

# 1 Thermal, Mechanical and Shape Memory Properties of Nano-rubber 2 Toughened Epoxy-based Shape Memory Nanocomposites

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## 14 Abstract

15 Epoxy-based shape memory polymer (ESMP) is a kind of the most promising engineering smart  
16 polymers. However, the inherent brittleness limits its application. The existing modification  
17 approaches are either based on complicated chemical reactions or at the cost of thermal  
18 properties of ESMP. In this study, a simple approach is made to the fabrication of ESMP aiming  
19 to improve its overall properties by introducing cross-linked carboxylic nitrile/butadiene  
20 nano-rubber (CNBNR) into ESMP network. The results show that the toughness of  
21 CNBNR/ESMP nanocomposites greatly improved at both room temperature and  $T_g$  in  
22 comparison with pure ESMP. Meanwhile, the increase of toughness has no sacrifice of other  
23 macroscopic properties. CNBNR/ESMP nanocomposites present improved thermal properties

1 with glass transition temperature ( $T_g$ ) in a stable range around 100 °C, enhanced thermal  
2 stabilities, and superior shape memory performance in terms of shape fixing ratio, shape  
3 recovery ratio, shape recovery time and repeatability of shape memory cycles. The combined  
4 property improvements and the simplicity in manufacture process demonstrate that  
5 CNBNR/ESMP nanocomposites are desirable candidates for large-scale application in  
6 engineering field as smart structural materials.

7 **Keywords:** A. Smart materials, Nano composites; B. Mechanical properties, Thermal properties,  
8 Thermomechanical properties

### 9 **1. Introduction**

10 Shape memory polymers (SMPs) as a class of smart materials are capable of returning to its  
11 initial shape from a temporary shape when they are actuated by heat, light, electrical or magnetic  
12 fields, moisture, and PH value, etc.<sup>1-6</sup> These smart characteristics enable SMPs potentially to be  
13 applied in the areas ranging from deployable aerospace structures to biomedical devices.<sup>7-12</sup>  
14 SMPs are generally divided into either thermoplastic or thermoset classes according to the  
15 chemical structures. The networks of thermoset SMPs are based on covalently cross-linking  
16 points, while those of thermoplastic SMPs are usually consisted of physically cross-linking  
17 points.<sup>1,10,13,14</sup> Compared with thermoplastic SMPs, thermoset SMPs always present high  
18 reliability and superior shape memory behavior because of their stable covalently cross-linking  
19 networks.<sup>15,16</sup> Owing to such unique features, thermoset SMPs have been investigated  
20 extensively in recent years.

21 Epoxy-based SMPs (ESMPs) are one of the most important thermoset SMPs. Except for the  
22 general capabilities of thermoset SMPs, ESMPs also provide their own attractive properties,  
23 including adjustable and high glass transition temperature ( $T_g > 80$  °C), excellent thermal

1 performance, high modulus and fracture strength, rapid responsive speed, chemical durability,  
2 and easy processing, etc.<sup>17-22</sup> These characteristics make ESMPs extremely acceptable to be  
3 applied as engineering smart and structural materials. However, pristine ESMPs suffer from  
4 inherent brittleness caused by the relatively high cross-linking structures.<sup>23-26</sup> Such drawbacks  
5 induce ESMPs sensitive to fatigue and cracks, which severely hinders their way for practical  
6 applications.<sup>25</sup> To overcome this challenge, extensive researches to improve the toughness of  
7 ESMPs have been carried out worldwide.<sup>25,27-30</sup> For examples, Hartwig et al. prepared ESMPs  
8 with partially crystal structures by cationic polymerization with poly ( $\omega$ -pentadecalactone)  
9 (PPDL). Such epoxy/PPDL composite showed good shape-memory cycle stability and enhanced  
10 strength and toughness.<sup>27</sup> Huang et al. fabricated a novel ESMP by introducing oxyethylene  
11 groups to diglycidyl ether of 9,9-bis (4-hydroxyphenyl) fluorine (DGEBF). The cured  
12 9,9-bis [4-(2-hydroxyethoxy) phenyl] fluorine/4,4'-diamin-odiphenylsulfone (DGEBEF/DDS)  
13 polymeric network exhibited superior low water uptake, mechanical properties and thermal  
14 stability.<sup>28</sup> Xie, et al. recently reported a kind of ESMP with strain at break of 111% above  $T_g$   
15 and 212% at  $T_g$ , respectively.<sup>25</sup> They greatly improved the toughness of ESMPs at high  
16 temperature.

17 The above mentioned researches have significantly paved the way for improving the toughness  
18 of ESMPs. However, some of the modification methods rely on complicated chemical reactions  
19 which restrict large-scale applications of ESMPs, while others either sacrifice their thermal  
20 capabilities or mechanical properties at room temperature. It is still urgently needed to further  
21 enhance the overall performance and simplify the fabrication methods for ESMPs to enable their  
22 large-scale applications as smart structural materials in engineering and other necessary areas. To  
23 achieve this, simple and effective composite approaches always are used for the development of

1 ESMPs. Previous composite strategies generally focused on carbon nanotubes, carbon black,  
2 carbon fibers, iron oxide, and silicon carbide, etc.<sup>18,31-36</sup> These fillers greatly improved the  
3 thermal properties and mechanical strength of ESMPs. However, the toughness of such stiff  
4 fillers reinforced ESMP composites declined seriously. Moreover, it is quite difficult to use them  
5 as composite matrix for smart structures.

