EDIT: Enter Range of Var #'s to Edit:  
2-10

NOAA\_EDIT: Enter Range of Element #'s to Edit:  
406,415-419,483-502

Working...  
Done.

Currently, MOS has three unusable areas on the Blue array and one on the Red array for a total of 25 bad pixels out of 1024. These known *Elements* are the default response to the second prompt. There is currently no need to *EDIT* SIS data. In the *Variable Header Extension*, *NUM PTS EDITED* is updated with the number of bad points edited (see Appendix

5 for SIS and MOS *Extension* structures.)

## NOAA\_SMOOTH

MOS's holographic diffraction grating disperses a bandwidth of approximately 300 nm onto a 512 diode array detector, giving a potential spectral resolution of 0.6 nm. However, to increase sensitivity, a 250  $\mu\text{m}$  wide spectrograph entrance slit leads to a 2.6 nm or 4 pixel bandwidth. This allows the option to *SMOOTH* MOS data to reduce standard error without loss of spectral information. *SMOOTH* applies an N-point running-mean, even-weight smoothing function. The user is prompted to select which *Variable* to smooth and the number of points to use for window size.

NOAA> SMOOTH

NOAA\_SMOOTH: N-Point Running Mean Smooth  
rev: 22-Jul-1993

NOAA\_SMOOTH: Enter Range of Variable #'s to Smooth:  
2-8

NOAA\_SMOOTH: Enter # Points for Window (odd):  
5

Working...  
Done.

A five point window is the default and is typically used. *SMOOTH* skips the first and last  $N/2$  points, takes N *Elements* centered around each point, replaces any NAN's with the mean of surrounding elements, and sums the weighted N data to replace the middle *Element*. SIS  $E_s$  spectra are not smoothed.

$$\bar{X} = \sum_{j=1}^{j=M} \frac{X(\lambda_j)}{M} \quad (2)$$

Applying a running mean smooth with a 5 point window does not change the first and last 2 data *Elements*. For example, a simple 5 point spectra smoothed with a 5 point window would only update the third point.

| Before: | After:  |
|---------|---------|
| N       | $L_w$   |
| 1       | 2.47E-1 |
| 2       | 2.45E-1 |
| 3       | 2.45E-1 |
| 4       | 2.42E-1 |
| 5       | 2.39E-1 |

**NOAA\_ADJUST**

A typical SIS or MOS file or scan-set contains ten *Variables*: one wavelength, two dark scans, five radiance or irradiance scans, and two more dark scans. *ADJUST* averages and calculates the relative error of the four spectral dark *Variables*, averages and calculates relative error for radiance, subtracts average dark from average radiance, then calculates Signal to Noise Ratio, SNR. The user is prompted for *Var#*'s of wavelength, dark, and radiance data, and *Var#*'s to save the six output spectra (saving to *Var# 0* means do not save.)

NOAA&gt; ADJUST

NOAA\_ADJUST: SIS/MOS Radiometer Data Processing  
rev. 22-Jul-1993

NOAA\_ADJUST: Enter Wavelength Variable #: 1  
 NOAA\_ADJUST: Enter Range of Radiance Var #'s: 4-8  
 NOAA\_ADJUST: Enter Range of Dark Var #'s: 2,3,9,10  
 NOAA\_ADJUST: Enter Var #'s to Save: Avr.Rad, %Err, Avr.Drk, %Err, Rad.Drk, SNR 11-16  
 NOAA\_ADJUST: Divide by MOS Integration Time (Y/N): Y

Working...  
Done.

Relative error is calculated as the spectral quantity, root mean square error, RMSE:

$$RMSE = \sqrt{\frac{\sum_{i=1}^{i=N} [X_i(\lambda) - X_m(\lambda)]^2}{N}}$$

$$X_m(\lambda) = \frac{\sum_{i=1}^{i=N} X(\lambda)}{N} \quad (3)$$

where  $X(\lambda)$  represents radiances from the  $N$  scans. For SNR, the *signal* equals the radiance less the dark counts, while *environmental noise* is given by the error in radiance:

where  $L_M(\lambda)$  is the mean radiance or irradiance,

$$SNR(\lambda) = \frac{L_M(\lambda) - L_D(\lambda)}{RMSE_L(\lambda)} \quad (4)$$

$L_D(\lambda)$  is the mean radiance or irradiance dark count and  $RMSE_L(\lambda)$  is the RMSE from Eq. 3. For MOS *Variables*, data are optionally divided by the integration time. The SIS integration time is constant.

The average percent errors in the eight SeaWiFS bands are saved in the *Variable Header Description* of each %RMSE spectra. These eight mean errors are used as an indicator of "goodness" for the radiance or dark data. Also updated are the *Variable Header Extensions*: all analog values are averaged and saved. This is necessary, for example, to record with the Rad-Drk *Variable* the average depth of a MOS scan-set or the average time of a SIS surface irradiance scan-set. Average depth is read from the *Extension* during the *DERIVE* step to calculate diffuse attenuation coefficients (below). *Variable Header* scale parameters are setup and saved to allow for easy plotting.

**NOAA\_AVERAGE**

When more than one MOS scan-sets at a particular depth are to be used, or several surface irradiance SIS sets taken at different times need combining, data can be spectrally averaged via *AVERAGE*. This program prompts the user to enter the *Var#*'s to be averaged and the *Var#*'s to save the mean and %RMSE. These results will not be saved if *Var# 0* is selected.

NOAA&gt; AVERAGE

NOAA\_AVERAGE: Spectral Mean & %RMSE of Vars  
rev. 22-Jul-1993

NOAA\_AVERAGE: Enter Wavelength Var #: 1  
 NOAA\_AVERAGE: Enter Range of Var #'s to Average: 2-3,9-10  
 NOAA\_AVERAGE: Enter Var # to save Mean: 11  
 NOAA\_AVERAGE: Enter Var # to save %RMSE: 12  
 Working...  
Done.

Averages are calculated across rows to preserve spectral information. Analog data in *Variable Header Extensions* are also averaged and saved with the mean

*Variable's Extension.* Again, eight mean %RMSE's corresponding to the SeaWiFS bands are calculated as a quality index and saved in the %RMSE *Variable Header Description*.

## NOAA\_MERGE

The *MERGE* program assists the user in combining processed *Archive* files containing  $L_u$ ,  $E_d$ , and  $E_s$  data into *Workspace Variables* ready for the *DERIVE* step. The *MERGED Variable* order is:

### Variable #

1. MOS Corrected Wavelength
2. SIS Corrected Wavelength
- 3,4. MOS surface  $E_d$  and SNR
- 5,6. SIS  $E_s$  and SNR for Top  $E_d$
- 7,8. MOS surface  $L_u$  and SNR
- 9,10. SIS  $E_s$  and SNR for Top  $L_u$
- 11-18. Mid data as *Var#* 3-10
- 19-26. Bot data as *Var#* 3-10.

MOS *Variables* hold 1000 *Elements* (500 pixels from each of the two diode arrays) and SIS contain only 48 (38 scan channels plus 10 references). This is why both MOS and SIS wavelength *Vars* are needed. Merge works on the manually edited MERGE.LIS;2 file that was assembled during preprocessing (page 6).

NOAA> MERGE

NOAA\_MERGE: Load Radiometric Archive  
rev: 22-Jul-1993

NOAA\_MERGE:

Enter Filename:  
MERGE.LIS;1

Loading...

## NOAA\_CLIP

This program allows spectral data with a SNR less than 100:1 to be replaced with NaN. *CLIP* prompts the user for the *Variable* range to be clipped and the value of the SNR cutoff to be used.

NOAA> CLIP

NOAA\_CLIP: Replace Data if SNR < 100:1  
rev: 22-Jul-1993

NOAA\_CLIP:

Enter Range of Var #'s to Clip:  
1-25:2  
2-26:2

NOAA\_CLIP:

Enter SNR cutoff:  
100

Working...  
Done.

## NOAA\_DERIVE

From  $L_u$ ,  $E_d$ , and  $E_s$  *Variables* 1-26, *DERIVE* calculates diffuse attenuation coefficients  $K_L$  and  $K_E$ , solar-normalized water-leaving radiance,  $L_{WN}$ , SeaWiFS-weighted solar-normalized water-leaving radiances in eight SeaWiFS bands, and other products such as PAR and solar inclination.  $K$ 's are calculated between depths for a pair of  $L_u$  or  $E_d$ 's and are corrected for differences in associated  $E_s$ 's.  $K$ 's are calculated between the Top and Mid depths, between Top and Bot, and between Mid and Bot. Water-leaving radiance is obtained by attenuating  $L_u$  to just below the sea surface using a  $K_L$ , then propagating  $L_{u,0}$  across the water-air interface. Four such  $L_w$ 's are calculated: using the  $L_u$  Top with  $K_{L\_Top-Mid}$  and  $K_{L\_Top-Bot}$ ; using  $L_u$  Mid with  $K_{L\_Top-Mid}$ ; and the  $L_u$  Bot with  $K_{L\_Top-Bot}$ .

Between observation depths,  $z_1$  and  $z_2$ , irradiance is assumed to attenuate by a first-order absorption and scattering with a constant attenuation coefficient,  $K$ ,

$$\frac{E_{z_2}}{E_{z_1}} = e^{-K(z_2 - z_1)} \quad (5)$$

The diffuse attenuation coefficient is calculated by Eq. 6, where  $K$  denotes either  $K_L$  or  $K_E$ ;  $X$  denotes either  $L_u$  or  $E_d$  spectral data;  $Z$  are depths, and subscripts 2 and 1 indicate the deeper and shoaler depths, respectively.  $R_N$  (Eq. 7) is the incident

$$K = -\frac{\ln\left(\frac{X_2 R_{N2}}{X_1 R_{N1}}\right)}{(z_2 - z_1)} \quad (6)$$

irradiance normalization ratio determined from mean, spectrally-smoothed  $E_s$ , one ( $E_{s1}$ ) for the shoaler  $E_d$  or  $L_u$ , the other ( $E_{s2}$ ) for the deeper  $E_d$  or  $L_u$ .  $K$  cannot be derived if either of the two  $L_u$  or  $E_d$  scans or their corresponding surface irradiances  $E_s$  are missing.  $E_{sr}$  is the reference surface irradiance. This will normally be  $E_s$  taken for the surface-most (i.e. Top) scans.

$$\begin{aligned} R_{N1} &= \frac{E_{sx}}{E_{s1}} \\ R_{N2} &= \frac{E_{sx}}{E_{s2}} \end{aligned} \quad (7)$$

The depths of  $L_u$  and  $E_d$  scans are retrieved from *Variable Header Extension* analog data, converted to pressure units (dbar), corrected for "deck" pressure offset, and corrected for pressure offset between the sensor and pressure transducer.  $E_s$  spectra are used to normalize  $L_u$  and  $E_d$  scans taken under potentially different sky conditions.  $L_u$  and  $E_d$  are normalized to the time of the surface-most  $E_s$  scan. Normalization factors,  $R_N$ , can be calculated as a mean ratio or spectral ratio. For mean normalization,  $E_s$  spectra are summed across wavelengths, divided by the number of *Elements*, then ratioed. A spectral ratio is cubic spline interpolated to MOS wavelengths. If a spectral  $R_N$  ratio is used, however, MOS wavelengths outside the  $E_s$  bandwidth cannot be normalized and are replaced with NaN's.

Water-leaving radiance,  $L_w$ , is calculated by extrapolating a radiance spectrum from one Evening: (observation depth to the surface:

$$\begin{aligned} L_w &= 0.543 L_u e^{K_L(z_2 - z_1)} \\ 0.543 &= \frac{(1 - R_F)}{n_w^2} \end{aligned} \quad (8)$$

where  $R_F$  is water-air Fresnel reflectance and  $n_w$  is the index of refraction for salinity of 35 PSU.  $L_w$  cannot be calculated if any one of  $E_s$ ,  $L_u$  or  $K_L$  is missing.  $L_w$ 's can be solar normalized by the solar normalization factor,  $F_N$ , which is a function of

$$L_{WN} = \frac{L_w}{F_N} \quad (9)$$

atmospheric Rayleigh and ozone optical thicknesses,  $\tau_R$  and  $\tau_{oz}$ , solar zenith angle,  $\theta_0$ , and earth-sun distance,  $r_{es}$  (Eqs. 9,10,11).

