MODULAR INVERTER FOR ADVANCED CONTROL APPLICATIONS

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Modular Inverter for Advanced Control Applications

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In the fall of 2003, a team of graduate students was assembled to design and construct a research-grade inverter. The goal was to have available a set of well-documented inverters of various ratings capable of quickly implementing a new control algorithm. A body of research has already resulted from this project, with more in progress. This technical report contains all of the important specifications and design details required to use and repair modular inverters.

The project team was led by Jonathan Kimball. Important contributors include:

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Special thanks to the several undergraduates who assisted in the construction and assembly of the finished units. Thanks also to the ECE Machine Shop for modifying and fabricating enclosures and other hardware.

This work was supported by the Grainger Center for Electric Machinery and Electromechanics and was advised by Prof. Philip Krein and Prof. Patrick Chapman.

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Specification Document

Modular Inverter System Specification

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Abstract:

This document provides an overview of the modular inverter design project, as well as specifying interconnects where applicable. It is not intended to be comprehensive, but it does specify necessary functionality.

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Document Revision History

Issue	Date	Comments
000	8/15/2003	Released for comments and review. Not intended to be the final spec.
001	9/9/2003	Released as a "final" version after substantial review.
002	11/21/2003	Minor changes as project continues

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1. Introduction

The purpose of the modular inverter project is to provide test beds for future projects. Deliverables include:

- 40A, 30VDC inverter stage
- 20A, 60VDC inverter stage
- 40A, 400VDC inverter stage (possibly pushed off until the spring semester)
- Control box based on a TI 2812 DSP
- DSP software to provide interface to a PC
- DSP software for V/Hz operation

The desired time frame is to have functional hardware by the end of the fall semester of 2003, with at least the output stages thoroughly debugged. At least some software should also be done at this time. The complete software project should be finished by the beginning of fall '04.

This project is supported by the Grainger Center for Electric Machinery and Electromechanics.

1.1 Scope

The software developed will be primarily limited to minimal functionality such that someone doing a motor project can get up and running quickly, or someone can develop PC software to implement an advanced algorithm. Actual vector control algorithms will be implemented by the specific researcher. It is also desirable to use canned vector control algorithms such that a demo can be done for ECE333 or ECE468 during spring '04.

The hardware will be rugged and debugged well enough for the average graduate student to use it. It does not need to be rugged enough for classroom purposes at this time.

The initial designs are for the standard inverter topology. If possible, it would be nice to be able to change to an SR (switched reluctance) topology. If the added flexibility degrades the performance of the standard topology, then the SR topology will be pushed off to a future output stage design.

Initially, three of each unit will be built. Eventually, ten control boxes will be built so that many researchers can do different things at the same time.

1.2 Definitions

Control box: a box containing the DSP and various interface ports, which generates PWM commands.

Output stage: a box containing four halfbridges, interface to the control box, some logic, and gate drivers.

Power stage: subsystem of the output stage consisting of only the power handling devices.

Output connector: the connector between the control box and the output stage. Actually two connectors, one analog, one digital.

1.3 References

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2. Output Connectors

2.1 General Principles

The digital signals are transmitted as RS-422 differential pairs. The output stage should include pull-up and pull-down resistors such that when the connector is unplugged, the power stage is open-circuited.

The analog signals use a maximum range of ±10V. A Kelvin analog grounds (one or more) are included. The control box should treat all signals as differential with respect to the Kelvin.

There are two connectors, one analog and one digital. Both are ribbon cables. Latching headers are preferred. For the digital connector, use Vari-Twist cable, which pairs adjacent conductors. For the analog connector, consider using shielded ribbon cable if a suitable type can be found.

All of the "GND" connections are tied together at both ends of the cable. Within each box, it is recommended to separate digital, analog, and power grounds between the cable and the rest of the circuitry. "GND" is connected to earth via a resistor and a capacitor in parallel (relatively low impedance).

The power supplies on the connectors are intended to power analog and digital circuitry in the control box. They originate in the output stage. Current requirements are TBD.

It is assumed that the bus supply to the power stage is at a very different potential than earth. Full isolation is required between the output connectors and the power stage.

2.2 Digital Connector Pin-out

Pin	Signal	Pin	Signal
1	+5V	18	~D1
2	GND	19	D2
3	+5V	20	~D2
4	GND	21	ENABLE
5	A1	22	~ENABLE
6	~A1	23	FAULT
7	A2	24	~FAULT
8	~A2	25	uC_RESET
9	B1	26	~uC_RESET
10	~B1	27	RESERVED
11	B2	28	RESERVED
12	~B2	29	RESERVED
13	C1	30	RESERVED
14	~C1	31	RESERVED
15	C2	32	RESERVED
16	~C2	33	RESERVED
17	D1	34	RESERVED

2.3 Details of Digital Connector

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A1 corresponds to the upper device of phase A. A2 corresponds to the lower device of phase A. \A1 and \A2 are the complements of A1 and A2 respectively for RS-422. It is recommended to use DS26LS31 transmitters and DS26LS32 receivers, or equivalent or superior devices. These are quad line drivers and receivers. Remember to terminate the line properly, as well as inserting proper pull-up and pull-down resistors to bias the signal in the event of an open-circuit.

Similarly, (\)Bn correspond to phase B, (\)Cn correspond to phase C, and (\)Dn correspond to phase D. Typically, for a three-phase inverter, phases A, B, and C are used as a positive sequence, but other topologies and other sequences are possible and allowable.

FAULT, ENABLE, and uC_RESET are similar RS-422 signals. When everything is OK, FAULT and ENABLE should both be high and uC_RESET should be low. FAULT indicates that a fault has been detected in the output stage. ENABLE is low until the processor is ready to start providing PWM commands. uC_RESET pulses to clear a fault.

Note that only the first 26 pins are used at this time. A 34-pin connector is used to distinguish it from the analog connector, as well as providing room for future expansion. Leave the unused pins floating at this time. Note that it is possible to use 26-conductor Vari-Twist cable at this time, which is available from ECE Stores.

2.4 Analog Connector

Pin	Signal	Pin	Signal
1	GND	14	KELVIN2
2	+15V	15	RESERVED
3	-15V	16	RESERVED
4	GND	17	RESERVED
5	IA	18	RESERVED
6	IB	19	KELVIN3
7	IC	20	GND
8	ID	21	GND
9	KELVIN1	22	VA
10	VBUS	23	VB
11	T1	24	VC
12	T2	25	VD
13	IBUS	26	KELVIN4

2.5 Details of Analog Connector

IA, IB, IC, and ID correspond to phase currents on phases A, B, C, and D respectively. They are positive for current going out of the power stage. VA, VB, VC, and VD are phase voltages with respect to the negative bus, corresponding to phases A, B, C, and D respectively. Vbus is the total bus voltage. T1 and T2 are relevant temperatures. Scaling is discussed in section 3.

Kelvin ground connections are provided, one for each group of signals. All analog signals should be treated as differential with respect to the corresponding Kelvin connection. This eliminates voltage drop and noise in the current-carrying ground wires from influencing the analog measurements. Note that the groups are in fours, for either quad op amps or two dual op amps per Kelvin.

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3. Details of Output Stage Logic and Analog

3.1 Logic

At a minimum, the logic must prevent simultaneous turn-on of both devices in a halfbridge. Preferably, minimum deadtime will be enforced. The minimum deadtime must be specified, so that the software designer can account for it. Typically, the software will insert deadtime greater than the minimum, so that the output stage logic is transparent.

Faults will be detected as described in section 3.3. On any fault, the logic must latch, turn off all devices, and signal a fault on the output connector. Faults are reset on power-up, and only on power-up.

It is also desired to support a minimal command function, where only the upper device commands are supplied. This will be jumper selectable. The logic must then perform inversion with deadtime to generate the lower device commands.

3.2 Analog

The phase currents will be detected by closed-loop Hall-effect devices or equivalent. The analog circuitry will condition these signals, typically a current that is some fixed ratio of the phase current, into properly scaled voltage signals. Scaling is such that the rated RMS current (e.g. 20A) corresponds to 4.5V. This allows proper headroom for overload and ripple below the 10V maximum. The signals are bipolar, positive for outgoing current. It is desirable to include some means of reducing the scale factor to correspond to a lower rated RMS current, yielding greater signal amplitude for smaller machines. This can be a resistor change, a jumper, or changing the number of turns through the sensor.

The bus voltage and phase voltage sensing circuits must be isolated from the main analog circuitry. The lowest-tech way to perform isolation is through differential amplifiers with large resistors. In this case, the resistors must be sized so that at maximum voltage rating of the power stage, the resistor current is less than 5 mA. Take some care in designing the remainder of the circuit, particularly in choosing an op amp, to account for large resistor values with tolerance. These signals are mostly unipolar, although phase voltage does extend below the negative bus by at least a diode drop. These signals should be scaled so that maximum voltage rating corresponds to an 8V signal, for headroom.

Minimize the filtering on voltage and current signals. The control box is responsible for low-pass filtering to prevent aliasing of the A/D converter. Since the output stage designer has no control over the sampling rate, achieve the highest bandwidth possible in the analog signals and let the control box designer make the filtering decisions.

There is also allowance for up to two temperature feedback signals. These should be scaled so that 0°C = 0 V, 100°C = 5V. The sensors should be placed in relevant positions on e.g. the heat sink.

3.3 Fault Detection

Within the output stage, the following faults should be detected and latched:

- Short-circuit. This is sensed via desaturation detection. Even in MOSFET-based designs, short-circuits can be destructive and require shutdown within 10 µs.

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- Overcurrent. Trip at 9.75V of current feedback. Some filtering is allowable, but shutdown within 100 μs is advised.
- Overvoltage. Trip at an appropriate level that will prevent damage to any of the devices in the system. This should be above the 8V signal level, but perhaps not by much.

When a fault is detected, the priority is to turn off all of the devices. Some gate drivers include soft turn-off for short-circuit, which is fine. Presumably, before the logic can turn off the rest of the devices, the gate driver has completed its soft turn-off. The second priority is to alert the control box via the FAULT signal. The third priority is to indicate the fault in some way, such as an LED indicator (one for each type of fault for each halfbridge).

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4. Power Stage Design Principles

4.1 Topology

The power stage will be composed of four halfbridges. Each halfbridge is composed of two controlled switches (MOSFETs or IGBTs) with anti-parallel diodes. Although a MOSFET includes an integral body diode, it is advisable to include a place to insert a Schottky rectifier. This need may be eliminated by using a MOSFET co-packed with a Schottky, similar to an IGBT/diode co-pack. Three halfbridges are almost always used; the fourth may be for a brake or to control the neutral.

It is advisable to include a large diode on the input for reverse-polarity protection. In certain cases, this diode is not needed, and actually is a hindrance. For these cases, a jumper must be provided to allow bidirectional current flow. Additionally, there should be a relay that is powered from the same 120V feed that runs the logic supply. The normally-open contacts should be in series with the DC supply; the normally-closed contacts should connect a resistor across the bus to bleed down any capacitive energy.

As previously mentioned, it is desired to include a reconfiguration possibility for an SR topology, in which the halfbridge is split into two halves. If this compromises the performance of the normal halfbridge, then SR will be pushed to a future project.

It is necessary to be able to sense many voltages within the system. It is advisable to provide non-current-carrying binding post connections to every relevant voltage point.

4.2 Bus Capacitors

The input to the power stage is assumed to be well-filtered DC (ripple less than 5%), such as a Kenwood, HP or MagnaPower supply or an HP programmable load. It is necessary to at least include a snubber capacitor, a reasonably sized film capacitor close to the IGBTs/MOSFETs. It is also advisable to include a place to add some bulk capacitance (electrolytic) if that becomes necessary. A good rule of thumb is to size the bulk capacitance for approximately 6 ms of energy storage. Inrush control is necessary for the bulk capacitors as well. Note that regeneration will typically require some bus capacitance in order to maintain stability.

4.3 Thermal Design

Each power stage will have a continuous current rating (e.g. 20A) and a maximum bus voltage rating (e.g. 60VDC). Thermally, it must be possible to operate at these maxima indefinitely with junction temperatures below 100°C in lab ambient (25°C). Full rating is at 10 kHz switching for power stages under 100V, 5 kHz switching for higher voltages.

In addition, the power stage must be capable of overloads up to 125% of the continuous current rating (e.g. 25A) for 10 s with junction temperatures below 135°C. It is recommended to provide a derate curve, current vs. overload time, based on the final design, based on a maximum junction temperature of 135°C. It is anticipated that this will follow a curve of constant $(I_{actual}^2 - I_{rated}^2)\times t_{OL}$, or possibly some similar form with a different exponent, or possibly two curves to cover the total range.

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Some thought should be given to the removal of the heat from the box. For example, if the heat sink is entirely contained within the box, the total thermal resistance to ambient includes the thermal resistance of the box. This can lead to high internal ambient temperatures, inappropriate for maintaining high-performance analog circuitry.

The ratings chosen are generally larger than what is necessary, "just in case." Thermally, the design will probably be overkill for many applications. Consider using a thermostat to control the fan to reduce noise during low-power operation.

4.4 Power Supply

Each gate driver needs a power supply, possibly bipolar, referenced to the associated emitter/source connection. Several possibilities exist:

- One supply referenced to the negative bus, with bootstrap capacitors to power the upper devices. Not recommended due to uncertainty of the upper supply voltages.
- One supply referenced to the negative bus, with a switcher (forward, flyback) to generate the upper supplies.
- One supply referenced to approximately earth, with a switcher (forward, flyback) to generate all of the isolated supplies. This same supply can then be used for other "GND" referenced functions.

In any event, the source supply can be an off-the-shelf supply (of which we have cases). Before trying the second option, verify the isolation of the supply.

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5. Control Box Functional Requirements

5.1 Hardware

The control box must be highly flexible. To that end, it will contain a board with:

- Output connectors, which are RS-422 digital and ±10V differential analog
- A digital connector that is TTL
- An analog connector that is ±10V single-ended
- An analog connector that is 0-3V single-ended
- A connector for a keypad or similar user interface
- An encoder input and an encoder re-transmit

The TTL digital signals will be pass-throughs of the output connector, encoder input, and the keypad connector for use by a microprocessor, DSP, or PC via a DAQ card. Logic families should be 3.3V. The single-ended analog connectors will also be essentially pass-throughs, but with protection against overvoltages and other potentially harmful conditions.

This board will be in a box that has space reserved for a TI 2812 eZdsp board. The box will also have means to mount a keypad TBD.

Potential systems in this scheme include:

- A 2812 eZdsp running V/Hz, vector control, or other advanced control scheme
- A PC running xPC derived from a Simulink design
- A microcontroller and CPLD running some other control scheme

5.2 Software

It is anticipated that a typical project flow includes a quick design in Simulink followed by a detailed design in C on a 2812 DSP. To that end, software modules should be designed to assist a new user:

- Simulink subsystems for interfacing to the hardware, including fault and overload monitoring
- DSP subsystems for interfacing to the hardware, including fault and overload monitoring
- DSP functions that are generally useful, such as PWM generation, Park-Clarke transformations, PID loops
- DSP interface to the keypad, including parameter storage

Additionally, for people doing motor work, it is desired to have a simple V/Hz algorithm implemented in the DSP available. It should generate precise sine waves, including dead-time compensation and other means of attaining high fidelity.

To enable the use of a DAQ card, one seat of Real-Time Workshop and one seat of xPC Target will be purchased.

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6. Project Goals and Timeline

6.1 Output Stage Hardware and Software (as necessary)

- Block diagram and preliminary part selection: September 12, 2003
- Breadboard prototypes of critical circuits: October 10
- Complete schematic, with all part selection and footprints assigned: October 31
    - Order parts at this point for 1 week delivery or longer
- Layout complete and reviewed: November 14
- Boards stuffed and tested: December 12
- Next round of boards designed: January 16, 2004

6.2 Control Box Hardware

- Block diagram and preliminary part selection: September 12, 2003
- Breadboard prototypes of relevant circuits: October 3
- Complete schematic, with all part selection and footprints assigned: October 24
    - Order parts at this point for 1 week delivery or longer
- Layout complete and reviewed: November 14
- Boards stuffed and tested: December 12

6.3 Control Box Software

- Architecture defined and tasks partitioned: September 12, 2003
- Next task?
- Usable V/Hz system debugged: December 12

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Design Document

Modular Inverter Front-End

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Author: Wayne Weaver

Principal Investigator: P.T. Krein

Created: August 10, 2005

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Abstract:

The modular inverter project front-end module was designed to supply a clean, stable dc bus to the inverter stage of the project. The front-end consists of a passive rectifier (1 or 3 phase) and an active dc-dc converter (typically boost). The control board of the converter was designed to be flexible in the control method and implementation. The board also performs signal conditioning of data points related to the front-end operation and controls necessary mechanical switching of power.

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Document Revision History

Issue	Date	Comments
001	3/21/2005	Updates reflecting operational modifications of PB0041-C (section 2, 6.3)

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1. Introduction

This project provides ac to dc conversion module to supply the motor inverter stage of the project. However the load of the front-end is not necessarily limited to the modular inverter. For research purposes the front-end could supply power to any required dc load.

1.1 Scope

The front-end module was designed as half of the modular motor inverter project. The input to the front end is an ac power source and the output is a stable dc bus. The input ac power source can be a single or three phase source.

Because of the need to process high power levels all power processing devices are not physically located on the control board. The rectification device, converter switches and filtering devices are stand alone.

1.2 Definitions

Control Board – SK0041 rev C PCB that controls the contactors and gate drive of the front end unit.

DSP Daughter Board – SK0045 rev 1 that can be used as intelligent control and connects to the control board via J12, J13, J14, and J16.

Front-End Shelf – Bottom shelf of the modular inverter box that contains all the 208 3phase ac to 400Vdc hardware.

1.3 References

Front End Control Board Schematic: SK0041 rev C

Front End Control Board Layouts: PB0041 rev C

Front End Shelf Schematic: SK0068 rev 1

DSP Daughter Board Schematic: SK0054 rev 1

DSP Daughter Board Layout: PB0054 rev A

Modular Inverter Control Board Design Document DD00007-000

Analog PWM Daughterboard DD00008-000

eZDSP TMS320F28121 DSP Daughterboard DD00009-000

Modular Inverter Power Stage DD00010-000

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2. Known Issues / Revision Suggestions

1. Ground Pins 4&5 of U3 are not connected to the board analog ground. A jumper wire needs to be soldered from these pins to ground to ensure proper operation and limit the voltage applied to the GPIO of the eZDSP Board.
2. The 3.3V regulator (U21) has a bad placement on the PCB. The heat sink interferes with R27 and the DSP Daughter board.
3. Test points should be added at Bus high indicator (U26A-1) and the time delay for the inrush current control (R4-2).
4. For PB0041-C the Inrush contactor control logic is triggered off of the Vbus signal. While the bus capacitor is discharging after shutdown this causes an excessive amount of time before the inrush resistors are switched back in line in preparation of a restart. A better way is to use the Vrec signal since the voltage level drops quickly after shutdown. A modification to board PB0041-C is to cut trace from D21-1/U1-3 and jumper between U1-3 and D17-1.

3. Control Board Design Motivations

The control board was designed for maximum flexibility in the control of the gate of the front-end unit. Three analog gate drive signal schemes are on the board. Control signals external to the board can be used including from the DSP daughter board, Matlab xPC, from the inverter stage, or other sources. Digital control signals can be buffered and filtered in order to accept a broader range of signal types. A spare contactor control was included for use in experiments that may involve simulating a 'fault' on the system. The inductor current sensor LA55-P was chosen because it prevents the need for high voltage high current of the main power flow to go through the control board.

4. Gate Drive Control Modes

Three modes of control are designed with analog circuitry on the control board. In addition other methods can be implemented via external interfaces. The gate drive signal is selected by JMP7 then optically isolated through U14 before being gated by enable logic (section 5.1) and over-voltage protection (section 5.2). If the gate drive is enabled then MIC4420 U15 drives the gate connected to MTA100 J3.

4.1 External

An externally generated gate signal can be used to drive the converter gate. This signal can come from a connected DSP, the inverter stage, or some other external source (J15) and is selected by JMP4. Since the quality and voltage range of said signal is unknown, it is digitally buffered by an MIC4420 (U9 sheet 5). The MIC4420 can accept a wide range of inputs and standardize the output signal to the +15V board source regulated by zener D8.

4.2 Autonomous Feedback

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This mode is laid out on sheet 10 of SK0041C. In this control mode no external interface is required. The controlled system variable can be either the bus voltage or inductor current (chosen by JMP8). The chosen variable is compared to a reference set by R48, and then using a PI gain is generated into PWM by TL494 chip U17. The frequency of the PWM signal is controlled by R49. The gain of the PI loop is controlled by R45, with a time constant dictated by C27. Since the system was designed primarily around a boost converter, a upper limit on the PWM duty cycle was built into the circuit. The upper limit on the duty cycle is controlled by R50.

As an example: If the user wants to control the desired bus voltage to be 400Vdc, then JMP8 should be in 1-2 position. Adjust R48 so that the voltage on TP37=400V*(.013/2)=2.6V.

4.3 Hysteretic Feedback

This mode is laid out on sheet 9 of SK0041C. The controlled system variable can be either the bus voltage or inductor current (chosen by JMP8). For example, if the dc-dc converter is a boost, then the inductor current would be chosen, and if the converter is a buck, then the bus voltage can be used. This mode uses an externally supplied reference signal compared to the system variable through a Schmitt trigger hysteretic circuit to generate the gate switching signals. The hysteretic band around the reference signal is controlled by R41.

4.4 External Reference PWM

This mode is laid out on sheet11 of SK0041C. This is an open loop control mode that uses an externally supplied reference to generate the PWM signal via a TL494 (U18). R56 trims the references signal. R57 controls the frequency of the generated PWM, and R59 sets an upper limit on the PWM duty cycle.

5. Gate Enable and Over-voltage Protection

The gate drive must be enabled by and enabling circuit, and the over-voltage protection circuit. These signals are gated by CMOS AND gate U12 before passing to the gate drive U15.

5.1 Enable

The converter gate enable signal is chosen among three options: bypass, DSP, external, and inrush control enable. The selection is by JMP6 then is optically isolated before being logically gated with the over-voltage protection signal and the gate signals. The bypass jumper setting permanently enables the gate.

5.2 Over-voltage Protection

Because a boost converter is unstable at light loads, over-voltage protection is required to keep the bus voltage from running away while the inverter stage or an alternative load is not active. This situation typically occurs during start-up, where the front end would be active before the load. Alternatively, a ballast load is required on the dc bus, usually in the form of a power resistor. This circuitry is shown on sheet 8 of SK0041, and consists of a Schmitt trigger hysteretic circuit. R34 sets the threshold, and R37 controls the band around the threshold. When the bus voltage exceeds the high threshold band, the gate is disabled until the voltage falls below the low band.

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6. Contactor Control

Because of the potential for relatively high voltage (>200Vac) and high power (>100W) mechanical contactors are required to control the flow of power at the ac input of the front-end module. All 3 contactor control contacts can share a single power source via selection of JMP9. The connections of the main power contactor and inrush current control contactor can be seen in SK0068. Connections for the general contactor are left up to the user, based on usage.

6.1 Main Contactor

The main contactor is the primary power disconnect of the front-end module. The control board circuit is laid out on sheet 4 of SK0041. One of three sources can be chosen to actuate the main contactor through JMP3. The first is from a connection to a switch on the front panel of the module J6. The second is a signal from a connected DSP, and the third is from an alternative external source J15. Since all three possible sources are not necessarily of the same signal type, the chosen signal is buffered through a MIC4420 (U7). Because larger mechanical contactors usually have a 120Vac coil, a PCB relay (U8) is actuated by the signal buffer. The connection to the PCB relay can then be connected to the appropriate power source and the contactor coil.

6.2 General Contactor

For research purposes circuitry similar to that described in section 6.1 is included to actuate a spare or general contactor. This general contactor is signaled by either the DSP or an external signal through JMP2. Foreseeable uses of the general contactor include switching 'fault' resistors into the ac power lines to simulate a fault in the system, to study the response of the converter.

6.3 Inrush Current Control

Due to bus capacitance, a large inrush current can result when the main power is initially connected. To mitigate this, circuitry on sheet3 of SK0041 actuates a contactor to switch in extra resistance to the ac power lines, until the bus capacitance is appropriately charged. This circuit compares the conditioned bus voltage signal described in section 9.1.2 through an adjustable (R4) time delay with a reference threshold (R1) and hysteretic band (R5). When the rectified voltage has met the requirements then the inrush contactor is actuated, effectively switching out the added line resistance.

7. DSP Interface

The front-end module is designed to interface and operate with Modular Inverter DSP Daughter Board (SK0054). The control board can be configured to accept a direct gate drive signal from the DSP, or to filter the DSP PWM into an analog signal for use as a reference in the analog gate logic of section 4.

7.1 DSP/External Interface

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Circuitry shown on sheet 6 of SK0041_C is the interface between the DSP and any given external source. Three generic digital IO points are provided, as well as analog signal from the external source to the DSP. The analog signal is voltage divided from a 0-10V range to a 0-3V range, then buffered with a op-amp follower (U10).

7.2 Control Board/DSP Analog Interface

Three generic analog reference signals to the DSP daughter board are shown on sheet 6 of SK0041. R105, 106 and 107 trim a 0-3.3V signal to the DSP on VBUS_LOW, T1_LOW, and T2_LOW shown on Sheet 2 of SK0054. These signals can be used to adjust DSP parameters without a change in DSP programming.

7.3 Inverter Interface

The DSP unit can communicate with the inverter stage via differential IO lines generated by a DS26L32AC (U20) and DS26LS31C (U19) shown on sheet 12. Four IO lines are from the Inverter to the front end. They are ENABLE, FAULT, RESET, and GENERIC. The functionality of these IO is up to the user to implement. A single IO line from the front-end to the inverter is also provided

8. External Interface

The external interface connection J15 was primarily designed to operate with a Matlab xPC Target system using a National Instruments 6025E data acquisition card. However, any external source or instrument can be used if the proper pinout (see section 11.1) is used.

9. Signal Conditioning

9.1 Voltage

Both voltage measurements are accomplished using op-amp (TL082) gain to bring anticipated measurements into the desired range. The first stage brings the voltage to a 0-10V range for use by external xPC. A second stage divides the signal again by a third to a 0-3.3V range for use by the DSP. Both stages have clamping Zener diodes to guarantee the voltage range is not violated. In addition, a position for a filtering capacitor is provided at the input to the second stage.

Note: Resistances can be changed for any range of input voltage.

9.1.1 Vbus

For a nominal of Vbus=400 the nominal output of stage 1 is 5V. Using standard resistor values:

R80=R82=1M Ω

R79=R83=13k Ω

This yield a nominal output of 5.2V and maximum input voltage of 769V for the 0-10V conditioned signal.

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9.1.2 Vrec

For a nominal of Vrec=285 the nominal output of stage 1 is 5V. using standard resistor values:

R80=R82=1M Ω

R79=R83=18k Ω

This yield a nominal output of 5.13V and maximum input voltage of 555V for the 0-10V conditioned signal.

9.2 Inductor Current

The LA55-P current sensor has a 0-50A input range (U23). The output of this sensor is a current source at 1/1000 of the input. A burden resistor of 100Ω (R90) is used to produce a voltage signal. The voltage signal is then amplified with adjustable gain set by R91. The measurement range can also be modified by increasing the number of turns through the sensors window. However, using 12 AWG wire, 6 turns is the maximum.

10. Setup and Testing

The following are procedures for setting up and testing the control board (PB0041_C) and the complete front end shelf (SK0068). These procedures are not all inclusive; rather they establish a framework for future users to start with. All setup and test procedures are assuming a nominal bus voltage of 400V and 3-phase 208V input to the rectifier.

10.1 Offline Control board

This section includes procedures to test and setup the functionality of the control board alone (PB0041_C). All procedures are done offline (not connected as in SK0068). The only connections to the board should be power (J9, J10), and those outlined below.

10.1.1 Power

Connect power to J9 (see section 11.1 for pinout). LED's D13, D15 and D16 should light up.

10.1.2 Contactors

10.1.2.1 Inrush

1. Switch Out resistors at Vbus>200V (200*(13000/1000000)=2.6V=SO)
2. Switch In resistors at Vbus<20V (200*(13000/1000000)=.26V=SI)
3. Connect signal generator to TP64 with square signal ~1Hz, 4Vp-p, 5V offset
4. Connect Scope
    a. Ch1 TP64
    b. Ch2 R2-1
    c. Ch3 TP5
5. Jumper JMP1 1-2
6. Adjust R4 until ch2 crosses SO at desired delay (250ms)
7. Adjust R1, R5 until desired SO and SI achieved (iterative)

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10.1.2.2 Main Power

5. Remove jumper on JMP3
6. Jumper +5 to TP13
7. D3 should be lit and Relay U8 closed

10.1.2.3 Spare

1. Remove jumper on JMP2
2. Jumper +5 to TP9
3. D2 should lit on and Relay U6 closed

10.1.3 Bus High Indicator

1. Jumper +1V (1V/.013= 76Vbus) to TP64
2. Adjust R102 threshold until D23 is lit

10.1.4 Gate Drive Analog Control Modes

10.1.4.1 Analog Reference PWM

1. Jumper +5 to TP19
2. Scope TP41
3. Adjust frequency R57) to 10kHz
4. Adjust upper limit to ~35% R59
5. Trim reference with R56

10.1.4.2 Autonomous Closed-loop PWM

1. Jumper +5 to post 2 on JMP8
2. Scope TP38
3. Adjust frequency (R49) to 10kHz
4. Max Duty Cycle (R50) ~35%

10.1.4.3 Hysteretic Control

1. Connect signal generator (sinusoid,100Hz, 1Vp-p, 2.5V offset) to post 2 of JMP8
2. Connect +5 to TP19
3. Scope TP35 (band) and TP34 (output)
4. Adjust hysteretic band (R41)

10.1.5 Over-voltage Protection

1. Connect signal generator (sinusoid,100Hz, 1Vp-p, 2.5V offset) to TP64
2. Set threshold and band for hysteretic (R34, R37)
   a. Over voltage at 420 (420*(13000/1000000)=5.46V)
   b. Resume at 380 (380*(13000/1000000)=4.94V)

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3. Verify at TP32
4. Power gate drive (PWR-B)
5. Enable gate (JMP6 1-2)
6. Use Reference or autonomous PWM circuit to generate pwm to Gate drive.
7. Verify over-voltage protection (it is disabling gate) at TP 28.

10.1.6 DSP interface

Testing of the analog functions of the board should be done and verified first before the eZDSP is used. The programming of the eZDSP board can be accomplished via the Matlab Simulink RTW toolbox, or manually via the code composer studio (see eZDSP TMS320F28121 DSP Daughterboard design document DD00009-000 for details)

It is recommended that the control of the inrush current contactor and main power contactor stay a function of the analog control board. However, these function can be controlled by the eZDSP via a change in jumper (see section 11.2).

10.2 Front End Commissioning

It is assumed that all desired control board functions were setup, tested and verified by the user before the control board is integrated into the front end shelf unit (SK0068).

WARNING, o***perate unit with great caution, nominal voltages are at dangerous levels.***

10.2.1 Contactor

Connect system as indicated in SK0068, with exception of the connection power to inverter unit (use resistive load).

1. Press main power button on front panel, and verify power and inrush current contactor operation.
2. Make adjustments to delay (R4) and thresholds (R4,R1) as needed.

Figure 1 shows oscilloscope screen capture of a startup with inrush current control, the autonomous feedback control is used to drive the IGBT gate. Channel 1 is bus voltage measured directly from a differential scope probe, channel 2 is the conditioned bus voltage signal from TP64 of the control board, channel 3 is the rectified voltage conditioned signal from TP58 and channel 4 is the conditioned inductor current signal on TP61. Note at time 0sec when the inrush resistors are first switched out, the bus voltage overprotection disables the gate and the voltage drops until it reaches the turn on limit, then the system settles to the nominal set-point.

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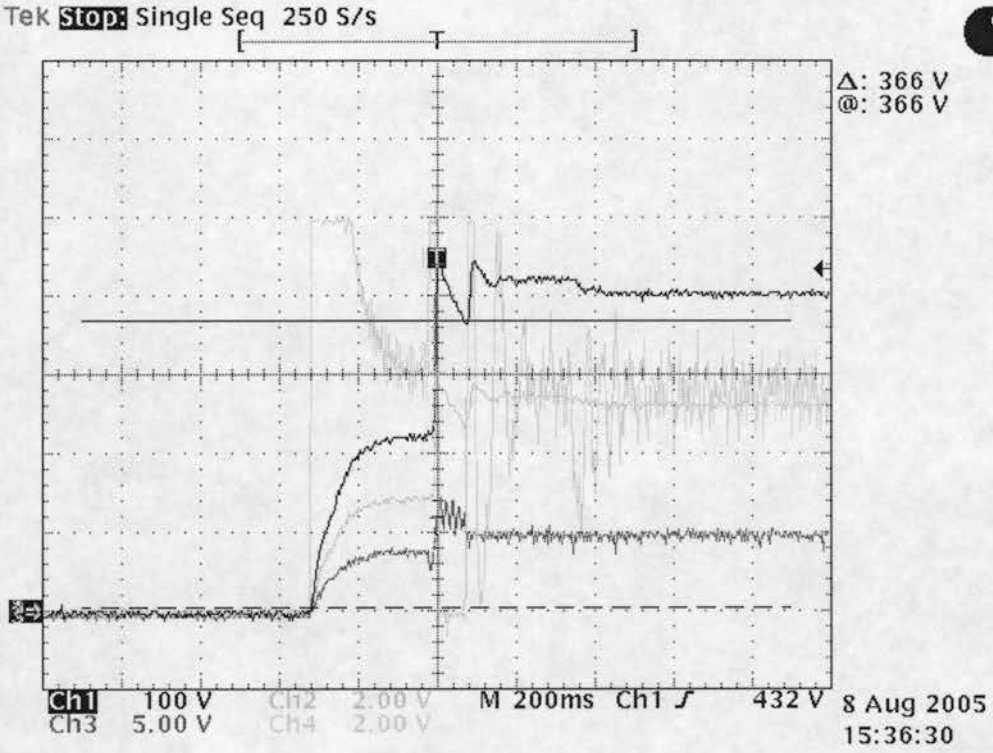

Figure 1. Startup with inrush current control.

10.2.2 Signal Conditioning

10.2.2.1 Bus Voltage

Measure bus voltage with DVM and verify 0-10V bus voltage conditioned signal at TP 64 (Vbus_signal~.013*Vbus), and 0-3.3V signal at TP67.

10.2.2.2 Rectified Voltage

Measure rectified voltage with DVM and verify 0-10V rectified voltage conditioned signal at TP 58 (Vrec_signal~.018*Vrec), and 0-3.3V signal at TP60.

10.2.2.3 Inductor Current

Operate system at rated load and adjust current signal gain (R91) until conditioned signal (TP61) is at desired level (~5V on 0-10V range). Verify signal on 0-3.3V output (TP63).

10.2.3 Over-Voltage Protection

Operate converter with a bus voltage set-point above the over-voltage limit set in section 10.1.5 and verify over-voltage operation. LED D11 should flicker as the IGBT gate is disabled and enabled. The frequency is dependent on the values of the energy storage elements of the converter.