6 Cross-lined carboxylic nitrile/butadiene nano-rubber (CNBNR) powder is well-known for  
7 toughening epoxy without cost of their heat resistance.<sup>37,38</sup> Meanwhile, CNBNR is easy to be  
8 uniformly dispersed in epoxy resins and preserve the characteristic of epoxy for composite  
9 matrix.<sup>39,40</sup> Therefore, such kind of elastomeric nanoparticles may be one of the best choices of  
10 fillers for ESMP-based composites to achieve excellent comprehensive performances. Based on  
11 these advantages, in this study, CNBNR was introduced into ESMP network for improving the  
12 toughness and maintain other macroscopic properties of such smart material to broaden their  
13 engineering applications. A systematic research is constructed on CNBNR/ESMP  
14 nanocomposites. The macroscopic capabilities, including thermal properties, thermal stabilities,  
15 and mechanical properties are investigated in detail. The potential mechanism of CNBNR for  
16 improving the overall properties of CNBNR/ESMP nanocomposites are discussed. We achieve  
17 the optimized content of CNBNR for the excellent overall properties, and the shape memory  
18 performance of nano-rubber toughed materials are first systematically investigated.

19 **Materials and Methods**

20 **2.1 Materials**

21 The epoxy-based shape memory polymer (ESMP) was prepared according to our previous  
22 studies, which was a kind of thermoset cross-linking network containing three ingredients-epoxy  
23 resin, hardener and accelerator.<sup>30</sup> Cross-linked carboxylic nitrile/butadiene nano-rubber powder

1 (CNBNR, Narpow VP-501 particle size distribution: 50-100 nm,  $T_g$ : -29.1 °C, acrylonitrile  
2 content: 26 wt.%), was supplied by Beijing Research Institute of Chemical Industry, China. To  
3 remove the moisture, CNBNR was dried in an oven at 50 °C for 24 h under vacuum before  
4 mixing.

## 5 **2.2 Methods**

### 6 **2.2.1 Sample preparation**

7 Firstly, a masterbatch was prepared. 20 phr (per hundred parts epoxy resin) CNBNR was added  
8 into a baker containing 100 phr epoxy resin and premixed by manual stirring for 10 min. The  
9 obtained mixture was transferred to ARE 500 planetary centrifugal mixer for speed mixing at  
10 300 rpm for 3 min, 500 rpm for 2 min and 1000 rpm for 1 min. To achieve homogeneous  
11 masterbatch, the above blend was further dispersed by three-roll mill for 6 times with gradually  
12 reduced the gap between rollers (from 30  $\mu\text{m}$  to 5  $\mu\text{m}$ ). The ready masterbatch was then divided  
13 into four parts with equal weight. Different amounts of epoxy resin (75, 25, 8.3, 0 g) and  
14 hardener (80, 40, 26.7, 20 g) were added into each part, respectively, to prepare 5, 10, 15, and 20  
15 phr CNBNR/ESMP nanocomposites. The mixing process was proceeded by continuously  
16 mechanical stirring with speed gradually increasing from 300 rpm to 1000 rpm at 80 °C. After 45  
17 min, accelerator was given with the weight ratio of accelerator/(epoxy resin+ hardener) = 1/50,  
18 and mixed for another 10 min at 1000 rpm. Such blend was degassed in a vacuum oven at 80 °C  
19 for 15 min to remove bubbles. Then, it was put into preheated glass molds with different  
20 thickness and cured at 80 °C for 2 h, 100 °C for 3 h, and 150 °C for another 5 h. The  
21 CNBNR/ESMP nanocomposites could be achieved by cooling down to room temperature. For  
22 comparison, pure ESMP was fabricated by directly mixing epoxy resin, hardener and accelerator  
23 by mechanical stirring at 300 rpm. The curing condition of pure ESMP was set the same with

1 CNBNR/ESMP nanocomposites. The nomenclature and the composition of the prepared  
2 materials are given in Table 1.

### 3 **2.2.2 Characterizations**

4 **Thermal Analysis.** Differential Scanning Calorimetry (DSC: DSC/700/1410, Mettler-Toledo)  
5 was used to study the phase transition behaviors. The temperature ranged in 25~200 °C with a  
6 rate of 5 °C /min under nitrogen atmosphere. The thermal stabilities were tested by  
7 Thermogravimetric Analysis (TGA: TGA/DSC1 SF1942, Mettler-Toledo) under nitrogen  
8 atmosphere with the temperature changing from 25 °C to 600 °C at 10 °C /min. The chemical  
9 structures were conducted using a Fourier Transform Infrared (FTIR: Spectrum One,  
10 PerkinElmer) spectrometer by dispersing powder sample in a KBr pellet. The test was  
11 undertaken in a spectral range of 4000–370  $\text{cm}^{-1}$  and a resolution of 4  $\text{cm}^{-1}$ .

12 **Static Mechanical Analysis.** The static mechanical properties at room temperature ( $25\pm 2$  °C)  
13 and 100 °C were characterized by a universal material testing machine (Z050, Zwick/Roell) with  
14 a thermal chamber under tensional mode. Dog-bone shaped specimens (ASTM D638, Type IV)  
15 were cut off from the prepared plates by a laser cutting machine. A crosshead speed of 5 mm/min  
16 was utilized for testes at both room temperature and at 100 °C. The fractured surfaces were  
17 observed by Scanning Electron Microscopy (SEM: VEGA3SB, Tescan) after sputter-coating  
18 with gold.