The normalized SeaWiFS response functions, Wt1...Wt8, (Appendix 6) are applied by their spectral multiplication with the solar-normalized water-leaving radiances.

$$F_N = \frac{t(\lambda, \theta_0)(1 - \rho(\theta_0)) \cos(\theta)}{r_{es}^2} \quad (10)$$

$$t(\lambda, \theta_0) = \exp\left(-\frac{0.5 \tau_R + \tau_{oz}}{\cos(\theta_0)}\right)$$

The earth-sun distance  $r_{es}$  in astronomical units is given approximately by Eq. 11, where D is the Julian day of the year, and the solar zenith angle  $\theta_0$  is

$$r_{es} = 1 + 0.0167 \cos\left(\frac{2\pi(D-3)}{365}\right) \quad (11)$$

determined from time of the Top  $L_{WN}$ , station latitude and longitude from MLML DBASE library procedures based on the solar ephemeris of Von Flandern and Pulkkinen (1979).

The eight SeaWiFS-weighted solar-normalized water-leaving radiances along with the Photosynthetically active radiation, PAR (Eq. 12), the solar zenith angle, and earth-sun distance are saved in the MOS *File Header Extensions*.

$$PAR = \sum_{\lambda=400}^{\lambda=700} \frac{\lambda}{hC} E(\lambda) d\lambda \quad (12)$$

All 41 *Variables* are setup with *Header* information and scale parameters tailored to the *Var* type and units. Default scale ranges are set for  $L_u$ ,  $E_d$ ,  $E_s$  and  $L_w$ 's while  $K_L$  and  $K_E$  scales are adjusted for their ranges. Time of each  $E_s$  set is retrieved from *Var Header Extension*, converted, formatted, and saved in the *Var's* description. Converted and corrected depth of each  $L_u$  and  $E_d$  scan is saved in their *Var* descriptions. If average incident ratios were used, the  $R_N$  value is recorded with the diffuse attenuation *Var* description.

Because all variables have been formed by previous

processing the *DERIVE* program requires only two input arguments and operates on the currently loaded data:

NOAA> DERIVE

NOAA\_DERIVE: Derived Radiometric Parameters:  
rev: 22-Jul-1993

Var# 1-26: Lambda\*2; Ed,SNR,Es,SNR,Lu,SNR,Es,SNR\*3  
Derives Var# 27-41: Ke,Kl \*3; Lw \*4; Lwn \*4

NOAA\_DERIVE: Enter Data Units 1=Raw 2=Cnvrtd:  
1  
NOAA\_DERIVE: Enter Ratio Type 1=Mean 2=Spcrtl:  
1

Working...  
Done.

## NOAA\_GRAPH

Graphical output of spectral data is provided via *GRAPH* (Figs 1 and 2). Plots can be sent to a graphics terminal or PostScript file or printer. Color or black-and-white plots are available. Two pages are produced, each with three X-Y plots. Page one shows  $E_d$ ,  $L_u$  and  $E_s$  (Fig. 1), and page two shows  $K_E$ ,  $K_L$  and  $L_w$  (Fig. 2). X-axis wavelength range is selectable as either full-scale, 300 to 900 nm, or clipped, 400 to 700 nm. Y-axis units are selectable between raw units (counts/sec) and (counts), or converted units ( $\mu\text{W}/\text{cm}^2/\text{nm}$ ) and ( $\mu\text{W}/\text{cm}^2/\text{sr/nm}$ ). Cruise and station name, position and date (found in *File Header* strings# 1 to 3) are labeled on each page, and the user can enter an optional page title and footer to be printed. *Vars* 1 to 36 are assumed to be in the order previously described, however empty *Vars* are acceptable and do not plot.

NOAA> GRAPH

NOAA\_GRAPH: 2-Page 3-Panel Radiometric X-Y Plots  
rev: 22-Jul-1993

NOAA\_GRAPH: Enter Output Port  
(1=FALCO 2=\$LASER: 3=\$LJ4: 4=File):  
1

NOAA\_GRAPH: Enter Data Units (1=Raw, 2=Cnvrtd): 1  
NOAA\_GRAPH: Enter Wavelength Range  
(1=300-900, 2=350-750 nm):  
1

NOAA\_GRAPH: Enter Title for each page:  
MODIS Marine Optical Characterization Experiment 1  
NOAA\_GRAPH: Enter Bottom Left Footer:  
MLML 23 Jul 93

NOAA\_GRAPH: Color Plot? (Y/N)  
Working... N

Plotting data...  
Done.

## NOAA\_LIST

Tabular output of spectral data is provided by *LIST*. The output device is selectable as either the user's terminal, a printer, or an ASCII file. *LIST* prints columns of user selectable  $E_d$ ,  $L_u$ ,  $E_s$ ,  $K_E$ ,  $K_L$ ,  $L_{wsn}$  data and rows of wavelengths at user specified intervals. Two such tables are normally produced: the first showing observed radiance and irradiance spectra for the Top, Mid and Bot depths (Fig. 3); the other showing derived attenuation coefficient and water-leaving radiance spectra (Fig. 4). Cruise and station information is labeled at the top of each page along with Secchi disk depth, Munsell color, SeaWiFS-weighted solar-normalized water-leaving radiances, PAR, solar zenith angle, and an optional user-entered title and page footer.

NOAA> LIST

NOAA\_LIST: Radiometric Data Report Listing  
rev: 22-Jul-1993

NOAA\_LIST: Change Output Device or File? (Y/N):  
N

NOAA\_LIST: Enter Range of Var #'s to List:  
??

NOAA\_LIST: Enter Wavelength Interval to List:  
??

NOAA\_LIST: Enter Title for each page:  
MODIS Marine Optical Characterization Experiment 1 L

Working...  
Done.

## Batch Mode Processing

NOAA/MLML data processing may be done in batch-mode to automate repetitive steps. A text file is created containing keystrokes used to invoke the *NOAA* programs and respond to program prompts. For example, a raw MOS scan-set is loaded and the first four processing programs run sequentially by the following batch file:

```
! Load the raw scan-set from disk Archive file
load
!
! apply MOS system response to Var#'s 2-10
noaa convert mos_response 2 2-10
!
! apply MOS immersion factor to Var#'s 2-10
noaa convert mos_response 3 2-10
!
```

```

! throw out MOS bad data in Var#'s 2-10
noaa edit **

!
! smooth w/ 5 pt running mean Var#'s 2-10
noaa smooth 2-10 *

!
! subtract dark counts, get %Error
noaa adjust *****
!

! plot the results
graph
!
! record processed set
record

```

Other batch files can be created to process SIS sets, *AVERAGE* multiple sets, *MERGE* processed sets, and *DERIVE* radiometric quantities. If the above file's name is PROC1.MLCOM, it is run by typing:

```
ML> @PROC1.MLCOM
```

Any lines beginning with the exclamation mark in a batch file are comments and are not executed. When a *PLOT* or *NOAA* command is missing a parameter, or is supplied an improper parameter, the program will prompt the user for necessary input. In the above batch file, for example, the *LOAD* command will prompt the user for the filename and *Variable* range to load, and at which *Workspace Variable* to begin loading. Notice the use of asterisks (\*) to use default values.

## **NOAA\_PROCESS**

Batch file processing can be automated for a set of file names by using the *ALIAS* command. If the *ALIAS* file SIS.ALIAS is created at the VMS command level,

```
$ ALIAS *SIS*.MLDAT SIS
```

then all the files referenced by SIS.ALIAS can be manipulated by *NOAA\_PROCESS* program. The aliased files are referenced by an apostrophe followed by the alias file name, for example,

'SIS.ALIAS'

The *NOAA\_PROCESS* program can invoke all *NOAA* programs (Table 1), which derive much of their flexibility from their ability to operate on lists of files.

## **Acknowledgements**

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## Appendix 1. SeaWiFS standard radiometry symbols.

|                        |                                                                                                                                                                                                                                                                                                                                                                                                 |
|------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| $E_d(z, \lambda)$      | Downwelled spectral irradiance at depth = $z$ ( $\mu\text{W}/\text{cm}^2/\text{nm}$ )                                                                                                                                                                                                                                                                                                           |
| $E_u(z, \lambda)$      | Upwelled spectral irradiance at depth = $z$ ( $\mu\text{W}/\text{cm}^2/\text{nm}$ )                                                                                                                                                                                                                                                                                                             |
| $L_u(z, \lambda)$      | Upwelled spectral radiance at depth = $z$ ( $\mu\text{W}/\text{cm}^2/\text{nm}/\text{sr}$ )                                                                                                                                                                                                                                                                                                     |
| $E_s(\lambda)$         | Surface spectral irradiance ( $\mu\text{W}/\text{cm}^2/\text{nm}$ ) measured on ship well above the water                                                                                                                                                                                                                                                                                       |
| $E_s(t, \lambda)$      | Surface spectral irradiance measured at time = $t$ ( $\mu\text{W}/\text{cm}^2/\text{nm}$ )                                                                                                                                                                                                                                                                                                      |
| $E_d(0^-, \lambda)$    | Surface incident spectral irradiance ( $\mu\text{W}/\text{cm}^2/\text{nm}$ ) in-water measurement at infinitesimal depth below surface ( $z = 0^-$ ) extrapolated from $E_d(z, \lambda)$ estimated by propagating $E_s(\lambda)$ through the sea surface from a radiometer floated just below the surface ( $z = z_r$ ) varies due to fluctuations in cloud cover and aerosols, and time of day |
| $L_u(0^-, \lambda)$    | Upwelled spectral radiance ( $\mu\text{W}/\text{cm}^2/\text{nm}/\text{sr}$ ) in-water measurement at infinitesimal depth below surface ( $z = 0^-$ ) extrapolated from $L_u(z, \lambda)$                                                                                                                                                                                                        |
| $K(z, \lambda)$        | Spectral diffuse attenuation coefficient (1/m)                                                                                                                                                                                                                                                                                                                                                  |
| $K_E(z, \lambda)$      | Spectral diffuse attenuation coefficient for downwelled irradiance (1/m) derived from $E_d(z, \lambda)$ measured over upper few optical depths                                                                                                                                                                                                                                                  |
| $K_L(z, \lambda)$      | Spectral diffuse attenuation coefficient for upwelled radiance (1/m) derived from $L_u(z, \lambda)$ measured over upper few optical depths                                                                                                                                                                                                                                                      |
| $K_d(z, \lambda)$      | Spectral diffuse attenuation coefficient for downwelled irradiance (1/m)                                                                                                                                                                                                                                                                                                                        |
| $K_u(z, \lambda)$      | Spectral diffuse attenuation coefficient for upwelled irradiance (1/m)                                                                                                                                                                                                                                                                                                                          |
| $\tau(z, \lambda)$     | Spectral optical depth integral of $K(z, \lambda)$ (for either radiance or irradiance depending on context) from the surface to a given depth $z$                                                                                                                                                                                                                                               |
| $\tau_{oz}$            | Atmospheric ozone optical thickness                                                                                                                                                                                                                                                                                                                                                             |
| $\tau_R$               | Atmospheric Rayleigh optical thickness                                                                                                                                                                                                                                                                                                                                                          |
| $L_W(\lambda)$         | Water-leaving radiance ( $\mu\text{W}/\text{cm}^2/\text{nm}/\text{sr}$ ) "measured" via propagating $L_u(0^-, \lambda)$ upward through sea surface                                                                                                                                                                                                                                              |
| $L_{WN}(\lambda)$      | Normalized water-leaving radiance ( $\mu\text{W}/\text{cm}^2/\text{nm}/\text{sr}$ ) derived for clear-sky zenith sun at mean earth-sun distance                                                                                                                                                                                                                                                 |
| $L_u(z, \theta, \phi)$ | Submerged upwelled radiance distribution ( $\mu\text{W}/\text{cm}^2/\text{nm}/\text{sr}$ )                                                                                                                                                                                                                                                                                                      |
| $R_L(z, \lambda)$      | Remote sensing reflectance $L_U(z, \lambda)/E_d(z, \lambda)$                                                                                                                                                                                                                                                                                                                                    |
| $F_i(\lambda)$         | Immersion correction factor (for radiance or irradiance)                                                                                                                                                                                                                                                                                                                                        |

## Appendix 1. (continued) SeaWiFS standard radiometry symbols.

---

|                           |                                                                                                                                                                                         |
|---------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| $h(\lambda)$              | Sensor response function                                                                                                                                                                |
| $n_w(\lambda)$            | Spectral index of refraction of seawater                                                                                                                                                |
| $T_a(\lambda)$            | Spectral solar atmospheric transmission                                                                                                                                                 |
| $T_s(\lambda)$            | Spectral transmittance through the surface                                                                                                                                              |
| $T_w(\lambda)$            | Spectral transmittance through a water path                                                                                                                                             |
| $a(z,\lambda)$            | Spectral absorption coefficient (inherent optical property, IOP)(1/m)                                                                                                                   |
| $b(z,\lambda)$            | Total spectral scattering coefficient (IOP) (1/m)                                                                                                                                       |
| $c(z,\lambda)$            | Spectral beam attenuation coefficient (IOP) (1/m)                                                                                                                                       |
| $b_b(z,\lambda)$          | Spectral backscattering coefficient (IOP) (1/m)                                                                                                                                         |
| $b_r(\lambda)$            | Total Raman scattering coefficient (1/m)                                                                                                                                                |
| $\beta(z,\lambda,\theta)$ | Spectral volume scattering function (IOP) (1/m)                                                                                                                                         |
| $Q(\lambda)$              | $L_u(0^{\circ},\lambda)$ to $E_d(0^{\circ},\lambda)$ relation factor not well determined at present (theoretically equal to $\pi$ )<br>Assumed equal to 5 at all wavelengths and depths |
| $\theta_0$                | Solar zenith angle                                                                                                                                                                      |
| $t(\lambda,\theta_0)$     | Diffuse spectral atmospheric transmittance                                                                                                                                              |
| $r_{es}$                  | Earth-sun distance (astronomical units)                                                                                                                                                 |
| $\rho(\theta_0)$          | Fresnel reflectance for the air-water interface at incident angle $\theta_0$                                                                                                            |

---

Adapted from Mueller, et al. 1991.