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11. Appendix

11.1 Control Board (SK0041 rev C) Pin-out

Connector	Name	Description	In/Out	pin	pin description
J1	Vrec	Rectified Voltage Measurement	In	1	+ Vrec
				2	-Vrec
J2	Vbus	Bus Voltage Measurement	In	1	+ Vbus
				2	- Vbus
J3	Gate	Converter Gate Drive	out	1	+Gate drive
				2	Isolated ground (gnd b)
J4	Bus High	Bus Energized fron pannel indicator	out	1	Bus High signal
				2	Ground
J5	Inrush	Inrush contactor coil relay contacts	out	1	
				2	
J6	Front Pannel Power Switch	Front Pannel Power Switch	In	1	Switch in
				2	+15Va
J7	Main	Main Power contactor coil relay contacts	out	1	
				2	
J8	Spare	Spare contactor coil relay contacts	out	1	
				2	
J9	Power A	Main power board connection	in	1	+15V
				2	Ground
				3	-15V
				4	+5V
J10	Power B	Isolated gate drive power	in	1	+15V
				2	Isolated ground (gnd b)
J11	CON10	Inverter stage communications	out	1	Gin
			out	2	~Gin
			in	3	Gout
			in	4	~Gout
			in	5	~Enable
			in	6	Enable
			in	7	~Reset
			in	8	Reset
			in	9	Fault
			in	10	~Fault

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J13	CON20	Primary General I/O connection to DSP	in	1	Inrush contactor control
			in	2	Main power contactor control
			in	3	General/Spare contactor control
			in	4	Enable Gate
			in	5	General from Inverter stage
			out	6	General to Inverter Stage
			in	7	Enable from Inverter
			in	8	Reset from Inverter
			in	9	Fault from Inverter
			out	10	Generic to external connector J15
				11	no connection
			i/o	12	Generic to external connector J15
				13-15	no connection
			i/o	16	Generic to external connector J15
				17-20	no connection
J14	CON16	Secondary General I/O connection to DSP	i/o	1-5	no connection
				6	Gate control signal
				7-16	no connection
J12	CONN 34	Low Voltage Analog Connection to DSP	out	1	Vbus signal
				2	Analog Ground
			out	3	Vrec signal
				4	Analog Ground
			out	5	Inductor current signal
				6	Analog Ground
			out	7	general analog from external
				8	Analog Ground
			out	9	general analog from control board

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				10	Analog Ground
			out	11	general analog from control board
				12	Analog Ground
			out	13	general analog from control board
				14-34	Analog Ground
J16	CONN 14	DSP Power Connection	out	1	+15V
				2	Analog Ground
			out	3	-15V
				4	Analog Ground
			out	5	+5V
				6	Digital Ground
			out	7	+5V
				8	Analog Ground
			out	9	+3.3V
				10	Digital Ground
			out	11	+3.3V
				12	Analog Ground
				13	Digital Ground
				14	Analog Ground
J15	XPC	External (XPC) i/o connection		1	Analog Ground
				2	Analog Ground
			out	3	Vbus signal
			out	4	Vrec signal
			out	5	Inductor current signal
				6-19	no connection
			In	20	Analog reference
			in	21	General DSP analog signal
				22	no connection
			in	23	Analog Ground
			in	24	Digital Ground
			in	25	External Digital Control signal
			in	26	Inrush contactor control
			in	27	Main power contactor control
			in	28	General/Spare contactor control

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			in	29	Enable Gate
			i/o	30	Generic Digital io to DSP
			i/o	31	Generic Digital io to DSP
			i/o	32	Generic Digital io to DSP
				33	Digital Ground
				34-50	no connection

11.2 Control Board Jumpers

Jumper	Sheet	Description	Pos 1-2	3-4	5-6	7-8
JMP1	3	Source of Inrush Control	On-board analog comparator	DSP	External	
JMP2	4	Spare Contactor Control	DSP	External		
JMP3	4	Main Power Contactor Control	Front Panel Switch	DSP	External	
JMP4	5	Digital Buffer Input	Inverter Stage	DSP	External	
JMP5	5	Analog Reference Signal Source	Filtered Digital Buffer	External		
JMP6	7	Gate Enable	Bypass	DSP	External	On-Board Inrush Control
JMP7	7	Gate Drive Source	External	Autonomous PWM	Hysteretic	Referenced PWM
JMP8	10	Control Variable Selection	Bus Voltage	Inductor Current		

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11.3 Potentiometers

Pot	Sheet	Value	Function
R1	3	10k	Threshold value of schmitt trigger comparator inrush current contactor
R3	3	2M	band for schmitt trigger comparator inrush current contactor
R4	3	100k	Time delay of inrush contactor
R34	8	2k	nominal value for schmitt trigger comparator for bus over-voltage protection
R37	8	2M	band forschmitt trigger comparator for bus over-voltage protection
R41	9	2M	band for schmitt trigger comparator of hysteretic gate control mode
R45	10	5k	PI gain for autonomous pwm gate drive control mode
R48	10	5k	Bus Voltage set-point for autonomous pwm gate drive control mode
R49	10	10k	Frequency of PWM in autonomous PWM gate drive control mode
R50	10	5k	Duty cycle upper limit for autonomous PWM gate drive control mode
R56	11	5k	Reference trim for external reference PWM gate drive control mode
R57	11	100k	Frequency of PWM in external reference PWM gate drive control mode
R59	11	5k	Duty cycle upper limit for external reference PWM gate drive control mode
R91	14	50k	Gain for inductor current sensor
R102	15	2k	Threshold for front panel bus high indicator

11.4 Test Points

Test Point #	Sheet	Description
1	3	Threshold voltage of schmitt trigger comparator for inrush current control
2	3	Onboard analog inrush contactor signal
3	3	voltage band of schmitt trigger comparator for inrush current control
4	3	Input to inrush contactor driver
5	3	Output of inrush contactor driver
6	3	Inrush Relay contact 1
7	3	Inrush Relay contact 2
8	4	Spare Relay contact 1
9	4	Input to spare contactor driver
10	4	Output of spare contactor driver
11	4	Spare Relay contact 2

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12	4	Main power Relay contact 1
13	4	Input to main power contactor driver
14	4	Output of main power contactor driver
15	4	Main power Relay contact 2
16		
17	5	Input to digital gate buffer
18	5	Output of digital gate buffer
19	5	Analog reference signal
20	6	Generic Digital IO 1
21	6	Generic Digital IO 2
22	6	Generic Digital IO 3
23	7	Overvoltage opto-isolator output
24	7	Overvoltage / Enable And gate output
25	7	Gate enable opto-isolator input
26	7	Gate enable opto-isolator output
27	7	Gate driver input
28	7	Gate driver output
29	7	Gate drive opto-isolator input
30	7	Gate drive opto-isolator output
31	8	Threshold voltage of schmitt trigger comparator for overvoltage protection
32	8	Overvoltage output signal
33	8	Voltage band of schmitt trigger comparator for overvoltage protection
34	9	Hysteretic gate signal
35	9	Hysteretic band
36	10	Control signal divider
37	10	Reference voltage
38	10	Autonomous gate signal
39	10	Upper duty cycle limit
40	10	PI voltage
41	11	Reference gate signal
42	11	reference trim
43	11	Upper duty cycle limit
44	12	To inverter generic output
45	12	From inverter generic input
46	12	From inverter reset input
47	12	From inverter fault input
48	12	From inverter enable input
49	13	+15V source A
50	13	+15V source B
51	13	Ground source A
52	13	Ground source B
53	13	+5V source A
54	13	+3.3V regulator output
55	13	-15V Source A
56	13	+15V analog power
57	13	Analog ground

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58	14	Vrec signal (0-10V)
59	14	Vrec + input
60	14	Vrec signal (0-3.3V)
61	14	Amplified current signal (0-10V)
62	14	Current sensor output
63	14	Amplified current signal (0-3.3V)
64	15	Vbus signal (0-10V)
65	15	Vbus + input
66	15	Vbus - input
67	15	Vbus signal (0-3.3V)
68	15	Bus high threshold (on 0-10V range)

11.5 DSP Interface Connections and Simulink Blocks

Function	SK0041C		SK0054			ezDSP			Simulink Embedded Target for TI C2000 DSP		
	Connector	Pin	Connector	Pin	Jumper	Connector	Pin	Description	Block	IO Mux	Bit
Inrush contactor Control	J13	1	J1	1	JP2 2-3	P8	23	SPI_SDI / SPISIMOA	C28x GPIO DO	GIOF	0
Main Contactor Control	J13	2	J1	2	JP1 2-3	P8	24	SPI_SDO / SPISOMOA	C28x GPIO DO	GIOF	1
General Contactor Control	J13	3	J1	3	JP4 2-3	P8	25	SPI_SCK / SPICLKA	C28x GPIO DO	GIOF	2
Gate Enable	J13	4	J1	4	JP5 2-3	P8	26	SPI_SS_1 / SPISTEA	C28x GPIO DO	GIOF	3
Inverter stage generic communication in	J13	5	J1	5		P4	2	XINT2/ADCSOC	C28x GPIO DO	GIOE	1
Inverter stage generic communication out	J13	6	J1	6		P8	5	XINT1n/XBIOn	C28x GPIO DO	GIOE	0
Inverter stage enable	J13	7	J1	7		P8	6	CAP1/QEP1	C28x GPIO DO	GIOA	8
Inverter stage reset	J13	8	J1	8		P8	7	CAP2/QEP2	C28x GPIO DO	GIOA	9
Inverter stage fault	J13	9	J1	9		P8	8	CAP3/QEP11	C28x GPIO DO	GIOA	10
External Generic Communication 1	J13	10	J1	10		P8	9	PWM1	C28x GPIO DO	GIOA	0
External Generic Communication 2	J13	12	J1	12		P8	11	PWM3	C28x GPIO DO	GIOA	1
External Generic Communication 3	J13	16	J1	16		P8	15	T1PWM/TICMP	C28x GPIO DO	GIOA	6

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Gate Drive Control	J14	6	J5	6		P8	30	PWM7	C28xPWM or C28x GPIO DO	Output1 or GPIOB	0
Vbus Signal	J12	1	J11	1		P9	2	ADCINA0	C28x ADC	ADCINA0	
Vrec Signal	J12	3	J11	3		P9	4	ADCINA1	C28x ADC	ADCINA1	
Inductor Current	J12	5	J11	5		P9	6	ADCINA2	C28x ADC	ADCINA2	
External Analog	J12	7	J11	7		P9	8	ADCINA3	C28x ADC	ADCINA3	
Generic Analog (R105)	J12	9	J11	9		P9	10	ADCINA4	C28x ADC	ADCINA4	
Generic Analog (R106)	J12	11	J11	11		P9	12	ADCINA5	C28x ADC	ADCINA5	
Generic Analog (R107)	J12	13	J11	13		P9	14	ADCINA6	C28x ADC	ADCINA6	

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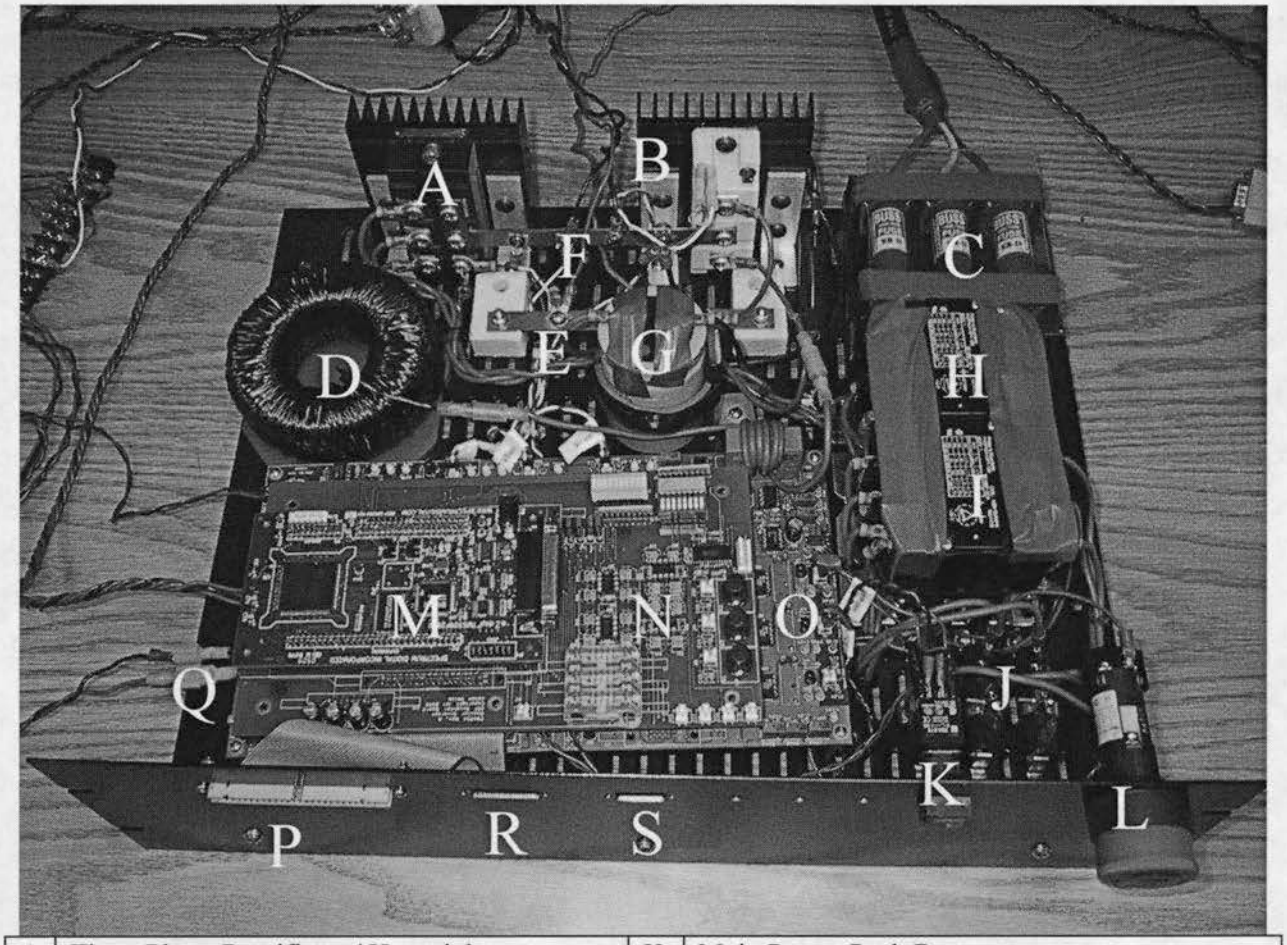
11.6 Picture of Front-End Shelf



A	Three Phase Rectifier w/ Heat sink	K	Main Power Push Button
B	IGBT w/ Heat sink	L	Emergency Stop
C	Fuse Block	M	eZdsp Board TMS320F2812
D	Inductor	N	DSP Daughter Board PB0054 rev A
E	Positive Bus Bar	O	Front-End Control Board PB0041 rev C
F	Negative Bus Bar	P	XPC/External interface
G	Bus Capacitor	Q	120Vac power
H	Main Power Contactor	R	eZdsp parallel port programming interface
I	Inrush Current Control Contactor	S	Inverter/Front-end SPI Buss interface
J	Inrush Current Control Resistors		

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Design Document

Modular Inverter Control Board

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Status: Issued

Author: Z. Sorchini / J. Wells

Principal Investigator: J. Kimball

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Abstract:

This document briefly describes the functionality and characteristics of the control board for the modular inverter.

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Issue	Date	Comments
000	3/6/2006	Initial release.

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1. Introduction

The control board for the modular inverter provides an interface between the power stage, the front-end and the main control circuit (daughterboard). Analog information together with status information is collected from the power stage and the front-end and is conditioned and made available to the main control circuit (i.e., the daughterboard). The switching signals are routed to the power stage. Additionally, interfaces for ISP peripherals, keypad, encoder and hall sensors are available.

1.1 Scope

The control board is intended to be used as part of the modular inverter, together with the power stage. Front-end is optional since an external dc source can be used. Primary use is for research.

Most of the functionality is available when the CPLD is properly programmed. The final user is responsible for correctly programming the CPLD.

1.2 References

Schematic: SK0038 rev 2

Layout: PB0038 rev B

Specification document: SD0004, Modular Inverter System Specification

Front-end: SK0041 and PB0041

Power stage: SK0031 and PB0031

Analog PWM daughterboard: SK0048 and PB0048

DSP daughterboard: SK0054 and PB0054

1.3 Known Issues

There are no ground test points near the analog signal processing blocks.

The resistors specified in the schematic for the unipolar analog blocks, where the signal is reduced to 3 V (voltage divider before the ouput buffer) are wrong. Resistor values of 23.2k and 10k should work.

The bus current signal from the Inverter Board is never routed from the connector. If required, it can be made available by cutting a trace (signal B1 from J17 pin 6 is recommended) and then connecting the signal (pin 13 from J16) to it. Notice that this signal was not present in the original specification document for the modular inverter.

2. Main Board

2.1 Power Stage Interface

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The interface to the power stage is made through connectors J7 (digital signals) and J16 (analog signals). For details on the signals refer to the modular inverter system specification document. Analog signals can be in the range ±15 V, but the used range is only ±10 V. Digital signals are differential in the range 0 to 5 V.

If the digital cable is not connected the FAULT signal defaults to active (faulted). The CPLD implementation must always make use of this signal to send switching signals to the power stage.

2.2 Interface Logic

2.2.1 CPLD

A CPLD is used mainly as a multiplexer to route digital signals between the interfaces, the daughterboard, the front end and the power stage. Pins intended to interface to the daughterboard are mostly generic I/O although some pins on the CPLD are optimized for particular applications (global set/reset and global clocks).

Since the modular inverter is intended primarily as a research tool, the final user is responsible for programming the CPLD to guarantee proper operation. A generic CPLD template is available as SW0022.

A JTAG interface (J19) is available for in-circuit programming.

2.2.2 Microcontroller

The microcontroller is primarily intended to communicate with the keypad and additional SPI devices. Extra pins are routed to the CPLD for flexibility, with some pins routed via jumpers (JP3, JP4) to make almost all the functionality of the microcontroller available.

The microcontroller clock is 10 MHz, the maximum for the 3.3 V part. The device has to be correctly configured for the oscillator and the logic voltage (the device has an under-voltage lockout function).

An ICD (in-circuit debugger) and ICP (in-circuit programmer) interface is available (J22).

2.3 Analog Signal Conditioning

The analog signals from the power stage and the generic analog connector are conditioned into ±10 V and 0-3 V levels for generic use (high voltage) and DSP specific (low voltage), respectively.

Each analog signal goes through a conditioning block. Clamp and offset voltages are created with zener diodes and a precision voltage reference, respectively. Depending on the signal, a bipolar or unipolar conditioning block is used for bipolar signals (e.g. currents) or unipolar signals (e.g. temperature, voltages) to make optimal use of the input range of the DSP's A/Ds. Bipolar signal range is ±10 V, unipolar range is 0 to 10 V.

Within the signal conditioning block, a jumper allows the selection of filtering or no filtering. Filtering is done by a second-order low-pass filter, whose cut-off frequency can be changed by changing components (see the schematic for details).

It was a design choice not to implement integration of channels (e.g. flux estimation) because it is not compatible with unipolar blocks. Any additional analog processing is intended to be done in the daughterboard implementation.

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2.4 Digital Signal Conditioning

This section translates between differential signals and TTL compatible signals. Both signals are in the range of 0 to 5 V. The FAULT signal defaults to active (faulted) if the digital cable is not connected.

2.5 Encoder and Hall Sensor Interface

The encoder interface consists of differential and TTL inputs (selected via jumper JP1) and encoder retransmit (differential only). The hall-effect sensor interface has both differential and TTL inputs (selected via jumper JP2) but no retransmit. All signals are in the range 0 to 5 V.

The encoder retransmit signals are routed first to the CPLD to provide any required processing (e.g., to convert from quadrature signals to direction + clock). The final user is responsible for making sure that the CPLD is correctly configured to use the encoder retransmit.

The TTL inputs have pull-up resistors (10 k) and are routed through Schmitt-trigger inverters to allow slow transitions of the input voltage.

The encoder input connector (J6) has power (5 V, pin 10) and ground (pin 11) available to power an encoder.

2.6 Front-End Interface

The front-end interface reroutes the enable, fault, and reset signals of the power stage to the front-end. Additionally, generic digital input and output signals are provided (signal level between 0 and 5 V). Analog interfacing can be done via the generic analog connector.

2.7 SPI Bus Interface

Provides a SPI clock, data in, data out and enable signals for a generic SPI peripheral. Uses differential signaling (0 to 5 V).

SPI devices must be configured as slaves, since the microcontroller is setup as a master. The SPI bus connects the external SPI interface, the keypad interface and the daughterboard SPI interface to the microcontroller.

2.8 Keypad Interface

An interface for a Baldor keypad (smart motor keypad) is provided. Communication is done via the microcontroller, which is configured as a master. A basic communication template for the keypad is available (SW0020). Interface signaling is TTL compatible.

2.9 Enable Signals

Each inverter phase can be disabled via dip switch SW1. Additionally, a master enable signal is available, intended to be controlled by a panel-mount switch.

The functionality of these signals must be programmed into the CPLD.

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3. Daughter Board Interface

3.1 Physical Layout

Daughter boards are intended to be about 5 inches wide and at least 9 inches long. The length can be extended, but no extra mounting holes are provided on the control board for mechanical support. It is not recommended to extend the width of the daughterboard.

Mounting holes are available every 4 inches in a 4x8 inch section.

With respect to the front of the control board (the edge that has the front panel connectors), the relative position of the daughterboard connectors is as follows (in mils):

1. The left bottom mounting hole is defined to be at (0,0)
2. Power connector pin 1 is at (1200,0)
3. Low voltage analog connector pin 1 is at (2100,400)
4. High voltage analog connector pin 1 is at (4900,900)
5. Primary general I/O connector pin 1 is at (4600,3700)
6. Secondary general I/O connector pin 1 is at (1800,3700)

3.2 Digital Interface

Generic digital signals are available in two connectors, J2 and J5. The primary connector J2 has generic clock, and set/reset signal capabilities, but they can still be used as generic I/O. There is no particular definition of signals. Routing must be programmed within the CPLD.

3.3 Analog Interface

The processed analog signals are available in low voltage (J15, 0-3 V intended for the DSP daughterboard) and high voltage (J18, ±10 V for generic use). All analog signals (i.e., power stage and generic ones) are available.

3.4 Power

All power levels (±15 V, 5 V and 3.3 V) are available to the daughter board. Digital and analog grounds are available. The 3.3 V source is a TO-220 regulator fed from the 5 V source (1 A max). Refer to Table 1 for maximum power available to the daughterboard.

Table 1. Daughterboard design power with Kyosan KVL40-02 power supply (40 W)

	Control Board (typical)	Daughterboard (max)
+15 V	10 W	20 W
-15 V	2.2 W	2.2 W
5 V	6 W (includes 3.3 V power)	9 W (including 3.3 V power)
3.3 V	1.7 W	1.7 W (independent of power supply rating)

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Combined (±15 V and 5 V)	18 W	22 W

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Design Document

Analog PWM Daughterboard

Reference: DD00008

Issue: 001

Status: Issued

Author: Zakdy Sorchini

Principal Investigator: Jonathan Kimball

Created: March 6, 2006

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Abstract:

This document briefly describes the functionality and characteristics of the analog PWM daughterboard for the modular inverter. Sine-triangle PWM is implemented.

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Document Revision History

Issue	Date	Comments
000	6/27/2005	Initial release.
001	3/6/2006	Added a reference to the control board CPLD software.

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1. Introduction

The analog PWM daughterboard is one of the control modules for the modular inverter. It provides four sine-triangle PWM channels with pulse-by-pulse over-current protection. The triangular waveform is obtained from a discrete IC to have better stability and linearity.

1.1 Scope

The analog PWM daughterboard is intended to be used as part of the modular inverter, together with the control board. Primary use is for research.

The over-current functionality is only available when the control board CPLD is programmed to synchronize the over-current signal with the PWM clock. The signal cannot be used directly to disable transistors.

1.2 References

Schematic: SK0048 rev 1

Layout: PB0048 rev A

Control board: SK0038 and PB0038

CPLD software for Control Board: SW0018

1.3 Known Issues

The over-current protection circuits are active high, must be active low for the wired-OR configuration to work. Just reverse all the input signals (not the positive feedback) to the comparators (U1, U3, U4 and U5) by cutting traces and reconnecting.

2. Interface

2.1 Power

The analog PWM daughterboard requires ±15 V, ±12 V, 5 V and 3.3 V. The ±12 V supply is used by the triangle waveform generator and is created from the ±15 V supply using zener diodes. The logic voltage is either 5 V or 3.3 V, selected via jumper JP1.

2.2 Analog Signals

The daughterboard uses the high voltage analog connector. The signals used are the currents (pins 1, 3, 5 and 7) and the modulating signals (pins 23, 25, 27 and 29). The current signals must be preferentially unfiltered for the pulse-by-pulse over-current protection to work properly. All signals can be up to ±15 V, but the range used is ±10 V (the carrier is set for this last range).

2.3 Digital Signals

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Only the primary digital connector is used. The PWM signals are available on pins 1-4, the over-current signal on pin 5 and the PWM clock on pin 6. All digital signals can be in the range of 0 to 5 V.

3. Timing

3.1 Triangle waveform

An LM565 (phase lock loop IC) is used as the triangle waveform source. The IC requires ±12 V which is made available from Zener regulators. The frequency of oscillation is adjustable via an external panel-mounted pot (20 k) and a timing capacitor (selected via jumper J5). The frequency is adjustable from 200 Hz up to 100 kHz. (A particular capacitor setting allows a change in frequency of roughly one decade.)

The stability of the frequency and the linearity of the waveform were significantly better than a discrete implementation of a triangle waveform oscillator.

The signal on the LM565 has a dc offset, so the signal is buffered and then AC coupled to an amplifier stage to set the amplitude of the triangle to ±10 V.

3.2 PWM Clock

The LM565 IC also provides a clock signal synchronized with the triangle waveform (pin 4), but has zero dc offset. A comparator is used to make the signal TTL compatible. Resistors R54 and R56 are typically not required.

4. PWM Channels

The implemented PWM is sine-triangle PWM. The PWM signals are obtained by comparing the (buffered) modulating signals with the triangle waveform. Small positive feedback is used to avoid false pulses at the output of the comparator. Signal level is 0 to 5 V or 0 to 3.3 V, depending on the selected voltage.

5. Over-current Protection

Pulse-by-pulse over-current protection is implemented in a per-channel basis, but with only a single over-current signal (flag) available. The over-current signal is intended to directly control the enable of the power stage, after synchronizing it with the PWM clock (this is done in the control board CPLD).

The current signal is rectified (the diode drop is not critical since only the peak of the current waveform is of interest) and compared to an adjustable trip voltage. The current signal goes first through a first order passive low pass filter, and then fed to both positive and negative half-wave rectifiers. The resulting signals are then fed to the positive and negative pins of the comparator. The trip voltage is fed to the negative pin and the positive is connected to an additional balancing resistor network, with a pot (R8, R16, R29 and R37). The potentiometer must be adjusted to ensure symmetric over-current detection (i.e., adjust until the over-current signal is active at the same level on both the positive and negative cycle).

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All the over-current channels are in a wired-OR configuration to create the over-current signal the goes to the control board. This signal cannot be used directly to control the ENABLE of the power stage, since it is not synchronized to the PWM clock.

Within the control board CPLD, a D type flip-flop must be used with a 1 on the input, the PWM clock as the clock input and the over-current signal connected to the asynchronous clear. The output of the flip-flop directly controls the enable. This disables the gates as long as the over-current condition is present, but only allows the gates to be enabled in synch with the PWM clock, i.e., the gates can only be enabled every PWM cycle.

6. Control Board CPLD

The software for the control board CPLD can be found in the Power Design Archives under Software as SW0018.

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Design Document

eZDSP TMS320F2812 DSP Daughterboard

Reference: DD00009

Issue: 000

Status: Issued

Author: J. Wells / Z. Sorchini

Principal Investigator: Jonathan Kimball

Created: July 5, 2005

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Abstract:

This document briefly describes the functionality and characteristics of the eZDSP TMS320F2812 DSP daughter board. Additionally, several useful documents are referenced which can aid the new user in understanding how to make the most of the available functionality.

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Document Revision History

Issue	Date	Comments
000	3/8/2006	Initial release.

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1. Introduction

The eZDSP TMS320F2812 DSP daughterboard is one of the control modules for the modular inverter. The board provides peripheral circuitry needed to take advantage of many of the functionalities of the TMS320F2812 core. Extensive information regarding the capabilities of the DSP core can be found at:

http://focus.ti.com/docs/prod/folders/print/tms320f2812.html

1.1 Scope

The eZDSP TMS320F2812 DSP daughterboard is primarily intended to be used as part of the modular inverter, together with the control board. Primary use is for research. It should be noted that the board can be used as a stand alone board to develop code for the DSP as well.

1.2 References

Schematic: SK0048

Layout: PB0048

Control board: SK0038 and PB0038

CPLD software for Control Board: SW0026

Guide to Programming the eZDSP TMS320F2812 DSP through Matlab: TU00003

1.3 Known Issues/Suggested Revisions

- 10 Pin serial headers (J13, J14) should be fixed such that the pin connections match correctly with a standard serial connector.
- Resistor R2 should be changed to 470 ohms to provide ample current to drive the LED bank.
- Matlab does not appear to support pin level input/output configuration. It appears that such configuration is done at the port level. As such, when using Matlab, only the input switches (SW1) or the output LEDs (D1) can be used at a given time.
- The next revision of the board should improve the label layout on the physical board for easier reading.
- The physical position of connectors J17 and J18 should be swapped in a future revision.
- A possible addition to the next revision would be to include an improved 16 bit A/D chip as detailed in:

  http://focus.ti.com/docs/apps/catalog/resources/appnoteabstract.jhtml?abstractName=slaa167.
- A possible addition to the next revision would be to include an actual D/A chip which could be operated using the SPI bus of the DSP. See Application Note:

  http://focus.ti.com/docs/apps/catalog/resources/appnoteabstract.jhtml?abstractName=slaa176.

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2. Interface

2.1 Control Board Interface

2.1.1 Power

The eZDSP TMS320F2812 DSP Daughterboard requires ±15 V, 5 V and 3.3 V as supplied by the Control Board referenced in SK0038. If desired, the board can be run as a stand alone device by powering the eZDSP using the 5 V power supply provided by Spectrum Digital (www.spectrumdigital.com)

2.1.2 Analog Signals

The daughterboard uses the low voltage analog connector. DO NOT connect analog signals outside the 0-3 V range as this may cause damage to the DSP core. All analog signals are passed through a first order low pass filter. Note that the cutoff frequency was intended to be chosen by the user and may vary from board to board.

2.1.3 Digital Signals

Both the primary digital and secondary digital connectors are used to route signals to the control board. All digital signals are TTL compatible 3.3 V CMOS and are NOT 5 V tolerant.

2.2 Daughterboard External Connectors

2.2.1 Communications

SCI communications are available through connectors J13 and J14. SPI communications are available through connector J13. A CAN interface is available through connector J6. An RS-232 (serial port) communication channel is available through connector J7.

2.2.2 Filtered Analog Outputs

Four PWM channels (PWM1, PWM3, PWM5 and T1PWM/T1CMP) are available to be used as D/A converters. The PWM signals are filtered with 4^{th}-order low pass filters (Sallen Key implementation). Each channel can be connected to the filter with a dedicated jumper such that, if required, the digital PWM signals can be used directly. The analog signals are available in connectors J15-J18. The signal range is ±10 V.

2.2.3 Digital I/O

A generic digital input DIP switch (SW1) is available with 8 lines. Three toggle switches (S1-S3) are available, which can also be controlled with an external switch (J8-J10). Eight digital outputs are available visually on LEDs (D1). Refer to SK0048 for the specific DSP pins connected to each digital line. Assume all signals are in the 0 to 3.3 V range.

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Design Document

Modular Inverter Power Stage

Reference: DD00010

Issue: 000

Status: Issued

Author: Marco Amrhein / Brett Nee

Principal Investigator: J. Kimball

Created: July 25, 2005

v:\documents\design documents\dd00010-000 modular inverter power stage.doc

Abstract:

This document describes the functionality and design details of the power stage module from the Modular Inverter Project. The module itself consists of the power electronics components, gate drives, signal measurements and conditioning, fault logic and dead-time implementation for the gate signals. The power stage module was designed for a variety of voltage and power ranges and can be used with IGBTs and MOSFETs.

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1. Introduction

The power stage module is the output stage / inverter of the modular inverter. It applies the gate signals generated by the control stage to power electronics switches, handles hardware implemented faults and measures and conditions analog signals necessary for the control of the drive. It communicates with the control board, and takes the dc power from either the front end module or from an external dc power supply.

1.1 Scope

The power stage module of the modular inverter consists of four phase legs that can be controlled independently and configured with either IGBTs or MOSFETs. To control the gate drives corresponding to each switch, a CPLD is programmed with dead-time logic for each phase leg and with a fault-logic to stop the switching action in case of a fault. Various analog signals necessary for motor control and monitoring the drive operation are measured on the board, conditioned and fed back to the control stage. The power stage communicates exclusively with the control stage with analog and digital signals.

This document describes the power stage module and will give detailed information about each of the sub-modules on the board, the communication with the control board and the input power requirements. Also, the various configurations with IGBTs and MOSFETs as well as the various voltage and current ranges possible are discussed.

1.2 Definitions

1.3 References

Schematic: SK0031 rev 4

Layout: PB0031 rev D

Mechanical design: PJ0019, DR0016 (PCB mechanical outline)

CPLD program: SW0012, Inv_Logic_v3

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2. Electrical Design

2.1 Overview

The control signals (logic level) for the four phase-legs of the inverter arrive from the control board via a defined interface. A CPLD conditions those signals, applies a lockout mechanism and dead time, and sends the gate signals to the appropriate gate drives. The gate drives create gates signal from the logic-level signals that can drive the individual MOSFETs or the IGBTs.

The power stage can be configured in three different ways to accommodate the needs of the users. The configurations are given in Table I. The low-voltage high current (100V, $40A_{RMS}$) configuration and the high-voltage low-current (400V, $10A_{RMS}$) configuration use MOSFETs, and the high-voltage high-current (400V, $40A_{RMS}$) configuration uses IGBTs.

The phase outputs of the power electronics devices are routed through current sensors in order to measure each phase current. In addition, all phase voltages are measured, as well as the bus voltage. The bus current is calculated as the sum of the four phase currents. Two temperature measurement circuits are included on the board, but are not used for any specific tasks. All those signals are fed back to the control board via a defined interface. Minimum filtering is applied to those signals.

Overcurrent and overvoltage detection circuits are used in order to detect overcurrents in the four phases or an overvoltage in the dc bus voltage. Together with the fault signals created by the gate drive chips in case of a gate drive fault, these faults are fed back to CPLD, which in-turn disables all gate drives and communicates a fault to the control board. This state can only be reset by a RESET command from the control board, or the built-in reset-button from the power stage.

A general comment about the operation amplifiers used in the power stage module is necessary at this point. Since the voltage and current measurements are measuring the actual waveform of the signal and not an average or rms value, fast devices that can adequately represent the switching waveforms need to be used. The operational amplifiers chosen are the TLE2082 (dual opamp) and the TLE2084 (quad opamp), which have a three times higher slew rate and twice the bandwidth of a conventional TL082.

2.2 Power Electronics Devices and Power Connections

As was mentioned previously, the board can be configured to work with IGBTs or MOSFETs. The setup of the two different possibilities is described in this Section. The main difference is that the IGBTs cannot be mounted on the PCB, meaning that the power path of the dc bus is removed from the board (the IGBTs are connected with bus bars). However, the MOSFETs are mounted on the PCB, meaning that the main power path of the dc bus is actually on the board.

Table I. Inverter Power Stage Configurations

Max. dc bus voltage	Rated RMS current	PE Devices	PE Component
100 V	40 A	MOSFET	IRFPS3815
400 V	10 A	MOSFET	IRFPS40N50L
400 V	40 A	IGBT	BSM100GB60DLC

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The two electrolytic dc bus capacitors C161 and C162 (1200 µF, 450 V_{dc}, Part # ECE-T2WP122FA from Panasonic-ECG) are mounted on the board for both IGBTs and MOSFETs due to simplicity. However, in order to avoid dc bus loops on the PCB when IGBTs are used, the positive dc bus copper plane (TOP plane at the top of the layout) was split. This way, the two electrolytic capacitors can be connected to the dc bus without creating any dc bus loop on the PCB.

All wires to and from the PCB board are intended to be connected through soldering holes, which are large enough to support 14 gauge wires for the power connections, and 20 gauge wires for the gate drive connections, where applicable. For both configurations, the phase output wires need to be connected to J28, J29, and J30 for Phase A, to J34, J35, and J36 for Phase B, to J40, J41, and J42 for Phase C, and to J46, J47, and J48 for Phase D. Three wires in parallel support at least a current of about 60 A_{RMS} continuously, which is large enough for the capabilities of the inverter.

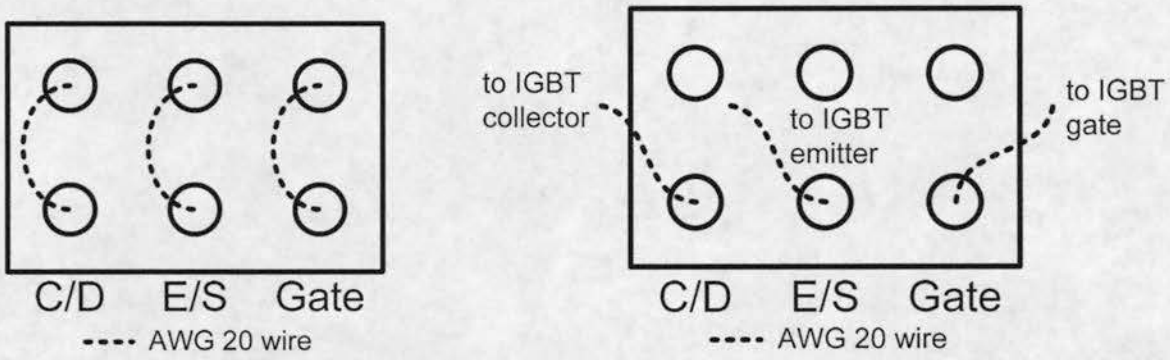
2.2.1 MOSFET-Version

Any MOSFETs can be used that fit a TO-274AA (Super-247) package. The MOSFETs are clamped to the heatsinks, so no mounting holes need to be provided. The MOSFETs that are intended to be used are IRFPS3815 for a low-voltage high-current configuration (100 V_{dc}, 40 A_{RMS}) of the inverter, and IRFPS40N50L for a high-voltage low-current configuration (400 V_{dc}, 10 A_{RMS}).

In the MOSFET configuration, the positive dc bus input can be connected either to J13, J14, and J15 (next to C162) or to J16, J17, and J18 (next to C161). Do not connect to both sets at the same time to avoid loops. Analog, the negative dc bus input can be connected either to J19, J20, and J21, or to J122, J23, and J24. In addition, the split in the positive dc bus needs to be short-circuited by using 14-gauge wire bridges from J62 to J63, J64 to J65, J66 to J67, and J68 to J69.

In the gate drive section of each MOSFET, jumper wires are necessary in order to connect the MOSFET correctly to the gate drive. For example, for the Phase A high-side MOSFET (Q1), jumper connections need to be made on component J3 from each bottom hole to the corresponding hole on the top, using 20 gauge wire, as shown in Fig. 1a. The same connections need to be made at the components J4 through J10.

Additional capacitors (C157, C158, C159, and C160) need to be mounted close to each pair of MOSFETs in order to improve the switching performance. The capacitors are film capacitors, 0.56 µF, rated for 630 V_{dc} (Cornell Dubilier, Part # DME6P56K).



a) MOSFET b) IGBT

Fig. 1. Gate drive jumper connection diagram.

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2.2.2 IGBT-Version

The IGBTs used are Eupec's BSM100GB60DLC, a 600 V_{dc} single-phase IGBT bridge rated for 100 A_{RMS}. The four modules required for the inverter are mounted to the heatsinks. The dc bus is connected to the IGBTs via bus bars, meaning that the main power does not need to be connected to the power stage PCB. However, the two electrolytic capacitors need to be wired to the dc bus. For C161, the positive dc bus needs to be wired to J16, J17 or J18 (one single 14 gauge wire is sufficient), and the negative dc bus to J22, J23, or J24. Similar, for C162, the positive dc bus needs to be connected to J13, J14, or J15, and the negative dc bus to J19, J20, or J21.

An additional capacitor (2 µF 1000 V_{dc}, Cornell Dubilier, Part # SCD205K102A3Z25) is mounted directly on each IGBT module. Therefore, the components C157 to C160 are left empty. Also, the positive dc bus on the left and on the right side of the board is not connected together to avoid loops.

The gate drives are connected to the IGBTs using 20 gauge wires as shown in Fig. 1b. The IGBT modules have separate pins for gate and emitter connections. The collector wire needs to be connected to the positive dc bus for the high-side IGBTs in each phase-leg, and to the individual phase output for the low-side IGBTs. The connections should be as short as possible to minimize the inductance. The three holes on the top of each jumper shall be left unconnected.

The phase output of each IGBT module needs to be wired back to the PCB board for current and voltage measurements using three 14 gauge wires. Wire connections above the current sensor are available in for each phase (Phase A: J25, J26, J27, Phase B: J31, J32, J33, Phase C: J37, J38, J39, Phase D: J43, J44, J45).

2.3 PCB Power Requirements

The various circuits on the PCB require different supply voltages for analog and logic components. The analog circuits and the isolated power supplies for the gate drives require ±15 V_{dc} and roughly 0.7 A, whereas the logic circuits require +5 V_{dc} and about 0.8 A. The connector J49 (4-pin MTA156) is used for those supply voltages plus GND. Two footprints for NTC resistors (CL-160, RT1 and RT2) are provided in case the inrush current needs to be limited on the ±15 V_{dc} to avoid power supply faults. Normally, RT1 and RT2 can be short-circuited.

Support capacitors footprints are provided throughout the board for all voltage levels. At the connection to the power supplies, 220 µF electrolytic capacitors and 0.1 µF film capacitors should be used (C164 to C169). Additional 10 µF electrolytic capacitors and 0.1 µF film capacitors footprints are provided along the main power traces and can be stuffed if needed.

Two power control LEDs are mounted on the front panel of the power stage module, and indicate if both +15 V and –15 V power is available. These LEDs are connected via a 3-pin MTA100 connector (J61).

2.3.1 Grounding

Two different grounds are provided on the board, analog ground (COM_A) and logic or digital ground (COM_D). They are separated in order to keep the logic signals, which include all the gate signals plus fault indication, as noise-free as possible. These two grounds are connected to the power supply via resistors R121 for COM_A and R122 for COM_D. R121 and R122 should be short-circuited (COM_A = COM_D).

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Earth ground can be connected to the board if desired through wire connector J60 (14 gauge wire), which will connect the power supply ground to earth ground. Footprints are provided for a resistor and a capacitor between power supply ground and earth ground.

2.3.2 Isolated Power Supplies for Gate Drives

The isolated power supplies required for the gate drives are on separate PCBs (PB0032). They draw the power from the ±15 V supply, and are connected via 3-pin MTA100 connectors. Each high-side gate drive requires one isolated power supply, and all low-side gate drives require another one. The connector configuration (J50 for Phase A high-side power supply, J52 for Phase B, J54 for Phase C, J56 for Phase D, and J58 for low-side power supply) is as follows: Pin 1 is +15 V, Pin 2 COM_D. and Pin 3 –15 V.

The isolated output voltages of each power supply are +15 V, +5 V, GND, and roughly–7 V. For the four high-side gate drives, +5 V is not required. Thus, the power supplies are connected via 3-pin MTA100 connectors (J51 for Phase A, J53 for Phase B, J55 for Phase C, and J57 for Phase D) with the following pin configuration: Pin 1 is +15 V, Pin 2 is GND, and Pin 3 is –7 V. The low-side power supply needs to deliver the +5 V output in order to power the isolated voltage amplifiers, which are, similar as the low-side gate drives, referenced to the negative dc bus. A 4-pin MTA100 connector is used (J59), with Pin 4 connected to +5 V, and the other pins connected like the other power supplies.