19 **Shape memory behavior.** Dynamic Mechanical Analysis (DMA: Q800, TA Instruments) under  
20 single-cantilever mode was carried out to evaluate the thermal-mechanical properties. The  
21 temperature ranged from 25 °C to 150 °C at a rate of 5 °C/min. A frequency of 1Hz was  
22 employed during the whole test. Sample dimension is  $35\times 13\times 3$   $\text{mm}^3$ . A bending-recovery test  
23 was carried out to qualitatively investigate the shape memory behavior. A rectangular specimen

1 with dimension of  $30 \times 5 \times 1 \text{ mm}^3$  was defined as original shape. First, it was heated to  $T_g$  and  
2 bended into a “U”-like shape after it became flexible. Then, temporary shape was achieved by  
3 cooling down the deformed shape to room temperature under external force. The shape recovery  
4 phenomenon was monitored by imaging process when reheating the deformed sample to  $T_g$ . The  
5 shape recovery time and the shape recovery angle as a function of time were obtained from the  
6 recorded images. Shape memory cycle (SMC) proceeded on DMA (Q800, TA Instruments) was  
7 utilized to characterize the shape memory behavior quantitatively. The test was performed under  
8 tensional film fixture and a preload of 0.01N was imposed ( $30 \times 4 \times 1 \text{ mm}^3$ ) to protect specimen  
9 from slide. The procedures for the SMC include (Figure S1): 1) Heat the sample to  $T_g$  for  
10 deformation. 2) Isothermally stretch the soft sample to a certain strain with a constant stress. 3)  
11 Cool down the deformed sample to room temperature under the same load to maintain the  
12 temporary shape. 4) Elevate temperature to  $T_g$  to induce the active shape recovery. Shape fixed  
13 ratio ( $R_f$ ) and shape recovery ratio ( $R_r$ ) were obtained by the following equations<sup>19,41-43</sup>:

$$14 \quad R_f = \frac{\varepsilon_f}{\varepsilon_{load}} \times 100\% \quad 1$$

$$15 \quad R_r = \frac{\varepsilon_f - \varepsilon_{rec}}{\varepsilon_f} \times 100\% \quad 2$$

16 where  $\varepsilon_{load}$  stands for the strain under external stress,  $\varepsilon_f$  is the strain after unloading,  $\varepsilon_{rec}$   
17 represents for residual strain after recovering.

### 18 **3. Results and Discussion**

#### 19 **3.1 Thermal properties**

20 Figure 1 shows the thermal analysis results for pure ESMP, CNBNR and CNBNR/ESMP  
21 nanocomposites. The typical DSC curves in Figure 1a reflect the thermal transition behavior of  
22 the prepared materials. To eliminate the influence of heating history, the secondary heating scan

1 is used in this analysis. The step in Figure 1b indicates the occurrence of glass transition during  
2 heating process. The DSC results qualitatively show that the introduction of CNBNR has no  
3 negative effects on  $T_g$ . Instead, most  $T_g$  of CNBNR/ESMP nanocomposites are slightly higher  
4 than that of pure ESMP. Those results agree with previous studies done for the CNBNR toughed  
5 commercial epoxy composites.<sup>38,39</sup>

6 Thermal stabilities of CNBNR/ESMP nanocomposites can be evaluated in Figure 1c-1d. For  
7 each sample, only one degradative stage is found (Figure 1c), which is caused by the  
8 decomposition of polymeric backbone. Important thermal elements, including  $T_d$  (temperature  
9 relating to 5% weight loss), char yield,  $T_{max}$  (temperature of peak value in DTG curves) are  
10 extracted and listed in Table 2. Obviously, the decomposition of all the materials (relating to  $T_d$ )  
11 starts at above 325 °C, and most of them are higher than 347 °C. The major decomposition,  
12 judging by  $T_{max}$ , occurs at about 380 °C. These results demonstrate that the fabricated smart  
13 nanocomposites could be manipulated safely around their  $T_g$  range. Further observation find that  
14 CNBNR/ESMP nanocomposites show higher  $T_d$ ,  $T_{max}$  and char yield in comparison with the pure  
15 ESMP (except for the sample of 20 phr). It indicates that the thermal stabilities of  
16 CNBNR/ESMP nanocomposites are slightly improved by introducing CNBNR to the polymeric  
17 network.

18 From the consequences, it is easy to conclude that CNBNR/ESMP nanocomposites with addition  
19 of CNBNR less than 15 phr possessed better thermal capabilities than pure ESMP network. To  
20 study the possible reasons, FTIR tests were carried out and the results are shown in Figure 2. It  
21 can be obtained from Figure 2a that the improvement of the thermal properties is not caused by  
22 chemical reaction between CNBNR and ESMP, since there is no difference in their FTIR  
23 characteristic peaks. A close observation from the selected part in Figure 2a finds that the



1 absorption peaks belonging to hydroxyl group gradually move to a lower frequency as the  
2 content of CNBNR increasing (Figure 2b). It indicates the presence of enhanced hydrogen  
3 bonding between ESMP and CNBNR, which is the explanation for the increased thermal  
4 performance.<sup>37,38</sup> However, sample 20 phr is discovered for a decreased thermal properties and  
5 thermal stabilities comparing with pure ESMP. This is because when large amount of low  $T_g$   
6 material is added to a system, the part not join the network will not only decrease the interaction  
7 between nano-fillers and polymer matrix, but also result in a less cross-linking degree of the  
8 material system. In that case, lower  $T_g$  and  $T_d$  are achieved.