---

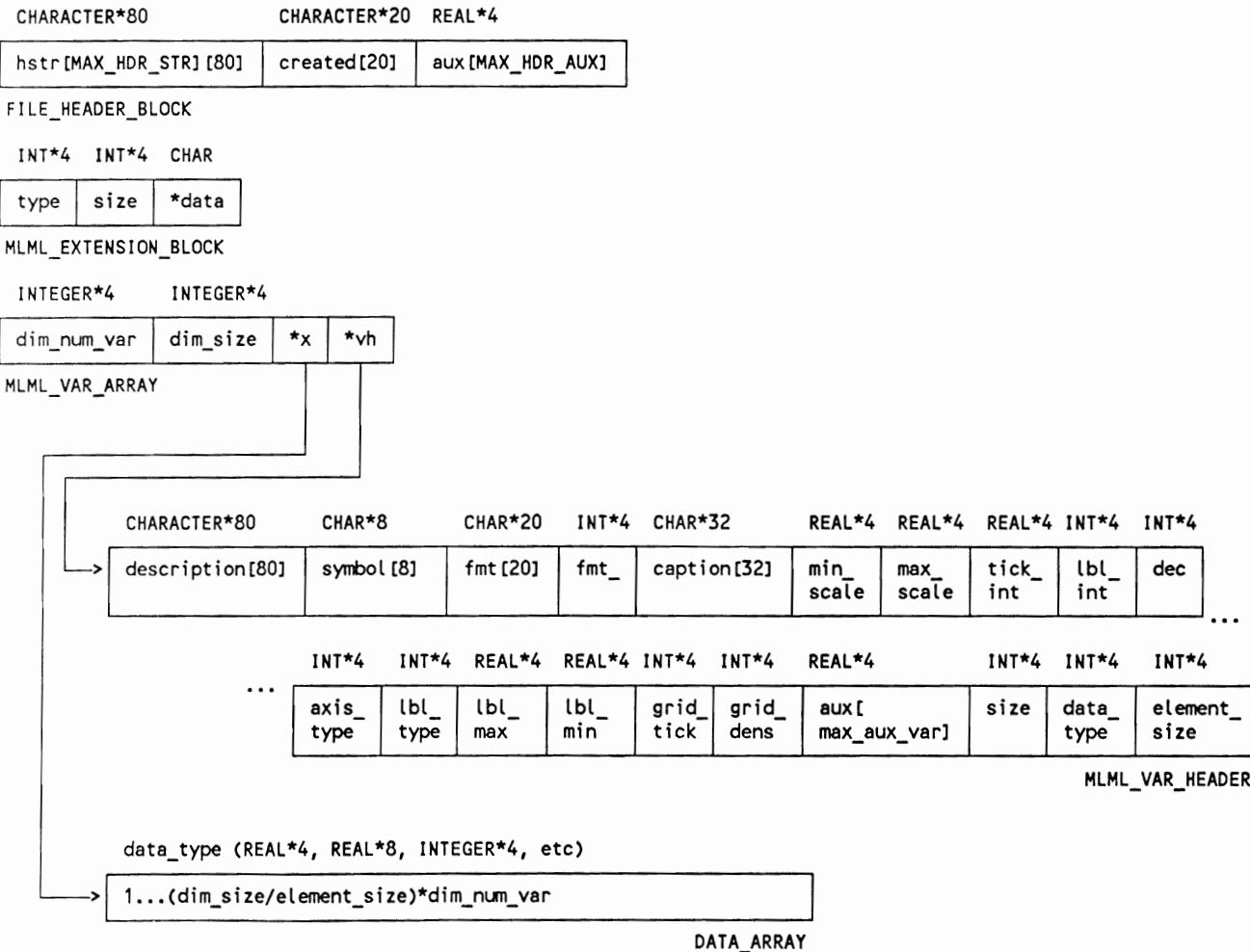
**Appendix 2. Glossary of acronyms used in text.**

---

|         |                                                                |
|---------|----------------------------------------------------------------|
| Bot     | Bottom or deepest sampling depth at a radiometer station       |
| CTD     | Conductivity, temperature and depth profiling instrument       |
| CZCS    | Costal Zone Color Scanner                                      |
| FOV     | Field-of-view                                                  |
| FLH     | Fluorescent line height at 685 nm                              |
| FWHM    | Full-width half-maximum                                        |
| HPLC    | High performance liquid chromatography                         |
| IOP     | Inherent optical properties                                    |
| IR      | Infrared                                                       |
| Mid     | Middle sampling depth at a radiometer station                  |
| MLML    | Moss Landing Marine Laboratories                               |
| MOBY    | Marine Optical Buoy                                            |
| MOCE    | Marine Optical Characterization Experiment                     |
| MOS     | Marine Optical System                                          |
| NAN     | Not a Number, an IEEE standard value to represent missing data |
| NASA    | National Aeronautics and Space Administration                  |
| NESDIS  | National Environmental Satellite Data Information Service      |
| NOAA    | National Oceanographic and Atmospheric Administration          |
| PAR     | Photosynthetically available radiation (400-700 nm)            |
| SeaWiFS | Sea-viewing wide field-of-view spectrometer                    |
| SIS     | Surface Irradiance Spectrometer                                |
| SNR     | Signal-to-noise ratio                                          |
| Top     | Top sampling depth at a radiometer station                     |
| TSM     | Total Suspended Material                                       |

Appendix 3a. The MLML\_DBASE data structure. Variable types use FORTRAN notation. Pointers to variable are shown by \*.

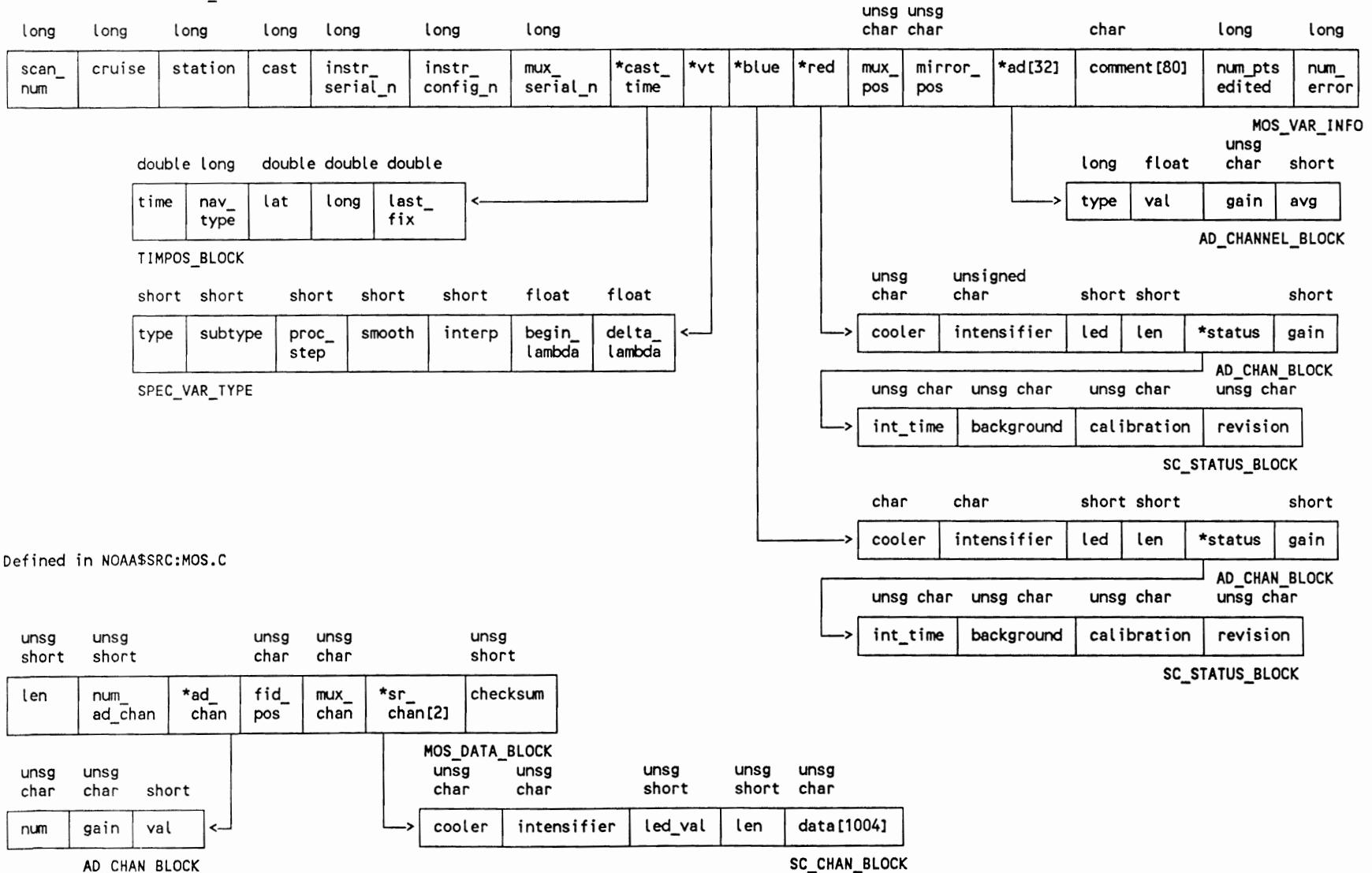
Defined in [MLML\_LIBRARY.MLCLIB]MLML\_DBASE.H



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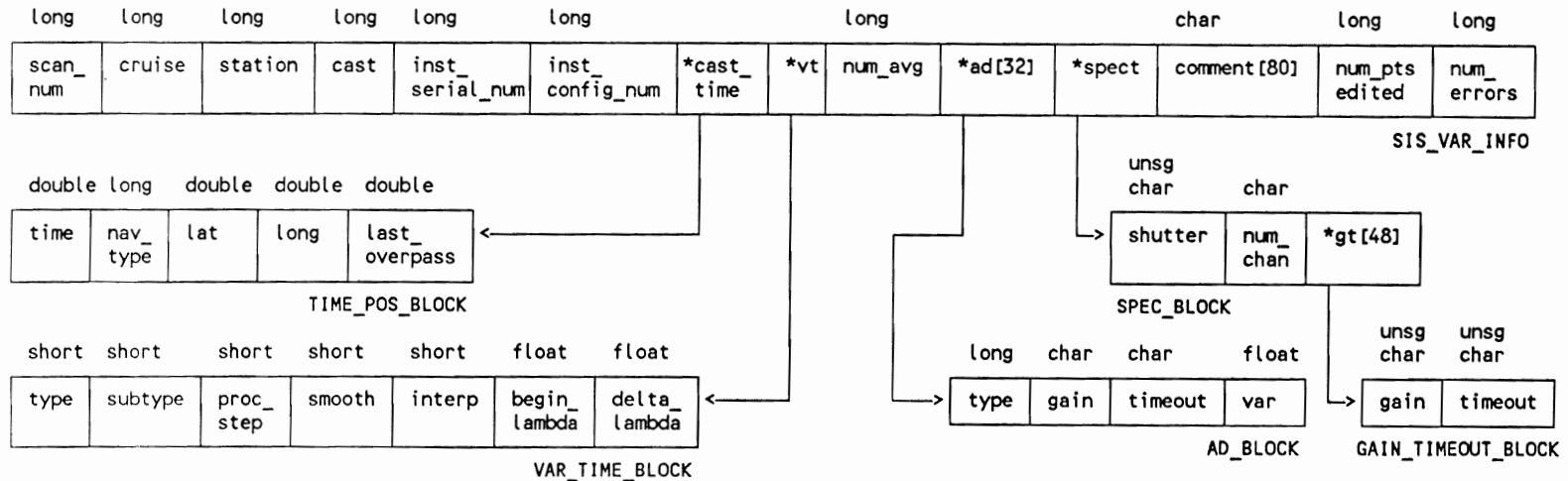
Appendix 3b. Data Structures used with MOS. Variable types use C notation. Pointers to variables are shown by \*. The structure, MOS\_VAR\_INFO, is an MLML\_DBASE File Header Extension. The structure, MOS\_DATA\_BLOCK, is an MLML\_DBASE Variable Extension and accompanies each SIS spectral Variable.