2.4 Gate Drives

Each power electronic device has its own gate drive, which basically consists of a single chip with some external components. The gate drive chip used is an HCPL-316J, a 16 pins surface-mount part. The chip takes logic-level switching signals, and outputs gate signals for the power electronics devices.

The circuitry for each gate drive is taken from the HCPL-316J datasheet. The gate signals are applied to the positive gate signal input pin, and the gate drive enable signal (~GD_ENABLE) is applied to the negative gate signal input pin. The gate drive turns on only when the positive pin is logic high, and the negative pin logic low. Thus, the negative input pin is used to disable the gate drives and the power electronic devices in case of a fault.

On the output side of the gate drive, all resistors need to be ½ W, 1% tolerance (except where indicated) due to the large power dissipation. The capacitors need to be rated for at least 25 V. Few components need to be selected according to the configuration of the power stage module. Values for the gate resistance R_g and the resistance R_c are given in Table II. The capacitance C_g is added in the schematic to provide the flexibility of increasing the gate capacitance. In general, this component does not need to be stuffed, and there are no recommended values available.

For the low-voltage inverter configuration (100 V), the DESAT diode used is a 1N4148 (5 in series). For the high-voltage inverter configuration (400 V), the DESAT diode is one MUR160, and the other four positions need to be short-circuited. The DESAT diode specifications are given in Table II

The connection of each power electronics device to the gate drive needs to be done via the 6-position jumpers is described in Sections 2.2.1 and 2.2.2 and in Fig. 1.

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Table II. Gate Drive Configurations

Inverter Configuration	PE devices	Rg	Rc	DESAT diode
100 V / 40 A_{RMS}	MOSFET	15 Ω ($^1/_2$ W)	0 Ω	1N4148 (4 or 5 in series)
400 V / 10 A_{RMS}	MOSFET	47.5 Ω ($^1/_4$ W)	0 Ω	MUR160 (only 1, the other pos. short-circuited))
400 V / 40 A_{RMS}	IGBT	47.5 Ω ($^1/_4$ W)	0 Ω	MUR160 (only 1, the other pos. short-circuited)

2.4.1 DC-Bus Connection for Low-Side Gate Drives

The layout has one issue with the ground connection of the four low-side gate drives. They are powered by the same power supply, which is referenced to the negative dc bus. Short-circuiting jumper J70 (close to dc bus capacitor C162) connects the ground of the low-side gate drives to the negative dc-bus at one connection.

2.5 Control Board Interface

Two interface connectors for communication with the control board were specified at the beginning of the project, one for analog and one logic signals. The physical connection is established with non-shielded flat ribbon cable through vertical LATCON connectors. The specification of the 26-pin connector for the analog signals is given in Table III, and of the 34-pin connector for the logic signals in Table IV.

The analog signals are transmitted through buffer circuits / voltage followers (U16, U17, U18). The logic signals are transmitted as RS-422 differential pairs, using a DS26LS31 transmitter (U37) and DS26LS32 receivers (U39, U40, U41). For the receivers, the transmission lines are terminated with 143 Ω resistors. Critical signals such as ENABLE and uC_RESET are tied to COM_D,

Table III. Analog Connector to Control Board.

Pin	Signal	Description	Pin	Signal	Description
1	COM_A	Analog ground	14	KELVIN2	Analog ground
2	NC	Not connected	15	RESERVED	
3	NC	Not connected	16	RESERVED	
4	COM_A	Analog ground	17	RESERVED	
5	IA	Phase A current	18	RESERVED	
6	IB	Phase B current	19	KELVIN3	Analog ground
7	IC	Phase C current	20	COM_A	
8	ID	Phase D current	21	COM_A	
9	KELVIN1	Analog ground	22	VA	Phase A voltage
10	VBUS	Dc bus voltage	23	VB	Phase B voltage
11	T1	Temperature 1	24	VC	Phase C voltage
12	T2	Temperature 2	25	VD	Phase D voltage
13	IBUS	Dc bus current	26	KELVIN4	Analog ground

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respectively their complementary signals to +5 V, through 1 kΩ resistors in order to guarantee that the inverter is disabled when no communication is present between the power stage and the control board. For those signals (and the reserve signals), the terminating resistors are 200 Ω, which together with the 1 kΩ resistors result in a terminating resistance of 143 Ω.

2.6 Current Sensors and Current Measurement

Closed-loop current transducers using the Hall effect from LEM are used. For the two different current ranges featured in the power stage, two current sensors were chosen that fit in the same footprint, see Table V. The transducers output a current that is proportional to the actual current, and is converted into a voltage via a burden resistance. The burden resistor can be adjusted for each phase to four different values using the switches SW1, SW2, SW3, and SW4, and the DIP-resistors RN1, RN2, RN3, and RN4. Activating the switches adds more resistors in parallel to the burden, thus increasing the measured current at a certain output voltage level. The output voltage is calculated using the formula

$$V_I = I_m \cdot \frac{R_b}{x} \cdot \frac{1}{scale}, \quad (1)$$

Table IV. Logic Connector to Control Board.

Pin	Signal	Description	Pin	Signal	Description
1	NC	Not connected	18	~D1	
2	COM_D	Logic ground	19	D2	Gate signal D2
3	NC	Not connected	20	~D2	
4	COM_D	Logic ground	21	ENABLE	Switching enable
5	A1	Gate signal A1	22	~ENABLE	from control
6	~A1		23	FAULT	Inverter fault to
7	A2	Gate signal A2	24	~FAULT	control
8	~A2		25	uC_RESET	Fault reset from
9	B1	Gate signal B1	26	~uC_RESET	control
10	~B1		27	RESERVED	
11	B2	Gate signal B2	28	RESERVED	
12	~B2		29	RESERVED	
13	C1	Gate signal C1	30	RESERVED	
14	~C1		31	RESERVED	
15	C2	Gate signal C2	32	RESERVED	
16	~C2		33	RESERVED	
17	D1	Gate signal D1	34	RESERVED	

Table V. Current Transducer Choices

Inverter max. phase current	Current transducer	Max. current rating	Current scaling
40 A_{RMS}	LAH 100-P	100 A_{RMS}	1:2000
10 A_{RMS}	LAH 25-NP	25 A_{RMS}	1:1000

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where R_b is the burden resistance, x the number of burden resistors in parallel, and *scale* the scaling factor of the current transducer. Given a 1.8 kΩ burden resistance and an output voltage V_I of 4.5 V at rated RMS current of the inverter, the possible current ranges for both transducer choices are given in Table VI. Other values for the burden resistance can be used, but the gain needs to be adjusted in the filter stage such that the output voltage is 4.5 V at the rated RMS current for proper functioning of the overcurrent detection circuit.

2.6.1 Dc Bus Current Calculation

The bus current is defined as the current flowing from the positive dc bus to the negative dc bus through the power electronics devices. Assuming that they are ideal, the bus current is equal to the sum of all phase currents through the high-side devices. Since an inverting adder circuit is used, the bus current is calculated as the negative sum of all phase currents signals through the low-side devices, i.e.

$$I_{bus} = \sum D_{high} \cdot I_{phase} = -\sum D_{low} \cdot I_{phase} . \quad (2)$$

A DG212CJ (quad SPST CMOS analog switch) is used to feed the corresponding current signal to the adder circuit when one of the low-side switching devices is on. A small first-order filter with a cut-off frequency of 1 MHz is used to band limit the bus current signal.

2.7 Phase and dc Bus Voltage Measurement

Each of the four phases as well as the dc bus voltage is measured with respect to the negative dc bus. The principle of the measurement is very simple. An isolated voltage amplifier measures translates the actual voltage into a low-level signal. This signal is then scalded and offset adjusted such that the voltage signal is within a voltage range of ±10 V_{dc}. The actual calibration is that 8 V corresponds to nominal dc bus voltage of the inverter (100 V or 400 V).

2.7.1 Isolated Voltage Amplifier

The isolated voltage amplifier used on this board is an HCPL-7800A with an integrated optical isolation barrier. It requires two +5 V_{dc} voltages supplies, one referenced to the negative dc bus, and one referenced to common ground. The dc bus referenced voltage is taken from the isolated power supply that powers all low-side gate drives. The logic supply voltage with its logic ground (COM_D) is used for common ground referenced voltage supply. This works although the measured signal is an analog signal and is referenced to analog ground (COM_A), because the isolated voltage amplifier chip has a differential input and output.

Table VI. Possible Current Ranges with 1.8 kΩ Burden Resistor and 4.5 V Output Voltage at RMS Current.

Switch positions closed	# of parallel resistors x	Total burden resistance	RMS current for LAH 100-P	RMS current for LAH 25-NP
None	1	1.8 kΩ	5 A_{RMS}	2.5 A_{RMS}
1	2	900 Ω	10 A_{RMS}	5 A_{RMS}
1 and 2	4	450 Ω	20 A_{RMS}	10 A_{RMS}
All	8	225 Ω	40 A_{RMS}	20 A_{RMS}

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For accurate operation of the isolated voltage amplifier, the differential input voltage should be less than 200 mV. This is achieved by using up to four ¼ W resistors in series with a 1 kΩ precision pot. In the dc bus measurement schematic, these resistors are R126, R127, R130 and R133, and the precision pot is R134. The values for the four resistors (R_V in the schematic) are chosen according to Table VII for the different voltage ratings.

2.7.2 Offset Adjustment and Signal Amplification

The isolated voltage amplifier has a gain of roughly eight. In order to get an 8 V signal from the rated dc bus voltage, an additional gain stage is necessary. The total gain required from the differential input of the isolated voltage amplifier to the voltage signal is at least

$$g_{min} = \frac{V_{out}}{V_{diff_max}} = \frac{8V}{0.2V} = 40. \quad (3)$$

The resistor combination in the amplifier stage yields a gain of 6.85. Combined with the isolated voltage amplifier gain, the required differential input voltage for an 8 V signal is

$$V_{diff} = \frac{V_{out}}{g} = \frac{8V}{8 \cdot 6.85} = 146mV, \quad (4)$$

which can be achieved by adjusting the 1 kΩ precision pot. The gain stage is has a band limit of about 300 kHz, enforced through a capacitor in the additional gain stage.

One phenomenon observed with the isolated voltage amplifier is that it tends to have an offset voltage at the differential outputs of varying magnitude up to about 300 mV. In order to correct for that, an offset compensation was added to the circuit. Using 10 V zener diodes (1N4740), an offset voltage determined by a 1 kΩ precision pot is subtracted from the differential output signal of the isolated voltage amplifier.

2.7.3 How to Calibrate the Voltage Measurements

Disconnect the phase connections and the dc bus connections from the board. The rated dc voltage needs to be applied at the dc bus and at each of the phase terminals in order to calibrate each of the voltage measurements. The analog and logic circuits need to be powered with the power supplies used in the actual inverter to avoid incorrect voltage measurements once the power stage is mounted in the inverter box.

First, the dc bus terminals (respectively the phase terminals to negative dc bus) need to be shorted. With the 1 kΩ precision pot, the voltage measurement signal needs to be adjusted to 0 V. Then, the short is removed, and rated dc voltage is applied to the dc bus or phase terminal, respectively. With the 1 kΩ precision pot, the voltage signal can be adjusted to 8 V. This will likely introduce a small offset voltage in the voltage signal when the terminal voltage is zero (important for the phase voltage measurements). This can be corrected for by repeating the calibrating process once or

Table VII. Resistance values in voltage measurements for various voltage ranges.

Inverter dc bus voltage rating	Resistor values R_V
100 V_{dc}	4 times 124 kΩ
400 V_{dc}	4 times 499 kΩ

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twice until the desired accuracy is obtained (measurement within a few milivolts of the desired value are possible).

The calibration process is described in more detail in the test procedure in Section 5.

2.8 Dc Bus-Overvoltage and Phase-Overcurrent Detection

The dc bus overvoltage protection should be activated when the bus voltage rises 17% above its rated value. With the 8 V signal at rated voltage, this results in a trip level of 9.3 V. An LM311 comparator (U5) is used to compare the trip level to the measured dc bus voltage signal. The trip level is generated using a 12V zener diode (1N4742) and with a resistive voltage divider. The resistor R9 provides positive feedback and stabilizes the comparator operation by introducing a hysteresis band of 50 mV.

The LM311 was chosen because its open-collector output transistor can be referenced to a separate emitter voltage level at pin 1 (ordinary comparators are reference to the negative voltage supply). Since all fault signals are logic-level signals, COM_D is connected to pin 1, and the pull-up resistor R11 is connected to +5 V.

The overcurrent detection was specified to trip at 216% of the rated rms current in each phase leg. With the corresponding rms current signal of 4.5 V, the trip level for an overcurrent fault is 9.71 V. Since the current is an ac signal, both positive and negative peaks need to be checked for an overcurrent in order to achieve an almost instant shutdown of operation. As in the overvoltage detection, the trip voltage is generated with a 12 V zener diode and a resistive voltage divider. LM311 comparators are used with wired-or outputs. The logic-level fault signal is generated the same way as in the overvoltage detection. The 499 kΩ resistor provides positive feedback and stabilizes the comparator operation by introducing a hysteresis band of 40 mV.

2.9 Logic

The logic for the gate signal handling and the fault detection is implemented with 5 V parts. The main part is a CPLD (U35, XC95108-PC84) that handles the gate-signal selection and lockout, the dead time and the fault procedures as described in the following Sections. Few additional logic components are needed for proper operation.

The CPLD runs on a 20 MHz clock (U38, ECS-100X-200 oscillator), which was chosen to minimize the possible dead time between the high-side and low-side signal of one phase leg. With the 20 MHz clock, the minimum dead time is 50 ns. The CPLD can be programmed through connector J12.

2.9.1 Gate Signal Selection and Lockout

The gate signals from the control board get to the CPLD via the quad receiver chips previously mentioned. Two modes of operation can be chosen. The first mode assumes that only the high-side gate signal of each phase leg is transmitted to the CPLD, and the low-side gate signals are generated as the complement of the high-side signals. The second mode assumes that both high- and low-side gate signals are available. This selection can be done externally with Jumper JP1. If it is set to +5 V (logic high), then the first mode (only high-side gate signals) is active, and if it is connected to COM_D (logic low), the second mode (all gate signals) is active. It is not possible to select the mode of operation for each individual phase leg, but rather for the whole inverter.

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To avoid that both gate drives in one phase leg receive a turn-on command, the two gate signals in one phase leg are fed through a lockout logic. This logic simply prevents both gate signals being logic high at the same time, and sets them to logic low.

For the detailed schematic, refer to SW0012, Inv_Logic_v3, Mode Selection.

2.9.2 Dead Time Implementation

Each phase leg has its own dead time logic. The dead time can be determined with the 8-bit switch SW5, by adding one to the corresponding decimal value and multiplying it by 50 ns. The lowest bit is on the right side of SW5, and the highest bit on its left side. Due to the implementation of the logic, it is not possible to turn all bits on or off at the same time. The maximum dead time possible is therefore

$$t_{d_max} = \left(2^8 - 1\right) \cdot 50ns = 12.75\mu s\,, \tag{5}$$

and the minimum dead time

$$t_{d_min} = 2 \cdot 50ns = 100ns\,. \tag{6}$$

The dead time logic enforces a certain amount of time where both gate signals of one phase leg are logic low (switch off) in between switching processes. Basically, every time one of the gate signals switches off, the dead time circuit prevents the other gate signal from turning on for a certain amount of time.

Since the CPLD runs on a fixed clock, the gate signals need to be synchronized to this clock first. After receiving the signals from the mode selection and lockout circuit, four D flip-flops detect falling edges in either one of the two gate signals of one phase leg. Each falling edge triggers an 8-bit counter to be loaded with the 8-bit dead time selected with SW5. The countdown process is automatically started by the fact that the counter state is not zero anymore, and stops as soon as the counter reaches zero.

The rising edge of a gate signal sets the output of a JK flip-flop to high, which is in turn used to prevent the other gate signal from being on (even if it would be commanded). This flip-flop is reset when the same gate signal turned off and the counter reached its zero state. After that, both gate signals have the possibility of turning on again. Two JK flip-flops are used per phase leg, one for each gate signal.

For the detailed schematic, refer to SW0012, Inv_Logic_v3, Dead Time Logic.

2.9.3 Fault-Logic

Nine different faults are monitored on the power stage board: four overcurrents (each phase), one overvoltage (dc voltage) and four gate drive faults (four pairs of gate drives that are wired-or connected). Each of the faults trips the fault logic in the CPLD, which activates the fault signal going to the control board (logic low). In addition, it disables all the gate drives by setting the negative gate signal input of each gate drive to logic high (GD_VIN_NEG in CPLD program, or GD_ENABLE in schematic). The faults are stored in the CPLD, and need to be reset either manually with a pushbutton or with the uC-RESET signal from the control board. Three different fault conditions are indicated with LEDs: overcurrent, overvoltage, and gate drive fault, in addition to the information in which phase the fault occurred in case of an overcurrent or gate drive fault. The LEDs are connected at J11.

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The fault-reset logic uses the two different reset signals (uC-RESET and PWR-UP) to create a low pulse on the GD-RESET signal (RESET-GD in schematic) for at least 50 µs, which is long enough to reset the gate drives if they are in fault state. On the rising edge of GD-RESET, the stored faults in the CPLD are reset, and the gate drives are enabled again. The uC-RESET signal from the control board needs to be a positive pulse of at least 100 ns. The PWR-UP signal is created by a pushbutton connected through J11 and a voltage supervisor U36. The voltage supervisor also takes care of the power-up of the board by setting the PWR-UP signal to low for about 1 s, which in turns disables the gate drives and prevents switching.

The gate drives also need to be enabled by the control box with the signal ENABLE. A high state will set the signal GD_VIN_NEG to a low-level if there is no fault present, which in turn enables the gate drives to switch.

For the detailed schematic, refer to SW0012, Inv_Logic_v3, Fault Logic.

2.10 Temperature Measurement

Two temperature measurements are provided in order to monitor device temperatures or ambient temperatures in the inverter box. The temperature signals are fed back to the control board, where they could be monitored and the inverter can be disabled if the temperature is too high. The sensors are LM35s in a TO-92 package (U1 and U3), which have a 10 mV/°C output signal. The signals are amplified such that 20°C correspond to 1 V.

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3. Mechanical Design

3.1 Physical Board Outline

The physical outline of the mounting holes for the mounting of the power supplies and the PCB itself are given in Fig. 2 below.

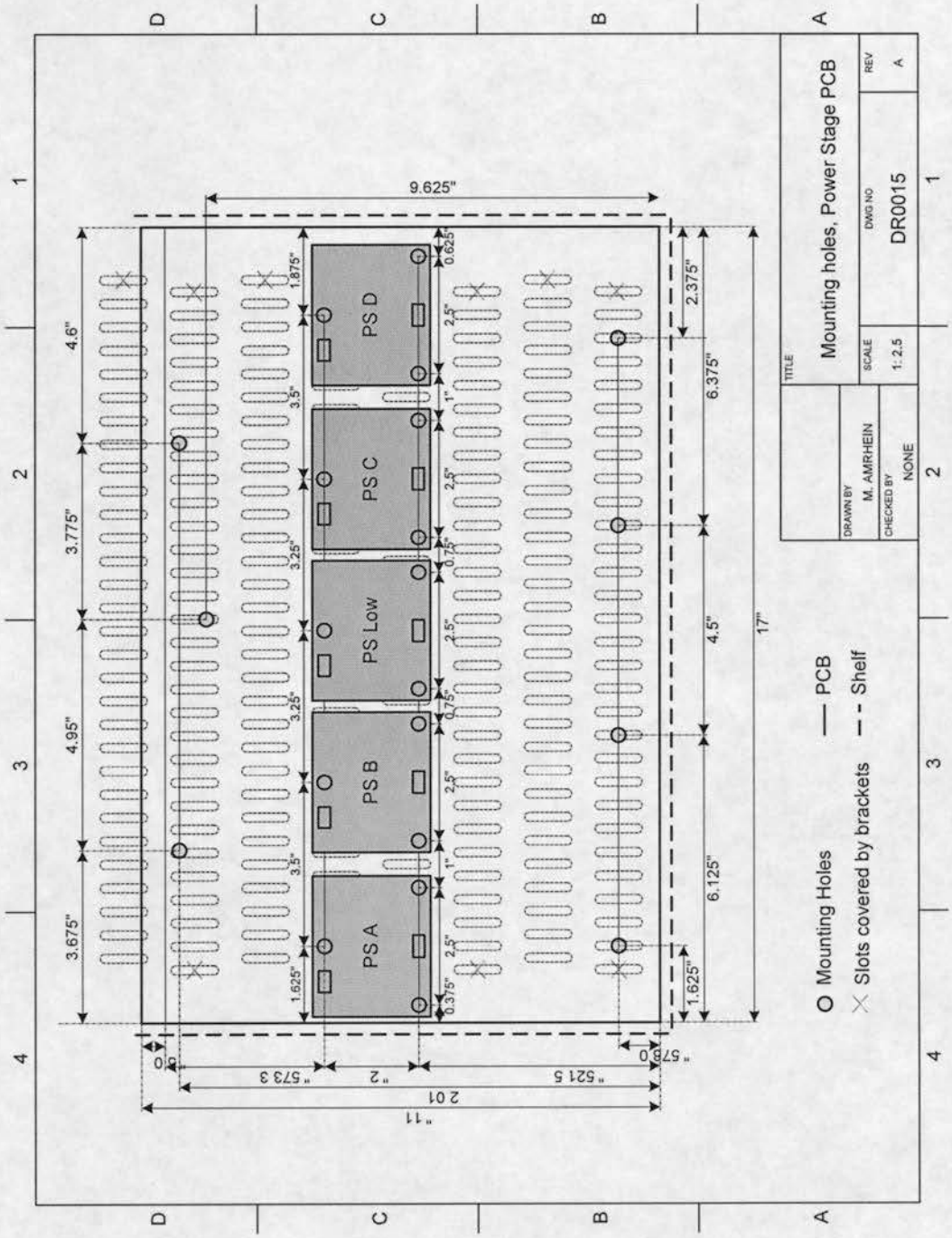

Fig. 2. Mechanical PCB outline with mounting shelf.

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3.2 Front Panel

The front panel layout of the inverter power stage is shown in Fig. 3. The fault signals are: OV – Overvoltage on dc bus; OC – Overcurrent in Phase A, B, C, or D; GD – Gate drive fault in Phase A, B, C, or D.

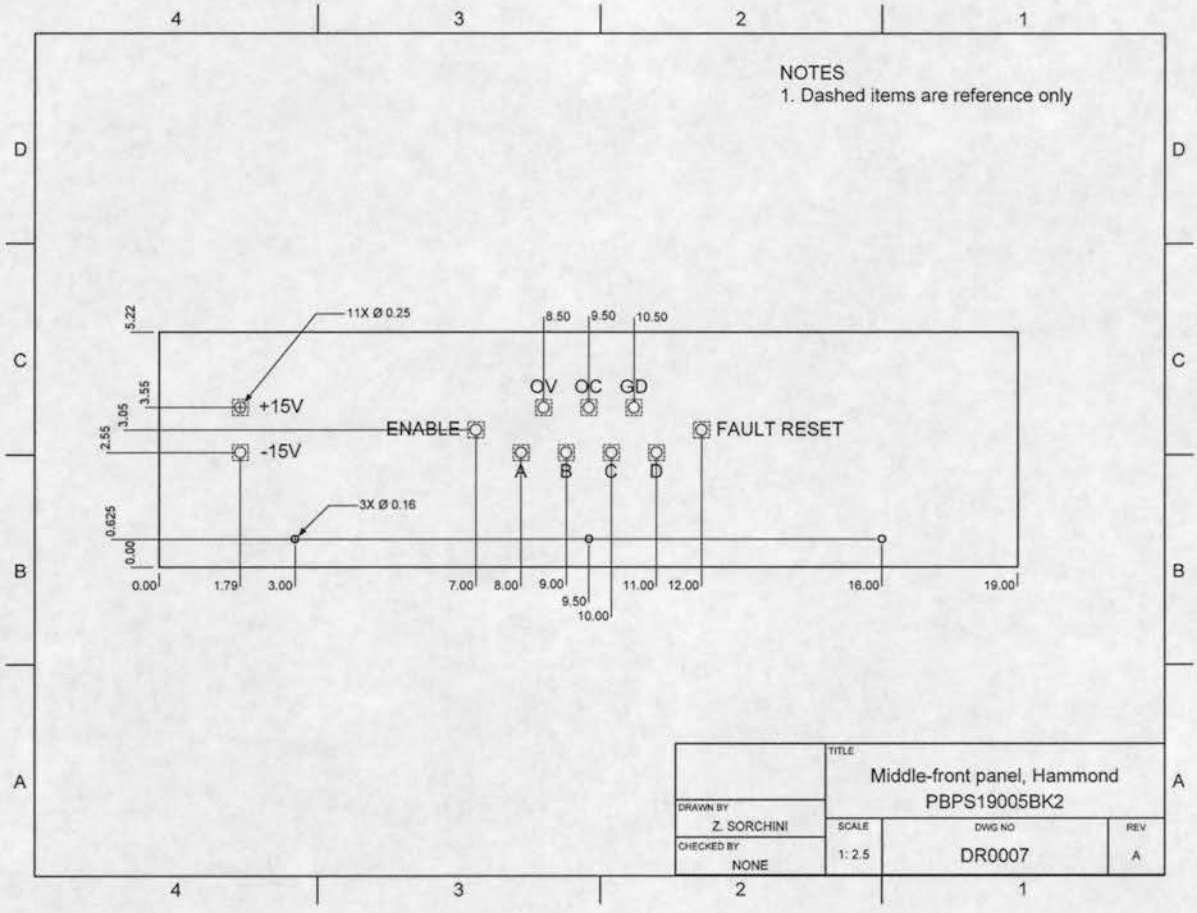

Fig. 3. Front panel layout.

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4. Known Issues

4.1 Dc-Bus and Phase Voltage Measurement

The isolated voltage amplifier introduces a 400 kHz ripple in the output signal of the voltage measurements that is not observed in the actual voltages. This ripple is due to the A/D conversion in the amplifiers (aliasing), which is described in detail in its datasheets. The ripple can be reduced by filtering the input signals (filter cut-off frequency is larger than 339 kHz, depending on resistance value of the 1 kΩ pot), and by filtering the output signals with two first-order filters with filter cut-offs of 344 kHz and 339 kHz, respectively.

The signals are in general noisy due to the ripple plus the switching of the power devices. It is recommended that the signals are filtered close to their actual use, as it is done on the control and DSP boards.

4.2 Low-Current Transducers

The smaller current transducers (LAH-25 P) introduce a dc offset in current measurements that cannot be compensated for on the inverter power stage. The offset is constant during normal operation of the inverter, but can change when power cycles on and off. Thus, the DSP needs to have a current compensation that is adjusted when the inverter is powered up.

For new boards, it is preferred to use the LAH-100 P current transducers.

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5. Test Procedure

The following paragraphs give a test procedure that should be followed for every new stuffed PCB. The procedure tests the overvoltage and overcurrent detection levels, the proper function of the fault logic, the gate drive signals and dead time, and the gate drives themselves. The voltage measurement calibration is included as well as a test under power of the board.

To start the tests, disconnect all isolated power supplies such that the gate drives do not receive power.

1. Overvoltage and overcurrent detection levels:
   - Turn on supply power (±15 V, +5 V) to the inverter board.
   - Measure voltage level at Pin 2 of U5 (overvoltage level). It should be about 9.3 V (± 0.1 V).
   - Measure voltage levels as Pin 2 of U8, U10, U12, and U14 (overcurrent levels). They should be about 9.7 V (± 0.1 V).

   If any of these voltage levels are wrong, check if the resistor values of the associated circuitry are correct.
2. Fault logic:
   - Turn on supply power (±15 V, +5 V) to the inverter board.
   - Make a quick short between TP1 (overvoltage logic signal) and COM_D. TP20 (fault signal) should switch to low level, and TP30 (gate drive enable) to high. If front panel is connected at J11, the overvoltage LED should turn on.
   - Reset the fault using the RESET pushbutton on the front panel or shorting TP32 to COM_D. Observe TP27 (gate drive reset) on scope. When faults are reset, this signal should be low for about 50 µs.
   - Short TP3, TP4, TP5, and TP6 sequentially (overcurrent logic signals) to COM_D. TP20 should switch to low level, TP30 (gate drive enable) to high, and the overcurrent LED and the corresponding phase LEDs should turn on.
   - Reset the fault.
   - Short resistor legs of R96, R97, R98, and R99 that are connected to the capacitors (gate drive faults) to COM_D. TP20 should switch to low level, TP30 (gate drive enable) to high, and the gate drive fault LED and the corresponding phase LEDS should turn on.
   - Reset the fault.

   Any problems observed could be because of an incorrect CPLD programming, or other obvious reasons like a bad solder connections.
3. Gate drive signals and dead time:
   - Remove U39, U40, and U41 (RS432 receivers) from the board.
   - Put jumper JP1 into position 'Top Gate Signals'.

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- Apply a square waveform, logic level, to TP41 (Phase A high-side gate signal). Observe the output gate drive signals from the CPLD on TP19 (high-side Phase A) and TP21 (low-side Phase A). Make sure the dead time (SW5) is on a meaningful value such (around 3 µs).
- Repeat last step for Phase B (input TP44, output TP23 and TP26, respectively), Phase C (input TP33, output TP28 and TP31, respectively), and Phase D (input TP36, output TP29 and TP24, respectively).
- Change the dead time at SW5 and observe the proper dead time changes between the high- and low-side phase signals.
- Put jumper JP1 into position 'All Gate Signals'.
- Check if gate signals get blocked out (meaning they are zero) if two logic high signals are applied to the input gate signals for the same phase. Input signals Phase A: TP41 (high-side) and TP42 (low-side), input signals Phase B: TP44 (high-side) and TP45 (low-side), input signals Phase C: TP33 (high-side) and TP35 (low-side), input signals Phase D: TP36 (high-side) and TP37 (low-side). Output gate signals see above.

Any problems observed could be because of the incorrect programming of the CPLD, or that the clock signal is not present (check TP34 for a 20 MHz clock signal).

4. Isolated power supplies:
   - With supply power turned off, connect all isolated power supplies (connectors J50 to J59, according to the schematic).
   - While turning on the supply voltage, measure the ±15 V voltage levels. If either one of the voltage magnitudes is below 13 V, turn it back off immediately. If that is the case, there might be a problem with one of the isolated power supplies. It is possible to test them by only connecting one or two power supplies to the supply voltage, and see how the supply voltage levels behave.

   To fix the supply voltage drop, not needed power supplies could be disconnected, or NTCs can be used at RT1 or RT2 to limit the inrush current (see Section 2.3 for the proper NTCs).
5. Gate drives:
   - Put jumper JP1 into position 'Top Gate Signals'.
   - Apply a square waveform, logic level, to TP41 (Phase A high-side gate signal). With a differential voltage probe, observe the gate drive signals going to the power (it should be around +15 V high and -5 to -7 V low). For Phase A high-side switch, connect probe between TP11 and TP73. If ok, observe Phase A low-side switch signal by connecting probe between TP12 and TP74. Make sure the dead time (SW5) is on a meaningful value such (around 3 µs).
   - Repeat for Phase B with input signal at TP44, high-side gate drive signal between TP13 and TP75, and low-side gate drive signal between TP14 and TP76.
   - Repeat for Phase C with input signal at TP33, high-side gate drive signal between TP15 and TP77, and low-side gate drive signal between TP16 and TP78.
   - Repeat for Phase D with input signal at TP36, high-side gate drive signal between TP17 and TP79, and low-side gate drive signal between TP18 and TP80.

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If some of the gate drives do not work, check the output voltages of corresponding isolated power supplies (+15 V and roughly -7 V). Also, check if the logic gate signals are actually applied at the gate drives (Pin 1). Another issue could be that there is a fault, meaning that Pin 2 of the gate drives is high. In that case, clear the fault and try again.

6. Voltage measurement calibration:

   In this test, measure the actual dc bus voltage constantly (for example between TP91 and TP90). **Do not change power connections if there is any voltage above 15 V on the dc bus!** The calibration procedure is also briefly described in Section 2.7.

   - With the board supply power off, connect a dc power supply capable of the voltage range of the inverter to Phase A (TP85) and the negative dc bus (TP90). Measure this voltage with a multimeter.
   - Turn on the supply power to the board. Also make sure that the isolated power supply for the low-side gate drives is connected and working properly (the one in the center).
   - Measure the voltage signal of Phase A (TP69) with a multimeter.
   - With the main power supply off (and its outputs to the board short-circuited to ensure zero voltage output), adjust pot R142 to get 0 V at the measured voltage signal.
   - Apply rated dc-bus voltage from main power supply (remove short!). Use pot R148 to adjust the measured voltage signal to its corresponding value (8V = rated voltage of inverter power stage -> see Section 2.2).
   - Repeat this process once or twice ensure proper calibration.
   - Turn off the main power supply, and wait until dc-bus voltage is less than 15 V before removing any wires.

   The steps given above need to be repeated for each of the phase and the dc-bus voltages:

   - Phase B: Connect power supply between TP86 and TP90. Measure phase voltage signal at TP70. Adjust this signal with pots R156 and R162, respectively.
   - Phase C: Connect power supply between TP87 and TP90. Measure phase voltage signal at TP71. Adjust this signal with pots R170 and R176, respectively.
   - Phase D: Connect power supply between TP88 and TP90. Measure phase voltage signal at TP72. Adjust this signal with pots R184 and R190, respectively.
   - Phase B: Connect power supply between TP91 and TP90. Measure phase voltage signal at TP68. Adjust this signal with pots R128 and R134, respectively.

   If there are any problems arising in this part, check if the isolated voltage amplifiers receive the 5 V power on both the high and the low side. Also, check the proper voltage levels across the zener diodes in the offset voltage adjustment (roughly ±10 V).

7. Full powered test:

   - Build an H-bride using two phases and a power resistor in between. Choose the power resistor such that about 1 A to 3 A is flowing in the power devices (for example about 100 Ω resistance), and adjust the dc bus voltage properly.
   - Put jumper JP1 into position 'Top Gate Signals'.

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- Supply a logic-level square waveform (roughly 2 kHz) to the high-side gate signal input of one phase used in the H-bridge, and the inverse signal to the high-side gate signal input of the other phase.
- Turn on the power supply to the inverter, and turn on the main dc power supply with its voltage set at 0 V. Also turn on the gate signals.
- Slowly raise the voltage. Observe the actual voltage waveform over the resistor in the H-bridge using a isolated voltage probe, and measure the current with a current probe.
- Observe the current waveforms measured on the board (TP7 to TP10 for Phases A to D, respectively). The measurement range can be adjusted with switches SW1 to SW4 for Phases A to D, respectively. The voltage level should be 4.5 V at the indicated current level next to the switches.
- Observe the phase voltage waveforms, and compare to the actual phase voltage waveform. The voltage magnitude should correspond to the actual dc-bus voltage (8 V equals dc-bus voltage rating of inverter power stage).

In case there are any problems, check the proper connection of all power supplies. Also, follow the propagation of the gate signals. All faults need to be cleared for proper operation.

This concludes the test procedure of the power stage. Note that a high power test is not included here, but should be administered once the power stage is properly connected and mounted in the box, with all heatsinks attached.