### 9 **3.3 Static mechanical properties**

10 To investigate the effectiveness of our proposed modification method on static mechanical  
11 properties, tensional tests were performed on CNBNR/ESMP nanocomposites at room  
12 temperature. Corresponding data are plotted in Figure 3a. The typical stress-strain curves vary  
13 from linearity to non-linearity gradually, indicating the mechanical behaviors of the prepared  
14 materials changing from brittle to ductile when the content of CNBNR is increased. Such  
15 phenomenon is also verified by the SEM images shown in Figure 4. The fractured surface of  
16 pure ESMP is extremely smooth, which reveals the highly brittle breakage (Figure 4a). However,  
17 the fractured cross-section in Figure 4b-4e become increasingly rough. Varied cracks  
18 propagations, plastic zone and shear flow become more and more visible and the amounts of  
19 them increases markedly as the content of CNBNR changing from 5 phr to 20 phr. It clearly  
20 indicates the fractured mode of the materials turns into ductile breakage.<sup>18,44</sup> In Figure 3b, an  
21 increase of *elongation at break* ( $\epsilon_b$ ) in the range of 49.5-736.4% can be seen by changing the  
22 content of CNBNR from 5 phr to 20 phr. However, only a slight drop of *Young's Modulus* ( $E$ )  
23 (5.6%-16.4%) is found as the CNBNR content varying from 5 phr to 20 phr, indicating the

1 remarkable improvement of  $\varepsilon_b$  has no dramatically negative effect on  $E$ . Meanwhile, *maximum*  
2 *strength* ( $\sigma_m$ ) improves by 29.2% when 10 phr CNBNR is used, although it presents a small  
3 decline after first increase. These results suggest that the introduction of CNBNR can greatly  
4 improve the ductility of CNBNR/ESMP nanocomposites and can maintain or slightly increase  
5 the strength at room temperature.

6 For ESMPs, it is equally important to investigate the static mechanical properties at temperature  
7 above  $T_g$ , because  $\varepsilon_b$  at rubbery state is an important parameter for their deforming performance.

8 In Figure 3c, the typical stress-strain curves demonstrate that the ductility at rubbery state boosts  
9 by the addition of CNBNR.  $\varepsilon_b$  values are improved from 22.1% for the pure ESMP to 44.7% for  
10 sample 20 phr CNBNR. It demonstrated the improvement of deformation capabilities of  
11 CNBNR/ESMP nanocomposites. Large deformation can be achieved at rubbery state without the  
12 breakage of the specimen, and this will be able to increase the safety and applications of ESMPs.

13 The area of strain-stress curve is always used for evaluating the toughness of the materials. From  
14 Figure 3d, it can be observed that both the toughness of CNBNR/ESMP nanocomposites at room  
15 temperature ( $KIC_{rt}$ ) and 100 °C ( $KIC_{100\text{ }^\circ\text{C}}$ ) greatly improved in comparison with pure ESMP.  
16 Such results indicate the effectiveness of CNBNR for toughening ESMP.

17 The enhancement of mechanical properties at both room temperature and high temperature are  
18 due to the introduction of flexible nano-fillers to the polymeric network. The ductile feature of  
19 CNBNR contributes to the high toughness of the materials, while the large surface energy caused  
20 by their nano-scale sizes and enhanced hydrogen bonding between CNBNR and ESMP are key  
21 driving elements for the high strength and modulus.<sup>38,39</sup> In general, CNBNR/ESMP  
22 nanocomposites show significantly enhanced mechanical properties.

### 23 **3.3 Shape memory properties**

1 Thermal-mechanical property was firstly studied as it has close relationship with shape memory  
2 behavior. Figure 5a shows that all the tested samples present a glassy platform at low  
3 temperature and follow by a sudden drop to the rubbery platform at high temperature. Such  
4 transformation reveals the occurrence of glass-rubber transition during heating process.  
5 Importantly, the changes of storage modulus between glassy state and rubbery state reach two  
6 orders of magnitude. It is the necessary pre-condition for shape memory function.<sup>30</sup> Peak value  
7 of loss factor is important reference for  $T_g$ . From Figure 5b and Table 2, it can be found that  $T_g$   
8 values vary in a narrow range around 100 °C. Moreover, the variation trend of  $T_g$  values obtained  
9 from DMA is similar to those obtained from DSC (Figure 2a). The increased  $T_g$  of  
10 CNBNR/ESMP nanocomposites in comparison of pure ESMP is attributed to the enhanced  
11 hydrogen bonding as we illustrated before. However, still no higher  $T_g$  is observed for sample 20  
12 phr. The underlying explanation can be found from SEM images in Figure 4. Different from  
13 others, some holes appear on the fractured surface of the sample 20 phr (Figure 4e), which can  
14 be clearly seen in Figure 4f. The presence of that indicates the nano-fillers aggregate into  
15 microscale particles, leading to less interfacial adhesion between CNBNR and ESMP. In that  
16 case, CNBNR acts as normal rubber.<sup>39</sup> Although it is still effective for improving toughness, no  
17 enhancement on thermal properties can be found.<sup>38</sup>