Defined in NOAA\$DIR:MOS\_TYPES.H

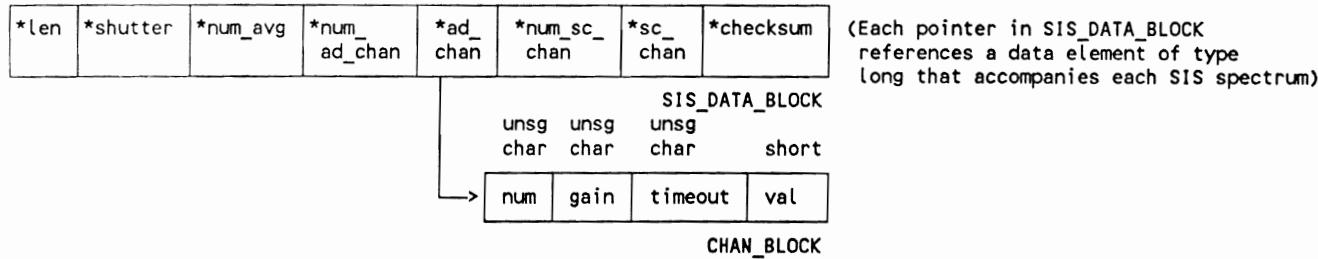


Appendix 3c. Data Structures used with SIS. Variable types use C notation. Pointers to variables are shown by \*. The structure, SIS\_VAR\_INFO, is an MLML File Header Extension. The structure, SIS\_DATA\_BLOCK, is an MLML Variable Extension and accompanies each SIS spectral Variable.

Defined in NOAA\$INC:SIS\_TYPES.H



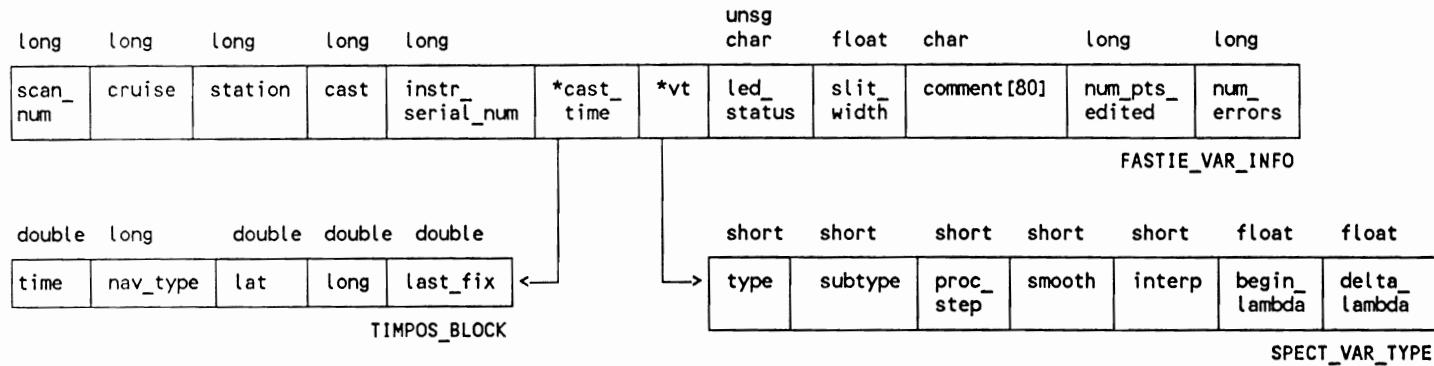
Defined in NOAA\$SRC:SIS.C



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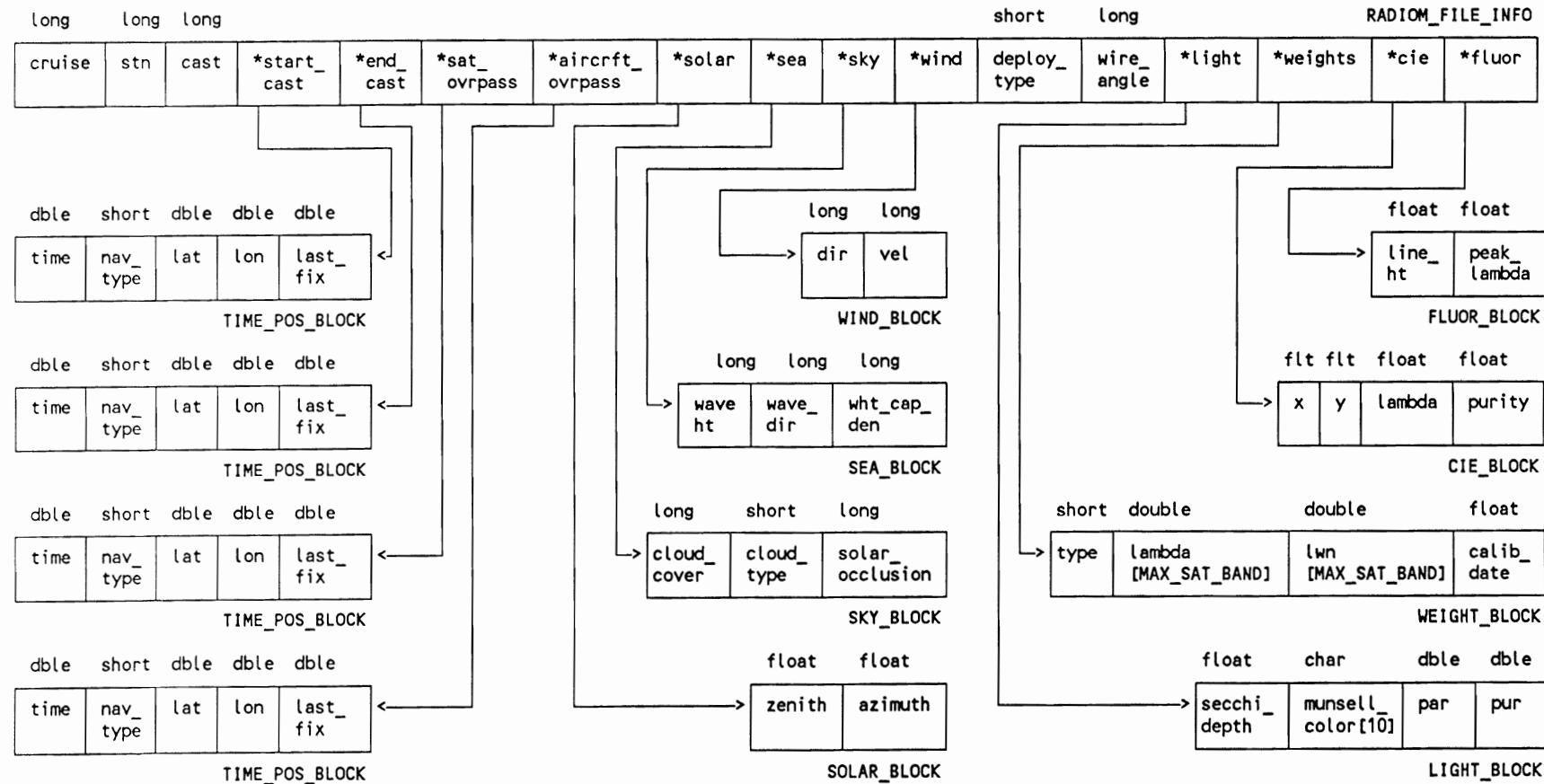
Appendix 3d. Data structures used with Fastie. Variable types use C notation. Pointers to variables are indicated by \*. The structure FASTIE\_VAR\_INFO is an MLML\_DBASE Variable Extension and accompanies each PLOT Variable which contains the spectral data.

Defined in NOAA\$INC:FASTIE\_TYPES.H



Appendix 3e. Data structures used with reduced NOAA radiometer files. Variable types use C notation. Pointers to variables are indicated by \*. The structure, RADIOM\_FILE\_INFO, is an MLML\_DBASE File Header Extension and accompanies each file, and accompanies each PLOT Variable which contains the spectral data.

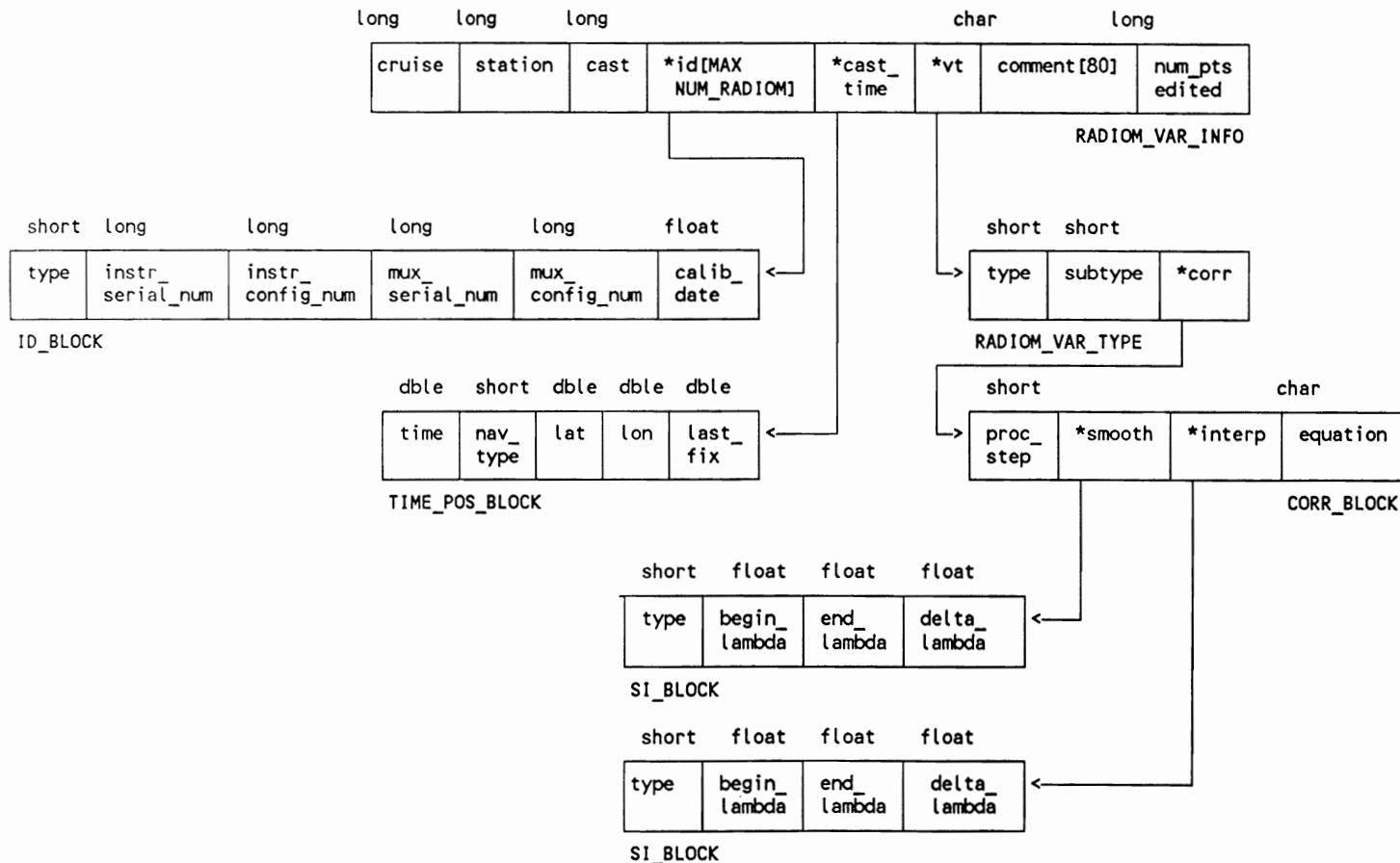
Defined in NOAA\$INC:RADIOM\_TYPES.H



Dec 1993

Appendix 3e. (continued) Data structures used with reduced NOAA radiometer files. Variable types use C notation. Pointers to variables are indicated by \*. The structure, RADIOM\_VAR\_INFO, is an MLML\_DBASE Variable Extension and accompanies each PLOT Variable which contains the spectral data.