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6. Appendix

6.1 Bill of Materials

Power Stage Design Hierarchy Revised: Wednesday, March 22, 2006
SK0031 Revision: 4

Bill Of Materials August 11,2005 12:46:04

Item	Qty	Reference	Value	Part Desc.	Manf.	Part #	Vendor	Order #
1	159	C1,C2,C3,C4,C5,C6,C7,C8, C9,C10,C11,C13,C14,C16, C17,C20,C21,C22,C23,C24, C25,C26,C27,C28,C29,C32, C33,C34,C35,C36,C37,C38, C39,C40,C41,C42,C43,C44, C45,C48,C49,C50,C51,C52, C53,C56,C57,C58,C59,C60, C61,C63,C65,C67,C70,C72, C75,C77,C78,C82,C83,C86, C88,C90,C93,C94,C96,C100, C102,C104,C106,C108,C111, C112,C115,C117,C120,C121, C123,C126,C129,C132,C133, C137,C138,C141,C142,C143, C144,C145,C147,C149,C151, C153,C155,C156,C165,C167, C169,C171,C173,C175,C177, C179,C181,C183,C185,C187, C189,C191,C193,C195,C196, C197,C198,C200,C201,C202, C204,C205,C207,C208,C209, C210,C212,C213,C215,C216,	0.1u	0.1uF 50V Mono Cap	Sprague	1C20Z5U104M050B	ECE	181201250

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		C217,C218,C220,C221,C223, C224,C225,C226,C228,C229, C230,C232,C233,C234,C236, C237,C238,C239,C240,C241, C242,C243,C244,C245,C246, C247,C261,C265,C269,C273, C277						
2	11	C15,C248,C249,C250,C251, C252,C253,C254,C255,C256, C257	200p	200pF 1kV Ceramic Cap	Vishay	75-5GAT20	ECE	180709000
3	8	C64,C73,C84,C91,C101, C109,C118,C127	100p	100pF 1kV Ceramic Cap	Vishay	75-5GAT10	ECE	180708000
4	4	C46,C47,C54,C55	150p	150pF 1kV Ceramic Cap	Vishay	75-5GAT15	ECE	180708500
5	16	C62,C68,C71,C76,C80,C87, C89,C95,C98,C105,C107, C113,C116,C122,C125,C130	100u	100uF 35V Elect. Rad. Cap	Panasonic	ECA-1VM101	Digikey	P5165-ND
6	8	C66,C74,C81,C92,C99,C110, C119,C128	22u	22uF 50V Elect. Rad. Cap	Panasonic	P5179-ND	ECE	180302500
7	8	C69,C79,C85,C97,C103, C114,C124,C131	undet. Cg	Gate capacitance				
8	24	C134,C146,C148,C150,C152, C154,C170,C172,C174,C176, C178,C180,C182,C184,C186, C188,C190,C192,C194,C199, C206,C214,C222,C231	10u	10uF 50V Elect. Rad. Cap	Panasonic	P5178-ND	ECE	180301500
9	9	C12,C18,C19,C30,C31,C135, C136,C139,C140	10n	10nF 50V Mono Cap	Sprague	1C20Z5U103M050B	ECE	181200250
10	4	C157,C158,C159,C160	0.56u or 2u	0.56uF 630V Film Cap (for MOSFETs) 2uF 1000V Film Cap (for IGBTs)	CDE CDE	DME6P56K SCD205K102A3Z25	Newark Mouser	16F8010 598-SCD205K102A
11	2	C161,C162	1200u	1200uF 450V Elect. Rad. Cap	Panasonic	ECE-T2WP122FA	Digikey	P10071-ND
12	1	C163	undet.	Ground capacitance				
13	3	C164,C166,C168	220u	220uF 25V Elect. Rad. Cap	Panasonic	P5153-ND	ECE	180305000
14	11	C203,C211,C219,C227,C235,	68p	68pF 1kV Ceramic Cap	BC Comp.	DD680	ECE	180707250

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		C259,C263,C267,C271,C272, C275						
15	9	C258,C260,C262,C264,C266, C268,C270,C274,C276	470p	470pF 1kV Ceramic Cap	Vishay	75-5GAT47	ECE	180711000
16	5	D1,D2,D3,D6,D7	1N4742	1W 12V Zener Diode	Fairchild	1N4742A	ECE	30103750
16	40	D10,D11,D12,D13,D14,D15, D16,D17,D18,D19,D20,D21, D22,D23,D24,D25,D26,D27, D28,D29,D30,D31,D32,D33, D34,D35,D36,D37,D38,D39, D40,D41,D42,D43,D44,D45, D46,D47,D48,D49	MUR160 or 1N4148	Rect. ultrafast, 600V, 1A axial 70V Diode	Onsemi Fairchild	MUR160 1N4148	Newark ECE	08F2048 30157300
17	10	D50,D51,D52,D53,D54,D55, D56,D57,D58,D59	1N4740	1W 10V Zener Diode	Motorola	1N4740A	ECE	30103250
18	1	JP1		2 pos. double row header	Berg	54102-S08-02	ECE	300430200
19	1	J1		34 pin straight solder header	3M Corp.	3431-6002	ECE	300307750
20	1	J2		26 pin straight solder header	3M Corp.	3429-6002	ECE	300307500
21	8	J3,J4,J5,J6,J7,J8,J9,J10		Gate signals connectors				
22	1	J11	MTA100-6	6 pos MTA100 header	AMP	571-6404566	ECE	300361300
23	1	J12	CON14A	CPLD prog. conn., 14pin, 2mm	Molex	87331-1420	Digikey	WM18063-ND
24	45	J13,J14,J15,J16,J17,J18, J19,J20,J21,J22,J23,J24, J25,J26,J27,J28,J29,J30, J31,J32,J33,J34,J35,J36, J37,J38,J39,J40,J41,J42, J43,J44,J45,J46,J47,J48, J60,J62,J63,J64,J65,J66, J67,J68,J69	AWG14	14 Gage wire connector for power wiring				
25	1	J49	MTA156-4	4 pos MTA156 header	AMP	571-6404284	ECE	300361600
26	1	J59	MTA100-4	4 pos MTA100 header	AMP	571-6404564	ECE	300361100
27	10	J50,J51,J52,J53,J54,J55, J56,J57,J58,J61	MTA100-3	3 pos MTA100 header	AMP	571-6404563	ECE	300361000
28	1	J70		Soldering connection for GND re-routing				
29	8	Q1,Q2,Q3,Q4,Q5,Q6,Q7,Q8		MOSFET, 150V, 105A	IRF	IRFPS3815	Newark	74C9925

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				MOSFET, 500V, 46A	IRF	IRFPS40N50L	Newark	74C9926
	4			IGBT, dual module, 600V, 100A	Eupec	BSM100GB60DLC	Mouser	641-BSM100GB60DLC
30	4	RN1,RN2,RN3,RN4	1k8 DIP	8x1.8kOhm isolated res, DIP14	Bourns	4114R-1-182	Mouser	652-4114R-1-1.8K
31	1	RN5	100 SIP	100Ohm bussed res, SIP10	Bourns	4310R-1-101-ND	ECE	150260000
32	1	RN6	10k SIP	10kOhm bussed res, SIP10	Bourns	4310R-1-103-ND	ECE	150262000
33	2	RT1,RT2	NTC	Current Limiter Inrush, 2.8A, 5Ohm	Thermom.	CL-160	Digikey	KC016L-ND
34	18	R21,R22,R37,R38,R51, R52,R53,R54,R55,R56,R57, R58,R59,R60,R61,R62,R95	10k	10kOhm res, 1%, 0.25W	Yageo		ECE	150103000
36	12	R3,R7,R195,R196,R197, R198,R199,R200,R201,R202, R203,R204	4k99	4.99kOhm res, 1%, 0.25W	Yageo		ECE	150103000
37	5	R9,R23,R24,R39,R41	499k	499kOhm res, 1%, 0.25W	Yageo		ECE	150103000
38	13	R10,R19,R20,R35,R36,R100, R101,R104,R107,R113,R114, R116,R119	143	143Ohm res, 1%, 0.25W	Yageo		ECE	150103000
39	1	R13	24k3	24.3kOhm res, 1%, 0.25W	Yageo		ECE	150103000
40	4	R25,R27,R43,R44	43k2	43.2kOhm res, 1%, 0.25W	Yageo		ECE	150103000
41	8	R63,R67,R71,R75,R79,R83, R87,R91	100	100Ohm res, 1%, 0.5W	Xicon	273-100	Mouser	273-100
42	8	R64,R68,R72,R76,R80,R84, R88,R92	undet. Rc	GD power resistance, 1%, 0.5W				
43	8	R65,R69,R74,R78,R82,R85, R90,R93	Rg	15.0Ohm res, 1%, 0.5W or 47.5 Ohm res, 1%, 0.25W	Xicon Yageo	273-15-RC	Mouser ECE	273-15-RC 150103000
44	8	R66,R70,R73,R77,R81,R86, R89,R94	47k5	47.5kOhm res, 1%, 0.5W	Xicon	273-47.5K	Mouser	273-47.5K
45	14	R102,R108,R111,R117,R125, R131,R139,R145,R153,R159, R167,R173,R181,R187	200	200Ohm res, 1%, 0.25W	Yageo		ECE	150103000
46	58	R1,R2,R4,R5,R6,R8,R11, R14,R15,R16,R17,R18,R26,	1k	1kOhm res, 1%, 0.25W	Yageo		ECE	150103000

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		R28,R31,R32,R33,R34,R40, R42,R47,R48,R49,R50,R96, R97,R98,R99,R103,R105, R106,R109,R110,R112,R115, R118,R123,R124,R129,R135, R137,R138,R143,R149,R151, R152,R157,R163,R165,R166, R171,R177,R179,R180,R185, R191,R193,R194						
47	10	R128,R134,R142,R148,R156, R162,R170,R176,R184,R190	1k Pot	1k Trim Pot, 25 turn	Bourns	3296W-1-102	ECE	150340600
48	3	R120,R121,R122	undet.	Ground resistance, 0.25W				
49	20	R126,R127,R130,R133,R140, R141,R144,R147,R154,R155, R158,R161,R168,R169,R172, R175,R182,R183,R186,R189	Rv	124kOhm res, 1%, 0.25W or 499kOhm res, 1%, 0.25W	Yageo Yageo		ECE ECE	150103000 150103000
50	10	R12,R132,R136,R146,R150, R160,R164,R174,R178,R188, R192	6k81	6.81kOhm res, 1%, 0.25W	Yageo		ECE	150103000
51	4	SW1,SW2,SW3,SW4		3-pos. DIP switch, SPST	Grayhill	76SB03	Newark	28F1451
52	1	SW5		8-pos. DIP switch, SPST	Grayhill	76SB08	ECE	240120500
53	32	TP1,TP3,TP4,TP5,TP6,TP19, TP20,TP21,TP22,TP23,TP24, TP25,TP26,TP27,TP28,TP29, TP30,TP31,TP32,TP33,TP34, TP35,TP36,TP37,TP38,TP39, TP40,TP41,TP42,TP43,TP44, TP45	TP white	Testpoint white	Keystone	5012	ECE	
54	10	TP2,TP7,TP8,TP9,TP10, TP68,TP69,TP70,TP71,TP72	TP yellow	Testpoint yellow	Keystone	5014	ECE	
55	24	TP11,TP12,TP13,TP14,TP15, TP16,TP17,TP18,TP73,TP74, TP75,TP76,TP77,TP78,TP79, TP80,TP85,TP86,TP87,TP88, TP89,TP90,TP91,TP92	TP orange	Testpoint orange	Keystone	5013	ECE	

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56	6	TP46,TP47,TP48,TP49,TP50, TP51	TP red	Testpoint red	Keystone	5010	ECE	
57	20	TP52,TP53,TP54,TP55,TP56, TP57,TP58,TP59,TP60,TP61, TP62,TP63,TP64,TP65,TP66, TP67,TP81,TP82,TP83,TP84	TP black	Testpoint black	Keystone	5011	ECE	
58	2	U1,U3		Precision Centigrade Temp Sensor, TO-92	National	LM35CZ	Newark	92F287
59	16	U2,U4,U7,U9,U11,U13,U15, U20,U22,U24,U26,U44,U46, U48,U50,U52		Dual Opamp, JFET Input, 8-DIP	TI	TLE2082ACP	Newark	26C1841
60	9	U5,U8,U10,U12,U14,U54, U55,U56,U57		Comparator, single, 8-DIP	National	LM311N	ECE	90111500
61	1	U6		Quad SPST, N.O., 16-DIP	MAXIM	DG212CJ	Newark	90C1245
62	3	U16,U17,U18		Quad Opamp, JFET Input, 14-DIP	TI	TL2084CN	Newark	08F9183
63	4	U19,U21,U23,U25		Current Transducer, CL, 100A nom or Current Transducer, CL, 25A nom	LEM LEM	LAH 100-P LAH 25-NP	Digikey Digikey	398-1009-ND 398-1007-ND
64	8	U27,U28,U29,U30,U31,U32, U33,U34		Octocoupler Gate Drive, 2A, 16-SOIC	Agilent	HCPL-316J	Newark	92F648
65	1	U35		CPLD 84-PLCC	Xilinx	XC95108-15PC84C	Digikey	122-1175-ND
66	1	U36		Voltage Supervisor, 8-DIP	TI	TLC7705IP	Newark	66F4591
67	1	U37		Quad Diff. Line Driver, 16-DIP	National	DS26LS31CN	Newark	07B5238
68	1	U38		20MHz 5V 14-DIP Oscillator	Mouser	520-TCF2000	ECE	140111000
69	3	U39,U40,U41		Quad Diff. Line Receiver, 16-DIP	National	DS26LS32ACN	Newark	07B5239
70	2	U42,U43		Hex Inverter IC, 14-DIP	TI	SN74LS04N	ECE	90501250
71	5	U45,U47,U49,U51,U53		Isolated Voltage Amplifier, 8-DIP	Agilent	HCPL-7800A	Newark	06F5493
72	1	U35		PLCC Socket, 84 pos, through hole	Mill-Max	940-99-084-24-000000	Mouser	575-842494
73	1	JP1		Mini Jump Jumpers 0.1"	Berg	65474-010	ECE	300425000
74	4	SW1,SW2,SW3,SW4		Solder Socket 6 pin, 6-DIP	Rob.-Nug.	ICE-063-S-TG	Mouser	517-ICE-063-S-TG
75	31	U2,U4,U5,U7,U8,U9,U10, U11,U12,U13,U14,U15,U20, U22,U24,U26,U36,U44,U45, U46,U47,U48,U49,U50,U51,		Solder Socket 8 pin, 8-DIP	Rob.-Nug.	ICE-083-S-TG	ECE	360120000

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		U52,U53,U54,U55,U56,U57						
76	5	U16,U17,U18,U42,U43		Solder Socket 14 pin, 8-DIP	Rob.-Nug.	ICE-143-S-TG	ECE	360120250
77	10	RN1,RN2,RN3,RN4,SW1, U6,U37,U39,U40,U41		Solder Socket 16 pin, 8-DIP	Rob.-Nug.	ICE-163-S-TG	ECE	360120500
78	15			4-40x1" Nylon Spacer	Smith	4062	ECE	820158400
79	12			4-40x1" Brass Hex Spacer	Smith	2334	ECE	830145750
80	30			4-40x1/4" Nylon Screw	McMaster	95000A106	ECE	830710500
81	10			3 pos MTA100 Housing	Amp	571-6404403	ECE	300360100
82	1			4 pos MTA100 Housing	Amp	571-6404404	ECE	300360200
83	1			4 pos MTA156 Housing	Amp	571-6404284	ECE	300361600

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Design Document

Modular Inverter Isolated Power Supply

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Author: Zakdy Sorchini

Principal Investigator: Jonathan Kimball

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Abstract:

This document briefly describes the functionality and characteristics of the isolated power supplies for the power stage. A push-pull forward converter with sensorless current mode control is implemented.

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Issue	Date	Comments
000	4/3/2006	Initial release.

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1. Introduction

The isolated power supplies are used to power the gate drive circuit of the Power Stage, for both IGBT and MOSFET versions. It provides loosely regulated gate drive voltage and regulated logic voltage. The power supplies implement a push-pull forward converter using sensorless current mode control.

1.1 Scope

The isolated power supplies are intended to be part of the modular inverter, used with the power stage board. They can also be used for other gate drive circuits or circuits that required minimum power. Primary used is for research.

1.2 References

Schematic: SK0032 rev 2

Layout: PB0032 rev B

Power stage board: SK0031 and PB0031

1.3 Known Issues

There is no output short-circuit protection. The MOSFETs or the current-limiting resistors will fail during an output short-circuit.

There is no soft-start in the original design. The circuit was modified to provide some degree of soft-start, but this is very dependent on the voltage source used to feed the power supply.

The schematic and PCB, as archived and manufactured, have to be modified to implement the power supplies. All the details of the modifications are included in the schematic.

The sensorless current mode control seems to give two different steady-state behaviors for the power supplies. The primary sided current can be at the intended frequency, or at double the intended frequency. The actual steady-state behavior for a given power supply seemed to be always the same, but among power supplies seems to be random.

2. Interface

2.1 Input Power

The power supplies require ±15 V only. Logic power is internally created, because it is required to be referenced to the -15 V rail. The input power connector is an MTA-100 (J1).

2.2 Output Power

The power supplies produce +15 V (Zener regulated) and -5 V (nominal, unregulated) and +5V regulated. The +15 and -5 V are used for the gate drive power. The +5V is used to power the actual gatedrive IC. The output power connector is an MTA-100 (J2).

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3. Power Circuit

The power supply is based on a push-pull forward converter. The full 30 V input voltage is applied to the transformer. This requires the gate drive circuit to be referenced to the -15 V rail. IRF630 MOSFETs are used (can substitute accordingly, recall that the MOSFETS should be able to block at least 60 V not considering overshoot). Output diodes are MBR1100 Schottky.

The output of the forward converter (nominally 20 V) is regulated to +15 V with a Zener diode. The Zener anode is the output common. The remaining part of the 20 V is the negative gate drive voltage. The +15 V is then fed to a 7805 regulator for logic power.

4. Control Circuit

The control circuit generates the required gate drive signals to operate the converter. First, the transformer input voltage is integrated (the integration time constant is adjustable to provide some control over the switching frequency). This "control voltage" is then compared to fixed positive and negative voltages. When the control voltage exceeds the reference, a latch is SET or RESET to keep the flux inside an hysteresis band.

The latch directly controls a MIC4428 buffer that in turn controls the gates of the MOSFETs. The gate voltage is 5 V. No deadtime is provided by the gate driver. Deadtime is achieved by using diodes in the gate path and using asymmetric resistance for turn-on and turn-off.

In general, it is possible to use a 100 kHz switching frequency, but 50 kHz is recommended. (Each individual power supply must be adjusted and monitored for saturation. If saturation occurs, raise the switching frequency. This is required because two different steady-state behaviors were observed during calibration.)

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Design Document

Software Development Guide for Modular Inverter

Reference: TU0003

Issue: 002

Status: Issued V1.0

Author: Guoliang Zhang

Principal Investigator: J. Kimball

Created: April 2, 2005

Abstract:

This document is intended to archive the modular inverter control software architecture, which is based on Matlab/Simulink Embedded Coder for TI C2000 toolbox. Some customized functions are described in detail.

This document also serves as instruction manual for power lab users that may use the modular inverter to develop digital motor control algorithms or other related applications. A fully functional example is included at the end of this document and links to the related files are provided.

Some useful resources are listed in the appendix to help users locate necessary knowledge base that are required to fulfill advanced functionalities.

Document Revision History

Issue	Date	Comments
001	2/17/2006	First release
002	3/3/2006	Added Flash part, updated TOC

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1. Introduction

1.1 Overview and Scope

EZdsp2812 is a board made by Spectrumdigital.com that utilizes a TI TS320F2812 DSP core. Full description on this chip can be found at TI.com. Some of the key features of this DSP controller are:

- **Extended Temperature Performance of −55°C to 125°C**

- **High-Performance Static CMOS Technology**
  - **150 MHz (6.67-ns Cycle Time)**
  - **Low-Power (1.8-V Core @135 MHz, 1.9-V Core @150 MHz, 3.3-V I/O) Design**
- **JTAG Boundary Scan Support**

- **High-Performance 32-Bit CPU (320C28x)**
  - **16 x 16 and 32 x 32 MAC Operations**
  - **16 x 16 Dual MAC**
  - **Harvard Bus Architecture**
  - **Atomic Operations**
  - **Fast Interrupt Response and Processing**
  - **Unified Memory Programming Model**
  - **4M Linear Program/Data Address Reach**
  - **Code-Efficient (in C/C++ and Assembly)**
  - **320F24x/LF240x Processor Source Code Compatible**

- **On-Chip Memory**
  - **Flash Devices: Up to 128K x 16 Flash (Four 8K x 16 and Six 16K x 16 Sectors)**
  - **ROM Devices: Up to 128K x 16 ROM**
  - **1K x 16 OTP ROM**
  - **L0 and L1: 2 Blocks of 4K x 16 Each Single-Access RAM (SARAM)**
  - **H0: 1 Block of 8K x 16 SARAM**
  - **M0 and M1: 2 Blocks of 1K x 16 Each SARAM**

- **External Interface (2812)**
  - **Up to 1M Total Memory**
  - **Programmable Wait States**
  - **Programmable Read/Write Strobe Timing**
  - **Three Individual Chip Selects**

- **Three 32-Bit CPU-Timers**

- **128-Bit Security Key/Lock**
  - **Protects Flash/ROM/OTP and L0/L1 SARAM**
  - **Prevents Firmware Reverse Engineering**

- **Motor Control Peripherals**
  - **Two Event Managers (EVA, EVB)**
  - **Compatible to 240xA Devices**

- **Serial Port Peripherals**
  - **Serial Peripheral Interface (SPI)**
  - **Two Serial Communications Interfaces (SCIs), Standard UART**
  - **Enhanced Controller Area Network (eCAN)**
  - **Multichannel Buffered Serial Port (McBSP)**

- **12-Bit ADC, 16 Channels**
  - **2 x 8 Channel Input Multiplexer**
  - **Two Sample-and-Hold**
  - **Single/Simultaneous Conversions**
  - **Fast Conversion Rate: 80 ns/12.5 MSPS**

- **Up to 56 General Purpose I/O (GPIO) Pins**

- **Development Tools Include**
  - **ANSI C/C++ Compiler/Assembler/Linker**
  - **Code Composer Studio IDE**
  - **DSP/BIOS**

- **Boot ROM (4K x 16)**
  - **With Software Boot Modes**
  - **Standard Math Tables**

Code Composer Studio (CCS) for C2000 is the software development tool for this DSP. Current version is V2.21. It is recommended to have only one CCS installed on one computer to avoid any confliction between applications.

Matlab/Simulink provides the automated code generating tool for this DSP family. Users can communicate with the DSP via Matlab Link for CCS. Under most cases, users should develop their control algorithms in Simulink and use the automatic RTW tool to generate/build/download the code to target DSP and run the executable program in CCS.

To use the digital controller system effectively and efficiently, certain skills/knowledge are required. Based on the complexity that might get involved during the development, two levels of users are defined:

Level 1: Control Algorithm developers

Example: motor control algorithm, digital pwm algorithm, filter designs, etc.

You need to have knowledge on

- basic usage of Matlab/Simulink
- fixed point data type, IQ math(just another form of fixed-point defined by TI)
- discrete time signal processing -specifically, discrete time integration, sample/hold, delay, Z transform.
- PWM parameter settings
- Hardware configuration on the modular inverter and its control board.
- Matlab GUI is a plus
- Real-Time multitask scheduling is a plus.

Level 2: Expanded function developers

Example: DAC, Communication, Stand alone applications, etc. Especially when your needs are beyond the capability provided by our library functions.

Except requirements to level 1 users, you also need knowledge on

- C/C++ and Library functions for C281x provided by TI.
- S-Function in Matlab/Simulink
- RTW(Real-Time Workshop) and TLC(Target Language Compiler)
- Hardware on TI 320F2812 DSP is a plus.

This document focuses on level 1 user. References will be provided to help level 2 users locate the necessary recourses.

A knowledge tree below shows the required skills/knowledge and their relationships for each group of users. Bold text indicates key skill needed for that group of users. Real Time Data Transfer function is only available with the update of CCS 2.20+ and Matlab R14 SP2+.

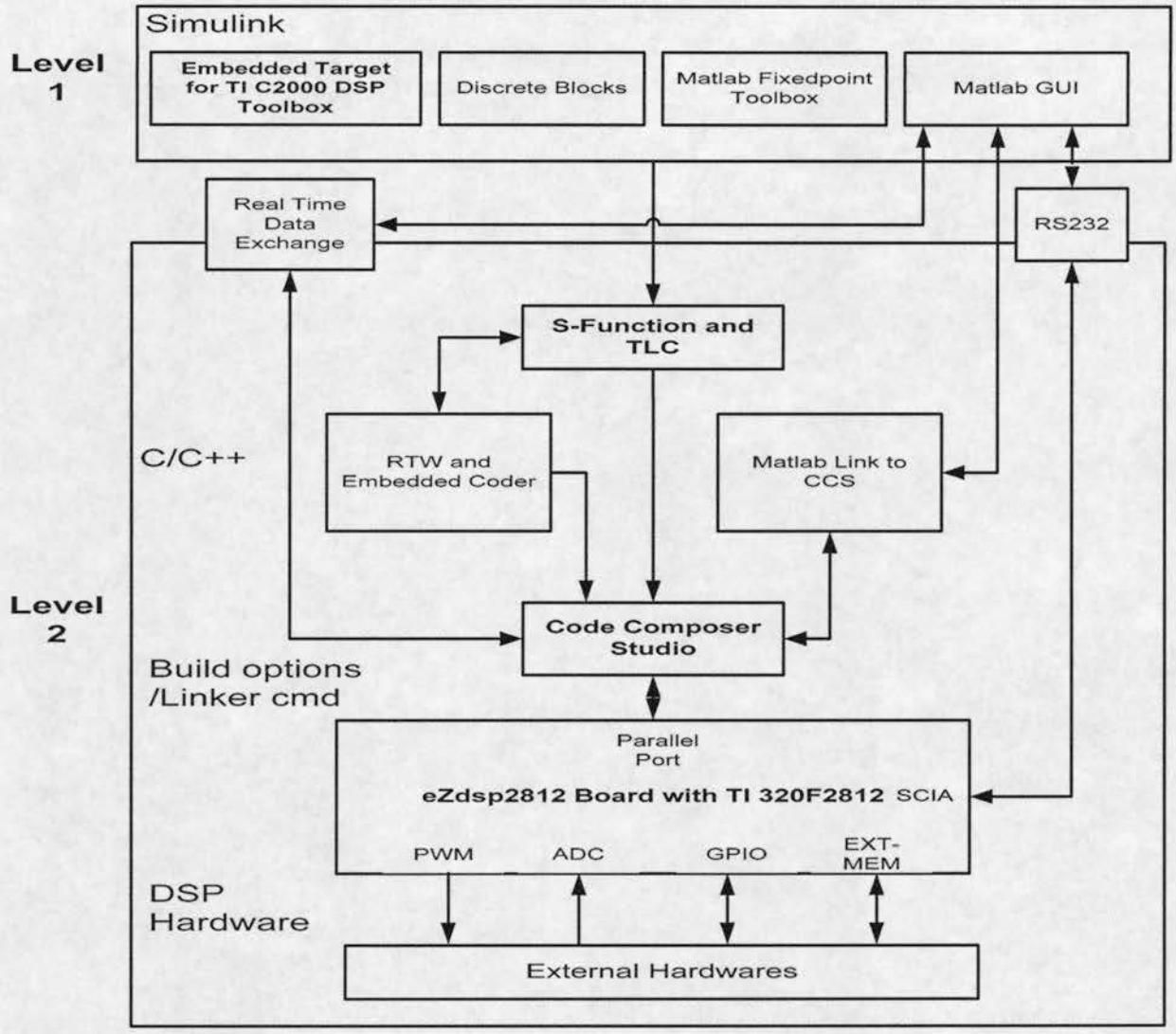


Figure 1 Knowledge Tree

1.2 Definitions

TI	Texas Instrument
DSP	Digital Signal Processing
CCS for C2000	Code Composer Studio, a software development tool for F281x provided by TI
UUT	Unit Under Test

1.3 References

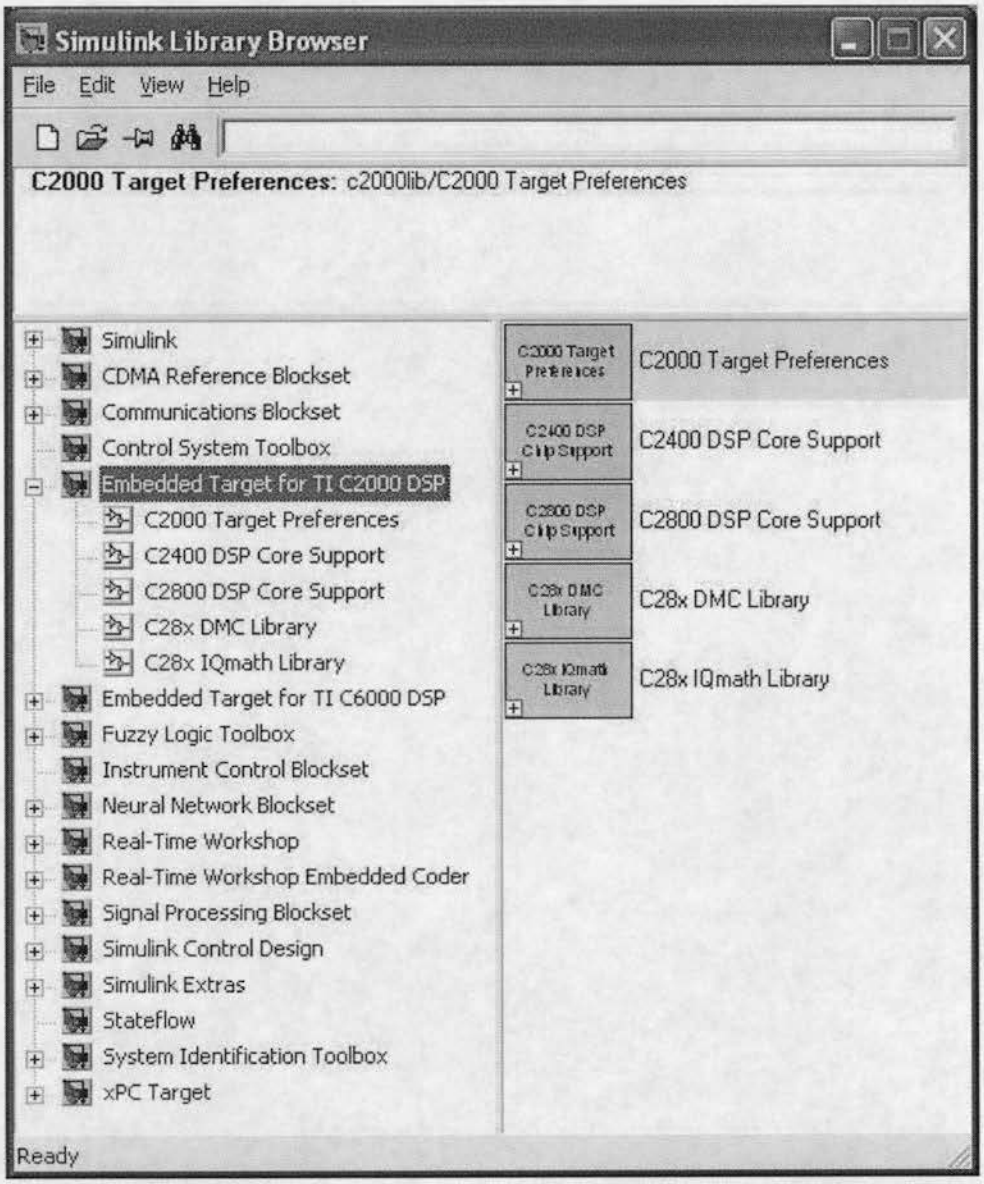
F2812 family Home --- http://focus.ti.com/docs/prod/folders/print/sm320f2812.html

2. User Interface

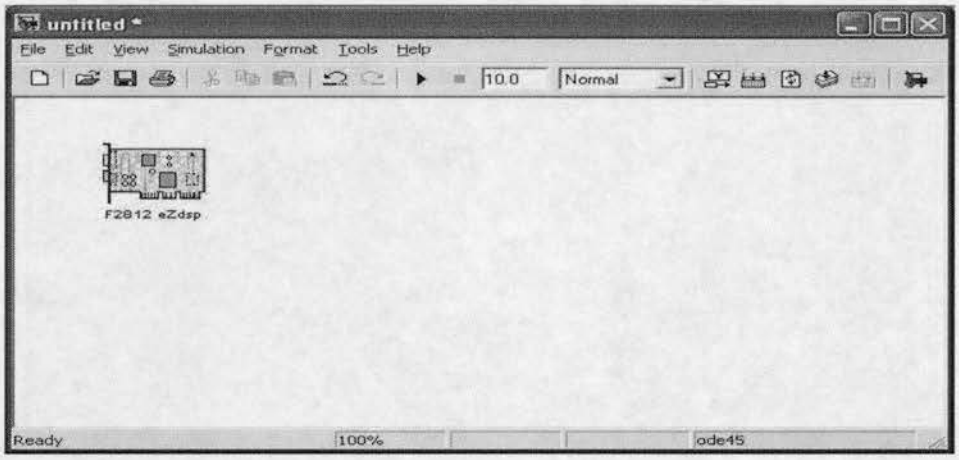
2.1 Matlab/Simulink Environment Setup

User will develop control algorithm under Simulink environment. To successfully run the process, several toolboxes are required. They are: Fixed Point Toolbox, RTW toolbox, Embedded Coder toolbox and Embedded Coder for TI C2000 Toolbox. Type "ver" at Matlab command window to see if all of those toolboxes are installed on the computer you plan to work on. We have one license for each toolbox for the whole group. Also, a Microsoft VC6.0 should be installed on the computer.

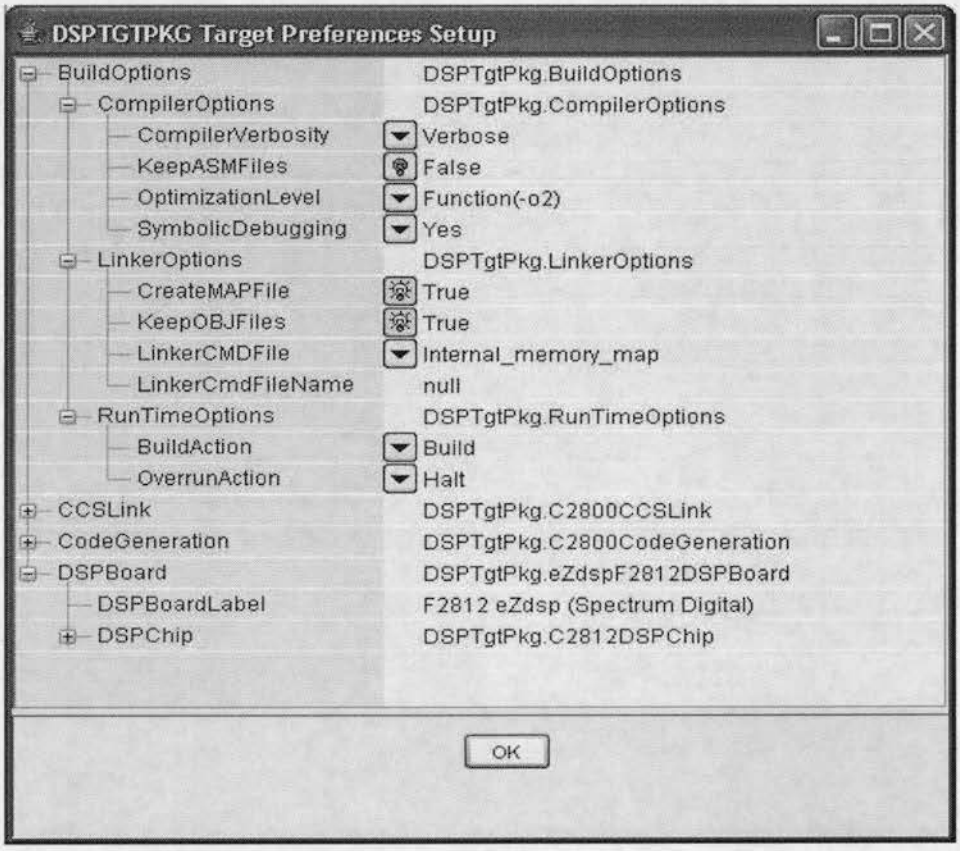
Upon opening the Simulink Library browser, an "Embedded Target for TI C2000 DSP" item should show up on the left, all the build-in functions can be found under this group of library modules.



The first thing to do after creating a blank model under Simulink is to choose the F2812 eZdsp target from "C2000 Target Preference" library. Now there should be a blank Simulink model window with target preference block, it should look like this:

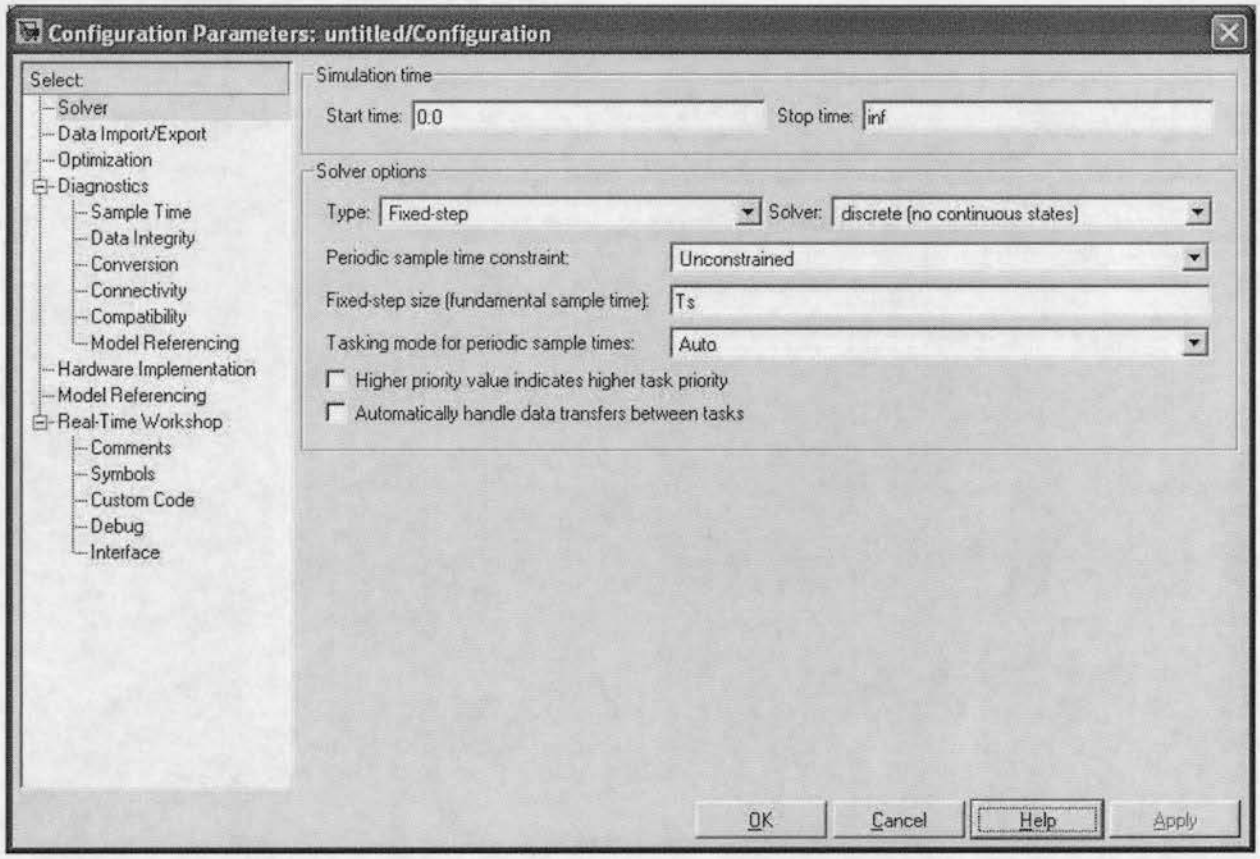


This block contains options for target board hardware configuration and compiler/linker preferences. You need to change some of the options to make it like this:



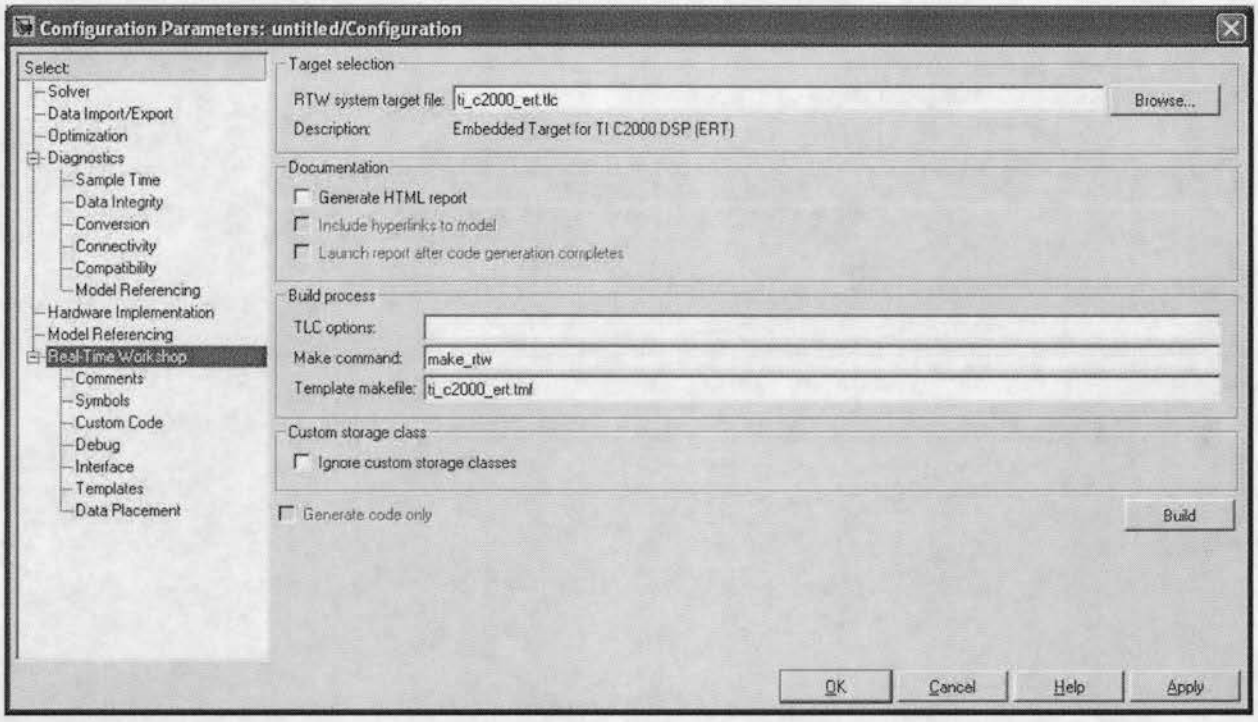
You might need to change the DSPBoardLabel option according to CC_SETUP definition. See 2.4.1 for more information. Other un-shown items should be kept as default.

Next Step is to configure the model parameters. Since the embedded software is running periodically forever, we need the model to be implemented in discrete time with no continuous state. Stop time should be inf under most cases. The solver setup page should be like:



Notice that the fundamental sample time must be fastest sample time in the model and all other blocks can only be run at integer times this rate. Faster tasks (blocks) have higher priority.

Another page need to be configured is the Real-Time Workshop preference. It will look like this after you change the RTW system target file name to "ti_c2000_ert.tlc" from the Browse…window.