18 DMA results reveal that all CNBNR/ESMP samples display glass-rubber transitions, dramatic  
19 changes of storage modulus during heating process and final flat rubbery platforms. It indicates  
20 that all CNBNR/ESMP specimens are supposed to possess shape memory functions.<sup>25</sup> Herein,  
21 sample 15 phr is chosen for deep investigation of shape memory behavior based on its relatively  
22 excellent thermal and mechanical properties. A bending-recovery experiment was conducted  
23 firstly to qualitatively characterize the shape memory behavior. The corresponding results are

1 shown in Figure 6a-6b. The temporary “U”-like shape unfolds to the initial “-”-like shape with a  
2 fairly fast responsive speed. The shape recovery angle increases rapidly with time, and the entire  
3 shape recovery process happens in merely 25 s with nearly 100% shape recovery. Such  
4 consequences visually demonstrate the excellent shape memory performance of CNBNR/ESMP  
5 nanocomposite. SMC test was carried out on DMA to quantitatively analyze the shape memory  
6 function for the sample of 15 phr. To eliminate the effect of stress history, a secondary SMC is  
7 presented in Figure 6c for analyzing. According to Eq. 1 and Eq. 2, the calculated  $R_f$  and  $R_r$  are  
8 up to 96.3% and 97.6%, respectively, which implies the high shape fixing and recovery  
9 performance of CNBNR/ESMP nanocomposite.

10 It can be concluded from both quantitative and qualitative characterizations that CNBNR/ESMP  
11 nanocomposites present excellent shape memory performance. Such results are owing to the  
12 introduction of CNBNR to the ESMP network. As reported, shape memory behavior of polymer  
13 is based on their two-phase structures. One is soft domain that function to the shape deformation,  
14 the other is hard domain which is responsible for memorizing the original shape and shape  
15 fixation [2, 4, 13]. The introduction of elastic CNBNR nano-fillers indicates the increase of soft  
16 domains in ESMP network. More movable molecular segments contribute the easy deformation  
17 and fast recovery of CNBNR/ESMP nanocomposite. Meanwhile, the enhanced hydrogen bonds  
18 between CNBNR and ESMP construct more hard domains in the network, which enables high  $R_f$   
19 and  $R_r$  for CNBNR/ESMP nanocomposite.

20 Ten SMCs were further carried out to verify the repeatability of shape memory behavior. In  
21 Figure 6d, it can be seen that these cycles present reproducibility and consistency with high  $R_f$   
22 and  $R_r$ . Importantly, no damages appear even after ten testing cycles. This suggests that the shape  
23 memory behavior of the CNBNR/ESMP nanocomposite is highly repeatable with superior

1 fatigue resistance due to the high toughness at both room temperature and 100 °C. The near  
2 perfect shape memory behavior enable CNBNR/ESMP desirable for engineering smart  
3 application.

#### 4 **4. Conclusions**

5 A series of thermosetting shape memory nanocomposites of CNBNR/ESMP were constructed  
6 successfully, and their overall properties were investigated systematically. The thermal  
7 properties of the prepared nanocomposites were slightly improved in comparison to pure ESMP.  
8 CNBNR/ESMP nanocomposites showed  $T_g$  values varying in a narrow range around 100 °C  
9 (according to DMA test), high  $T_d$  and  $T_{max}$  up to 350 °C and 380 °C, respectively. It was also  
10 found that CNBNR/ESMP nanocomposites provided greatly enhanced ductility and strength at  
11 both room temperature and above  $T_g$  without excessive decrease of modulus. FTIR and SEM  
12 analysis indicated that enhanced hydrogen bonding and dispersion status of the nano-fillers were  
13 two controlled elements for the improvement of macro-scope properties of CNBNR/ESMP  
14 nanocomposites. Moreover, CNBNR/ESMP nanocomposite was demonstrated to possess near  
15 perfect and highly repeatable shape memory behavior. This research provides a feasible way for  
16 fabrication ESMP-based nanocomposite with improved toughness, meanwhile, without sacrifice  
17 of other properties, especially thermal properties and Young's Modulus. Such combined  
18 improvement of properties enable their large-scale applications in engineering fields.