Defined in NOAA\$DIR:RADIOM\_TYPES.H



**Appendix 4. Spectral quantities used in radiometer algorithms.**

a) Air-water radiance immersion factors (Austin, 1976)

$$n = n_0 + \frac{C}{\lambda - \lambda_0}$$

$$F_w = n_w \frac{(n_w + n_g)^2}{(1 + n_g)^2}$$

| Material              | $n_0$   | C       | $\lambda_0$ |
|-----------------------|---------|---------|-------------|
| Seawater 35 psu 16° C | 1.32640 | 5.7689  | 159.0698    |
| Plexiglass            | 1.47380 | 7.5     | 174.71      |
| Borosilicate BK7      | 1.49891 | 7.61821 | 161.5089    |
| Fused Quartz          | 1.44291 | 6.8244  | 149.724     |

**Air-Water Radiance Factors**

| Wavelength | Plexiglass | BK7 Glass | Fused Quartz |
|------------|------------|-----------|--------------|
| 360        | 1.765      | 1.761     | 1.771        |
| 380        | 1.759      | 1.755     | 1.766        |
| 400        | 1.754      | 1.750     | 1.761        |
| 420        | 1.750      | 1.746     | 1.756        |
| 440        | 1.746      | 1.742     | 1.753        |
| 460        | 1.743      | 1.739     | 1.749        |
| 480        | 1.740      | 1.736     | 1.746        |
| 500        | 1.738      | 1.734     | 1.744        |
| 520        | 1.736      | 1.732     | 1.742        |
| 540        | 1.734      | 1.730     | 1.740        |
| 560        | 1.732      | 1.728     | 1.738        |
| 580        | 1.731      | 1.727     | 1.736        |
| 600        | 1.729      | 1.725     | 1.735        |
| 620        | 1.728      | 1.724     | 1.734        |
| 640        | 1.727      | 1.723     | 1.732        |
| 660        | 1.726      | 1.722     | 1.731        |
| 680        | 1.725      | 1.721     | 1.730        |
| 700        | 1.724      | 1.720     | 1.729        |
| 720        | 1.723      | 1.719     | 1.728        |
| 740        | 1.722      | 1.718     | 1.728        |

Appendix 4. Spectral quantities used in radiometer algorithms.  
 b) SeaWiFS Normalized Response Functions as applied to the prototype MOS.

| $\lambda$ | Band 1   | $\lambda$ | Band 2   | $\lambda$ | Band 3   | $\lambda$ | Band 4   | $\lambda$ | Band 5   | $\lambda$ | Band 6   | $\lambda$ | Band 7   | $\lambda$ | Band 8   |
|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|
| 385.8     | 0.000E+0 | 409.7     | 0.000E+0 | 462.3     | 0.000E+0 | 480.2     | 0.000E+0 | 525.2     | 0.000E+0 | 639.8     | 0.000E+0 | 734.9     | 0.000E+0 | 835.0     | 0.000E+0 |
| 386.4     | 5.984E-5 | 410.4     | 6.218E-5 | 462.9     | 2.901E-6 | 480.8     | 8.531E-5 | 525.9     | 4.387E-5 | 640.5     | 1.032E-4 | 735.5     | 2.195E-3 | 835.6     | 1.266E-3 |
| 387.0     | 1.438E-4 | 411.0     | 3.572E-5 | 463.5     | 8.067E-7 | 481.4     | 9.029E-5 | 526.5     | 7.896E-5 | 641.1     | 1.287E-4 | 736.1     | 2.498E-3 | 836.2     | 1.400E-3 |
| 387.7     | 2.658E-4 | 411.6     | 5.409E-6 | 464.1     | 3.961E-8 | 482.0     | 1.139E-4 | 527.1     | 1.207E-4 | 641.8     | 1.387E-4 | 736.7     | 2.932E-3 | 836.8     | 1.575E-3 |
| 388.3     | 4.000E-4 | 412.3     | 4.374E-5 | 464.7     | 1.236E-9 | 482.6     | 1.585E-4 | 527.7     | 2.040E-4 | 642.4     | 2.833E-4 | 737.4     | 3.382E-3 | 837.4     | 1.739E-3 |
| 388.9     | 2.151E-4 | 412.9     | 1.503E-4 | 465.4     | 1.632E-0 | 483.3     | 7.972E-5 | 528.3     | 7.094E-5 | 643.1     | 3.211E-4 | 738.0     | 3.930E-3 | 838.0     | 1.997E-3 |
| 389.6     | 6.392E-5 | 413.5     | 9.511E-5 | 466.0     | 1.573E-1 | 483.9     | 1.426E-4 | 528.9     | 1.143E-4 | 643.7     | 3.114E-4 | 738.6     | 4.506E-3 | 838.5     | 2.317E-3 |
| 390.2     | 1.510E-4 | 414.1     | 9.856E-5 | 466.6     | 2.118E-2 | 484.5     | 1.904E-4 | 529.5     | 7.412E-5 | 644.4     | 3.176E-4 | 739.2     | 5.182E-3 | 839.1     | 2.710E-3 |
| 390.8     | 5.001E-4 | 414.8     | 1.086E-4 | 467.2     | 2.774E-3 | 485.1     | 1.273E-4 | 530.1     | 1.520E-4 | 645.0     | 3.712E-4 | 739.9     | 5.962E-3 | 839.7     | 3.051E-3 |
| 391.4     | 3.793E-4 | 415.4     | 1.981E-4 | 467.8     | 2.888E-4 | 485.7     | 2.166E-4 | 530.7     | 1.155E-4 | 645.7     | 4.726E-4 | 740.5     | 6.828E-3 | 840.3     | 3.550E-3 |
| 392.1     | 1.792E-4 | 416.0     | 3.044E-4 | 468.5     | 4.096E-5 | 486.3     | 2.780E-4 | 531.3     | 1.083E-4 | 646.3     | 5.157E-4 | 741.1     | 7.769E-3 | 840.9     | 4.076E-3 |
| 392.7     | 3.024E-5 | 416.7     | 1.551E-4 | 469.1     | 5.910E-6 | 486.9     | 3.870E-4 | 531.9     | 4.107E-5 | 647.0     | 5.256E-4 | 741.7     | 8.743E-3 | 841.5     | 4.730E-3 |
| 393.3     | 6.146E-4 | 417.3     | 1.522E-4 | 469.7     | 7.681E-7 | 487.6     | 4.407E-4 | 532.5     | 9.267E-5 | 647.6     | 5.545E-4 | 742.4     | 9.800E-3 | 842.0     | 5.466E-3 |
| 394.0     | 2.195E-4 | 417.9     | 1.142E-4 | 470.3     | 9.333E-8 | 488.2     | 5.430E-4 | 533.1     | 2.372E-4 | 648.3     | 6.268E-4 | 743.0     | 1.088E-2 | 842.6     | 6.222E-3 |
| 394.6     | 2.685E-4 | 418.5     | 1.730E-4 | 470.9     | 1.463E-9 | 488.8     | 5.847E-4 | 533.7     | 2.880E-4 | 648.9     | 6.061E-4 | 743.6     | 1.204E-2 | 843.2     | 7.068E-3 |
| 395.2     | 3.787E-4 | 419.2     | 2.615E-4 | 471.5     | 1.704E-0 | 489.4     | 7.364E-4 | 534.3     | 2.772E-4 | 649.6     | 7.475E-4 | 744.2     | 1.322E-2 | 843.8     | 8.068E-3 |
| 395.9     | 8.087E-4 | 419.8     | 3.048E-4 | 472.2     | 2.011E-1 | 490.0     | 9.789E-4 | 534.8     | 3.551E-4 | 650.2     | 8.270E-4 | 744.9     | 1.435E-2 | 844.4     | 9.139E-3 |
| 396.5     | 1.215E-3 | 420.4     | 2.346E-4 | 472.8     | 2.375E-2 | 490.6     | 1.182E-3 | 535.4     | 4.599E-4 | 650.9     | 9.871E-4 | 745.5     | 1.554E-2 | 844.9     | 1.035E-2 |
| 397.1     | 1.690E-3 | 421.1     | 2.940E-4 | 473.4     | 2.940E-3 | 491.2     | 1.484E-3 | 536.0     | 5.706E-4 | 651.5     | 1.142E-3 | 746.1     | 1.665E-2 | 845.5     | 1.164E-2 |
| 397.8     | 2.315E-3 | 421.7     | 3.464E-4 | 474.0     | 3.665E-4 | 491.9     | 1.832E-3 | 536.6     | 7.265E-4 | 652.2     | 1.340E-3 | 746.7     | 1.769E-2 | 846.1     | 1.292E-2 |
| 398.4     | 3.291E-3 | 422.3     | 3.843E-4 | 474.6     | 4.672E-5 | 492.5     | 2.333E-3 | 537.2     | 9.316E-4 | 652.8     | 1.626E-3 | 747.3     | 1.864E-2 | 846.7     | 1.424E-2 |
| 399.0     | 5.271E-3 | 422.9     | 6.227E-4 | 475.3     | 6.062E-6 | 493.1     | 2.837E-3 | 537.8     | 1.337E-3 | 653.5     | 2.032E-3 | 748.0     | 1.958E-2 | 847.3     | 1.554E-2 |
| 399.7     | 6.349E-3 | 423.6     | 6.052E-4 | 475.9     | 7.556E-7 | 493.7     | 3.642E-3 | 538.4     | 1.590E-3 | 654.1     | 2.665E-3 | 748.6     | 2.034E-2 | 847.8     | 1.677E-2 |
| 400.3     | 8.530E-3 | 424.2     | 7.762E-4 | 476.5     | 9.519E-8 | 494.3     | 4.555E-3 | 539.0     | 2.061E-3 | 654.8     | 3.430E-3 | 749.2     | 2.100E-2 | 848.4     | 1.802E-2 |
| 400.9     | 1.270E-2 | 424.8     | 1.114E-3 | 477.1     | 1.181E-9 | 494.9     | 5.678E-3 | 539.6     | 2.765E-3 | 655.4     | 4.615E-3 | 749.8     | 2.160E-2 | 849.0     | 1.917E-2 |
| 401.5     | 1.591E-2 | 425.5     | 1.458E-3 | 477.7     | 1.470E-0 | 495.5     | 7.184E-3 | 540.2     | 3.613E-3 | 656.1     | 6.368E-3 | 750.5     | 2.211E-2 | 849.6     | 2.004E-2 |
| 402.2     | 1.940E-2 | 426.1     | 1.628E-3 | 478.3     | 1.772E-1 | 496.1     | 9.063E-3 | 540.8     | 4.788E-3 | 656.7     | 8.924E-3 | 751.1     | 2.251E-2 | 850.1     | 2.095E-2 |
| 402.8     | 2.375E-2 | 426.7     | 2.050E-3 | 479.0     | 2.084E-2 | 496.7     | 1.114E-2 | 541.4     | 6.586E-3 | 657.4     | 1.244E-2 | 751.7     | 2.277E-2 | 850.7     | 2.172E-2 |
| 403.4     | 2.803E-2 | 427.3     | 2.751E-3 | 479.6     | 2.404E-3 | 497.4     | 1.380E-2 | 542.0     | 8.549E-3 | 658.0     | 1.692E-2 | 752.3     | 2.302E-2 | 851.3     | 2.230E-2 |
| 404.1     | 3.224E-2 | 428.0     | 3.557E-3 | 480.2     | 2.731E-4 | 498.0     | 1.655E-2 | 542.6     | 1.117E-2 | 658.7     | 2.226E-2 | 752.9     | 2.327E-2 | 851.9     | 2.281E-2 |
| 404.7     | 3.219E-2 | 428.6     | 4.534E-3 | 480.8     | 3.065E-5 | 498.6     | 1.947E-2 | 543.2     | 1.437E-2 | 659.3     | 2.803E-2 | 753.5     | 2.347E-2 | 852.4     | 2.316E-2 |
| 405.3     | 3.327E-2 | 429.2     | 5.857E-3 | 481.4     | 3.367E-6 | 499.2     | 2.279E-2 | 543.8     | 1.807E-2 | 660.0     | 3.393E-2 | 754.2     | 2.356E-2 | 853.0     | 2.354E-2 |
| 406.0     | 3.490E-2 | 429.8     | 7.478E-3 | 482.0     | 3.585E-7 | 499.8     | 2.593E-2 | 544.4     | 2.239E-2 | 660.6     | 3.943E-2 | 754.8     | 2.378E-2 | 853.6     | 2.372E-2 |
| 406.6     | 3.787E-2 | 430.5     | 9.405E-3 | 482.6     | 3.808E-8 | 500.4     | 2.900E-2 | 545.0     | 2.694E-2 | 661.3     | 4.364E-2 | 755.4     | 2.379E-2 | 854.2     | 2.391E-2 |
| 407.2     | 3.988E-2 | 431.1     | 1.163E-2 | 483.3     | 4.000E-9 | 501.0     | 3.208E-2 | 545.6     | 3.183E-2 | 661.9     | 4.636E-2 | 756.0     | 2.386E-2 | 854.7     | 2.404E-2 |
| 407.9     | 3.893E-2 | 431.7     | 1.425E-2 | 483.9     | 4.143E-0 | 501.6     | 3.527E-2 | 546.2     | 3.613E-2 | 662.6     | 4.764E-2 | 756.6     | 2.387E-2 | 855.3     | 2.420E-2 |
| 408.5     | 4.109E-2 | 432.3     | 1.720E-2 | 484.5     | 4.259E-1 | 502.2     | 3.772E-2 | 546.8     | 3.993E-2 | 663.2     | 4.755E-2 | 757.3     | 2.397E-2 | 855.9     | 2.430E-2 |
| 409.1     | 4.376E-2 | 433.0     | 2.031E-2 | 485.1     | 4.371E-2 | 502.8     | 3.897E-2 | 547.4     | 4.328E-2 | 663.9     | 4.697E-2 | 757.9     | 2.402E-2 | 856.5     | 2.436E-2 |
| 409.7     | 4.242E-2 | 433.6     | 2.374E-2 | 485.7     | 4.409E-3 | 503.5     | 4.033E-2 | 548.0     | 4.583E-2 | 664.5     | 4.627E-2 | 758.5     | 2.404E-2 | 857.0     | 2.447E-2 |
| 410.4     | 4.260E-2 | 434.2     | 2.708E-2 | 486.3     | 4.447E-4 | 504.1     | 4.120E-2 | 548.5     | 4.700E-2 | 665.2     | 4.564E-2 | 759.1     | 2.413E-2 | 857.6     | 2.456E-2 |
| 411.0     | 4.380E-2 | 434.9     | 2.978E-2 | 486.9     | 4.505E-5 | 504.7     | 4.144E-2 | 549.1     | 4.749E-2 | 665.8     | 4.534E-2 | 759.7     | 2.402E-2 | 858.2     | 2.468E-2 |
| 411.6     | 4.373E-2 | 435.5     | 3.242E-2 | 487.6     | 4.473E-6 | 505.3     | 4.152E-2 | 549.7     | 4.800E-2 | 666.5     | 4.538E-2 | 760.3     | 2.393E-2 | 858.7     | 2.467E-2 |
| 412.3     | 4.379E-2 | 436.1     | 3.450E-2 | 488.2     | 4.412E-7 | 505.9     | 4.141E-2 | 550.3     | 4.820E-2 | 667.1     | 4.576E-2 | 761.0     | 2.399E-2 | 859.3     | 2.470E-2 |
| 412.9     | 4.420E-2 | 436.7     | 3.601E-2 | 488.8     | 4.365E-8 | 506.5     | 4.112E-2 | 550.9     | 4.854E-2 | 667.8     | 4.594E-2 | 761.6     | 2.398E-2 | 859.9     | 2.479E-2 |