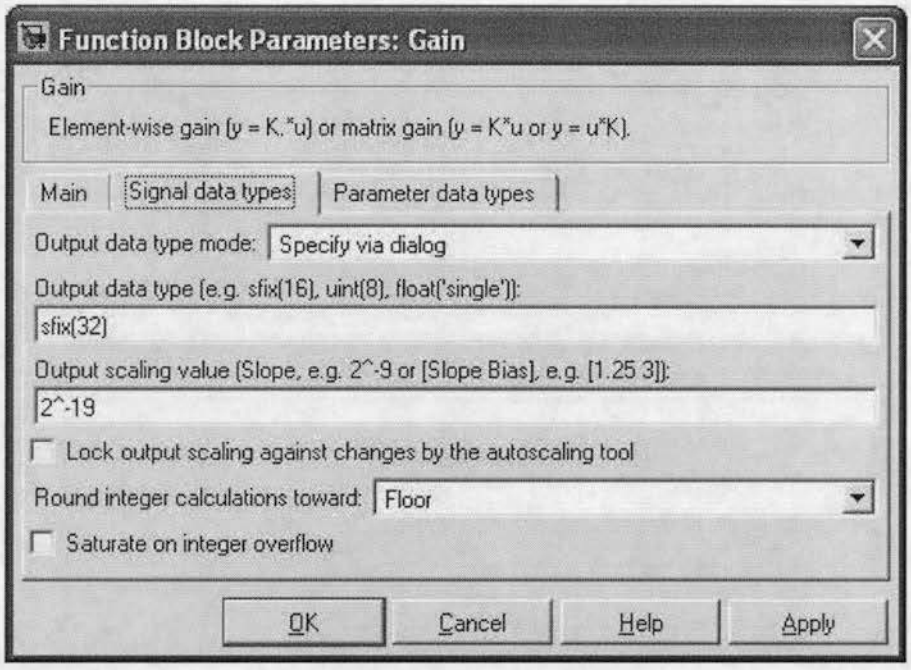
This finishes the configuration of the model. It is recommended to set the sampling color and data type of each port display options on from the simulink model window toolbar \Format\Port and Signal Displays option.

2.2 Developing Control Model in Simulink

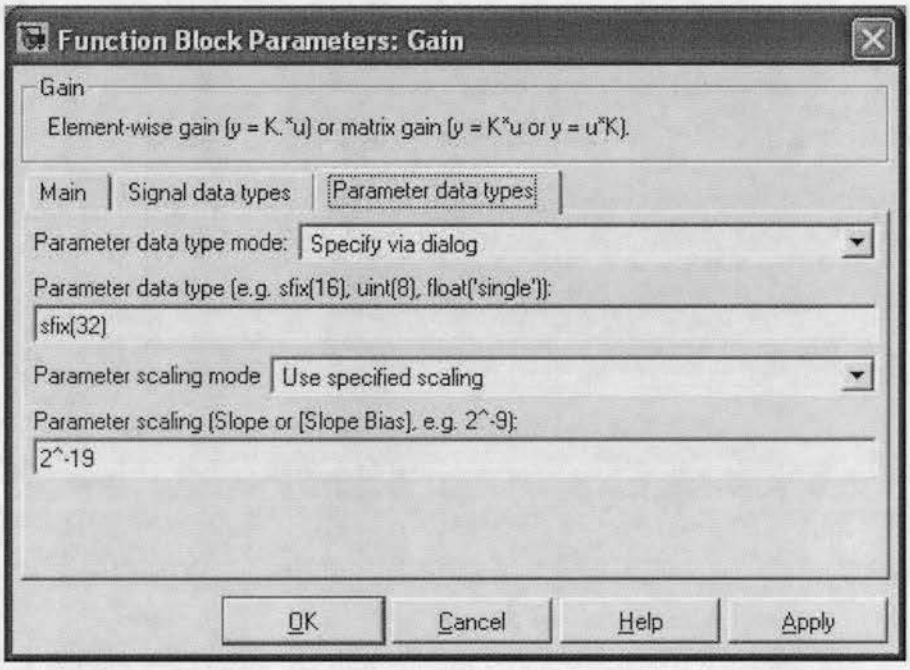
In this part, we describe some key concept to build a control model.

2.2.1 Fixed Point Datatype

Assume you are familiar with the fixed point data concept. In Simulink, to assign certain datatype to a specific block is done by changing signal/parameter settings in the block property tab. For example, we want to use a 32bit fixed point gain of 3.14159, and want 1/100000 resolution on the output within +/-2000. Then we need to setup the signal data type and parameter data type as:



And



32 ^-19 gives a resolution about 2e-6 for the fractional part of a 32bit number. And integer part gives us the range of 0 to +/- 4096, which would satisfy our requirements.

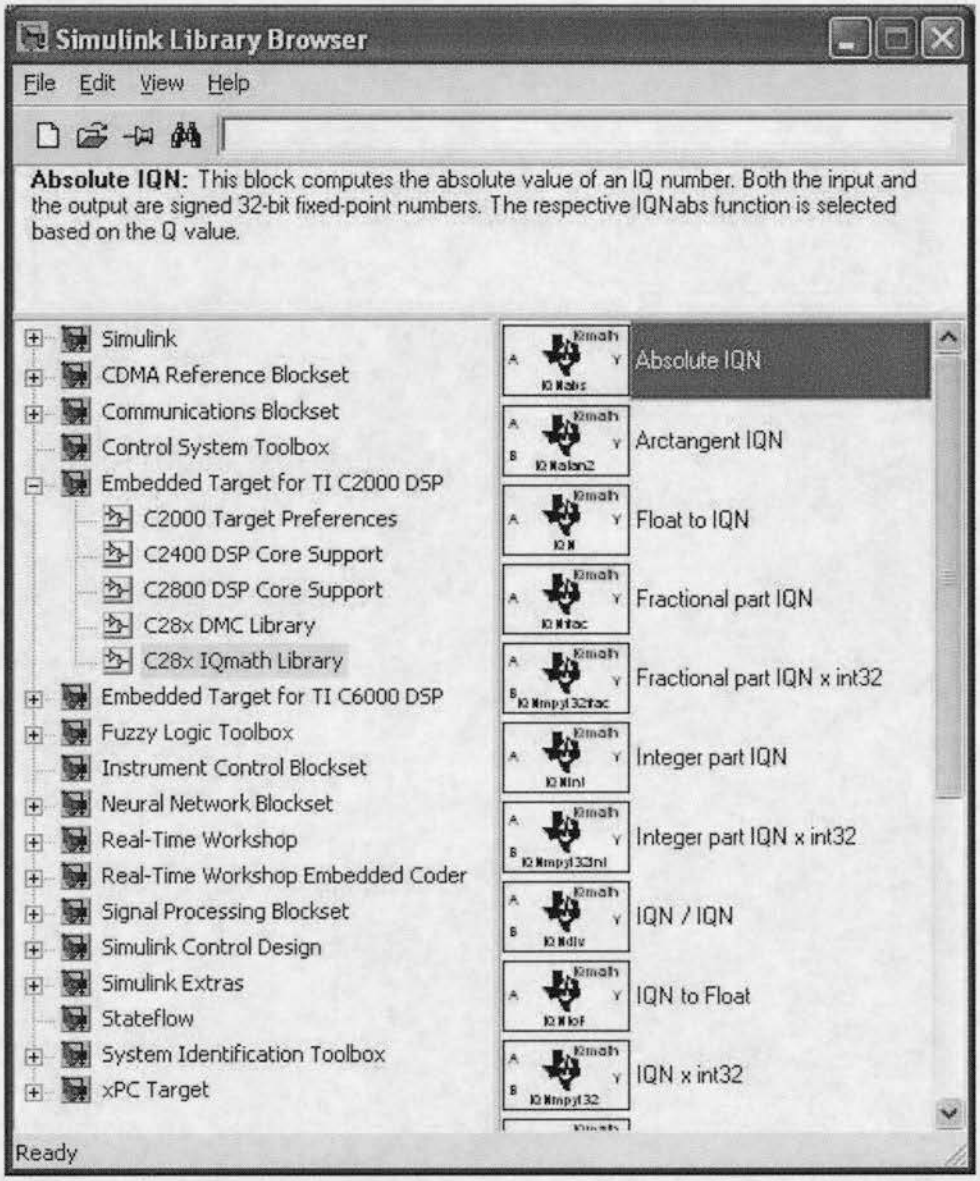
Important: it is crucial to have all signals that may flow in the model/control be falling into the data range you have defined. It is especially true when dealing with **discrete integrators** because the stepsize in our model are usually very small. Rule of thumb: use 32 ^-16 for all arithmetic operations, use 32 ^-26 for critical integrator internal signals. Notice that 32 ^-26 have the integer part range from -32 to 32 only, it's important not to have it overflow.

2.2.2 IQ Math Library and DMC Library

Under Simulink Library Browser, you can find C28x IQmath Library and DMC Library under Embedded Target for TI C2000 DSP toolbox. These are functions that would generate much more efficient code than using common Matlab blocks.

When choosing arithmetic operation blocks, you should always use the one from IQmath library instead the ones from Simulink Block sets. For example, to implement a gain, instead of using the gain from Simulin\Math Operations\Gain, you should use a constant with proper data type and an IQN x IQN or other multiplication functions under IQmath Library. In the DMC Library, there are transforms that have already been implemented in an integrated block format.

Some other functions like filters, discrete integrators should be implemented by blocks from Simulink\Descrete library.



2.2.3 Simulation

After a model is built, the next step is to simulate the system to see if the control is functional as expected and we might need to make necessary changes to the parameters or control structure.

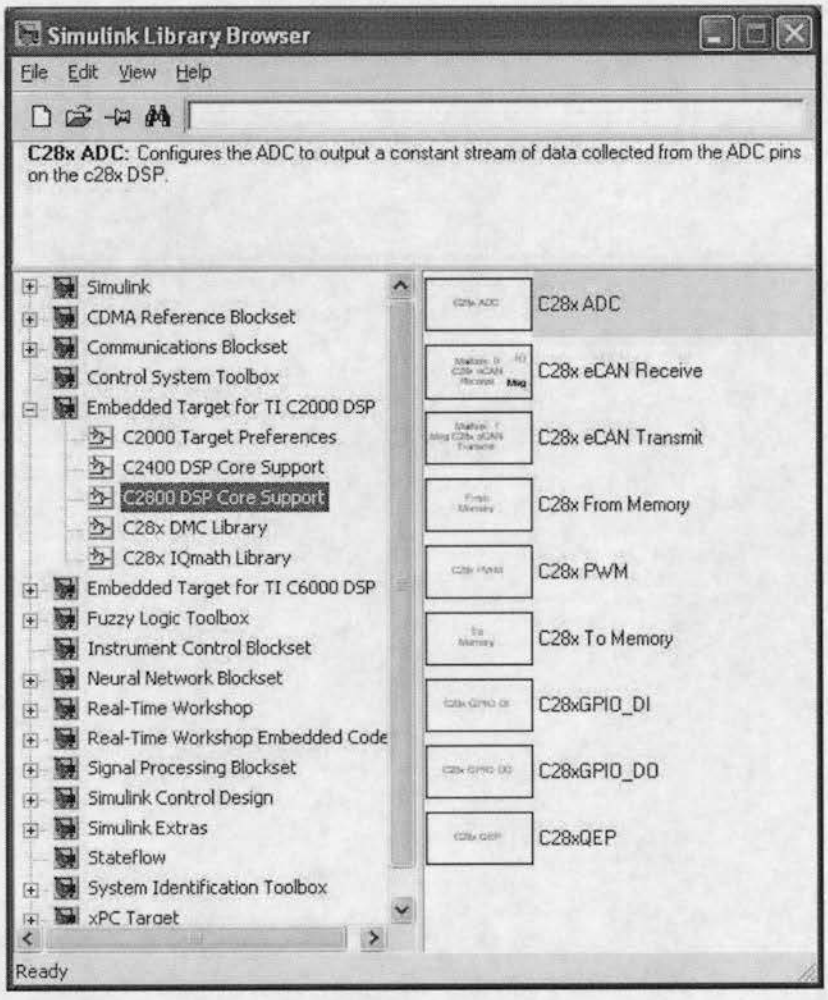
The simulation is no different than an ordinary Simulink model simulation. You can use the scopes and display blocks. You should be able to use any analysis tool provided in Simulink environment. When simulating controller with continuous plant model, choose proper solver in the simulation configuration page.

2.2.4 Integrate I/Os and core functions of the DSP into the control

It is recommended that the user to keep two copies of the model: One for simulation purpose and one for actual code generation purpose. The unit under test (UNT) should be kept identical in the two models.

In the code generation model, we replace the dummy/test inputs from simulation model with interface blocks that are supported by this DSP. We also remove the non-codable blocks which includes all continuous blocks and display blocks for simulation purpose only.

The I/O blocks are under C2800 DSP core support tab in the library browser.



Complete descriptions on these blocks can be found in the help files.

2.3 Generate Code and Run It on DSP

If all the software/toolboxes are installed properly and board configuration is correct, by clicking on the "build" button on top of the Simulink window, an automated process would be invoked and the code should have been built in CCS. Then an active CCS project should appear on the left side project manager window. In theory, the processor needs to be reset before loading the code into the target DSP. In practice, it might not be necessary. To load and run the program, select File/Load Program… from CCS main window, the *modelname*.out executable file usually appears by default. Otherwise, you should be able to locate it manually under *modelname_c2000_rtw/* directory. After the code is loaded in the DSP successfully, press F5 or choose "run" button to run the program on the target. If the target stops immediately after a run command, you might need to do File/Reload Program… and run it again. The code generation may take around 1-2 minutes depending on the complexity of the model and the computer you are using.

Explanations on some terms in this stage:

Generate Code: Matlab Target Language Compiler (TLC) to compile the Simulink model into C code and other resources needed by later process.

Create CCS Project: Matlab TLC creates a project file and include all necessary resources into the *modelname_c2000_rtw* directory.

Build: CCS C compiler is invoked to compile the project source files into .obj files.

Link: CCS Linker links all .obj files, library files from TI library into one executable *modelname*.out file.

Load: CCS loader load the *modelname*.out file to the RAM on DSP according to the linker command file *modelname*.cmd, which was generated by Matlab during "Generate Code" stage.

2.4 Errors, Faults and Exceptions

Some common errors, faults, exceptions and their possible causes are presented in this section.

2.4.1 Board name mismatch

Symptom: After clicking the "Build" button, error message saying board name not matching the label defined in Target Preference Block.

Cause: Board name defined in target preference block is different than that from CC_setup.

Solution: Change the target preference board information to whatever indicated by error message.

2.4.2 Could not find target board

Symptom: After clicking the "Build" button, error message saying cannot find board.

Cause: May caused by power loss on the target when Matlab is still running.

Solution: Make sure the power is connected to the board then reset the board from CCS Debug/Reset Emulator. Then go to Matlab command window and type >> clear CCS_Obj.

2.4.3 Model contains ADC blocks won't work under internal memory mode

Symptom: Loading error in CCS. Or the program is not running as expected if ADC is used and internal memory mode is selected in target preference block.

Cause: Bug in Matlab when generating the *model*.cmd file. A DSECT is declared to a section that would be used in ADC initialization. A DSECT-ed code section will not be loaded to the DSP RAM by the loader.

Solution: 2 ways, either one will work:

1, go to C:*MATLABroot*\toolbox\rtw\targets\tic2000\tic2000\src and open DSP281x_usDelay.asm file with any text editor, comment out the line of `.sect "ramfuncs" with ";"`.

2: go to `C:\MATLABroot\toolbox\rtw\targets\tic2000\tic2000` and open `ti_c2800_cmd.tlc` with any text editor, find the line of:

```
ramfuncs          : > PRAMH0,       PAGE = 0, TYPE = DSECT
```

Cross out the ", TYPE = DSECT" part of this line. So it looks like:

```
ramfuncs          : > PRAMH0,       PAGE = 0
```

2.4.4 Over-run detected

Symptom: After several tries of clicking the "run" button, the program goes to "Halt" position repetitively.

Cause: Over-run is detected, CPU overloaded.

Solution: Increase the stepsize in the model and recompile. Make sure that there are no unnecessary double precision or non-lookup-table type trigonometric functions in the model.

3. An Example

SW00025 folder contains documents (including this one) that are dedicated to the modular inverter control software architecture, which is based on Matlab/Simulink Embedded Coder for TI C2000

toolbox. The eZdspLib.zip file contains the matlab code and model needed for Modular Inverter dsp software generation and execution.

Extract the file to a folder that you are working under, and make sure this folder is included in the matlab path setting. Keep the HyperTerminal file some where convenient for easy access. Navigate in the matlab path selection tab and make the current work directory is your matlab pth/eZdspLib/VperHzTest. Two models are provided. One is using Serial communication the other is using RTDX communication. ezdsp2812_vphz32 is to be used with the HyperTerminal file you extracted earlier. ezdsp2812_vphz32_wRTDX is used with .m file under the same directory.

4. Create Flash Based Project

SW00025 also contains a Flash_Based.zip file. It is the project that derived from V/Hz project in the example but suitable to run as stand alone program.

To make a project generated from Matlab flashable. Follow the steps listed below:

i. Replace the .cmd file generated from Matlab/Simulink with the one in Fash_Based.zip .cmd file. Change the file name to your project name.

ii. Add two files to the project by right click on *project_name* and choose *Add files…* in CCS: coecsl.c and DSP281x_CodeStartBranch.asm

iii. Add one line in YourProjectName_main.c in main() so that it looks like:

```
void main(void)
{
 init_COECSL(); // memcpy from Flash to RAM

 init_board();
…
}
```

iv. Right click on project name, choose *Build Option…* click on *Linker* tab; change one of the linker options from –cr to –c.

v. Change the jumper 7 position from 2-3 to 1-2 on the DSP board.

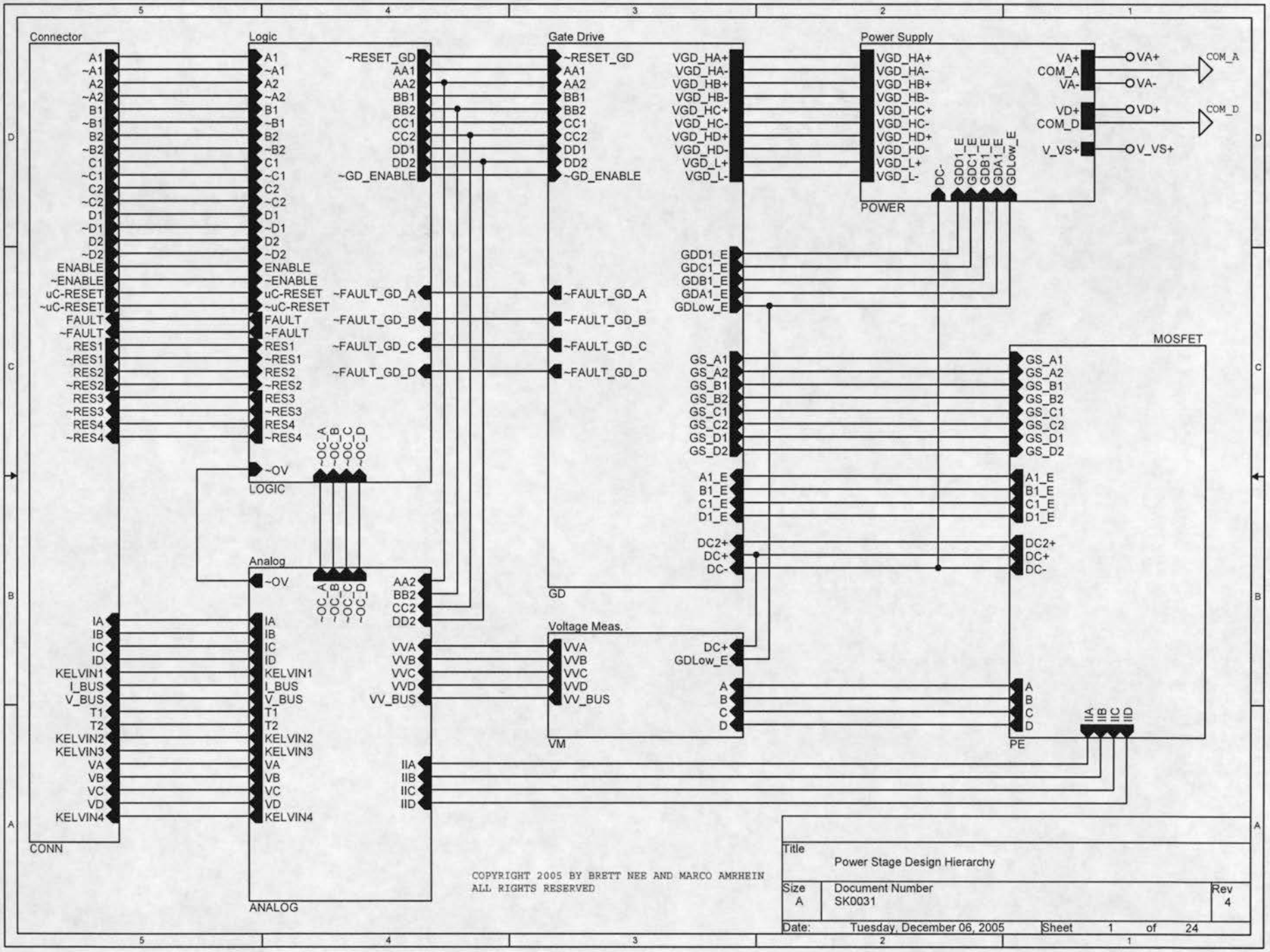
vi. Re-compile and build the project under CCS. DO NOT RECOMPILE UNDER SIMULINK, OTHERWISE YOU LOSE ALL YOUR WORK.

vii. Instead of "loading" your program to the RAM, now you need to use flash programmer under CCS *tools* to burn the flash.

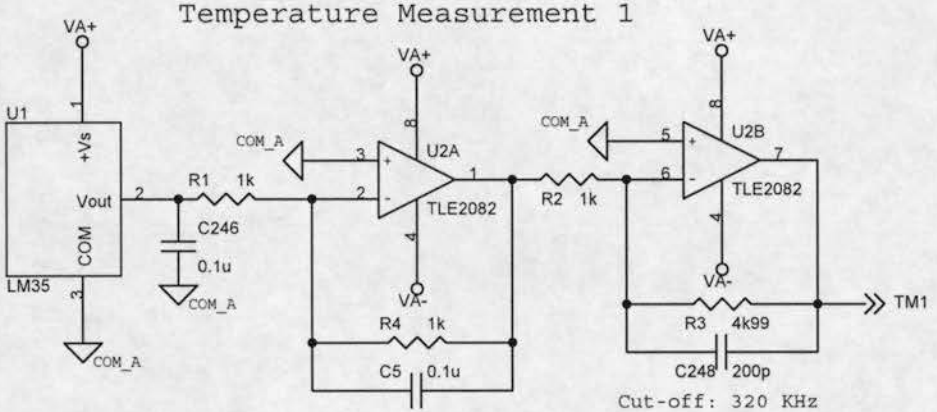
viii. After the process is done, reset the DSP and it should go.

NOTES:

1. All work in this chapter is not related to Matlab/Simulink any more. Work solely under CCS.
2. CCS software package that comes with the boards doesn't have a functional flash programmer. Need to update the flash API patch, which can be obtained from c2000flashprogsw_v112.zip under SW00025 directory. Or please check the latest version of CCS.
3. To save your work, change the directory name so that Matlab/Simulink won't erase it next time you recompile your model. Move it to a safer place.
4. Don't forget to change the jumper back to its original position when done.

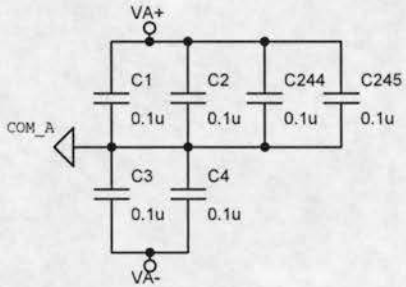

Connector
A1
~A1
A2
~A2
B1
~B1
B2
~B2
C1
~C1
C2
~C2
D1
~D1
D2
~D2
ENABLE
~ENABLE
uC-RESET
~uC-RESET
FAULT
~FAULT
RES1
~RES1
RES2
~RES2
RES3
~RES3
RES4
~RES4
CONN
Logic
~RESET_GD
~GD_ENABLE
~FAULT_GD_A
~FAULT_GD_B
~FAULT_GD_C
~FAULT_GD_D
~OC_A
~OC_B
~OC_C
~OC_D
~OV
LOGIC
Gate Drive
GD
Power Supply
VGD_HA+
VGD_HA-
VGD_HB+
VGD_HB-
VGD_HC+
VGD_HC-
VGD_HD+
VGD_HD-
VGD_L+
VGD_L-
DC-
GDD1_E
GDC1_E
GDB1_E
GDA1_E
GDLow_E
POWER
VA+
COM_A
VA-
VD+
COM_D
V_VS+
COM_A
COM_D
MOSFET
GS_A1
GS_A2
GS_B1
GS_B2
GS_C1
GS_C2
GS_D1
GS_D2
A1_E
B1_E
C1_E
D1_E
DC2+
DC+
DC-
A
B
C
D
PE
IIA
IIB
IIC
IID
Analog
IA
IB
IC
ID
KELVIN1
I_BUS
V_BUS
T1
T2
KELVIN2
KELVIN3
VA
VB
VC
VD
KELVIN4
VVA
VVB
VVC
VVD
VV_BUS
ANALOG
Voltage Meas.
VM
COPYRIGHT 2005 BY BRETT NEE AND MARCO AMRHEIN
ALL RIGHTS RESERVED
Title
Power Stage Design Hierarchy
Size
A
Document Number
SK0031
Rev
4
Date:
Tuesday, December 06, 2005
Sheet
1
of
24

Temperature Measurement 1



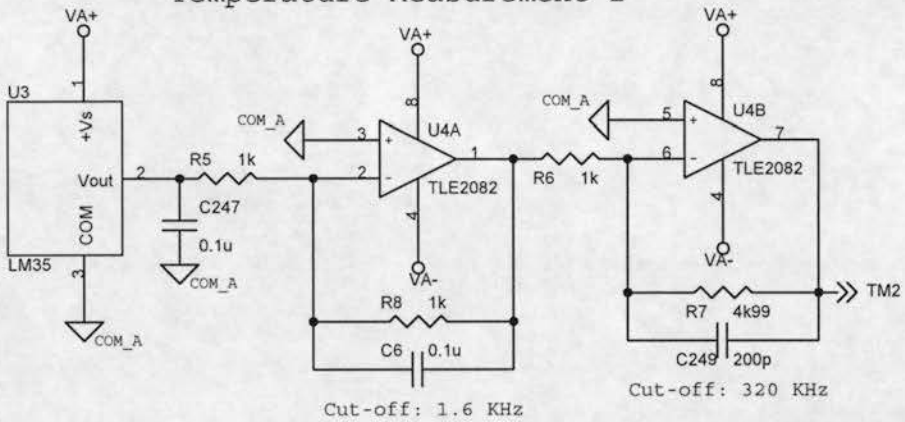
Cut-off: 1.6 KHz

Cut-off: 320 KHz



Cap. for IC-supply

Temperature Measurement 2



Cut-off: 1.6 KHz

Cut-off: 320 KHz

20°C correspond to 1 V output signal.

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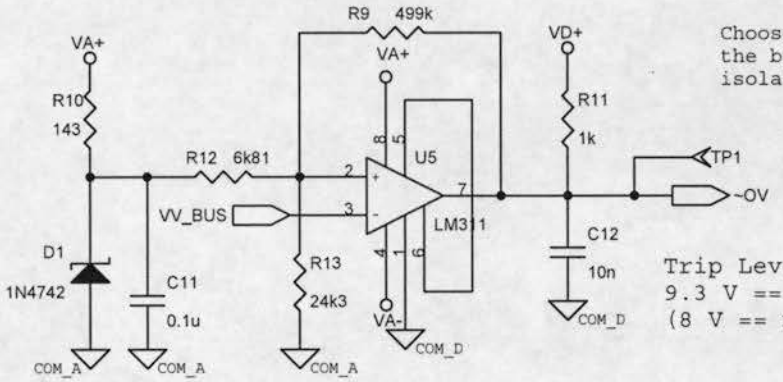
Title	Analog Design for Power Stage, Temperature Measurement	
Size A	Document Number SK0031	Rev 4
Date: Friday, December 09, 2005	Sheet 2 of 24	

Bus Voltage Signal Filtering and Overvoltage Detection

Bus-Overvoltage detection levels for various values of R12:
(Vph is U5 Pin 3 when U5 Pin 7 is high, and Vpl when U5 Pin 7 is low)

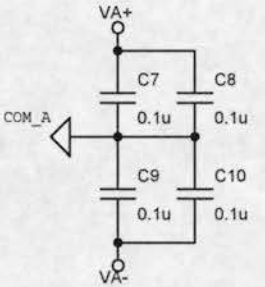
R12 = 10k: Vph=8.45V, Vpl=8.32V (106% of nominal dc bus voltage)
R12 = 7k87: Vph=9.02V, Vpl=8.96V (113% of nominal dc bus voltage)
R12 = 6k81: Vph=9.33V, Vpl=9.27V (117% of nominal dc bus voltage)
R12 = 6k04: Vph=9.57V, Vpl=9.52V (120% of nominal dc bus voltage)

Choose adequate resistance in terms of noise level seen on the bus voltage signal (ripple introduced through isolated-voltage amplifier and front end rectifier).



Trip Level:
9.3 V == 117% of nominal dc bus voltage
(8 V == nominal dc bus voltage)

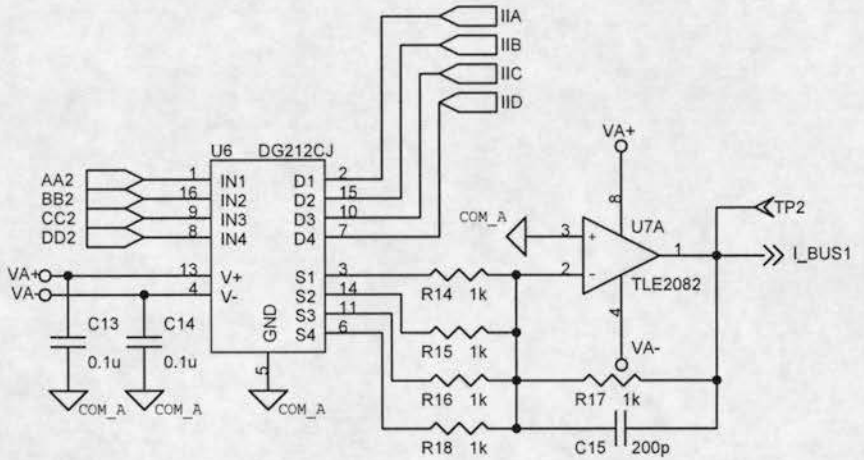
Hysterisis Band of 0.05V



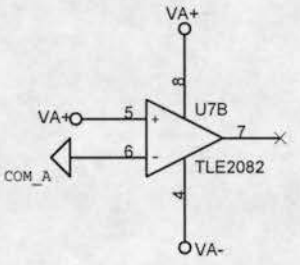
Cap. for IC-supply

Bus Current Calculation

(adds phase currents in bottom switch of each phase leg)



Cut-off: 796kHz



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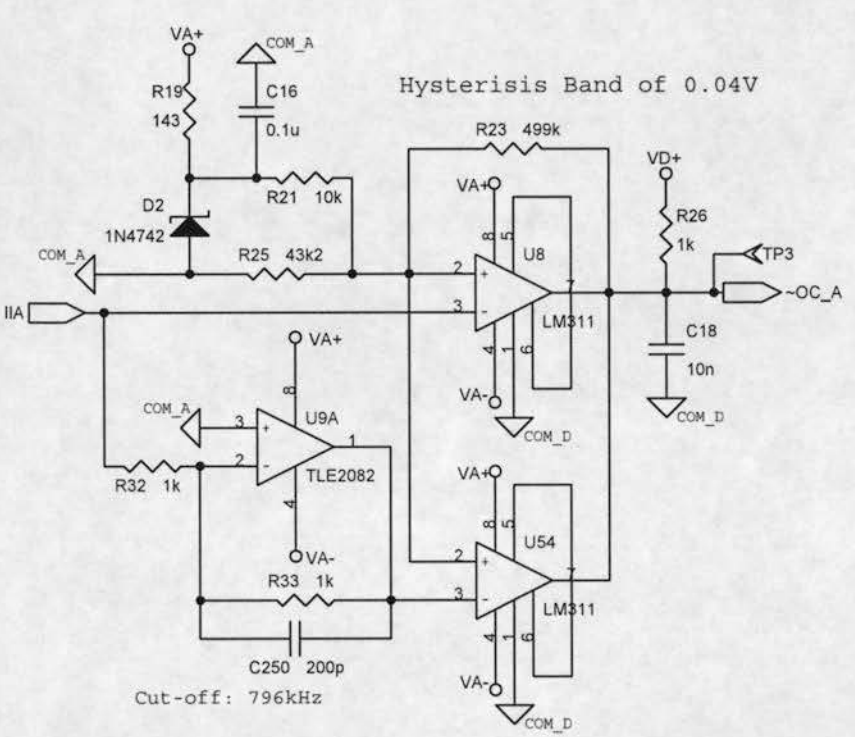
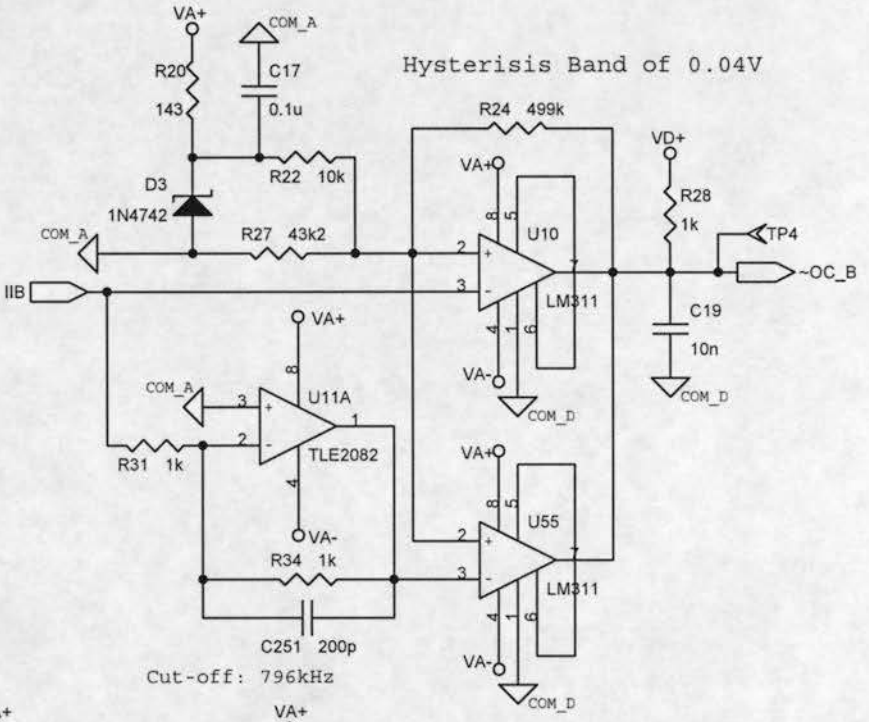
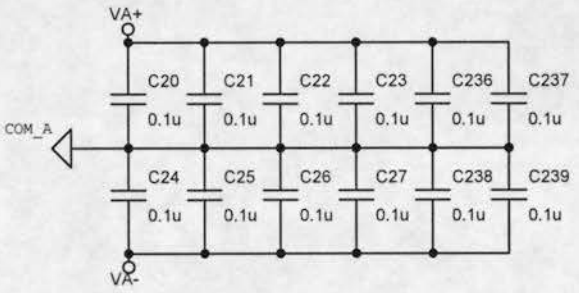
Title: Analog Design for Power Stage, bus overvoltage detection, bus current calculation		
Size: A	Document Number: SK0031	Rev: 4
Date: Thursday, March 23, 2006	Sheet 3 of 24	

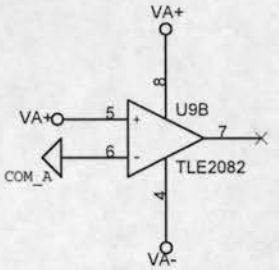
Overcurrent Detection
(Phase A & B)

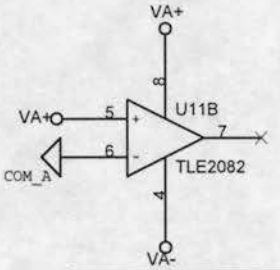
Trip Level:
9.71 V == 216% rated RMS current
(4.5V == max. rated RMS current)











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Title	Analog Design for Power Stage, Current Conditioning (1)	
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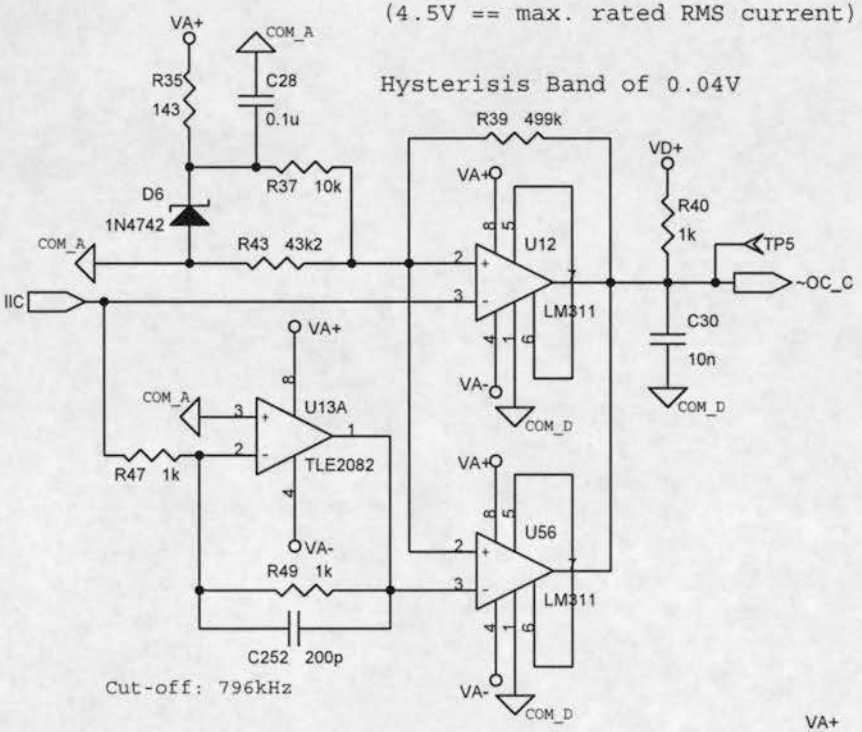
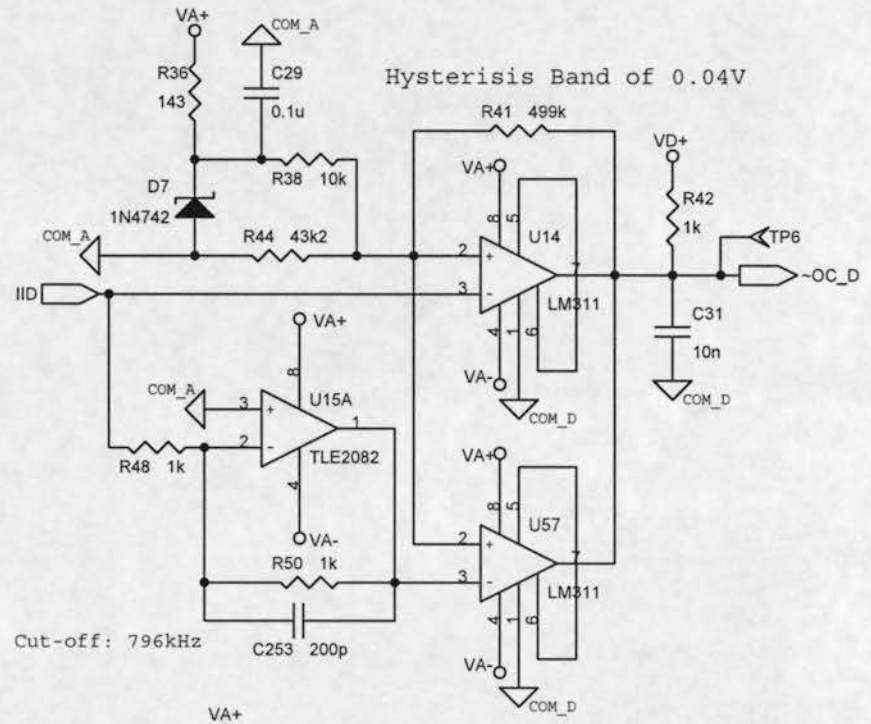
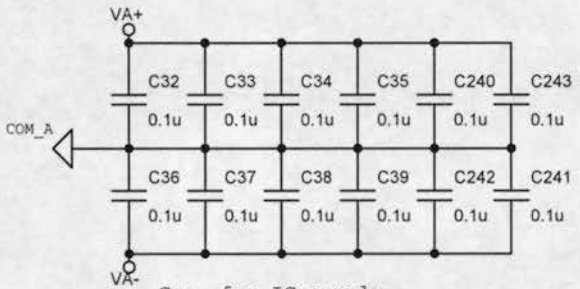
Date: Monday, April 24, 2006	Sheet 4 of 24	