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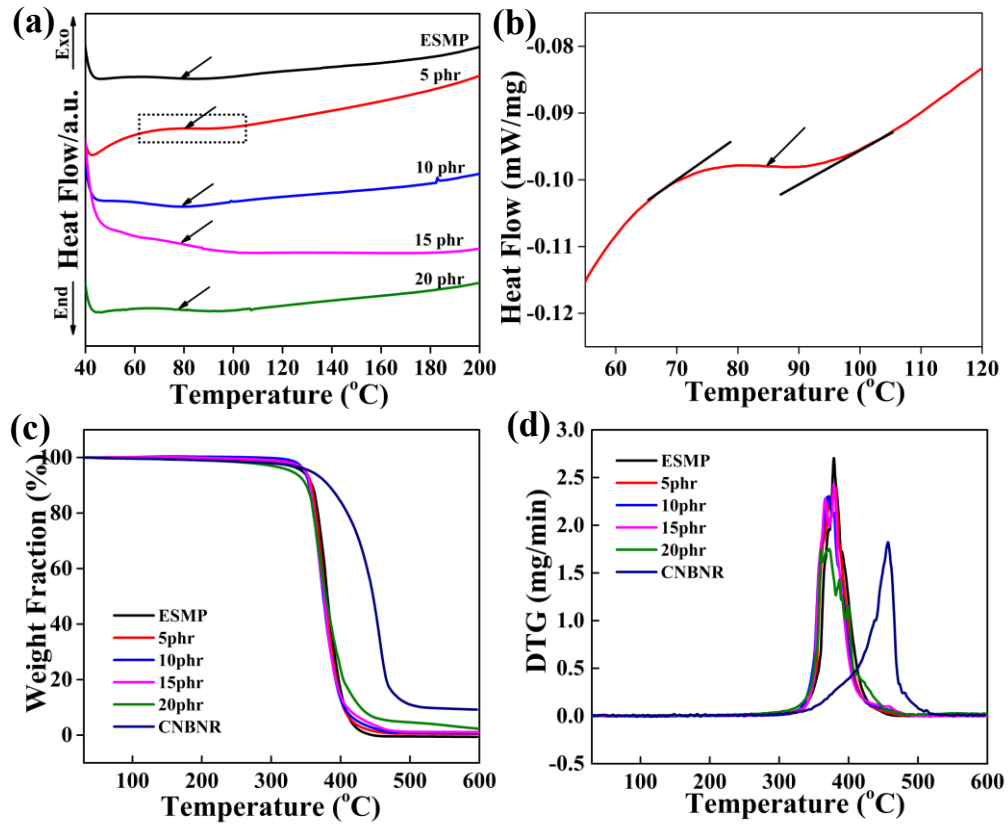
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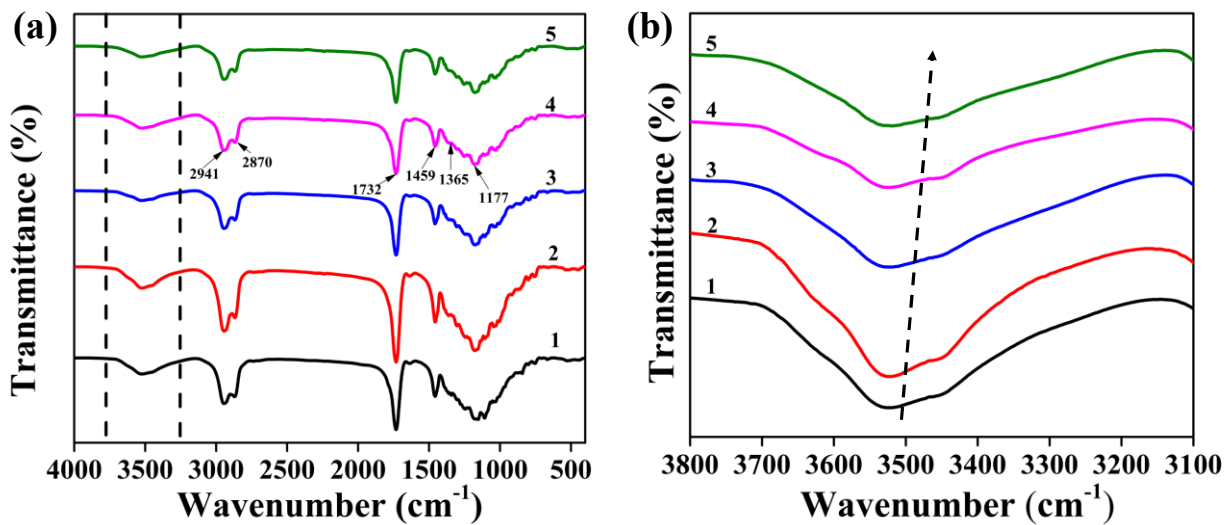
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Figure 1. Thermal properties of pure ESMP and CNBNR/ESMP nanocomposite: a. DSC thermo-grams; b. A magnification for selected part in Figure 1a; c. TG curves; d. DTG curves.