Appendix 4. Spectral quantities used in radiometer algorithms.  
b) (continued) SeaWiFS Normalized Response Functions as applied to the prototype MOS.

| $\lambda$ | Band 1   | $\lambda$ | Band 2   | $\lambda$ | Band 3   | $\lambda$ | Band 4   | $\lambda$ | Band 5   | $\lambda$ | Band 6   | $\lambda$ | Band 7   | $\lambda$ | Band 8   |
|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|
| 413.5     | 4.658E-2 | 437.4     | 3.708E-2 | 489.4     | 4.333E-9 | 507.1     | 4.064E-2 | 551.5     | 4.828E-2 | 668.4     | 4.634E-2 | 762.2     | 2.392E-2 | 860.4     | 2.475E-2 |
| 414.1     | 4.840E-2 | 438.0     | 3.761E-2 | 490.0     | 4.319E-0 | 507.7     | 4.017E-2 | 552.1     | 4.814E-2 | 669.1     | 4.663E-2 | 762.8     | 2.384E-2 | 861.0     | 2.475E-2 |
| 414.8     | 5.012E-2 | 438.6     | 3.928E-2 | 490.6     | 4.312E-1 | 508.3     | 3.988E-2 | 552.7     | 4.826E-2 | 669.7     | 4.693E-2 | 763.4     | 2.381E-2 | 861.6     | 2.470E-2 |
| 415.4     | 5.015E-2 | 439.2     | 4.053E-2 | 491.2     | 4.293E-2 | 508.9     | 3.940E-2 | 553.3     | 4.854E-2 | 670.4     | 4.705E-2 | 764.0     | 2.375E-2 | 862.1     | 2.463E-2 |
| 416.0     | 4.948E-2 | 439.9     | 4.188E-2 | 491.9     | 4.287E-3 | 509.5     | 3.950E-2 | 553.9     | 4.894E-2 | 671.0     | 4.684E-2 | 764.7     | 2.375E-2 | 862.7     | 2.449E-2 |
| 416.7     | 4.895E-2 | 440.5     | 4.237E-2 | 492.5     | 4.286E-4 | 510.1     | 3.970E-2 | 554.5     | 4.925E-2 | 671.7     | 4.692E-2 | 765.3     | 2.371E-2 | 863.3     | 2.445E-2 |
| 417.3     | 4.850E-2 | 441.1     | 4.255E-2 | 493.1     | 4.309E-5 | 510.7     | 4.003E-2 | 555.1     | 4.954E-2 | 672.3     | 4.689E-2 | 765.9     | 2.371E-2 | 863.8     | 2.443E-2 |
| 417.9     | 4.824E-2 | 441.7     | 4.348E-2 | 493.7     | 4.317E-6 | 511.4     | 4.036E-2 | 555.6     | 4.962E-2 | 673.0     | 4.670E-2 | 766.5     | 2.370E-2 | 864.4     | 2.425E-2 |
| 418.5     | 4.820E-2 | 442.4     | 4.427E-2 | 494.3     | 4.329E-7 | 512.0     | 4.078E-2 | 556.2     | 4.993E-2 | 673.6     | 4.629E-2 | 767.1     | 2.369E-2 | 865.0     | 2.401E-2 |
| 419.2     | 4.767E-2 | 443.0     | 4.537E-2 | 494.9     | 4.283E-8 | 512.6     | 4.109E-2 | 556.8     | 5.044E-2 | 674.3     | 4.551E-2 | 767.7     | 2.367E-2 | 865.5     | 2.375E-2 |
| 419.8     | 4.601E-2 | 443.6     | 4.622E-2 | 495.5     | 4.317E-9 | 513.2     | 4.175E-2 | 557.4     | 5.064E-2 | 674.9     | 4.441E-2 | 768.3     | 2.370E-2 | 866.1     | 2.359E-2 |
| 420.4     | 4.390E-2 | 444.2     | 4.668E-2 | 496.1     | 4.339E-0 | 513.8     | 4.210E-2 | 558.0     | 5.049E-2 | 675.6     | 4.265E-2 | 769.0     | 2.367E-2 | 866.6     | 2.323E-2 |
| 421.1     | 4.095E-2 | 444.8     | 4.655E-2 | 496.7     | 4.252E-1 | 514.4     | 4.248E-2 | 558.6     | 4.985E-2 | 676.2     | 4.028E-2 | 769.6     | 2.378E-2 | 867.2     | 2.293E-2 |
| 421.7     | 3.817E-2 | 445.5     | 4.719E-2 | 497.4     | 4.137E-2 | 515.0     | 4.264E-2 | 559.2     | 4.890E-2 | 676.9     | 3.723E-2 | 770.2     | 2.381E-2 | 867.8     | 2.266E-2 |
| 422.3     | 3.483E-2 | 446.1     | 4.790E-2 | 498.0     | 3.953E-3 | 515.6     | 4.256E-2 | 559.8     | 4.750E-2 | 677.5     | 3.372E-2 | 770.8     | 2.381E-2 | 868.3     | 2.235E-2 |
| 422.9     | 3.150E-2 | 446.7     | 4.836E-2 | 498.6     | 3.710E-4 | 516.2     | 4.214E-2 | 560.4     | 4.568E-2 | 678.2     | 2.980E-2 | 771.4     | 2.381E-2 | 868.9     | 2.193E-2 |
| 423.6     | 2.761E-2 | 447.3     | 4.803E-2 | 499.2     | 3.449E-5 | 516.8     | 4.207E-2 | 560.9     | 4.318E-2 | 678.8     | 2.571E-2 | 772.0     | 2.381E-2 | 869.4     | 2.163E-2 |
| 424.2     | 2.369E-2 | 448.0     | 4.708E-2 | 499.8     | 3.120E-6 | 517.4     | 4.126E-2 | 561.5     | 4.047E-2 | 679.4     | 2.180E-2 | 772.6     | 2.384E-2 | 870.0     | 2.135E-2 |
| 424.8     | 1.964E-2 | 448.6     | 4.677E-2 | 500.4     | 2.770E-7 | 518.0     | 4.051E-2 | 562.1     | 3.743E-2 | 680.1     | 1.812E-2 | 773.2     | 2.383E-2 | 870.5     | 2.115E-2 |
| 425.5     | 1.613E-2 | 449.2     | 4.606E-2 | 501.0     | 2.397E-8 | 518.6     | 3.910E-2 | 562.7     | 3.390E-2 | 680.7     | 1.472E-2 | 773.9     | 2.371E-2 | 871.1     | 2.096E-2 |
| 426.1     | 1.300E-2 | 449.8     | 4.483E-2 | 501.6     | 2.051E-9 | 519.2     | 3.734E-2 | 563.3     | 3.008E-2 | 681.4     | 1.199E-2 | 774.5     | 2.360E-2 | 871.7     | 2.071E-2 |
| 426.7     | 9.702E-3 | 450.5     | 4.367E-2 | 502.2     | 1.703E-0 | 519.8     | 3.493E-2 | 563.9     | 2.632E-2 | 682.0     | 9.836E-3 | 775.1     | 2.353E-2 | 872.2     | 2.057E-2 |
| 427.3     | 7.157E-3 | 451.1     | 4.259E-2 | 502.8     | 1.360E-1 | 520.4     | 3.188E-2 | 564.5     | 2.280E-2 | 682.7     | 7.970E-3 | 775.7     | 2.333E-2 | 872.8     | 2.037E-2 |
| 428.0     | 5.213E-3 | 451.7     | 4.050E-2 | 503.5     | 1.076E-2 | 521.0     | 2.839E-2 | 565.0     | 1.926E-2 | 683.3     | 6.434E-3 | 776.3     | 2.309E-2 | 873.3     | 2.036E-2 |
| 428.6     | 3.971E-3 | 452.3     | 3.858E-2 | 504.1     | 8.465E-3 | 521.6     | 2.450E-2 | 565.6     | 1.596E-2 | 684.0     | 5.254E-3 | 776.9     | 2.281E-2 | 873.9     | 2.038E-2 |
| 429.2     | 2.811E-3 | 452.9     | 3.647E-2 | 504.7     | 6.570E-4 | 522.2     | 2.079E-2 | 566.2     | 1.316E-2 | 684.6     | 4.297E-3 | 777.5     | 2.242E-2 | 874.4     | 2.035E-2 |
| 429.8     | 2.133E-3 | 453.6     | 3.313E-2 | 505.3     | 5.049E-5 | 522.8     | 1.748E-2 | 566.8     | 1.073E-2 | 685.3     | 3.550E-3 | 778.1     | 2.190E-2 | 875.0     | 2.049E-2 |
| 430.5     | 1.576E-3 | 454.2     | 2.917E-2 | 505.9     | 3.950E-6 | 523.4     | 1.425E-2 | 567.4     | 8.655E-3 | 685.9     | 2.899E-3 | 778.7     | 2.130E-2 | 875.5     | 2.064E-2 |
| 431.1     | 1.202E-3 | 454.8     | 2.546E-2 | 506.5     | 3.075E-7 | 524.0     | 1.149E-2 | 568.0     | 6.934E-3 | 686.5     | 2.403E-3 | 779.3     | 2.060E-2 | 876.1     | 2.080E-2 |
| 431.7     | 9.717E-4 | 455.4     | 2.090E-2 | 507.1     | 2.409E-8 | 524.6     | 8.789E-3 | 568.6     | 5.623E-3 | 687.2     | 1.968E-3 | 780.0     | 1.982E-2 | 876.6     | 2.112E-2 |
| 432.3     | 7.927E-4 | 456.1     | 1.669E-2 | 507.7     | 1.947E-9 | 525.2     | 6.622E-3 | 569.1     | 4.589E-3 | 687.8     | 1.671E-3 | 780.6     | 1.898E-2 | 877.2     | 2.141E-2 |
| 433.0     | 6.997E-4 | 456.7     | 1.313E-2 | 508.3     | 1.471E-0 | 525.9     | 4.908E-3 | 569.7     | 3.745E-3 | 688.5     | 1.433E-3 | 781.2     | 1.795E-2 | 877.7     | 2.180E-2 |
| 433.6     | 5.828E-4 | 457.3     | 1.007E-2 | 508.9     | 1.197E-1 | 526.5     | 3.614E-3 | 570.3     | 3.071E-3 | 689.1     | 1.284E-3 | 781.8     | 1.690E-2 | 878.3     | 2.214E-2 |
| 434.2     | 5.340E-4 | 457.9     | 7.546E-3 | 509.5     | 9.784E-2 | 527.1     | 2.617E-3 | 570.9     | 2.544E-3 | 689.8     | 1.006E-3 | 782.4     | 1.587E-2 | 878.8     | 2.241E-2 |
| 434.9     | 4.667E-4 | 458.5     | 5.627E-3 | 510.1     | 8.496E-3 | 527.7     | 1.865E-3 | 571.5     | 2.152E-3 | 690.4     | 8.370E-4 | 783.0     | 1.484E-2 | 879.4     | 2.271E-2 |
| 435.5     | 4.279E-4 | 459.2     | 4.171E-3 | 510.7     | 6.774E-4 | 528.3     | 1.370E-3 | 572.1     | 1.846E-3 | 691.1     | 7.071E-4 | 783.6     | 1.383E-2 | 879.9     | 2.301E-2 |
| 436.1     | 3.887E-4 | 459.8     | 3.139E-3 | 511.4     | 5.680E-5 | 528.9     | 1.013E-3 | 572.6     | 1.630E-3 | 691.7     | 6.072E-4 | 784.2     | 1.284E-2 | 880.4     | 2.321E-2 |
| 436.7     | 3.526E-4 | 460.4     | 2.344E-3 | 512.0     | 4.486E-6 | 529.5     | 7.785E-4 | 573.2     | 1.466E-3 | 692.3     | 5.312E-4 | 784.8     | 1.182E-2 | 881.0     | 2.330E-2 |
| 437.4     | 2.925E-4 | 461.0     | 1.807E-3 | 512.6     | 4.029E-7 | 530.1     | 6.170E-4 | 573.8     | 1.180E-3 | 693.0     | 4.509E-4 | 785.4     | 1.076E-2 | 881.5     | 2.326E-2 |
| 438.0     | 2.495E-4 | 461.6     | 1.281E-3 | 513.2     | 3.507E-8 | 530.7     | 4.917E-4 | 574.4     | 1.042E-3 | 693.6     | 4.062E-4 | 786.0     | 9.749E-3 | 882.1     | 2.313E-2 |
| 438.6     | 2.360E-4 | 462.3     | 9.671E-4 | 513.8     | 2.813E-9 | 531.3     | 3.791E-4 | 575.0     | 8.951E-4 | 694.3     | 3.446E-4 | 786.6     | 8.899E-3 | 882.6     | 2.268E-2 |
| 439.2     | 2.354E-4 | 462.9     | 7.725E-4 | 514.4     | 2.566E-0 | 531.9     | 3.161E-4 | 575.6     | 6.720E-4 | 694.9     | 3.128E-4 | 787.3     | 8.061E-3 | 883.1     | 2.212E-2 |
| 439.9     | 2.273E-4 | 463.5     | 6.015E-4 | 515.0     | 2.275E-1 | 532.5     | 2.445E-4 | 576.1     | 7.904E-4 | 695.5     | 2.319E-4 | 787.9     | 7.254E-3 | 883.7     | 2.142E-2 |
| 440.5     | 0.000E+0 | 464.1     | 5.336E-4 | 515.6     | 1.800E-2 | 533.1     | 2.074E-4 | 576.7     | 6.373E-4 | 696.2     | 2.362E-4 | 788.5     | 6.524E-3 | 884.2     | 2.057E-2 |