Overcurrent Detection
(Phase C & D)

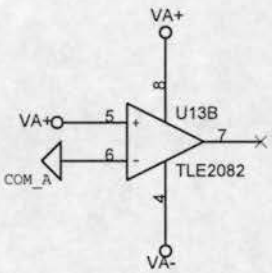
Trip Level:
9.71 V == 216% rated RMS current
(4.5V == max. rated RMS current)

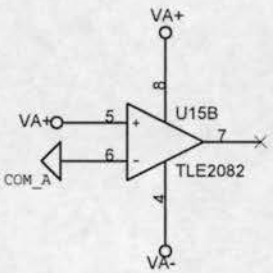






Cap. for IC-supply





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Title	Analog Design for Power Stage, Current Conditioning (2)	
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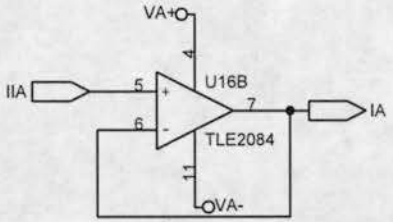
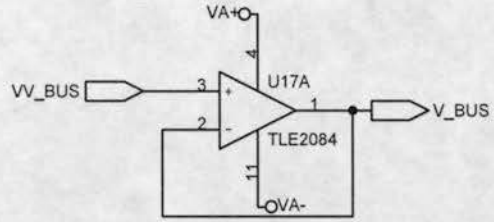
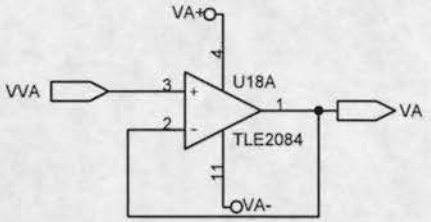
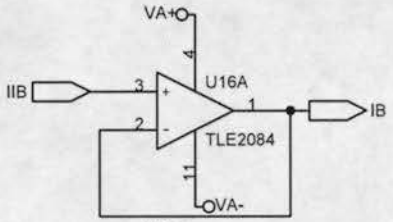
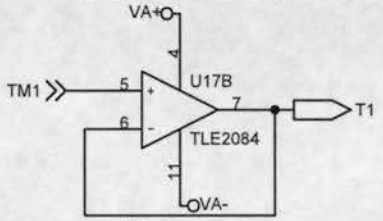
Generate Analog Signals for Control Box

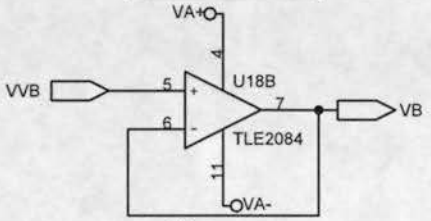


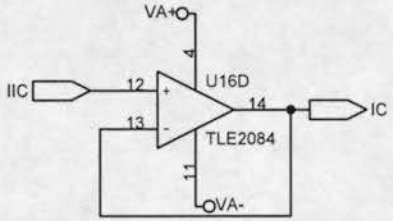


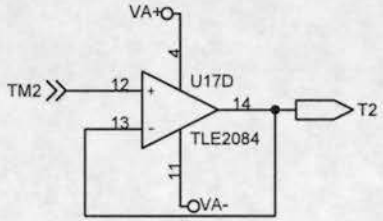


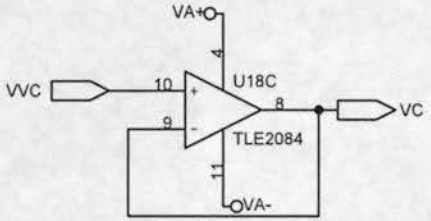


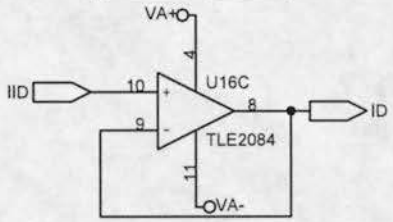


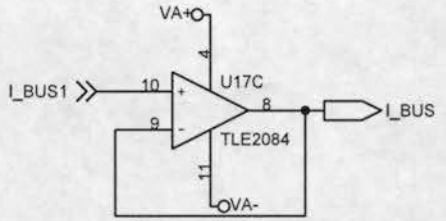


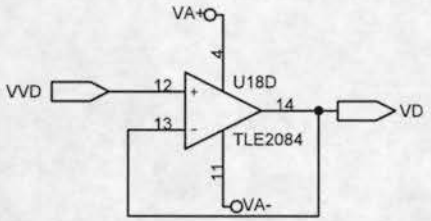


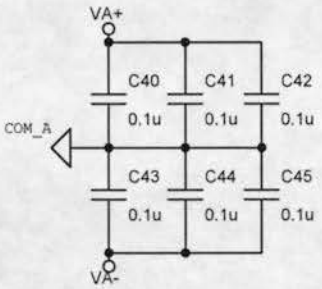












Cap. for IC-supply

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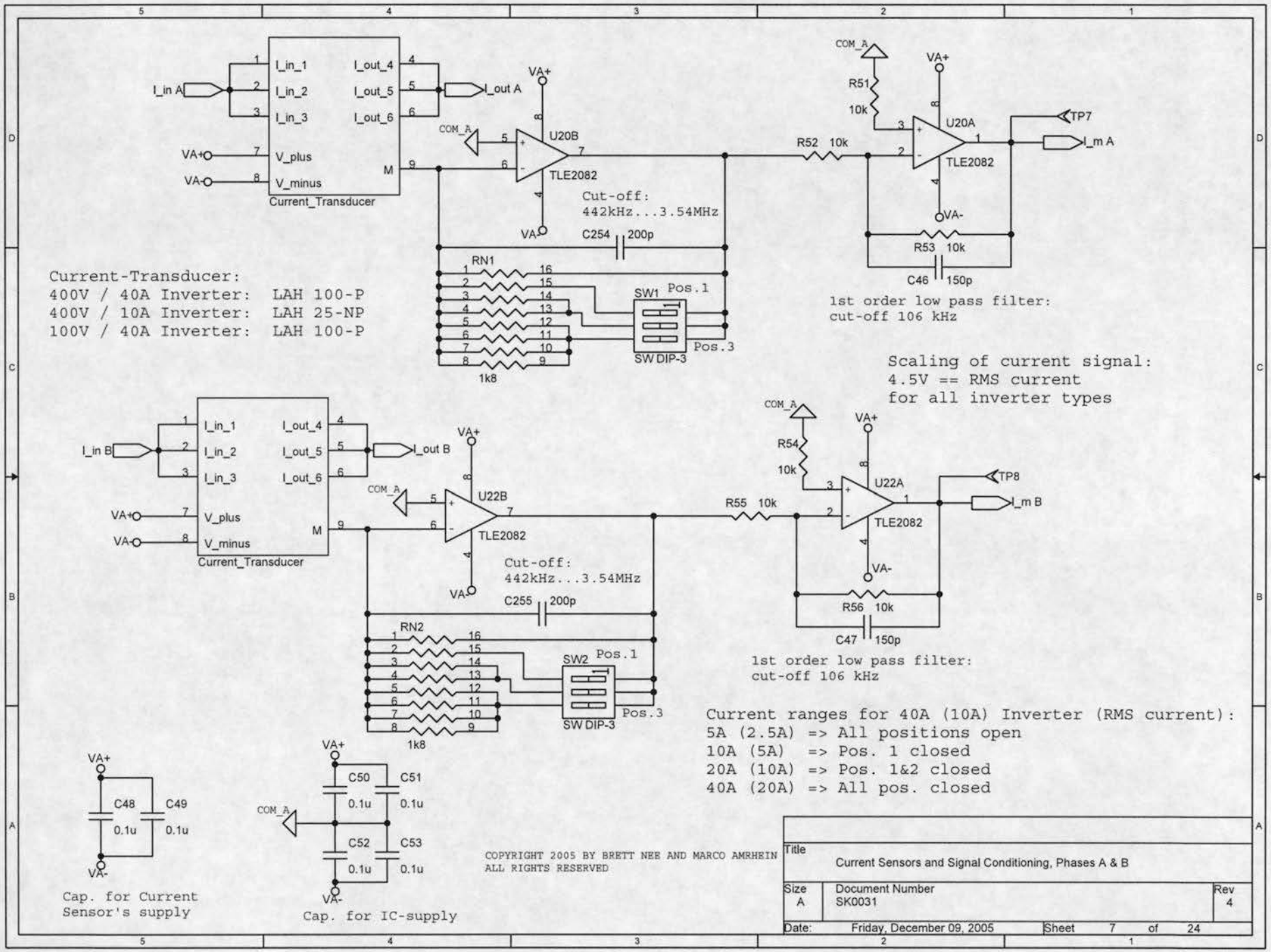

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Title	Current Sensors and Signal Conditioning, Phases A & B	
Size A	Document Number SK0031	Rev 4
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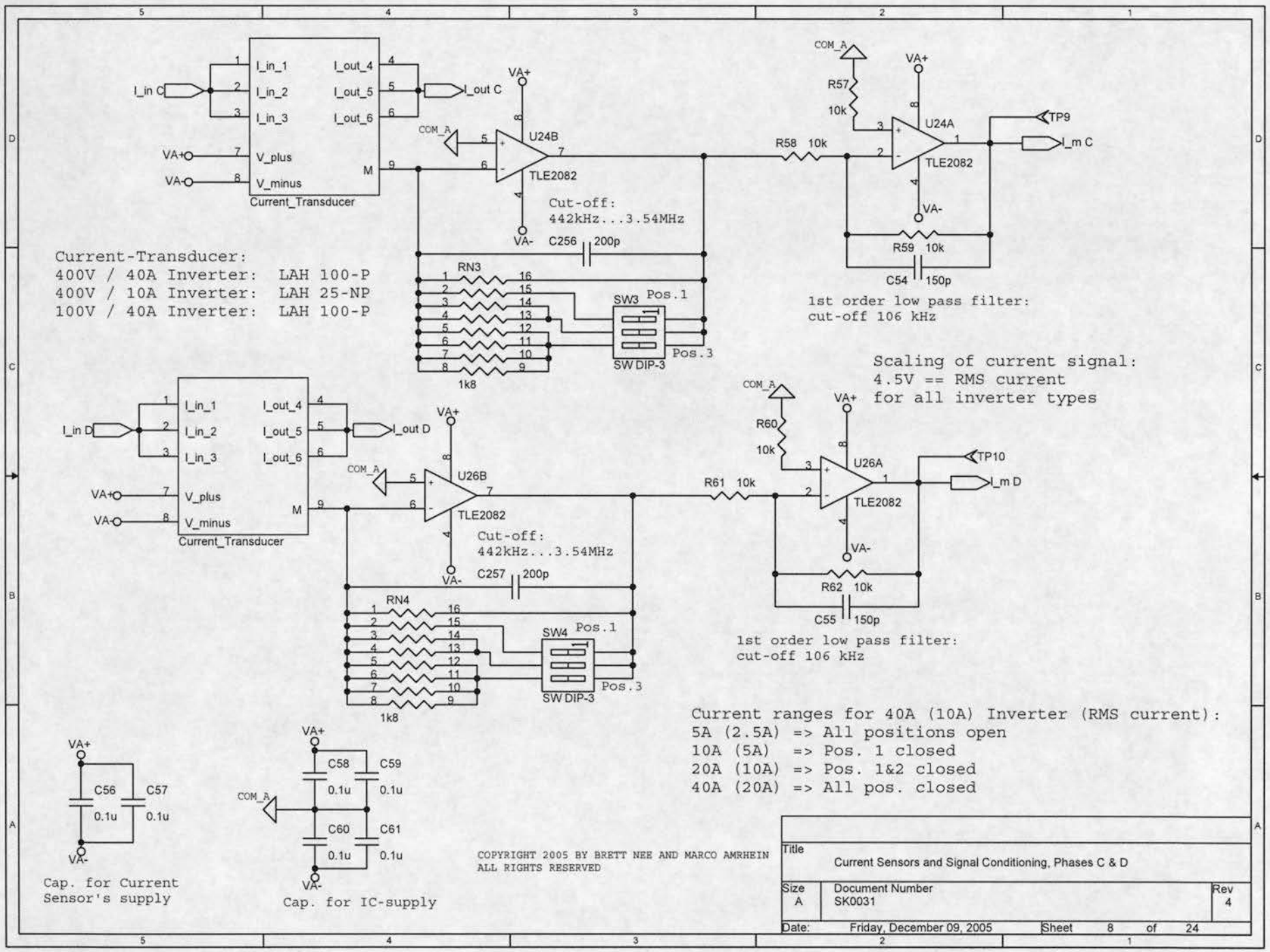

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Title	Current Sensors and Signal Conditioning, Phases C & D	
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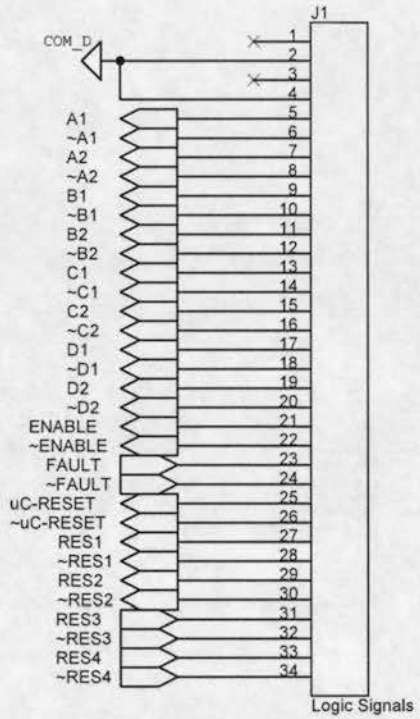

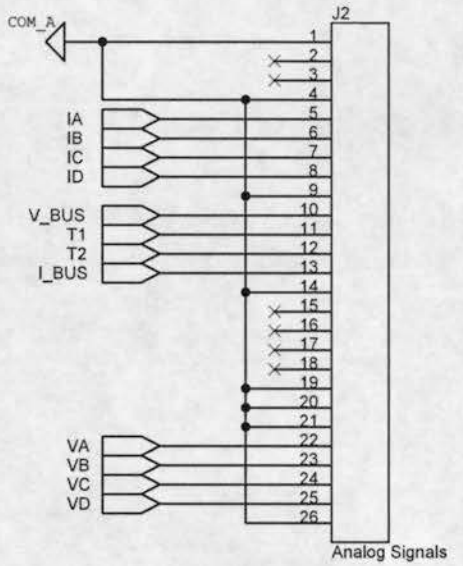

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Title	Connector to Control Board for Power Stage	
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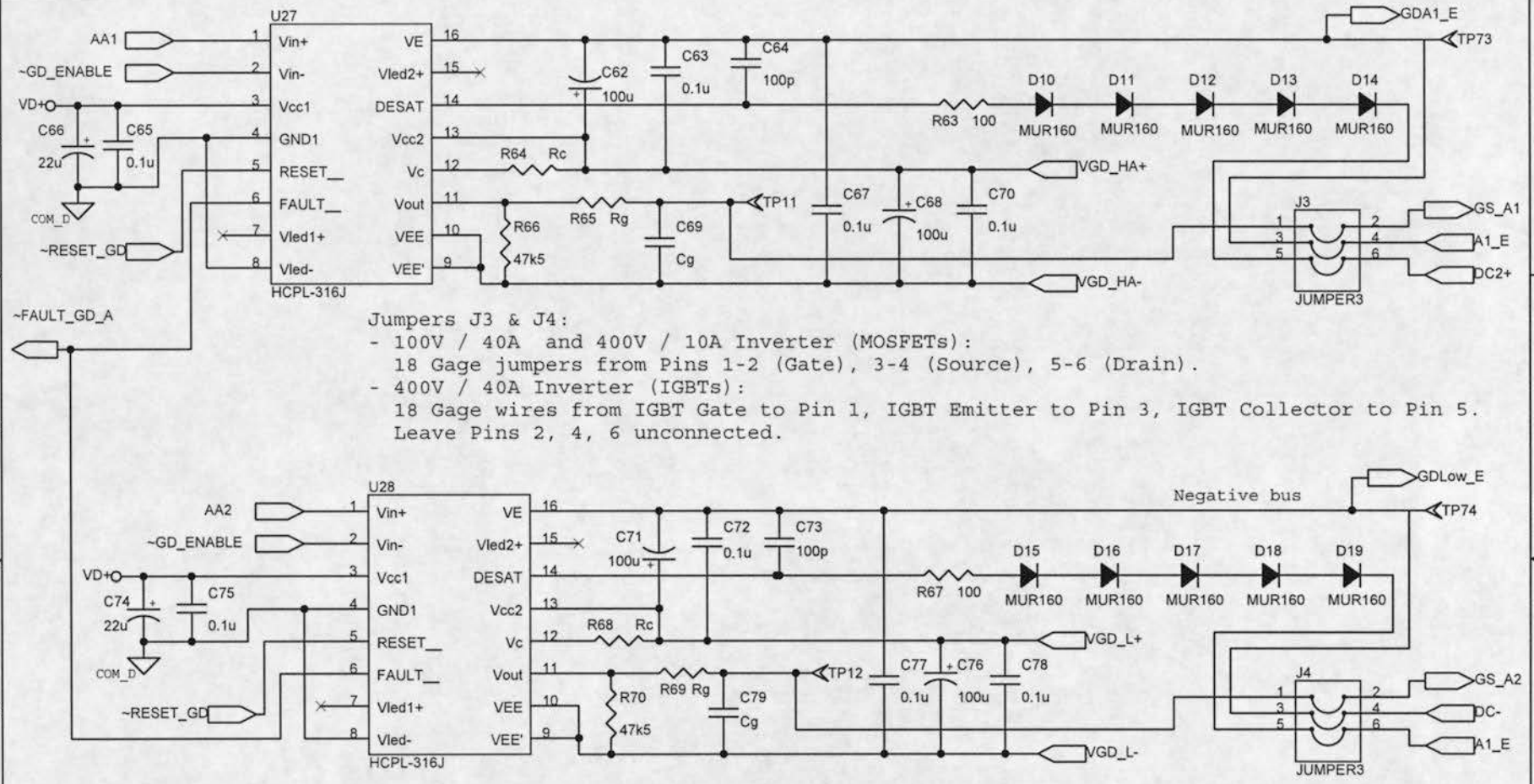

Additional notes:
- All resistors used should be 0.5 watt 1% TOL.
- All capacitors should be ceramic and at least a 25V rating.
- For 100V / 40A Inverter use 1N4148 Diodes.
- For 400V / 40A and 100V / 10A Inverter use ONE MUR160 Diode and short other terminals together.
- Cg provides the flexibility of adding more gate capacitance, but is in general not stuffed.

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Values for Rg and Rc:
- 100V / 40 A Inverter: Rg=15 , Rc=0
- 400V / 10 A Inverter: Rg= 47.5 (can be 1/4W), Rc=0
- 400V / 40 A Inverter: Rg= 47.5 (can be 1/4W), Rc=0

Title: Gate Drive Ph A		
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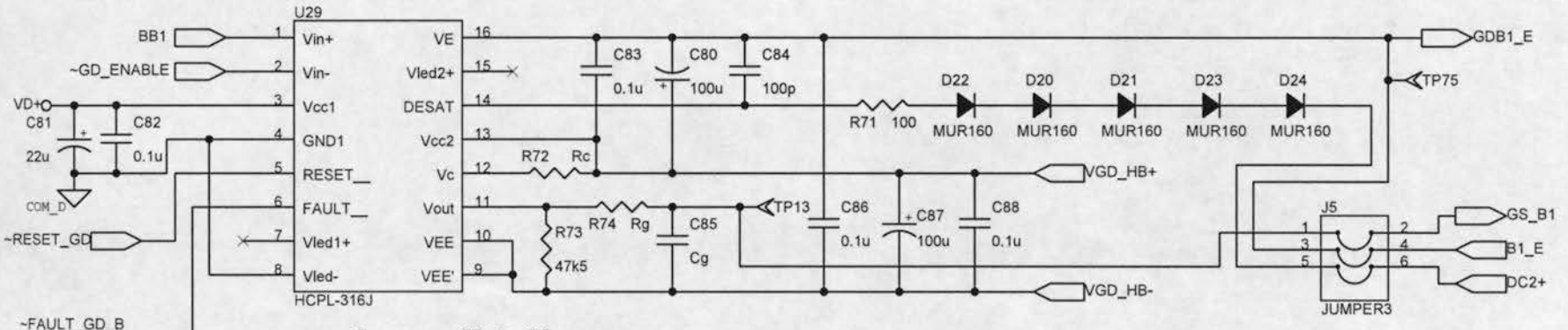
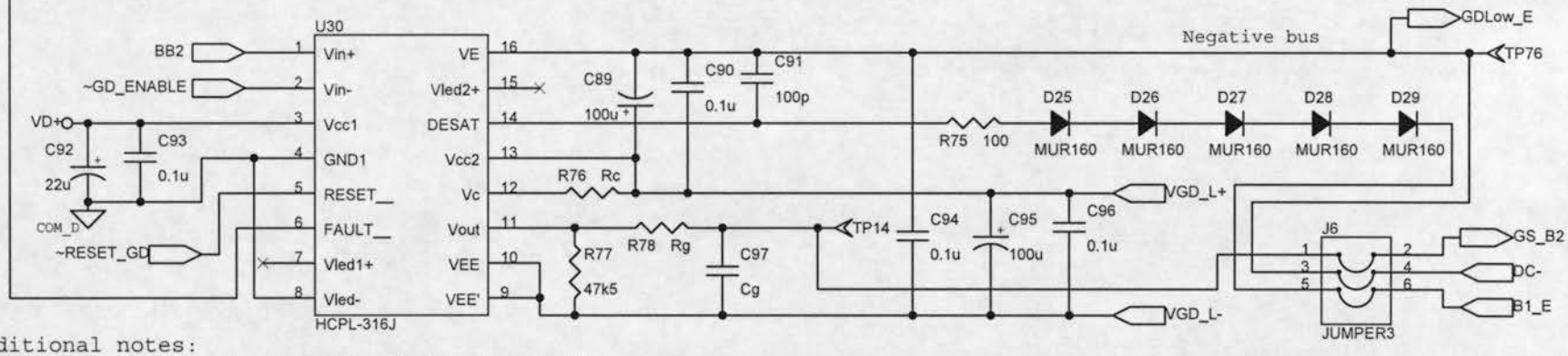


Jumpers J5 & J6:
- 100V / 40A and 400V / 10A Inverter (MOSFETs):
  18 Gage jumpers from Pins 1-2 (Gate), 3-4 (Source), 5-6 (Drain).
- 400V / 40A Inverter (IGBTs):
  18 Gage wires from IGBT Gate to Pin 1, IGBT Emitter to Pin 3, IGBT Collector to Pin 5.
  Leave Pins 2, 4, 6 unconnected.



Additional notes:
- All resistors used should be 0.5 watt 1% TOL.
- All capacitors should be ceramic and at least a 25V rating.
- For 100V / 40A Inverter use 1N4148 Diodes.
- For 400V / 40A and 100V / 10A Inverter use ONE MUR160 Diode and short other terminals together.
- Cg provides the flexibility of adding more gate capacitance, but is in general not stuffed.

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Values for Rg and Rc:
- 100V / 40 A Inverter: Rg=15 , Rc=0
- 400V / 10 A Inverter: Rg= 47.5 (can be 1/4W), Rc=0
- 400V / 40 A Inverter: Rg= 47.5 (can be 1/4W), Rc=0

Title: Gate Drive Ph B		
Size: A	Document Number: SK0031	Rev: 4
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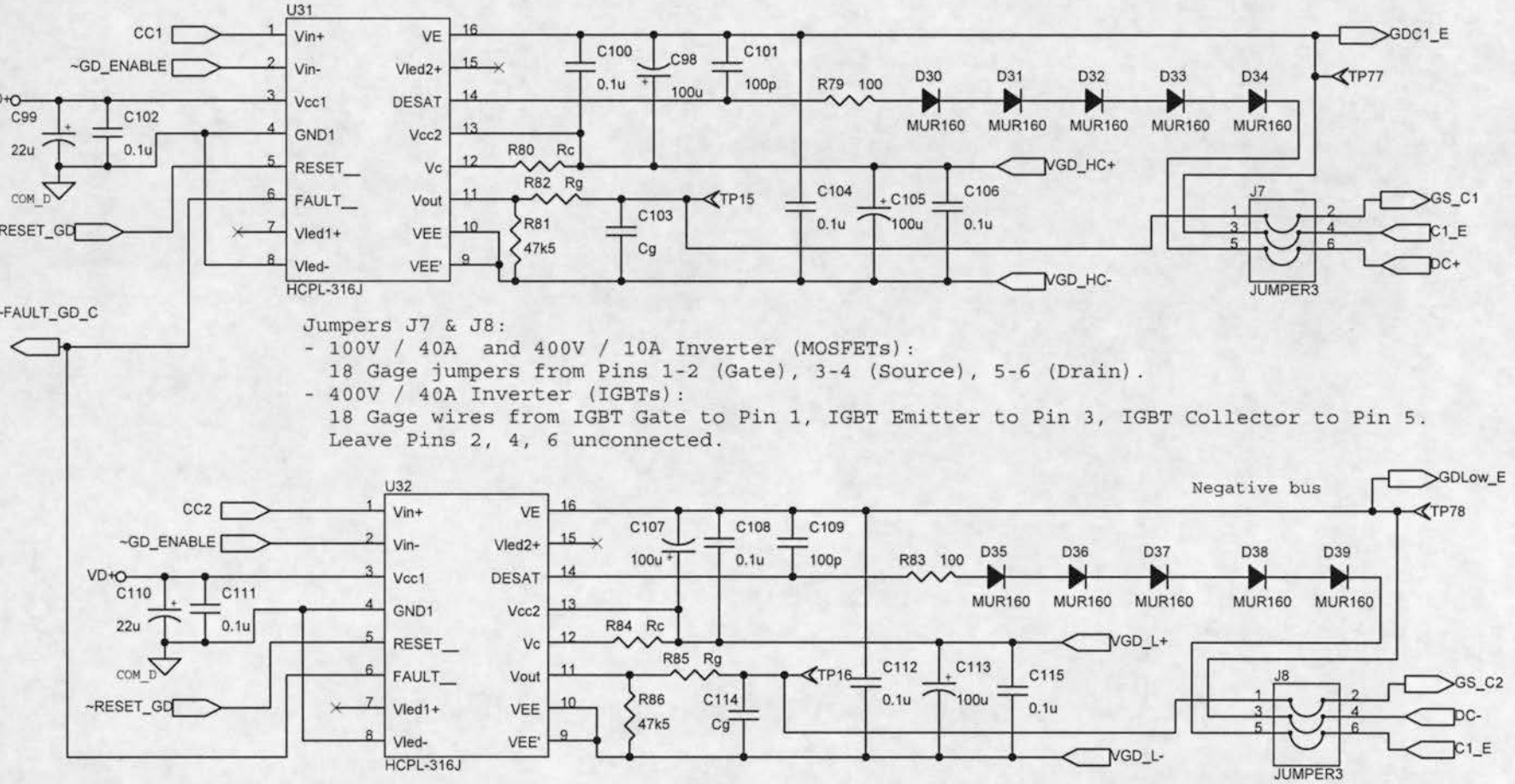

Jumpers J7 & J8:
- 100V / 40A and 400V / 10A Inverter (MOSFETs):
  18 Gage jumpers from Pins 1-2 (Gate), 3-4 (Source), 5-6 (Drain).
- 400V / 40A Inverter (IGBTs):
  18 Gage wires from IGBT Gate to Pin 1, IGBT Emitter to Pin 3, IGBT Collector to Pin 5.
  Leave Pins 2, 4, 6 unconnected.

Additional notes:
- All resistors used should be 0.5 watt 1% TOL.
- All capacitors should be ceramic and at least a 25V rating.
- For 100V / 40A Inverter use 1N4148 Diodes.
- For 400V / 40A and 100V / 10A Inverter use ONE MUR160 Diode and short other terminals together.
- Cg provides the flexibility of adding more gate capacitance, but is in general not stuffed.

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Values for Rg and Rc:
- 100V / 40 A Inverter: Rg=15 , Rc=0
- 400V / 10 A Inverter: Rg= 47.5 (can be 1/4W), Rc=0
- 400V / 40 A Inverter: Rg= 47.5 (can be 1/4W), Rc=0

Title: Gate Drive Ph C		
Size: A	Document Number: SK0031	Rev: 4
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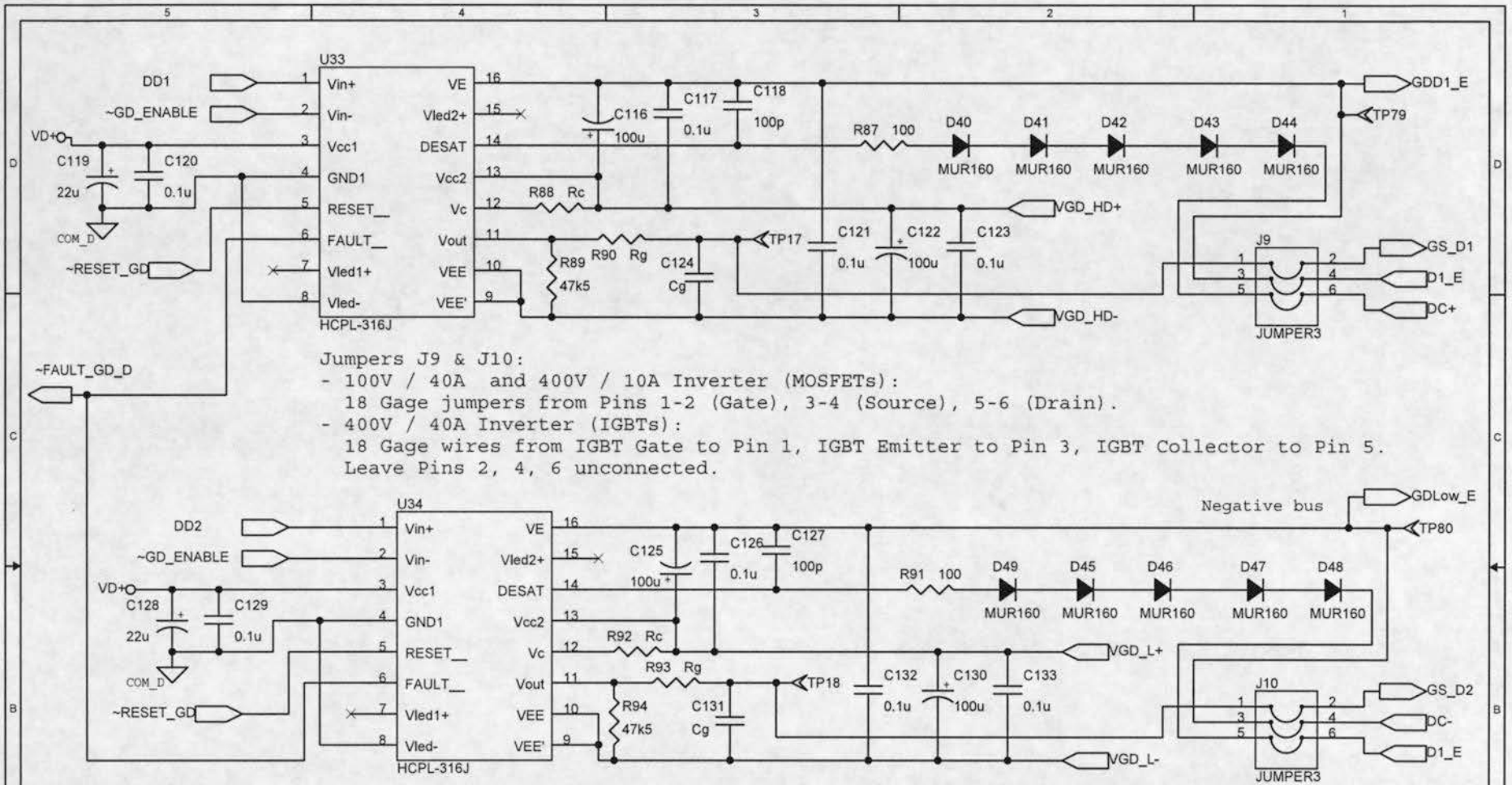

Additional notes:
- All resistors used should be 0.5 watt 1% TOL.
- All capacitors should be ceramic and at least a 25V rating.
- For 100V / 40A Inverter use 1N4148 Diodes.
- For 400V / 40A and 100V / 10A Inverter use ONE MUR160 Diode and short other terminals together.
- Cg provides the flexibility of adding more gate capacitance, but is in general not stuffed.

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Values for Rg and Rc:
- 100V / 40 A Inverter: Rg=15 , Rc=0
- 400V / 10 A Inverter: Rg= 47.5 (can be 1/4W), Rc=0
- 400V / 40 A Inverter: Rg= 47.5 (can be 1/4W), Rc=0

Title: Gate Drive Ph D		
Size: A	Document Number: SK0031	Rev: 4
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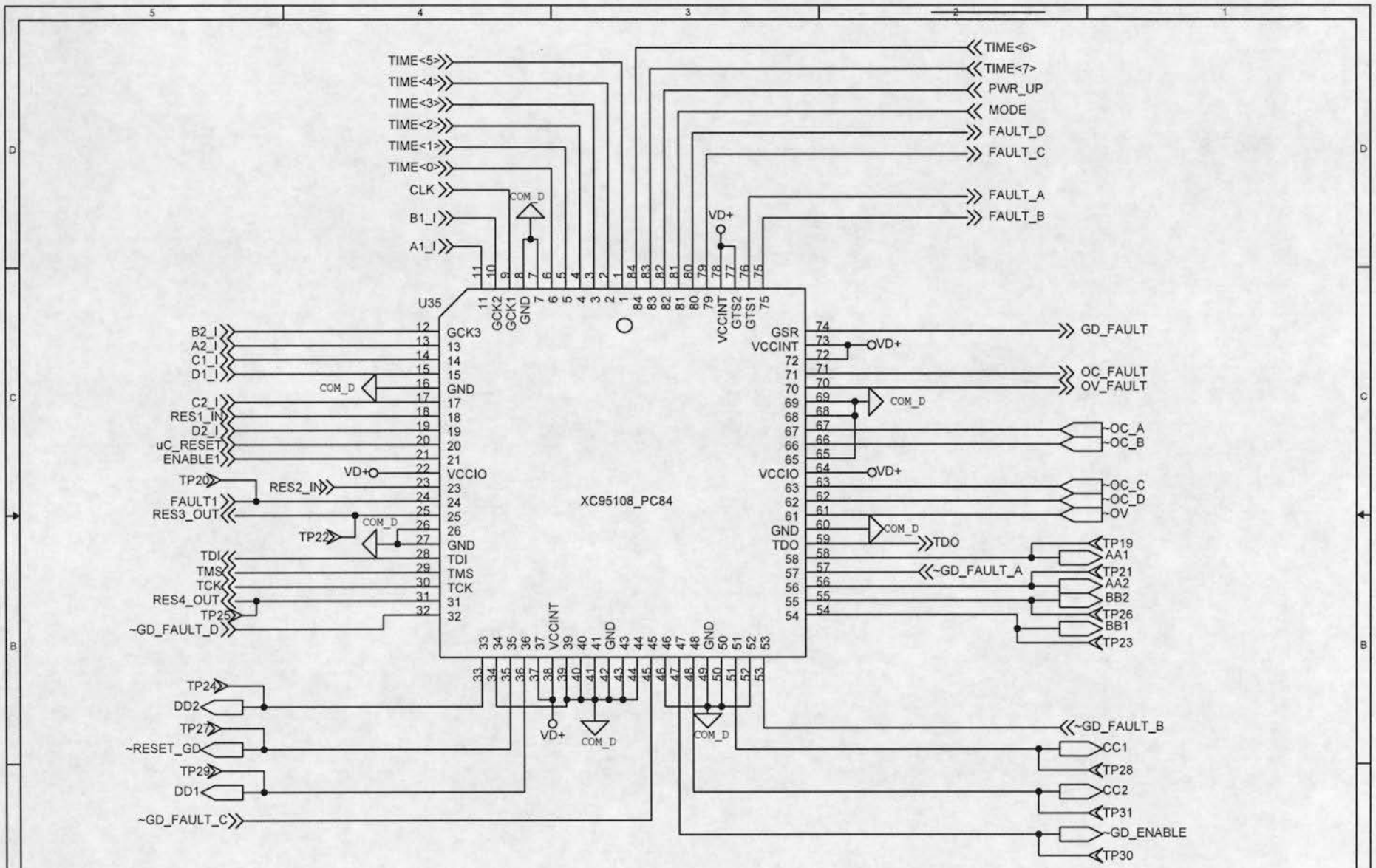

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Title	Logic Design for Power Stage, XC95108 Interface	
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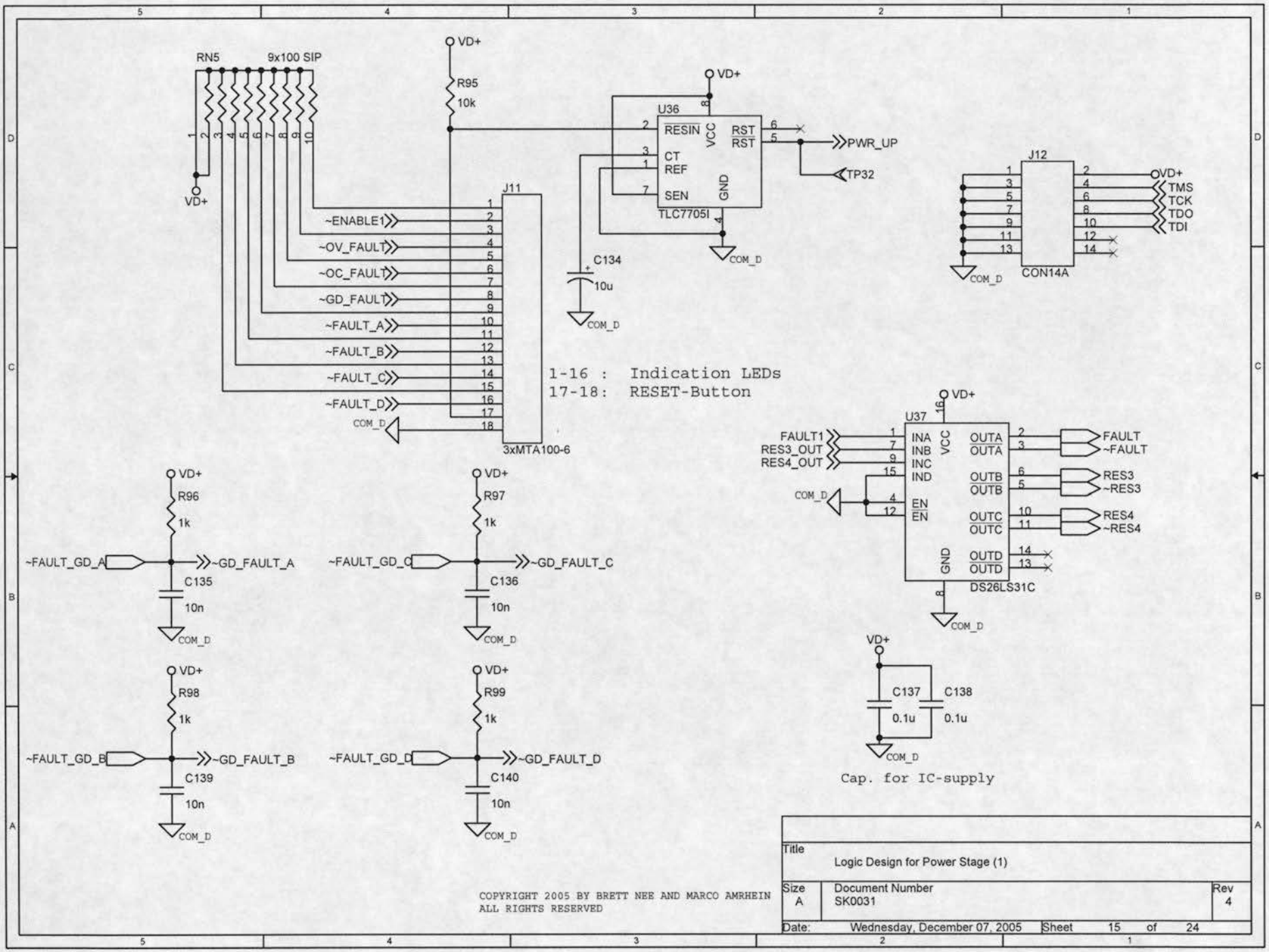