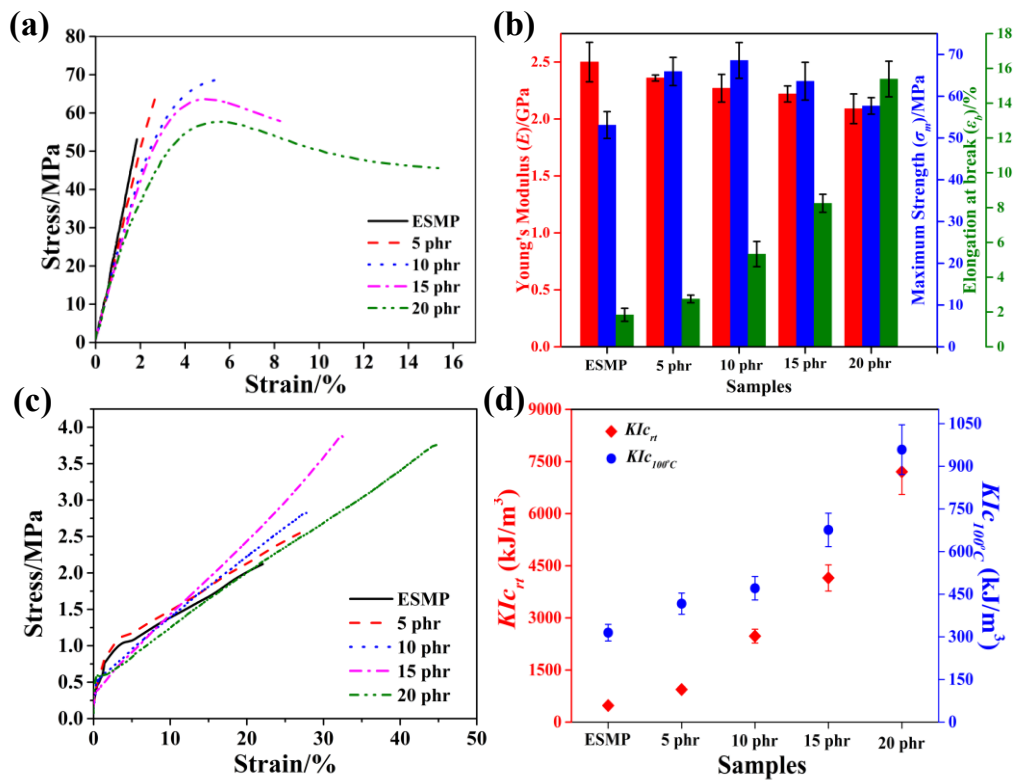




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 2 Figure 2. Chemical structure of pure ESMP and CNBNR/ESMP nanocomposites: a. FTIR  
 3 spectrums; b. The selected area in Figure 3a with high magnification. (1. pure ESMP; 2. 5phr; 3.  
 4 10 phr; 4. 15 phr; 5. 20 phr)

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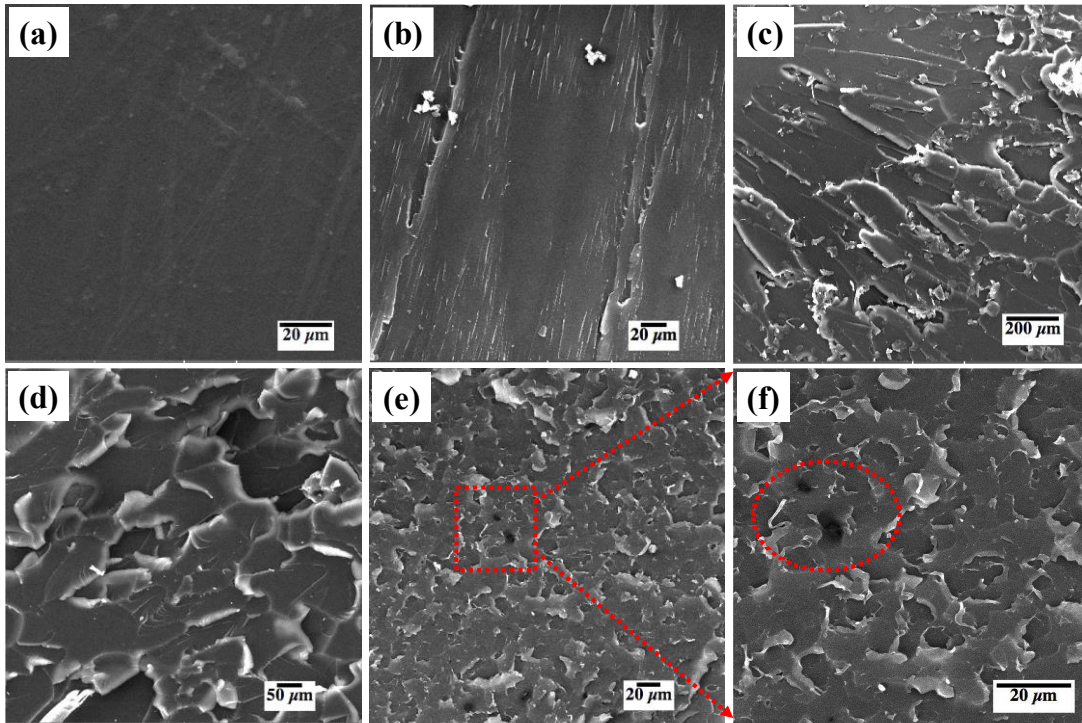
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4 Figure 3. Mechanical properties of pure ESMP and CNBNR/ESMP nanocomposites: a. Typical  
5 stress-strain curves at room temperature; b. Results of tensional test at room temperature; c.  
6 Typical stress-strain curves at 100 °C; d.  $KIc$  at room temperature and 100°C.

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Figure 4. SEM images of tensional fractured cross section of CNBNR/ESMP nanocomposite

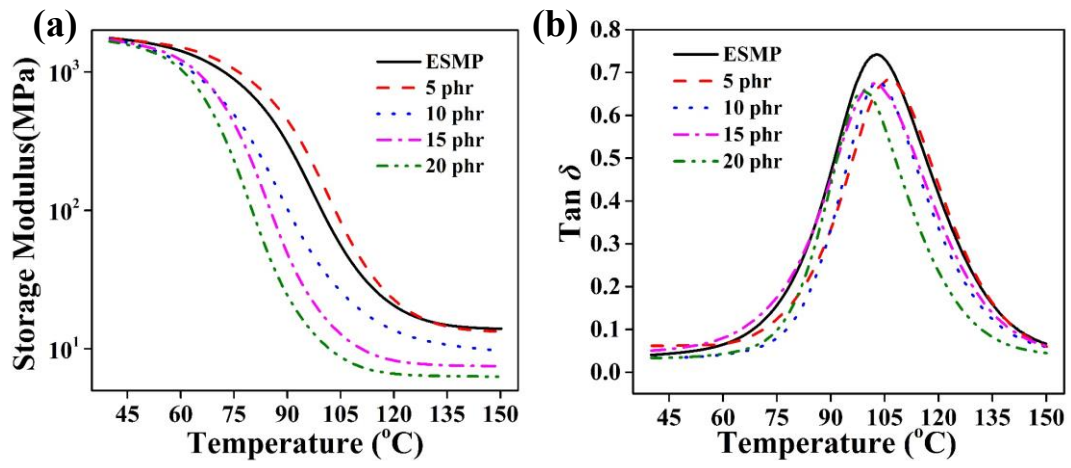
4 series: a. Pure ESMP; b. 5 phr; c. 10 phr; d. 15 phr; e. 20 phr; f. A magnification for selected part