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Appendix 4. Spectral quantities used in radiometer algorithms.  
 b) (continued) SeaWiFS Normalized Response Functions as applied to the prototype MOS.

| $\lambda$ | Band 1   | $\lambda$ | Band 2   | $\lambda$ | Band 3   | $\lambda$ | Band 4   | $\lambda$ | Band 5   | $\lambda$ | Band 6   | $\lambda$ | Band 7   | $\lambda$ | Band 8 |  |
|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|--------|--|
| 464.7     | 3.528E-4 | 516.2     | 1.711E-3 | 533.7     | 1.438E-4 | 577.3     | 5.747E-4 | 696.8     | 1.910E-4 | 789.1     | 5.890E-3 | 884.8     | 1.952E-2 |           |        |  |
| 465.4     | 2.790E-4 | 516.8     | 1.265E-4 | 534.3     | 1.041E-4 | 577.9     | 4.586E-4 | 697.5     | 2.004E-4 | 789.7     | 5.280E-3 | 885.3     | 1.816E-2 |           |        |  |
| 466.0     | 2.707E-4 | 517.4     | 1.426E-5 | 534.8     | 7.188E-5 | 578.5     | 4.319E-4 | 698.1     | 1.520E-4 | 790.3     | 4.738E-3 | 885.8     | 1.676E-2 |           |        |  |
| 466.6     | 1.785E-4 | 518.0     | 1.087E-6 | 535.4     | 5.647E-5 | 579.0     | 3.664E-4 | 698.8     | 1.791E-4 | 790.9     | 4.275E-3 | 886.4     | 1.531E-2 |           |        |  |
| 467.2     | 7.003E-5 | 518.6     | 1.266E-7 | 536.0     | 3.891E-5 | 579.6     | 3.163E-4 | 699.4     | 1.256E-4 | 791.5     | 3.878E-3 | 886.9     | 1.393E-2 |           |        |  |
| 467.8     | 5.464E-5 | 519.2     | 9.967E-8 | 536.6     | 3.544E-5 | 580.2     | 2.253E-4 | 700.0     | 1.034E-4 | 792.1     | 3.513E-3 | 887.4     | 1.253E-2 |           |        |  |
| 468.5     | 4.399E-5 | 519.8     | 6.882E-9 | 537.2     | 3.812E-5 | 580.8     | 2.907E-4 | 700.7     | 0.000E+0 | 792.7     | 3.202E-3 | 888.0     | 1.108E-2 |           |        |  |
| 469.1     | 8.728E-5 | 520.4     | 0.000E+0 | 537.8     | 9.822E-6 | 581.3     | 2.400E-4 |           |          | 793.3     | 2.862E-3 | 888.5     | 9.776E-3 |           |        |  |
| 469.7     | 2.362E-5 |           |          | 538.4     | 1.447E-5 | 581.9     | 1.958E-4 |           |          | 793.9     | 2.629E-3 | 889.0     | 8.573E-3 |           |        |  |
| 470.3     | 0.000E+0 |           |          |           | 539.0    | 1.497E-5  | 582.5    | 1.710E-4  |          |           | 794.5    | 2.404E-3  | 889.5    | 7.545E-3  |        |  |
|           |          |           |          |           | 539.6    | 3.778E-5  | 583.1    | 1.656E-4  |          |           | 795.1    | 1.874E-3  | 890.1    | 6.629E-3  |        |  |
|           |          |           |          |           | 540.2    | 0.000E+0  | 583.7    | 1.688E-4  |          |           | 795.7    | 0.000E+0  | 890.6    | 5.849E-3  |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 891.1     | 5.163E-3 |           |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 891.6     | 4.557E-3 |           |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 892.2     | 4.077E-3 |           |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 892.7     | 3.677E-3 |           |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 893.2     | 3.270E-3 |           |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 893.7     | 2.919E-3 |           |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 894.2     | 2.587E-3 |           |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 894.8     | 2.667E-3 |           |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 895.3     | 1.364E-3 |           |        |  |
|           |          |           |          |           |          |           |          |           |          |           |          | 895.8     | 0.000E+0 |           |        |  |

## Appendix 4. Spectral quantities used in radiometer algorithms.

c) Rayleigh and ozone atmospheric optical thicknesses.  $\tau_{oz}$  from Howard Gordon (personal communication).

| $\lambda$ (nm) | $\tau_R$ | $\tau_{oz}$ | $\lambda$ (nm) | $\tau_R$ | $\tau_{oz}$ |
|----------------|----------|-------------|----------------|----------|-------------|
| 340            | 0.7062   | 0.0188      | 625            | 0.0585   | 0.0352      |
| 345            | 0.6653   | 0.0070      | 630            | 0.0566   | 0.0326      |
| 350            | 0.6273   | 0.0032      | 635            | 0.0548   | 0.0301      |
| 355            | 0.5919   | 0.0007      | 640            | 0.0531   | 0.0279      |
| 360            | 0.5590   | 0.0000      | 645            | 0.0514   | 0.0254      |
| 365            | 0.5283   | 0.0000      | 650            | 0.0498   | 0.0232      |
| 370            | 0.4997   | 0.0000      | 655            | 0.0483   | 0.0214      |
| 375            | 0.4730   | 0.0000      | 660            | 0.0468   | 0.0199      |
| 380            | 0.4480   | 0.0000      | 665            | 0.0454   | 0.0185      |
| 385            | 0.4247   | 0.0000      | 670            | 0.0440   | 0.0166      |
| 390            | 0.4029   | 0.0000      | 675            | 0.0427   | 0.0152      |
| 395            | 0.3824   | 0.0000      | 680            | 0.0414   | 0.0137      |
| 400            | 0.3632   | 0.0000      | 685            | 0.0402   | 0.0123      |
| 405            | 0.3452   | 0.0000      | 690            | 0.0390   | 0.0108      |
| 410            | 0.3283   | 0.0000      | 695            | 0.0379   | 0.0090      |
| 415            | 0.3124   | 0.0000      | 700            | 0.0368   | 0.0079      |
| 420            | 0.2975   | 0.0000      | 705            | 0.0357   | 0.0075      |
| 425            | 0.2834   | 0.0000      | 710            | 0.0347   | 0.0064      |
| 430            | 0.2702   | 0.0003      | 715            | 0.0337   | 0.0057      |
| 435            | 0.2577   | 0.0007      | 720            | 0.0328   | 0.0052      |
| 440            | 0.2459   | 0.0010      | 725            | 0.0318   | 0.0047      |
| 445            | 0.2348   | 0.0010      | 730            | 0.0310   | 0.0042      |
| 450            | 0.2243   | 0.0010      | 735            | 0.0301   | 0.0038      |
| 455            | 0.2144   | 0.0018      | 740            | 0.0293   | 0.0034      |
| 460            | 0.2050   | 0.0029      | 745            | 0.0285   | 0.0031      |
| 465            | 0.1962   | 0.0029      | 750            | 0.0277   | 0.0028      |
| 470            | 0.1878   | 0.0025      | 755            | 0.0270   | 0.0025      |
| 475            | 0.1798   | 0.0043      | 760            | 0.0263   | 0.0022      |
| 480            | 0.1723   | 0.0065      | 765            | 0.0256   | 0.0020      |
| 485            | 0.1651   | 0.0072      | 770            | 0.0249   | 0.0018      |
| 490            | 0.1583   | 0.0065      | 775            | 0.0242   | 0.0016      |
| 495            | 0.1519   | 0.0079      | 780            | 0.0236   | 0.0015      |
| 500            | 0.1458   | 0.0101      | 785            | 0.0230   | 0.0013      |
| 505            | 0.1399   | 0.0137      | 790            | 0.0224   | 0.0012      |
| 510            | 0.1344   | 0.0145      | 795            | 0.0218   | 0.0011      |
| 515            | 0.1292   | 0.0137      | 800            | 0.0213   | 0.0009      |
| 520            | 0.1241   | 0.0163      | 805            | 0.0207   | 0.0008      |
| 525            | 0.1194   | 0.0195      | 810            | 0.0202   | 0.0008      |
| 530            | 0.1148   | 0.0228      | 815            | 0.0197   | 0.0007      |
| 535            | 0.1105   | 0.0254      | 820            | 0.0192   | 0.0006      |
| 540            | 0.1064   | 0.0261      | 825            | 0.0188   | 0.0005      |
| 545            | 0.1024   | 0.0279      | 830            | 0.0183   | 0.0005      |
| 550            | 0.0987   | 0.0304      | 835            | 0.0178   | 0.0004      |
| 555            | 0.0951   | 0.0323      | 840            | 0.0174   | 0.0004      |
| 560            | 0.0917   | 0.0348      | 845            | 0.0170   | 0.0003      |
| 565            | 0.0884   | 0.0388      | 850            | 0.0166   | 0.0003      |
| 570            | 0.0853   | 0.0421      | 855            | 0.0162   | 0.0003      |
| 575            | 0.0823   | 0.0431      | 860            | 0.0158   | 0.0002      |
| 580            | 0.0794   | 0.0424      | 865            | 0.0154   | 0.0002      |
| 585            | 0.0767   | 0.0402      | 870            | 0.0151   | 0.0002      |
| 590            | 0.0740   | 0.0392      | 875            | 0.0147   | 0.0002      |
| 595            | 0.0715   | 0.0417      | 880            | 0.0144   | 0.0001      |
| 600            | 0.0691   | 0.0450      | 885            | 0.0141   | 0.0001      |
| 605            | 0.0668   | 0.0450      | 890            | 0.0137   | 0.0001      |
| 610            | 0.0646   | 0.0428      | 895            | 0.0134   | 0.0001      |
| 615            | 0.0625   | 0.0402      | 900            | 0.0131   | 0.0001      |
| 620            | 0.0604   | 0.0377      |                |          |             |