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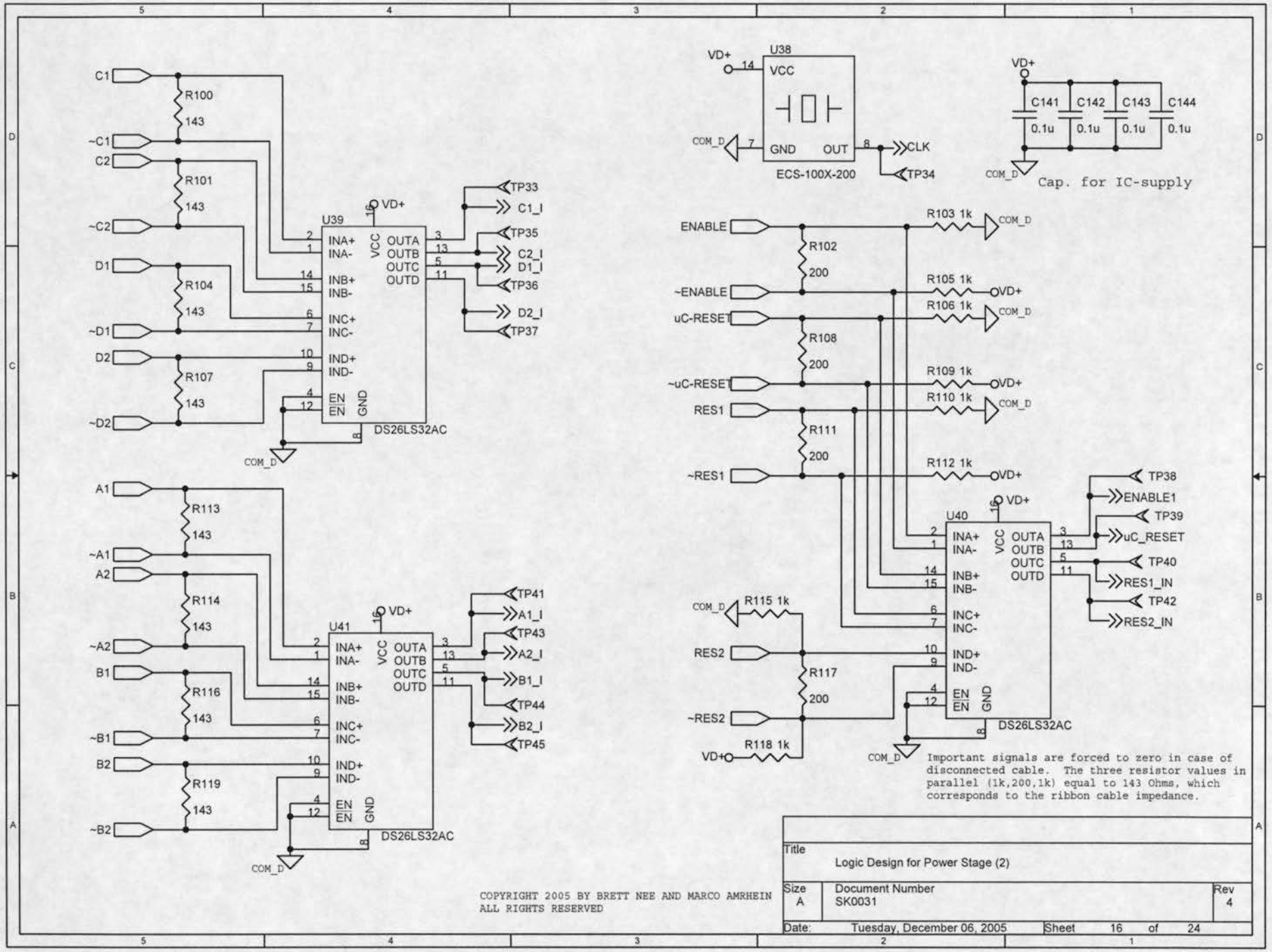
Title	Logic Design for Power Stage (1)	
Size A	Document Number SK0031	Rev 4
Date: Wednesday, December 07, 2005	Sheet 15 of 24	



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Title	Logic Design for Power Stage (2)	
Size A	Document Number SK0031	Rev 4
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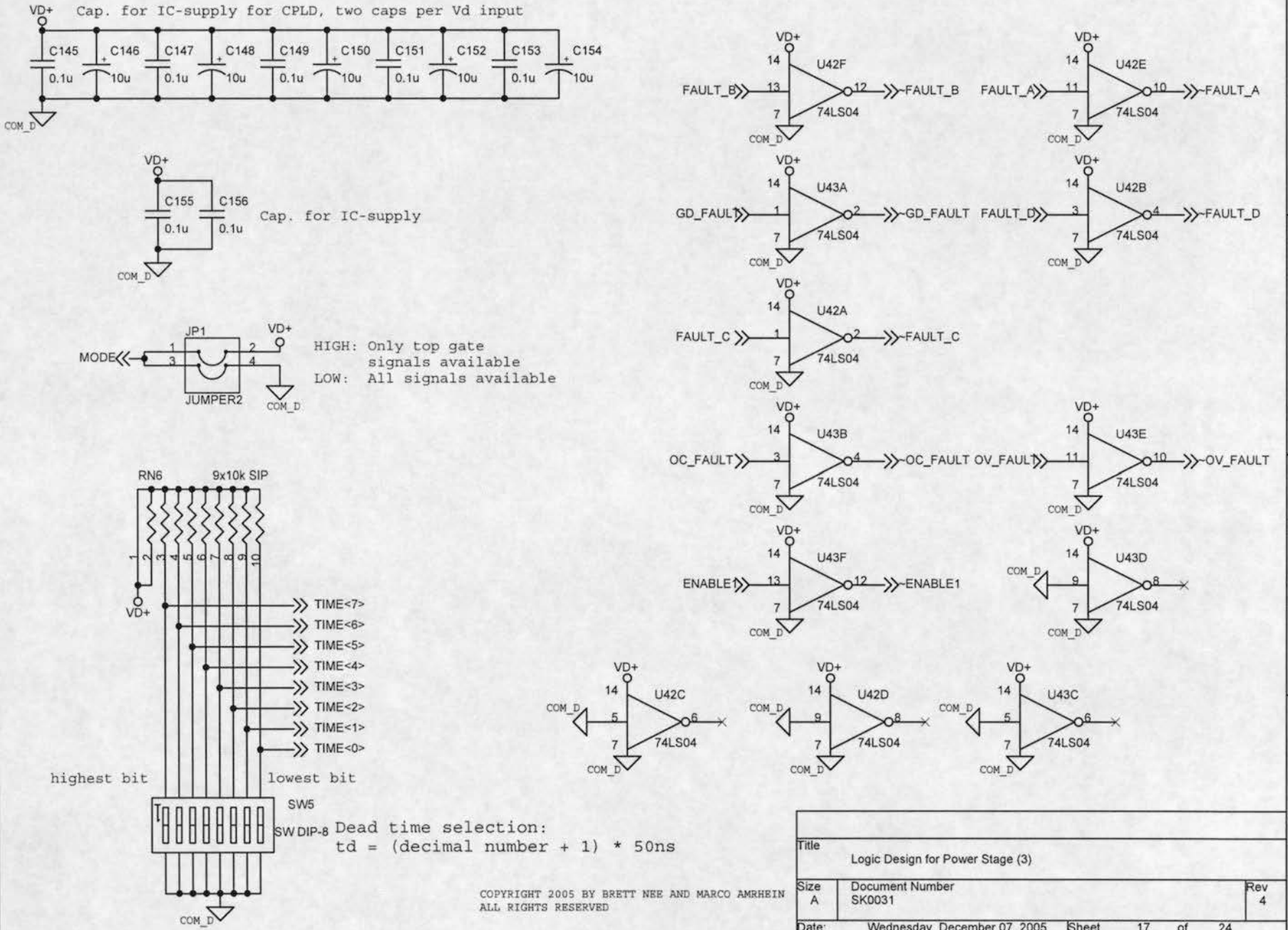

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Title	Logic Design for Power Stage (3)	
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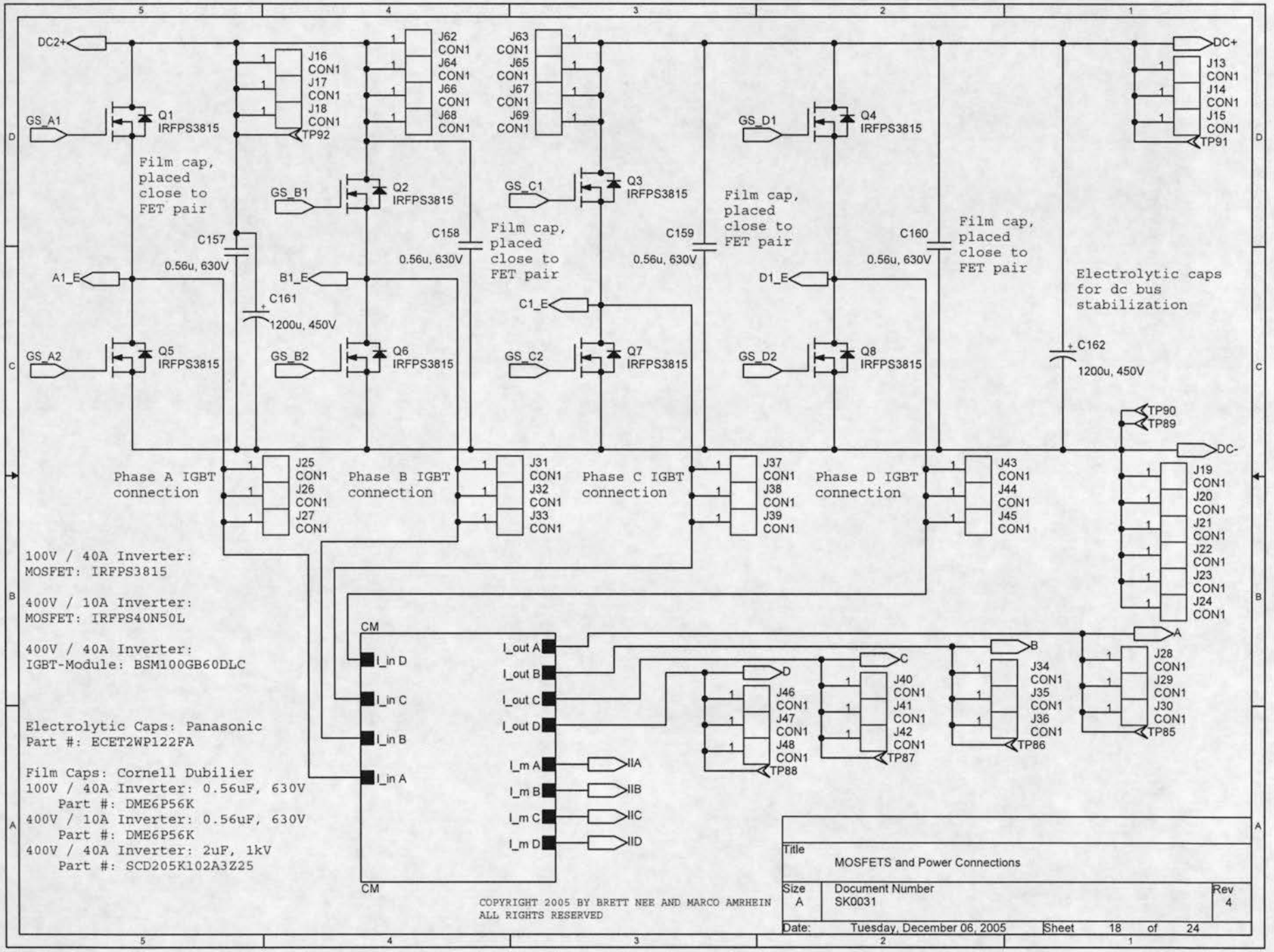
DC2+
GS_A1
Q1 IRFPS3815
J16 CON1
J17 CON1
J18 CON1
TP92
J62 CON1
J64 CON1
J66 CON1
J68 CON1
J63 CON1
J65 CON1
J67 CON1
J69 CON1
GS_D1
Q4 IRFPS3815
DC+
J13 CON1
J14 CON1
J15 CON1
TP91
Film cap, placed close to FET pair
GS_B1
Q2 IRFPS3815
GS_C1
Q3 IRFPS3815
C157
0.56u, 630V
C158
0.56u, 630V
C159
0.56u, 630V
C160
0.56u, 630V
A1_E
B1_E
C1_E
D1_E
C161
1200u, 450V
GS_A2
Q5 IRFPS3815
GS_B2
Q6 IRFPS3815
GS_C2
Q7 IRFPS3815
GS_D2
Q8 IRFPS3815
C162
1200u, 450V
Electrolytic caps for dc bus stabilization
TP90
TP89
DC-
Phase A IGBT connection
J25 CON1
J26 CON1
J27 CON1
Phase B IGBT connection
J31 CON1
J32 CON1
J33 CON1
Phase C IGBT connection
J37 CON1
J38 CON1
J39 CON1
Phase D IGBT connection
J43 CON1
J44 CON1
J45 CON1
J19 CON1
J20 CON1
J21 CON1
J22 CON1
J23 CON1
J24 CON1
100V / 40A Inverter:
MOSFET: IRFPS3815
400V / 10A Inverter:
MOSFET: IRFPS40N50L
400V / 40A Inverter:
IGBT-Module: BSM100GB60DLC
CM
I_in D
I_in C
I_in B
I_in A
I_out A
I_out B
I_out C
I_out D
I_m A
I_m B
I_m C
I_m D
IIA
IIB
IIC
IID
A
B
C
D
J46 CON1
J47 CON1
J48 CON1
TP88
J40 CON1
J41 CON1
J42 CON1
TP87
J34 CON1
J35 CON1
J36 CON1
TP86
J28 CON1
J29 CON1
J30 CON1
TP85
Electrolytic Caps: Panasonic
Part #: ECET2WP122FA
Film Caps: Cornell Dubilier
100V / 40A Inverter: 0.56uF, 630V
Part #: DME6P56K
400V / 10A Inverter: 0.56uF, 630V
Part #: DME6P56K
400V / 40A Inverter: 2uF, 1kV
Part #: SCD205K102A3Z25
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Title
MOSFETS and Power Connections
Size
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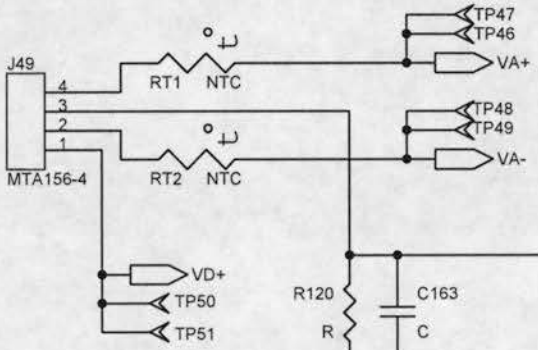
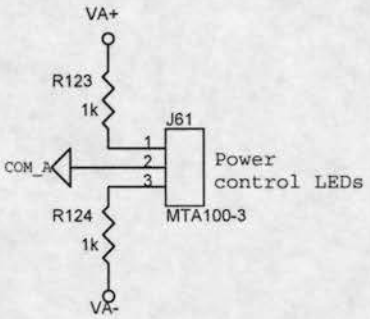
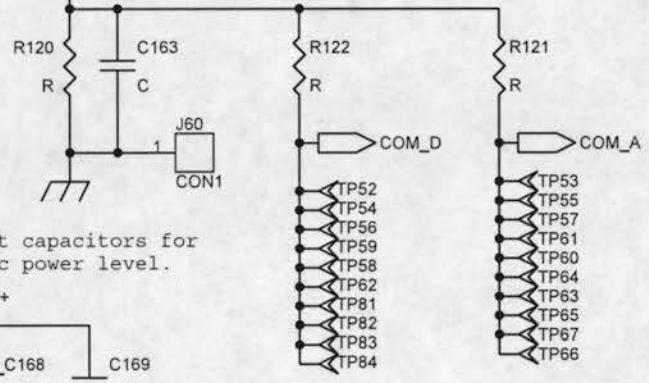
of
24

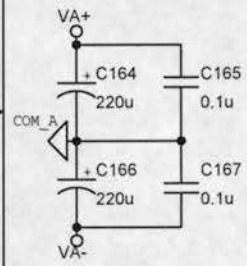
NTCs limit inrush current on +/-15V supply voltage from Kyosan power supply.



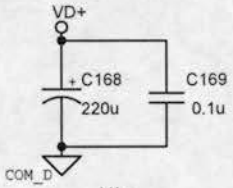


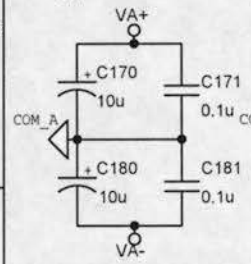


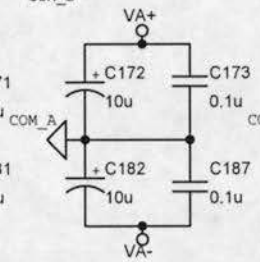
Input capacitors for analog power level.

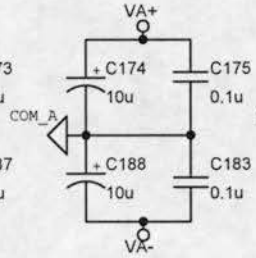


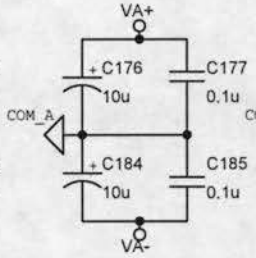
Input capacitors for logic power level.

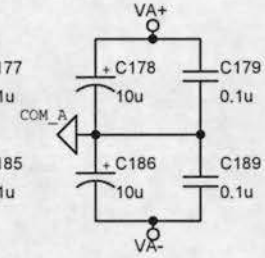


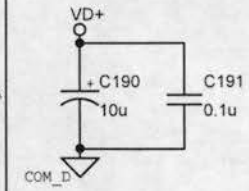


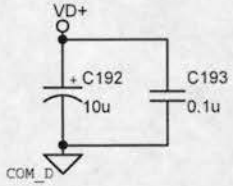


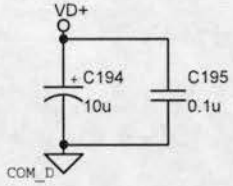






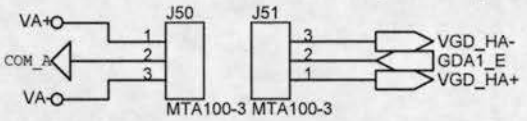




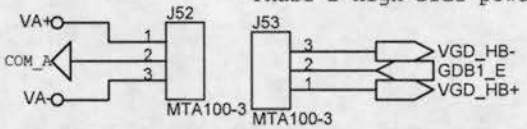


Stabilizing capacitors for analog and logic power.

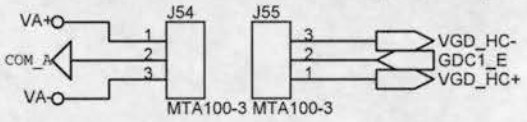
Phase A high-side power supply



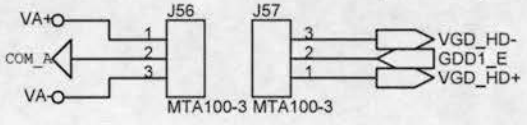
Phase B high-side power supply



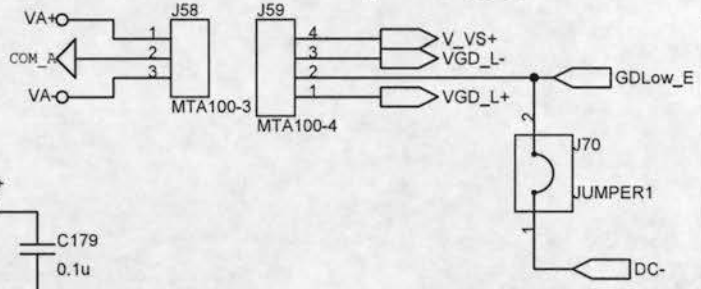
Phase C high-side power supply



Phase D high-side power supply



Low-side power supply



Note to J70:
This connection can be closed in order to eliminate ground loops from one low-side gate drives to another. If conected, all traces going to the low-side gate drives ground planes need to be cut. See design document for a detailed explanation.

Title: Analog and Logic Power Supply Connectors		
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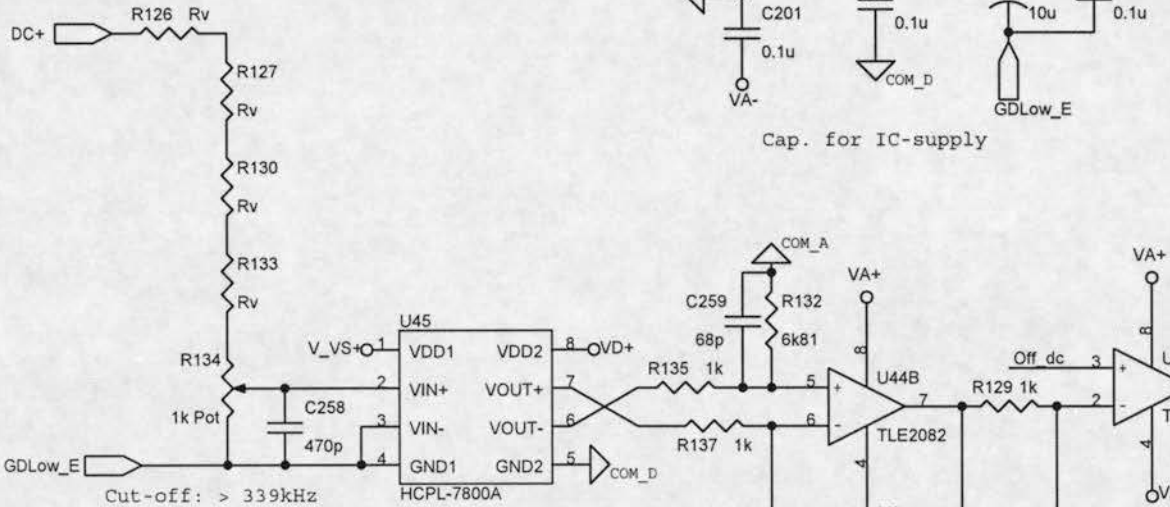
Dc Bus Voltage Measurement:
Rated dc bus voltage = 8V @ VV_BUS
(~150mV @ input of isolated amplifier)

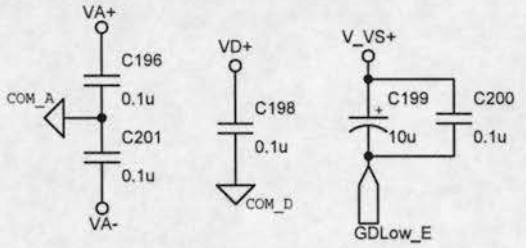
For 100V / 40A Inverter:
use 124k resistors for Rv (4 serial)

For 400V / 40A Inverter:
use 499k resistors for Rv (4 serial)

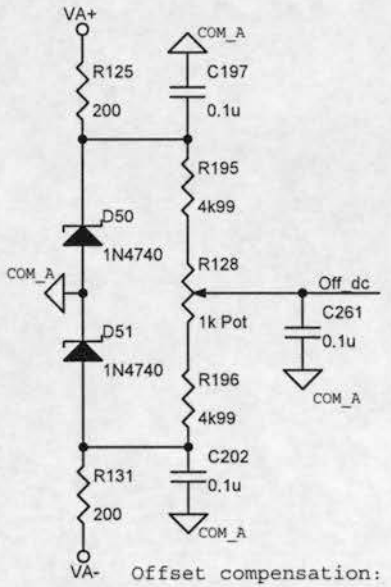
For 400V / 40A Inverter:
use 499k resistors for Rv (4 serial)

Range adjusting necessary due to uncertain gain off isolated amplifier to get 8V @ VV_BUS at RMS voltage input.





Cap. for IC-supply



Offset compensation:
Range -0.9V...0.9V

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Title: Isolated Voltage Measurement, Bus Voltage		
Size: A	Document Number: SK0031	Rev: 4
Date: Friday, December 09, 2005	Sheet 20 of 24	

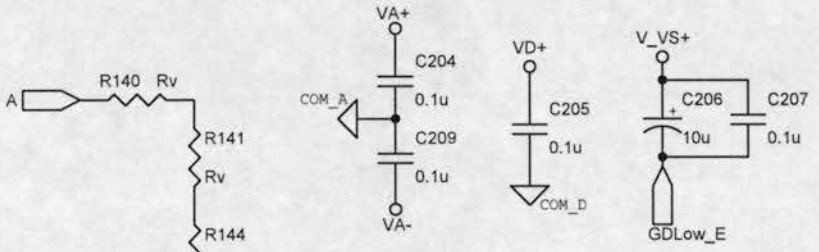
Phase A Voltage Measurement:
Rated dc bus voltage = 8V @ VVA
(~150mV @ input of isolated amplifier)

For 100V / 40A Inverter:
use 124k resistors for Rv (4 serial)

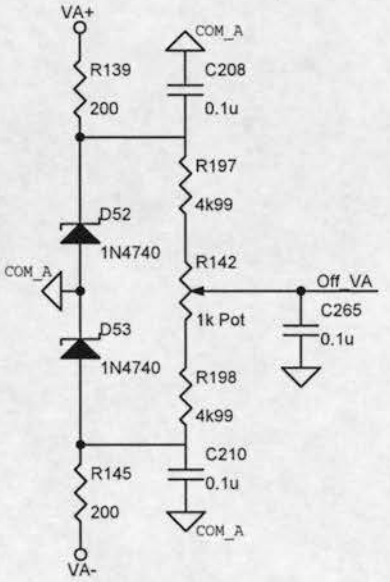
For 400V / 10A Inverter:
use 499k resistors for Rv (4 serial)

For 400V / 40A Inverter:
use 499k resistors for Rv (4 serial)

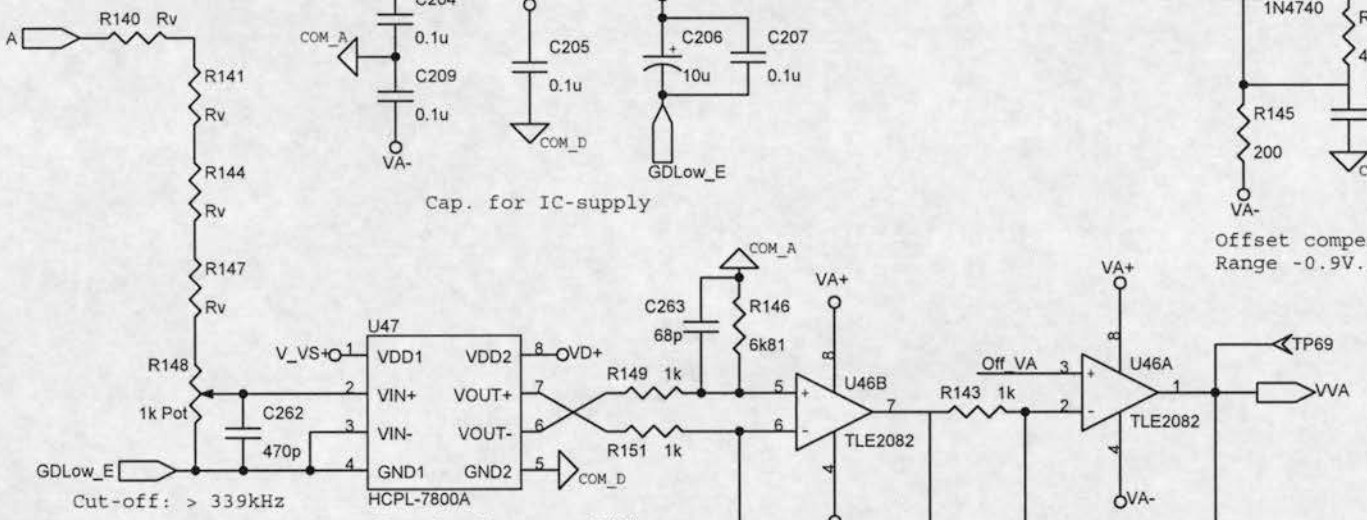
Range adjusting necessary due to uncertain gain off isolated amplifier to get 8V @ VV_BUS at RMS voltage input.



Cap. for IC-supply



Offset compensation:
Range -0.9V...0.9V



Cut-off: > 339kHz

Isolated voltage amplifier

Cut-off: 344kHz

Cut-off: 339kHz

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Title: Isolated Voltage Measurement, Phase A		
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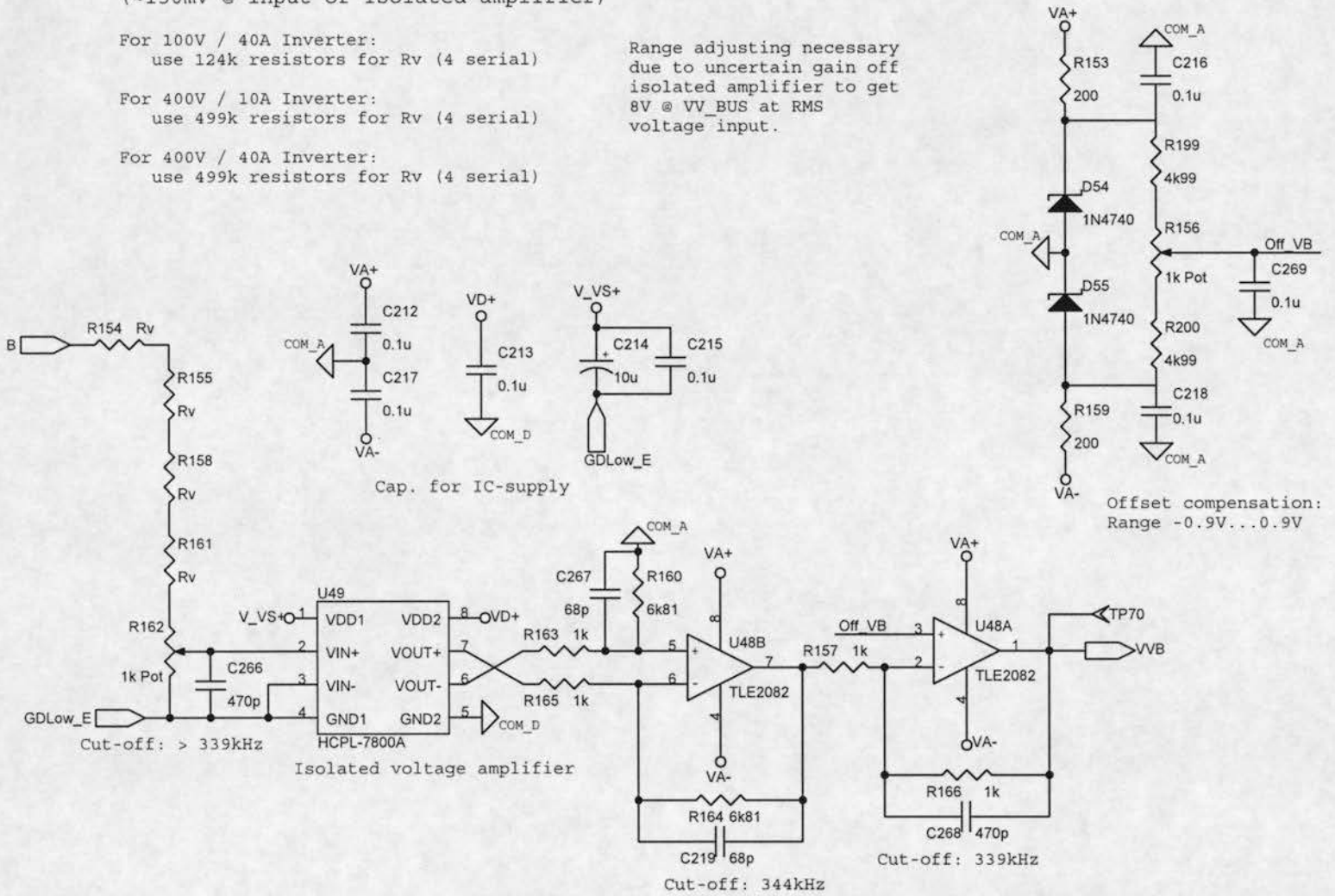
Phase B Voltage Measurement:
Rated dc bus voltage = 8V @ VVB
(~150mV @ input of isolated amplifier)

For 100V / 40A Inverter:
use 124k resistors for Rv (4 serial)

For 400V / 10A Inverter:
use 499k resistors for Rv (4 serial)

For 400V / 40A Inverter:
use 499k resistors for Rv (4 serial)

Range adjusting necessary due to uncertain gain off isolated amplifier to get 8V @ VV_BUS at RMS voltage input.



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Title: Isolated Voltage Measurement, Phase B		
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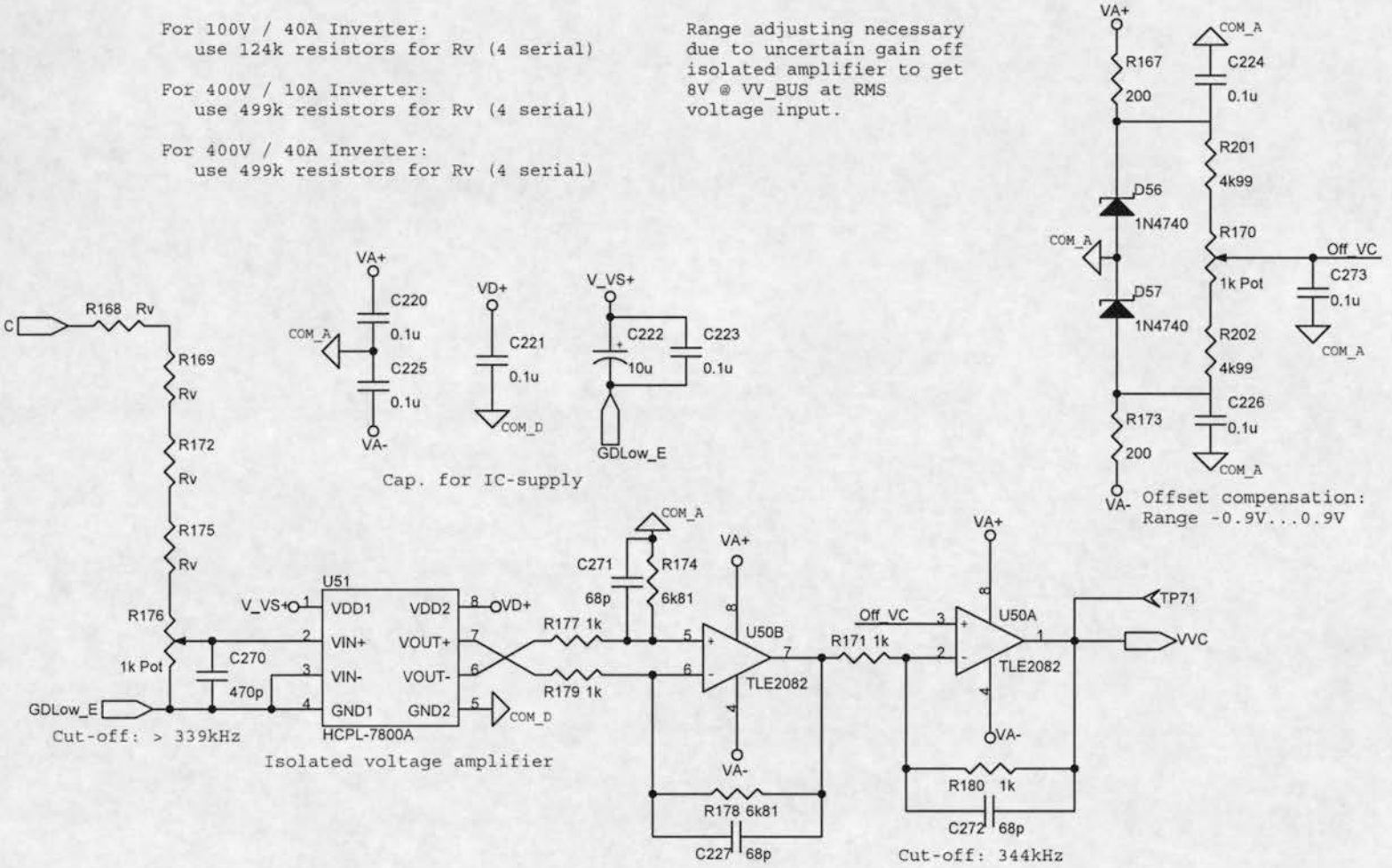
Phase C Voltage Measurement:
Rated dc bus voltage = 8V @ VVC
(~150mV @ input of isolated amplifier)

For 100V / 40A Inverter:
use 124k resistors for Rv (4 serial)

For 400V / 10A Inverter:
use 499k resistors for Rv (4 serial)

For 400V / 40A Inverter:
use 499k resistors for Rv (4 serial)

Range adjusting necessary due to uncertain gain off isolated amplifier to get 8V @ VV_BUS at RMS voltage input.