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in Figure 4e.

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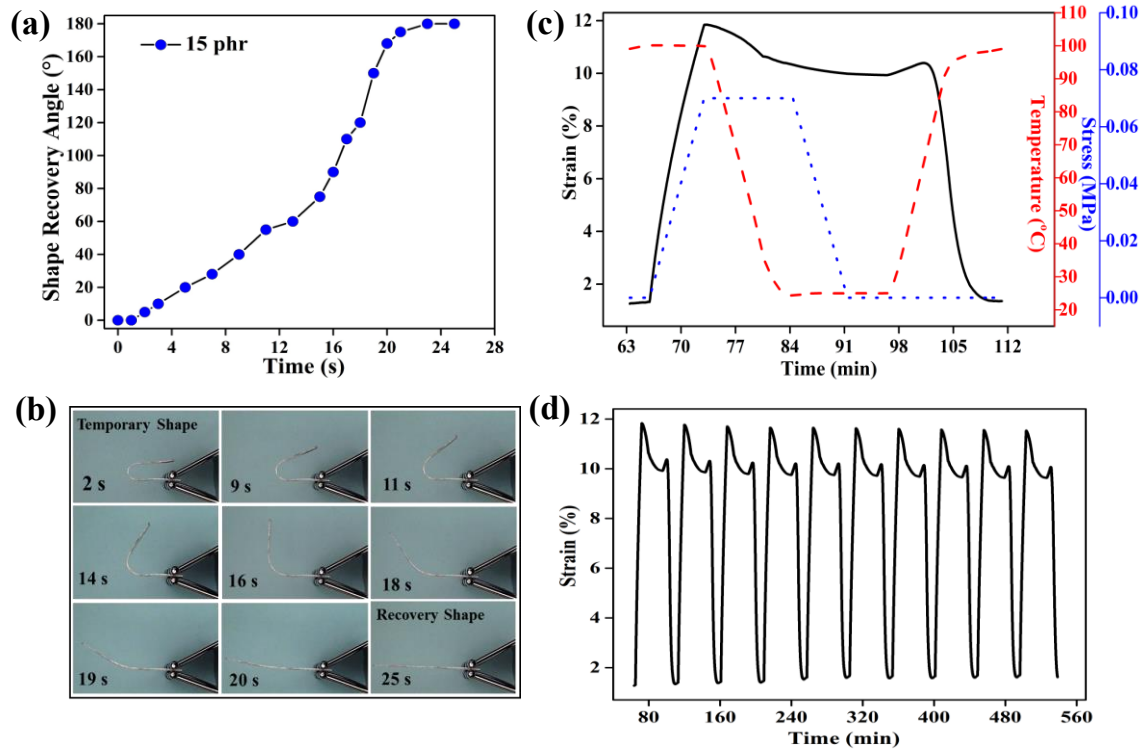
3 Figure 5. DMA results of pure ESMP and CNBNR/ESMP nanocomposites: a. Storage modulus

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and b.  $\text{Tan } \delta$  as a function of temperature.

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3 Figure 6. Characterization of shape memory behavior of sample 15 phr: a. Shape recovery as a  
4 function of time; b. Visual demonstration of shape memory behavior at 100 °C; c. The secondary  
5 SMC proceeded on DMA; d. Ten SMCs performed on DMA.

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Table 1. Compositions of CNBNR/ESMP nanocomposites

Sample \ Ingredient	Epoxy resin (g)	Hardener (g)	Accelerator (g)	CNBNR (g)
ESMP	25	20	0.9	0
5 phr	100	80	3.6	5
10 phr	50	40	1.8	5
15 phr	33.3	26.7	1.2	5
20 phr	25	20	0.9	5

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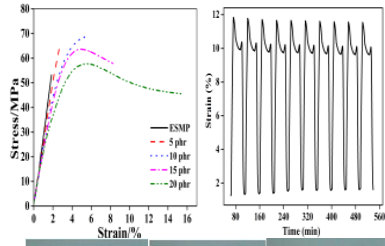
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Table 2. Thermal Properties of pure ESMP, CNBNR and CNBNR/ESMP nanocomposites

Sample Name	TGA			DMA
	$T_d$ (°C)	$T_{max}$ (°C)	Char yield (%)	$T_g$ (°C)
ESMP	344.9	378.6	0	102.9
5 phr	349.6	380.3	0.5	106.5
10 phr	347.8	378.9	0.7	103.5
15 phr	348.9	378.7	1.1	101.2
20 phr	329.7	375.0	2.3	99.5
CNBNR	357.3	457.1	9.2	-

# 1 Graphical Abstract



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