## Appendix 5. File Naming Conventions and Directory Structures.

### Device Names for Program and Data Directories:

|                |                            |                          |
|----------------|----------------------------|--------------------------|
| NSF::DUA1:     | ! VAX 4000 Model 300       | System Device = _DUA0:   |
| HYDRA::DKA300: | ! VAXstation 4000 model 60 | System Device = _DKA300: |
| SISSR::DKA100: | ! VAXstation 4000 model 60 | System Device = _DKA300: |

### Data Directories:

| [DATA]                    |                        |                                                 |
|---------------------------|------------------------|-------------------------------------------------|
| [DATA.COM]                | ! Data directory       | eg. SETUP.COM                                   |
| [DATA.COLLATED]           | ! Collated data        | eg. CZCS_RESPONSES.MLDAT LW_SN_CZCS_PIGS.MLDAT  |
| [DATA.cruise]             | ! Cruise subdirectory  | eg. MOCE_1 MOBY_2                               |
| [DATA.cruise.DOC]         | ! Cruise documentation | eg. STATION_LOG.TXT DATA_PROCESSING_SUMMARY.TXT |
| [DATA.cruise.MOS]         |                        |                                                 |
| [DATA.cruise.MOS.CAL]     | ! Calibration data     | eg. OPT420_S3W6D40_00CM_025SEC_01.MLDAT         |
| [DATA.cruise.MOS.RAW]     | ! Raw cruise data      | eg. STN01_01M_ED_01.MLDAT                       |
| [DATA.cruise.MOS.PRC]     | ! Processed data       | eg. STN01_01M_ED_01_PROC.MLDAT                  |
| [DATA.cruise.SIS]         |                        |                                                 |
| [DATA.cruise.SIS.CAL]     | ! Calibration data     | eg. FEL_50CM_100AVG_01.MLDAT                    |
| [DATA.cruise.SIS.RAW]     | ! Raw cruise data      | eg. STN01_WMOS_01M_ED_01.MLDAT                  |
| [DATA.cruise.SIS.PRC]     | ! Processed data       | eg. STN01_WMOS_01M_ED_01_PROC.MLDAT             |
| [DATA.cruise.FASTIE]      |                        |                                                 |
| [DATA.cruise.FASTIE.CAL]  | ! Calibration data     | eg. OPT420_S3W6D40_03CM_1000V_01.MLDAT          |
| [DATA.cruise.FASTIE.RAW]  | ! Raw cruise data      | eg. STN01_01M_1KV_01SEC_01.MLDAT                |
| [DATA.cruise.FASTIE.PRC]  | ! Processed data       | eg. STN01_01M_1KV_01SEC_01_PROC.MLDAT           |
| [DATA.cruise.CTD]         |                        |                                                 |
| [DATA.cruise.CTD.CAL]     | ! Calibration data     | eg. CTD_CALIB.TXT                               |
| [DATA.cruise.CTD.RAW]     | ! Raw cruise data      | eg. CTD_5000A_RAW.MLDAT                         |
| [DATA.cruise.CTD.PRC]     | ! Processed data       | eg. ROSETTE_BOTTLE_DATA.MLDAT                   |
| [DATA.cruise.CTD.TMP]     | ! Temporary data       | eg. CTD_BUF_01SEP92_1720.DAT                    |
| [DATA.cruise.TRANS]       |                        |                                                 |
| [DATA.cruise.TRANS.CAL]   | ! Calibration data     |                                                 |
| [DATA.cruise.TRANS.RAW]   | ! Raw cruise data      |                                                 |
| [DATA.cruise.TRANS.PRC]   | ! Processed data       |                                                 |
| [DATA.cruise.SPECTROM]    | ! Spectrophotometer    |                                                 |
| [DATA.cruise.LONGTRACK]   | ! Horizontal profiling | eg. STN01_TURNER.MLDAT                          |
| [DATA.cruise.STATION]     | ! Ancillary data       | eg. STN01_PUMP_CHL.MLDAT                        |
| [DATA.cruise.RADIOMETRIC] | ! Final processed      | eg. MOCE01_STN01.MLDAT                          |
| [DATA.cruise.ETC]         | ! Misc.                |                                                 |

### MLML\_DBASE Directories

| [MLDBASE]     |                     |                                 |
|---------------|---------------------|---------------------------------|
| [MLDBASE.BIN] | ! Executable files  | eg. MLML_ENTER.EXE              |
| [MLDBASE.COM] | ! VMS Command files |                                 |
| [MLDBASE.DOC] | ! Documentation     | eg. MLML_DBASE_INTRO.WP5        |
| [MLDBASE.ETC] | ! Misc.             | eg. TIDE_STATIONS.MLDAT         |
| [MLDBASE.INC] | ! Include files     | eg. MLML_DBASE.H MLML_DBASE.FOR |
| [MLDBASE.LIB] | ! Library files     |                                 |
| [MLDBASE.SRC] | ! Source code files | eg. MLML_ENTER.FOR              |
| [MLDBASE.TMP] | ! Temporary files   | eg. ?                           |

## Appendix 5. (continued) File Naming Conventions and Data Directory Structure.

**Program Directories:**


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|                  |                     |                                       |
|------------------|---------------------|---------------------------------------|
| [MLLIBRARY]      |                     |                                       |
| [MLLIBRARY.BIN]  | ! Executable files  | eg. HPL.EXE                           |
| [MLLIBRARY.DOC]  | ! Documentation     |                                       |
| [MLLIBRARY.LIB]  | ! Library files     | eg. MLCLIB.TLB MLLIB.OLB              |
| [MLLIBRARY.INC]  | ! Include files     |                                       |
| [MLLIBRARY.SRC]  | ! Source code files | eg. C_FILES.C UNESCO_83.FOR           |
| [NOAA]           |                     |                                       |
| [NOAA.BIN]       | ! Login directory   | eg. LOGIN.COM DECW*.*                 |
| [NOAA.COM]       | ! Executable files  | eg. MOS.EXE SIS.EXE                   |
| [NOAA.DOC]       | ! VMS Command files | eg. MOS.COM SIS.COM                   |
| [NOAA.ETC]       | ! Documentation     | eg. DATA_PROCESSING.TXT MOS_SETUP.WP5 |
| [NOAA.etc]       | ! Misc.             |                                       |
| [NOAA.INC]       | ! Include files     | eg. MOS_TYPES.H                       |
| [NOAA.LIB]       | ! Library files     |                                       |
| [NOAA.SRC]       | ! Source code files | eg. MOS.C SIS.C                       |
| [NOAA.TMP]       | ! Temporary files   | eg. ?                                 |
| [NOAA.DATA_FLEX] | ! DATAFLEX files    | eg. EQUIPMENT.FRM .FLX .DAT           |
| [NOAA.FORTH]     | ! FORTH code files  | eg. MOS.SCR                           |
| [CTD]            |                     |                                       |
| [CTD.BIN]        | ! Login directory   | eg. LOGIN.COM DECW*,*                 |
| [CTD.COM]        | ! Executable files  | eg. MLML_CTD_ACQ.EXE                  |
| [CTD.DOC]        | ! VMS Command files | eg. START_CTD.COM                     |
| [CTD.ETC]        | ! Documentation     | eg. CTD_SETUP.WP5                     |
| [CTD.etc]        | ! Misc.             |                                       |
| [CTD.INC]        | ! Include files     | eg. CTD_TYPES.H                       |
| [CTD.LIB]        | ! Library files     | eg.                                   |
| [CTD.SRC]        | ! Source code files | eg. MLML_CTD_ACQ.C                    |
| [CTD.TMP]        | ! Temporary files   | eg. ?                                 |

---

Appendix 5. (continued) Logical Name Table used in NOAA data processing programs.

### VMS Logicals:

---

Setup by SY\$MANAGER:SETUP\_NOAA\_LOGICALS.COM:

```
$ DEFINE/EXEC/SYS NOAA$ROOT USER$DEV: [NOAA.]
$ DEFINE/EXEC/SYS NOAA$DIR USER$DEV: [NOAA]
$ DEFINE/EXEC/SYS NOAA$SRC NOAA$ROOT: [SRC]
$ DEFINE/EXEC/SYS NOAA$BIN NOAA$ROOT: [BIN]
$ DEFINE/EXEC/SYS NOAA$COM NOAA$ROOT: [COM]
$ DEFINE/EXEC/SYS NOAA$LIB NOAA$ROOT: [LIB]
$ DEFINE/EXEC/SYS NOAA$INC NOAA$ROOT: [INC]
$ DEFINE/EXEC/SYS NOAA$DOC NOAA$ROOT: [DOC]
$ DEFINE/EXEC/SYS NOAA$ETC NOAA$ROOT: [ETC]
$ DEFINE/EXEC/SYS NOAA$TMP NOAA$ROOT: [TMP]
$ DEFINE/EXEC/SYS NOAA$FORTH NOAA$ROOT: [FORTH]
$ DEFINE/EXEC/SYS NOAA$SCRATCH NOAA$TMP
```

Setup by SY\$MANAGER:SETUP\_CTD\_LOGICALS.COM:

```
$ DEFINE/EXEC/SYS CTD$ROOT USER$DEV: [CTD.]
$ DEFINE/EXEC/SYS CTD$DIR USER$DEV: [CTD]
$ DEFINE/EXEC/SYS CTD$SRC CTD$ROOT: [SRC]
$ DEFINE/EXEC/SYS CTD$BIN CTD$ROOT: [BIN]
$ DEFINE/EXEC/SYS CTD$COM CTD$ROOT: [COM]
$ DEFINE/EXEC/SYS CTD$LIB CTD$ROOT: [LIB]
$ DEFINE/EXEC/SYS CTD$INC CTD$ROOT: [INC]
$ DEFINE/EXEC/SYS CTD$DOC CTD$ROOT: [DOC]
$ DEFINE/EXEC/SYS CTD$ETC CTD$ROOT: [ETC]
$ DEFINE/EXEC/SYS CTD$TMP CTD$ROOT: [TMP]
$ DEFINE/EXEC/SYS CTD$SCRATCH CTD$TMP
```

Setup by USER\$DEV: [DATA.COM]SETUP.COM:

```
$ DEFINE/EXEC/SYS DATA USER$DEV: [DATA.cruise.]
```

### VMS Symbols:

---

Setup by USER\$DEV: [NOAA]LOGIN.COM:

```
$ MOS === @NOAA$COM:MOS
$ SIS === @NOAA$COM:SIS
$ FASTIE === @NOAA$COM:FASTIE
$ GPS === SUBMIT/LOG=DATA:[STATION]GPS.LOG/NAME=GPS_LOGGER NOAA$COM:START_GPS
```

Setup by USER\$DEV: [CTD]LOGIN.COM:

```
$ CTD === @CTD$COM:START_CTD_ACQ
$ GPS === SUBMIT/LOG=DATA:[STATION]GPS.LOG/NAME=GPS_LOGGER NOAA$COM:START_GPS
```

Setup by USER\$DEV: [CTD]LOGIN.COM:

```
$ CTD === @CTD$COM:START_CTD_ACQ
$ GPS === SUBMIT/LOG=DATA:[STATION]GPS.LOG/NAME=GPS_LOGGER NOAA$COM:START_GPS
```