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Title: Isolated Voltage Measurement, Phase C		
Size: A	Document Number: SK0031	Rev: 4
Date: Friday, December 09, 2005	Sheet 23 of 24	

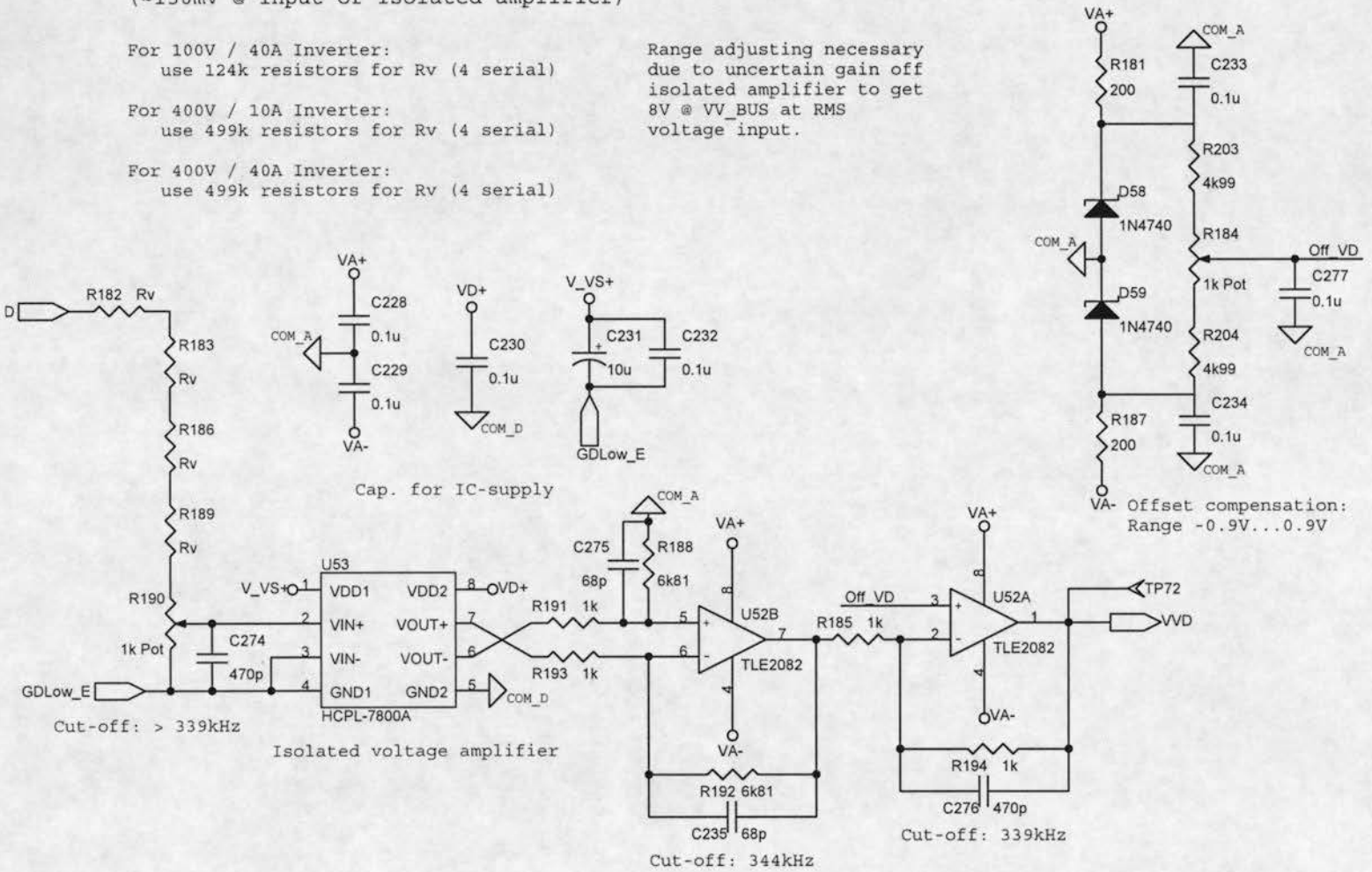
Phase D Voltage Measurement:
Rated dc bus voltage = 8V @ VVD
(~150mV @ input of isolated amplifier)

For 100V / 40A Inverter:
use 124k resistors for Rv (4 serial)

For 400V / 10A Inverter:
use 499k resistors for Rv (4 serial)

For 400V / 40A Inverter:
use 499k resistors for Rv (4 serial)

Range adjusting necessary due to uncertain gain off isolated amplifier to get 8V @ VV_BUS at RMS voltage input.



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Title: Isolated Voltage Measurement, Phase D		
Size: A	Document Number: SK0031	Rev: 4
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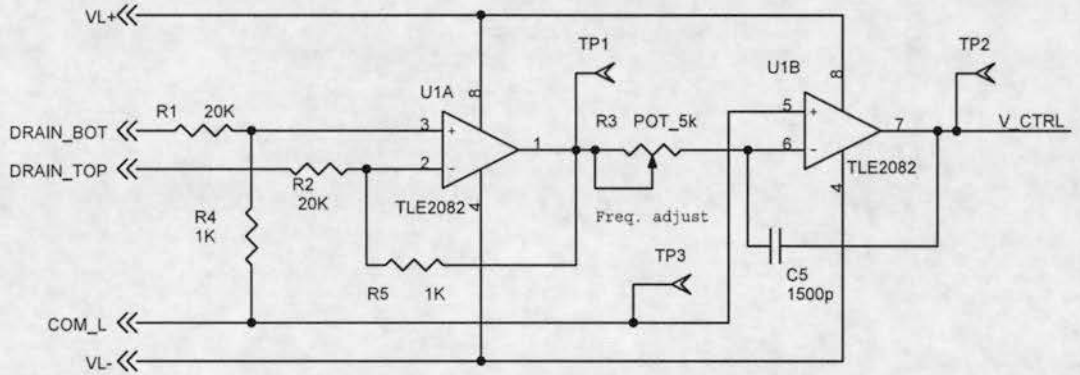
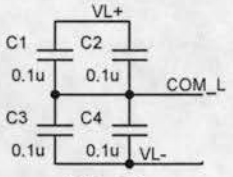
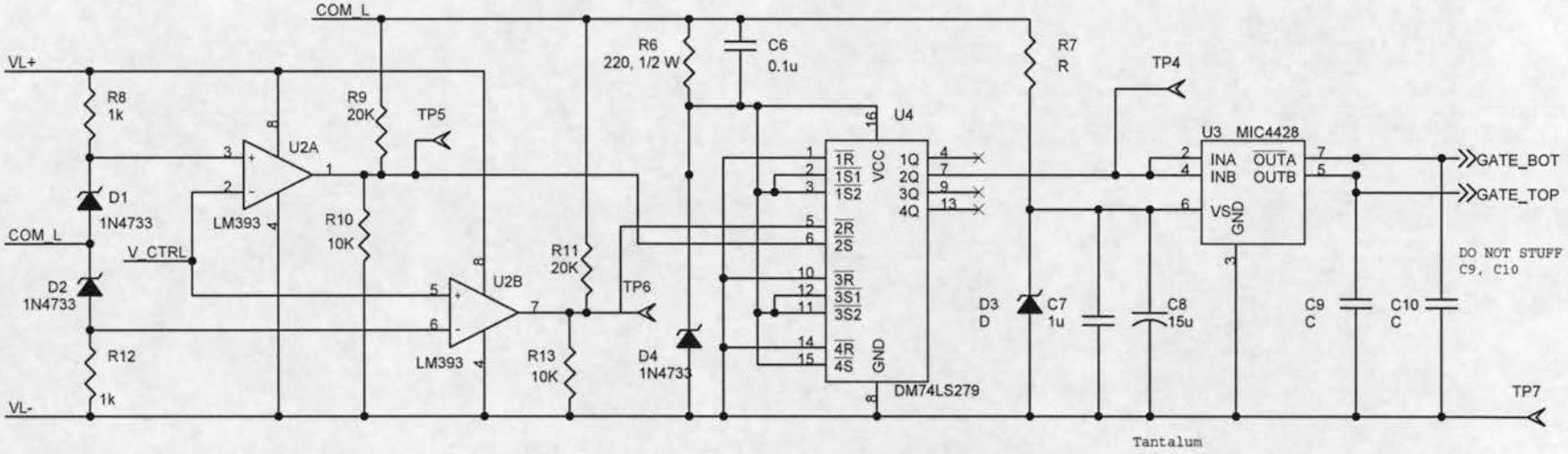




DO NOT STUFF D3, R7
Jumper pin 6 of U3 to pin 16 of U4 (Vcc)



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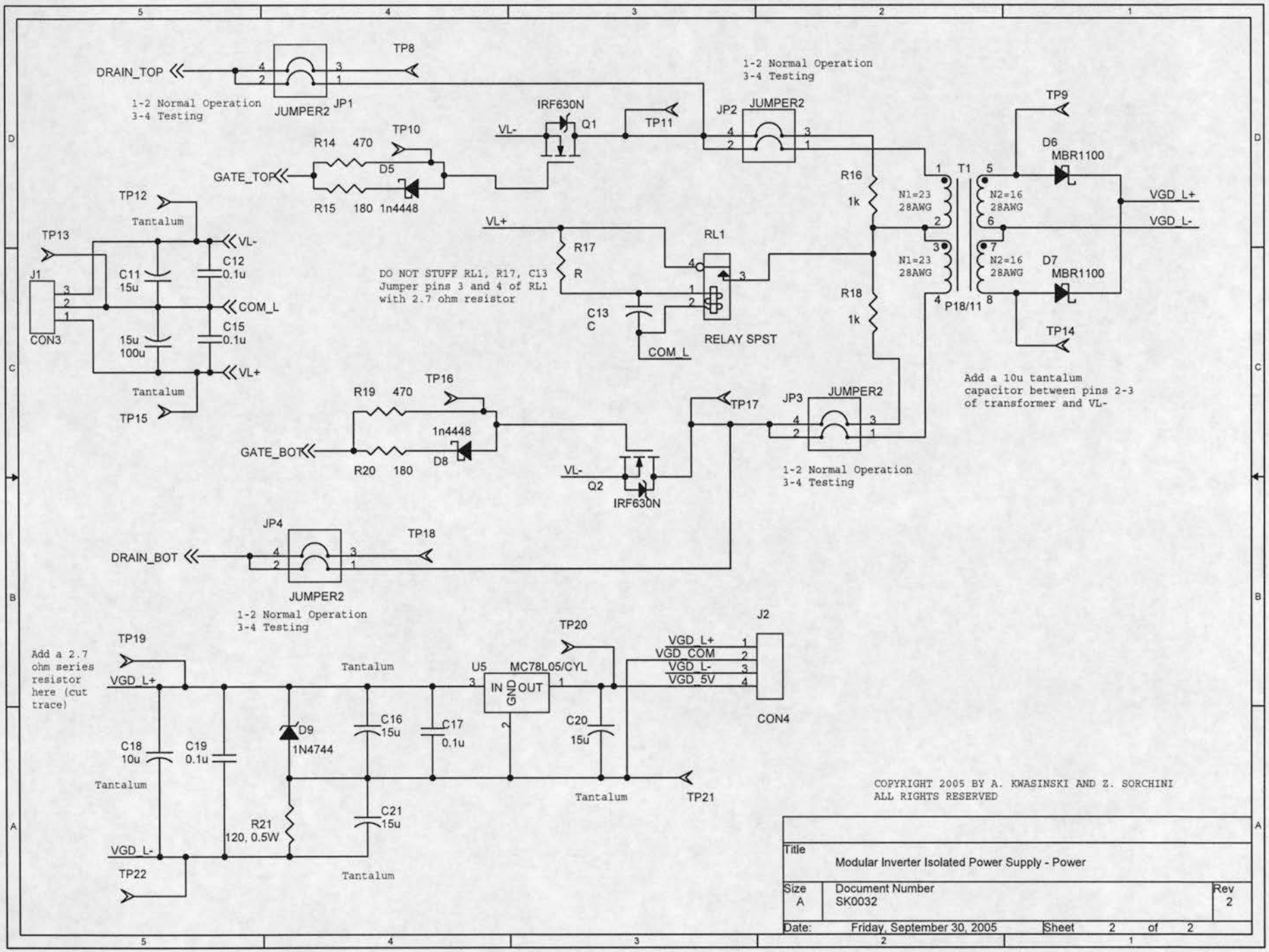
Title	Modular Inverter Isolated Power Supply - Control	
Size A	Document Number SK0032	Rev 2
Date: Friday, September 30, 2005	Sheet 1 of 2	


DRAIN_TOP
TP8
JP1
JUMPER2
1-2 Normal Operation
3-4 Testing
1-2 Normal Operation
3-4 Testing
IRF630N
Q1
VL-
TP11
JP2
JUMPER2
TP9
D6
MBR1100
TP10
R14 470
D5
GATE_TOP
R15 180 1n4448
R16
1k
T1
N1=23
28AWG
N2=16
28AWG
VGD_L+
VGD_L-
TP12
Tantalum
TP13
VL+
R17
R
RL1
DO NOT STUFF RL1, R17, C13
Jumper pins 3 and 4 of RL1
with 2.7 ohm resistor
C13
C
COM_L
RELAY SPST
R18
1k
P18/11
D7
MBR1100
TP14
J1
CON3
C11
15u
C12
0.1u
COM_L
C15
0.1u
15u
100u
VL+
TP15
Tantalum
TP16
R19 470
1n4448
D8
GATE_BOT
R20 180
TP17
JP3
JUMPER2
Add a 10u tantalum
capacitor between pins 2-3
of transformer and VL-
VL-
Q2
IRF630N
1-2 Normal Operation
3-4 Testing
JP4
TP18
DRAIN_BOT
JUMPER2
1-2 Normal Operation
3-4 Testing
TP19
Add a 2.7
ohm series
resistor
here (cut
trace)
VGD_L+
Tantalum
U5
MC78L05/CYL
IN
GND
OUT
TP20
J2
VGD_L+
VGD_COM
VGD_L-
VGD_5V
CON4
C18
10u
C19
0.1u
Tantalum
D9
1N4744
C16
15u
C17
0.1u
C20
15u
Tantalum
TP21
R21
120, 0.5W
C21
15u
VGD_L-
TP22
Tantalum
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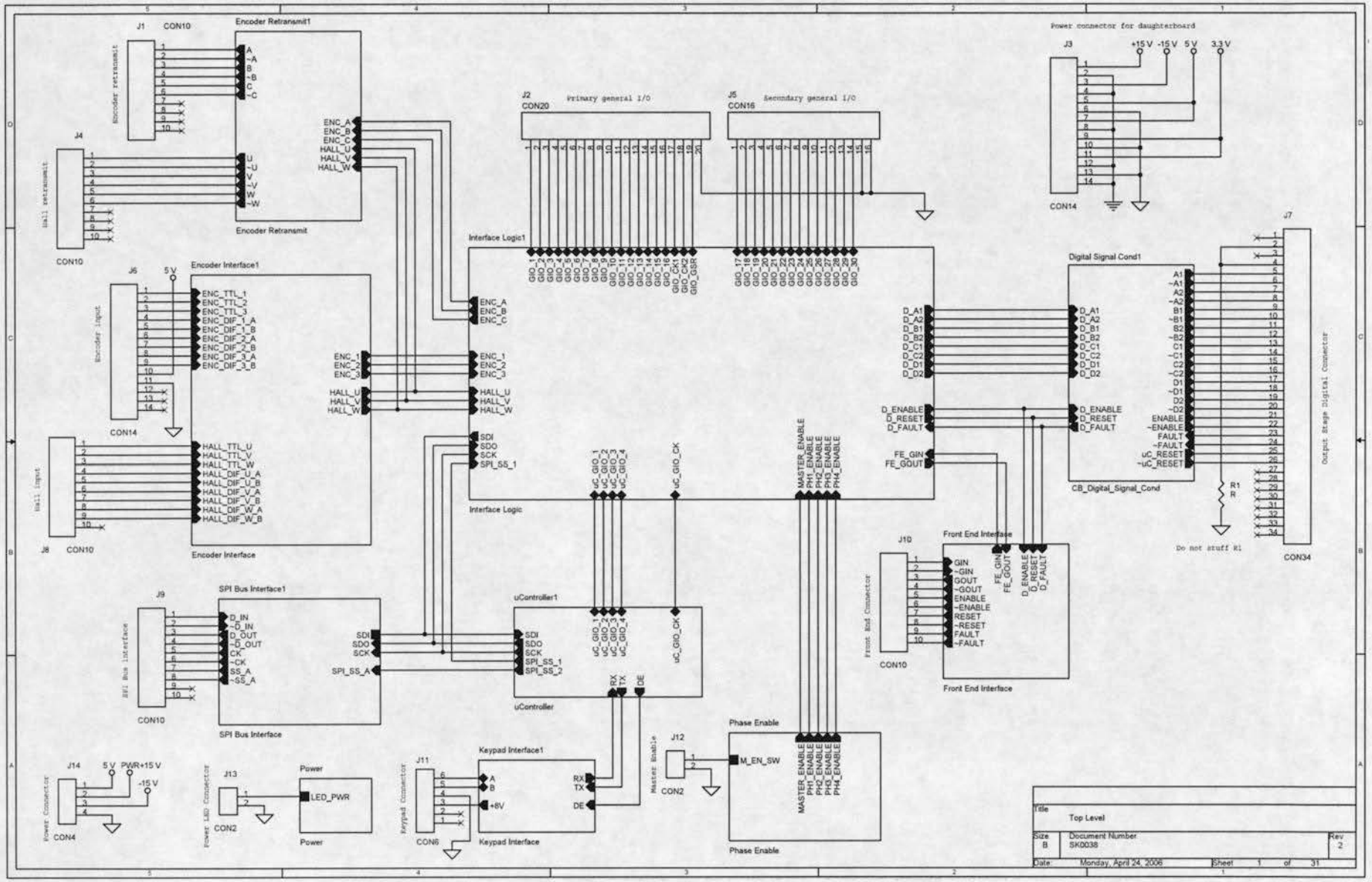
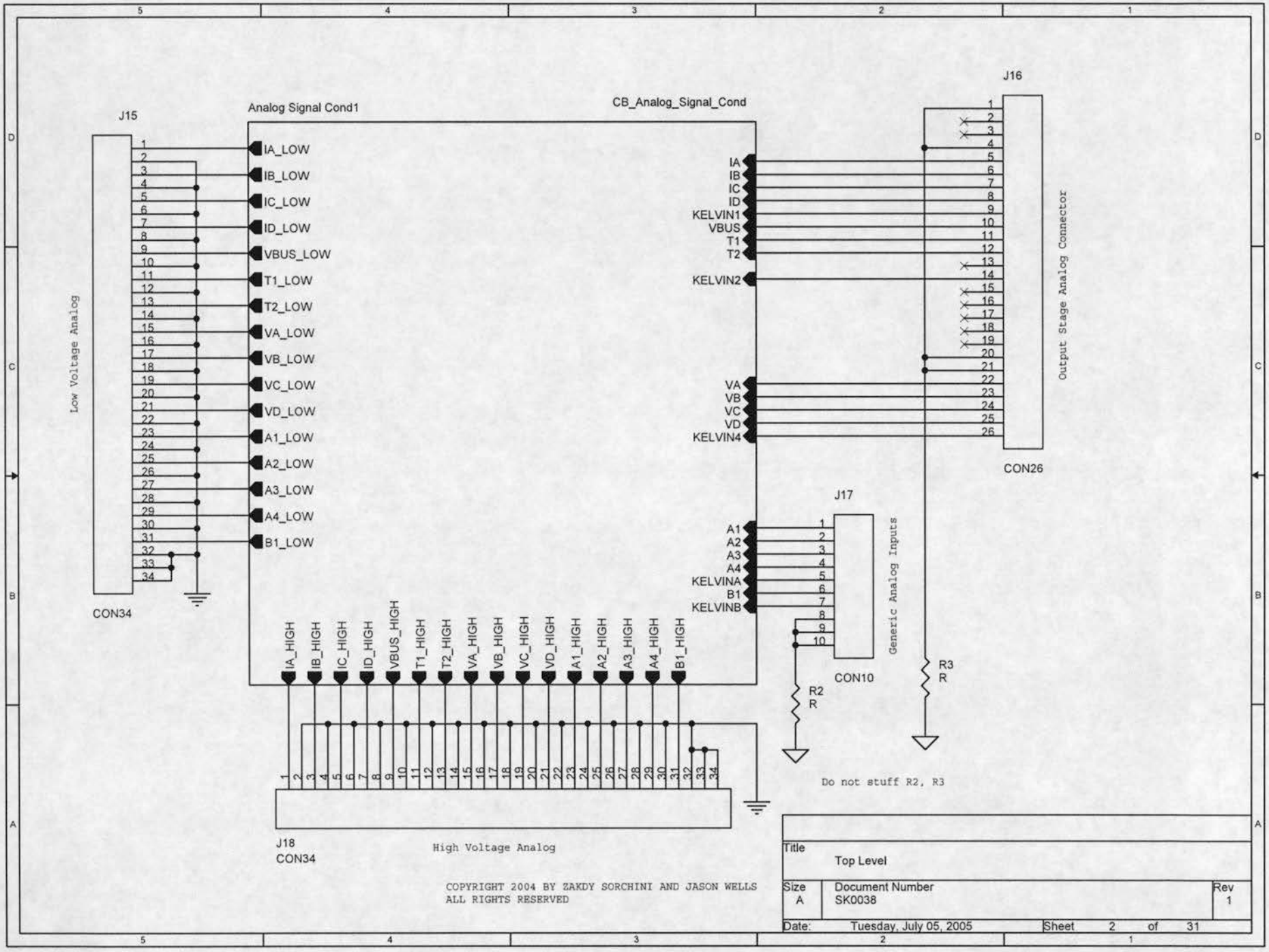
ALL RIGHTS RESERVED
Title
Modular Inverter Isolated Power Supply - Power
Size
A
Document Number
SK0032
Rev
2
Date:
Friday, September 30, 2005
Sheet
2
of
2


Encoder Retransmit1
Encoder Retransmit
Primary general I/O
Secondary general I/O
Power connector for daughterboard
Interface Logic1
Interface Logic
Digital Signal Cond1
CB_Digital_Signal_Cond
Encoder Interface1
Encoder Interface
SPI Bus Interface1
SPI Bus Interface
uController1
uController
Front End Interface
Keypad Interface1
Keypad Interface
Phase Enable
Output Stage Digital Connector
Do not stuff R1
Title
Top Level
Document Number
SK0038
Monday, April 24, 2006


J15
Low Voltage Analog
CON34
Analog Signal Cond1
IA_LOW
IB_LOW
IC_LOW
ID_LOW
VBUS_LOW
T1_LOW
T2_LOW
VA_LOW
VB_LOW
VC_LOW
VD_LOW
A1_LOW
A2_LOW
A3_LOW
A4_LOW
B1_LOW
IA_HIGH
IB_HIGH
IC_HIGH
ID_HIGH
VBUS_HIGH
T1_HIGH
T2_HIGH
VA_HIGH
VB_HIGH
VC_HIGH
VD_HIGH
A1_HIGH
A2_HIGH
A3_HIGH
A4_HIGH
B1_HIGH
J18
CON34
High Voltage Analog
CB_Analog_Signal_Cond
IA
IB
IC
ID
KELVIN1
VBUS
T1
T2
KELVIN2
VA
VB
VC
VD
KELVIN4
A1
A2
A3
A4
KELVINA
B1
KELVINB
J16
Output Stage Analog Connector
CON26
J17
Generic Analog Inputs
CON10
R2
R
R3
R
Do not stuff R2, R3
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Top Level
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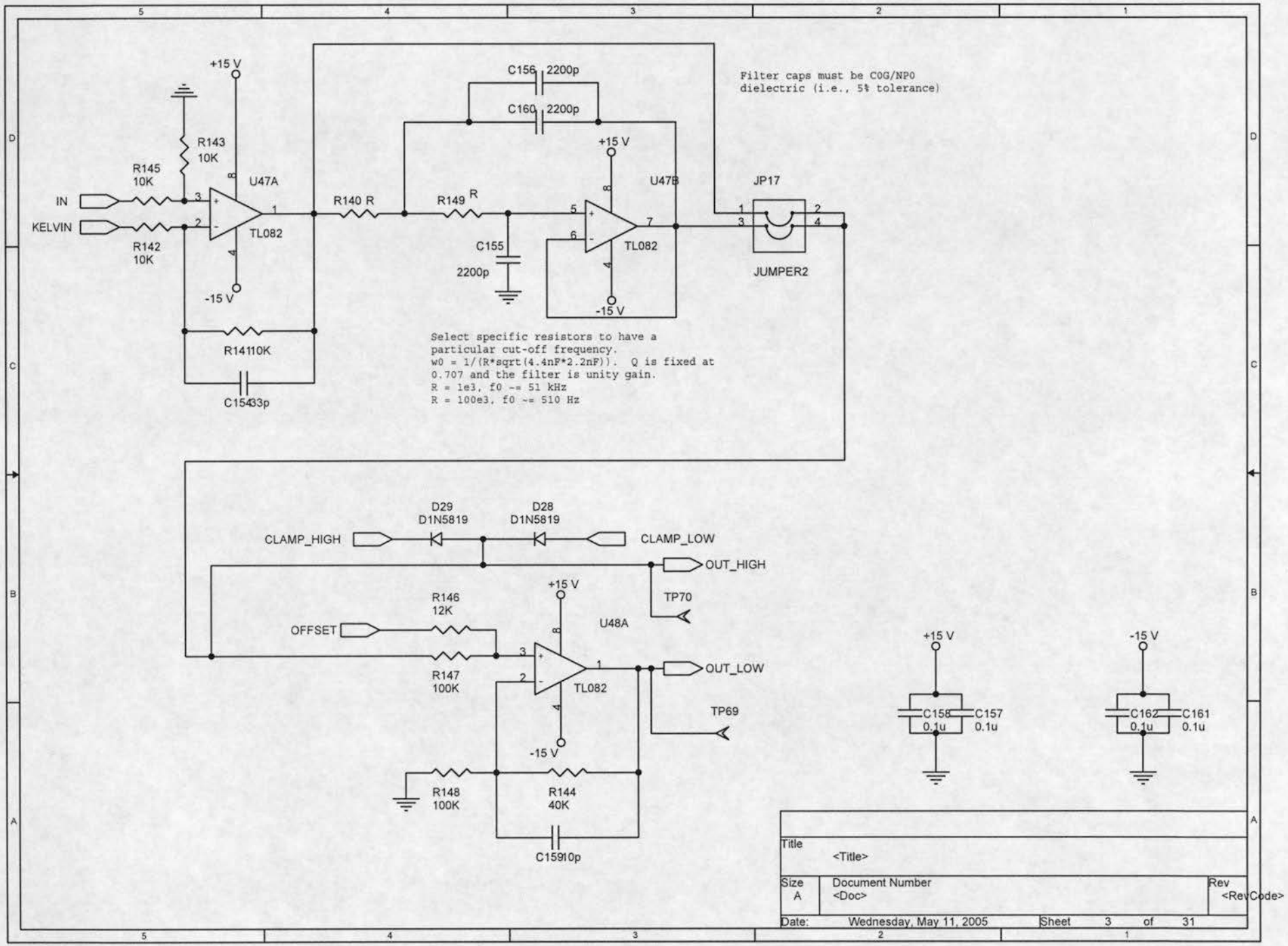

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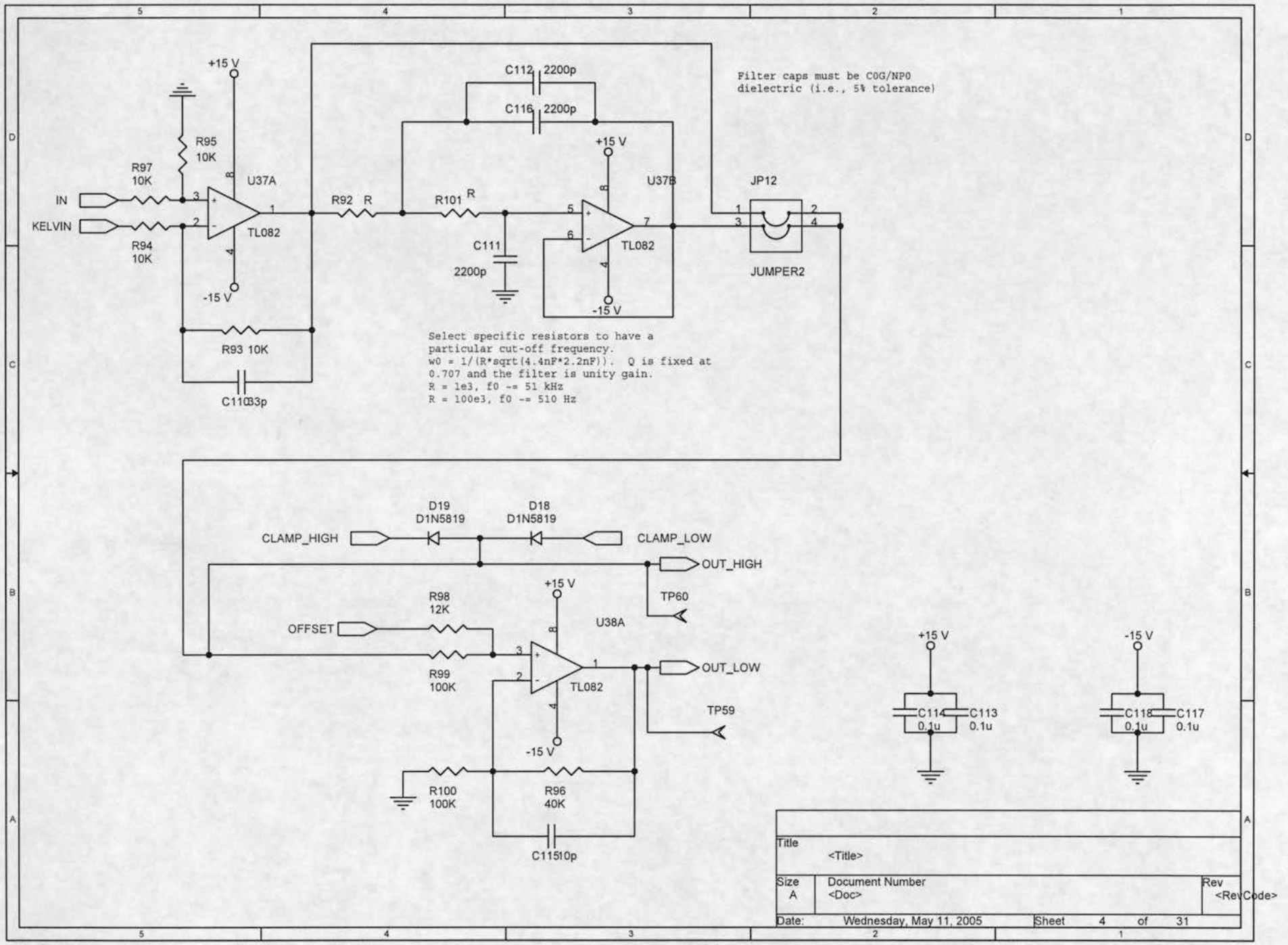

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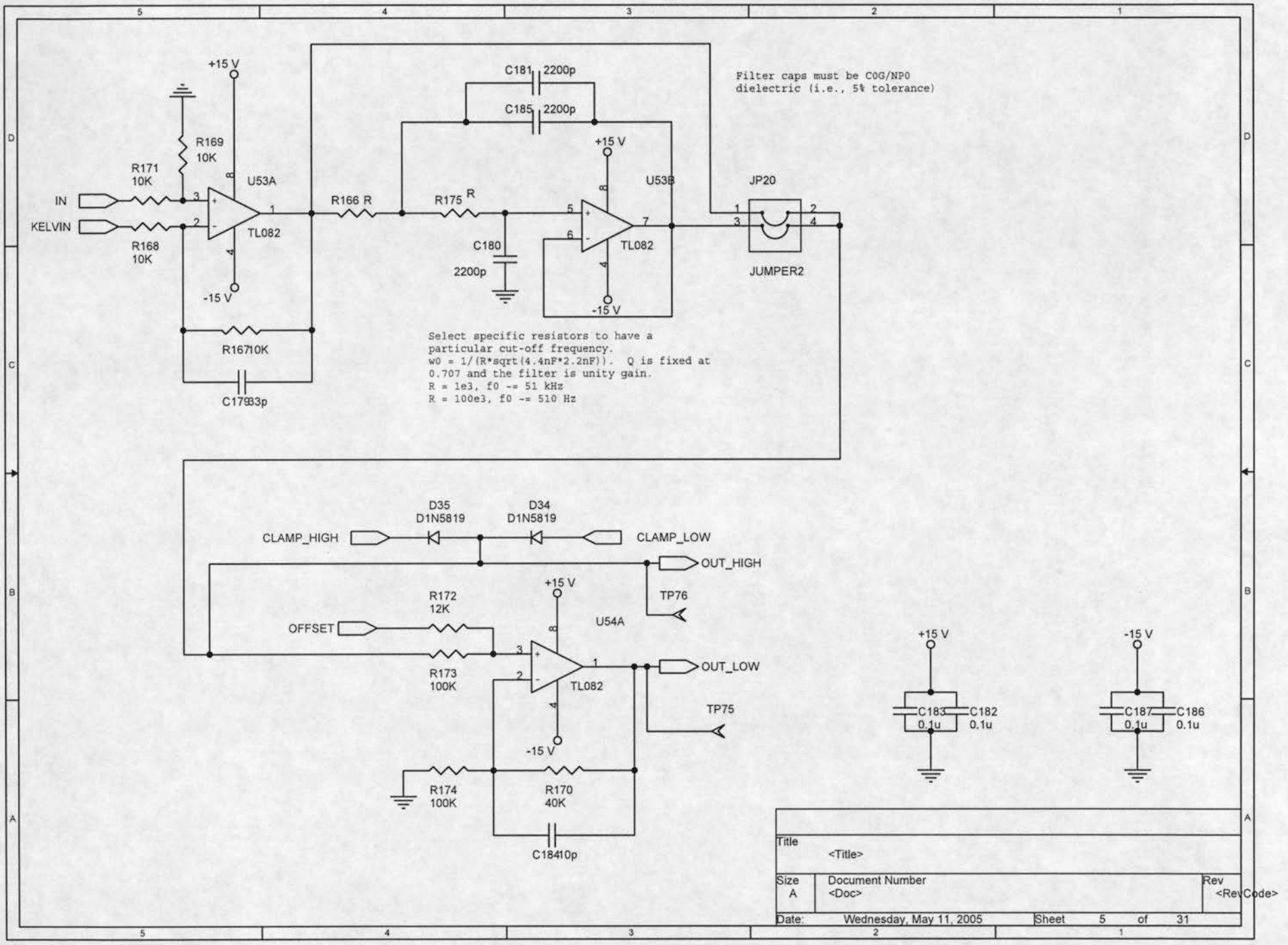
+15 V
C181 2200p
C185 2200p
Filter caps must be C0G/NP0
dielectric (i.e., 5% tolerance)
R169
10K
R171
10K
U53A
U53B
JP20
IN
KELVIN
R168
10K
TL082
R166 R
R175 R
C180
2200p
JUMPER2
-15 V
R167 10K
C179 33p
Select specific resistors to have a
particular cut-off frequency.
w0 = 1/(R*sqrt(4.4nF*2.2nF)). Q is fixed at
0.707 and the filter is unity gain.
R = 1e3, f0 ~= 51 kHz
R = 100e3, f0 ~= 510 Hz
D35
D1N5819
D34
D1N5819
CLAMP_HIGH
CLAMP_LOW
OUT_HIGH
TP76
R172
12K
U54A
OFFSET
R173
100K
OUT_LOW
TP75
R174
100K
R170
40K
C184 10p
C183
0.1u
C182
0.1u
C187
0.1u
C186
0.1u
Title
<Title>
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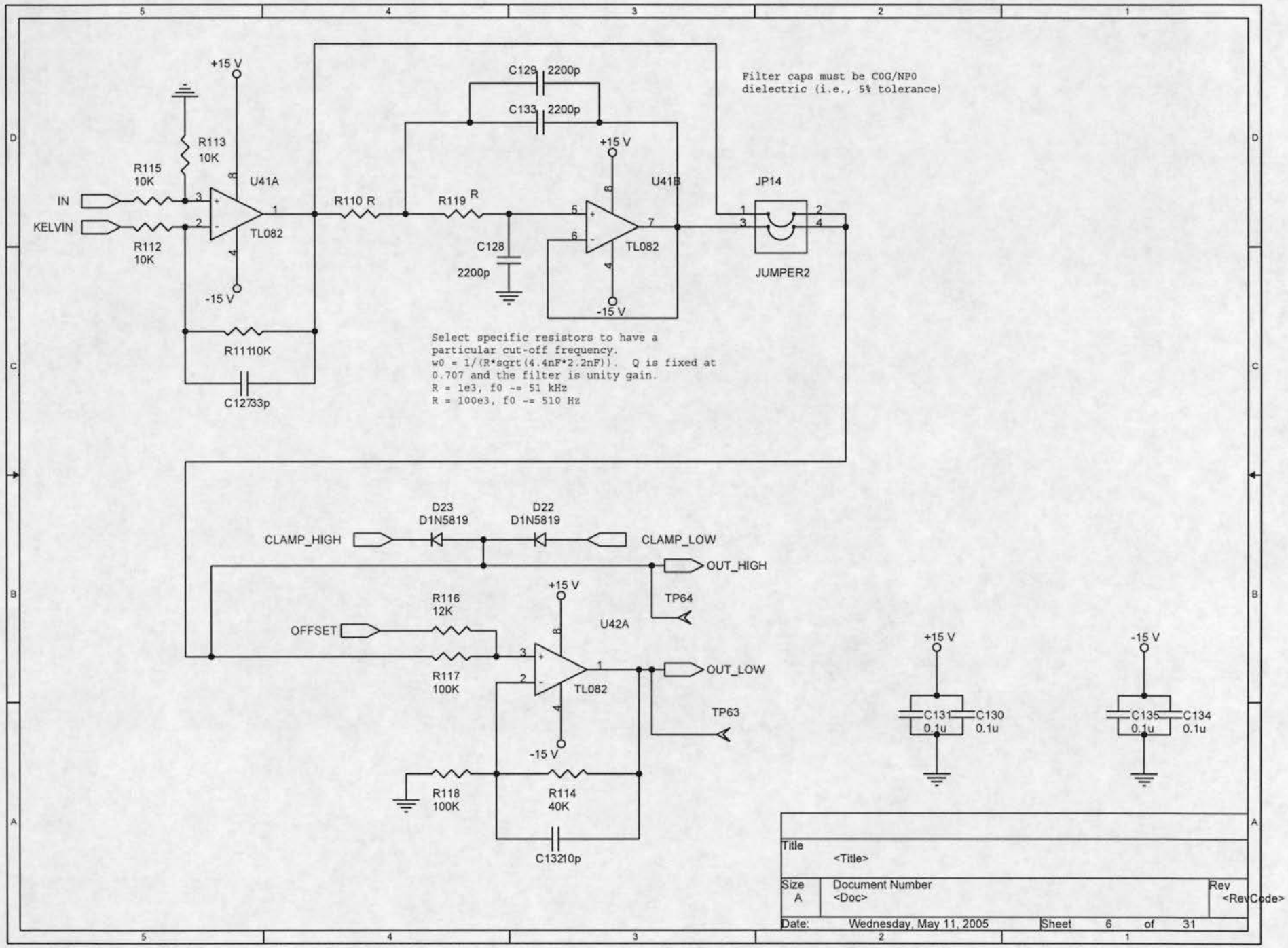
+15 V
C129 2200p
C133 2200p
Filter caps must be C0G/NP0
dielectric (i.e., 5% tolerance)
R113
10K
R115
10K
U41A
IN
KELVIN
R112
10K
TL082
-15 V
R110 R
R119 R
+15 V
U41B
JP14
C128
2200p
TL082
JUMPER2
-15 V
R111 10K
C127 33p
Select specific resistors to have a
particular cut-off frequency.
w0 = 1/(R*sqrt(4.4nF*2.2nF)). Q is fixed at
0.707 and the filter is unity gain.
R = 1e3, f0 ~= 51 kHz
R = 100e3, f0 ~= 510 Hz
D23
D1N5819
D22
D1N5819
CLAMP_HIGH
CLAMP_LOW
OUT_HIGH
TP64
+15 V
R116
12K
U42A
OFFSET
OUT_LOW
R117
100K
TL082
TP63
-15 V
R118
100K
R114
40K
C132 10p
+15 V
C131
0.1u
C130
0.1u
-15 V
C135
0.1u
C134
0.1u
Title
<Title>
Size
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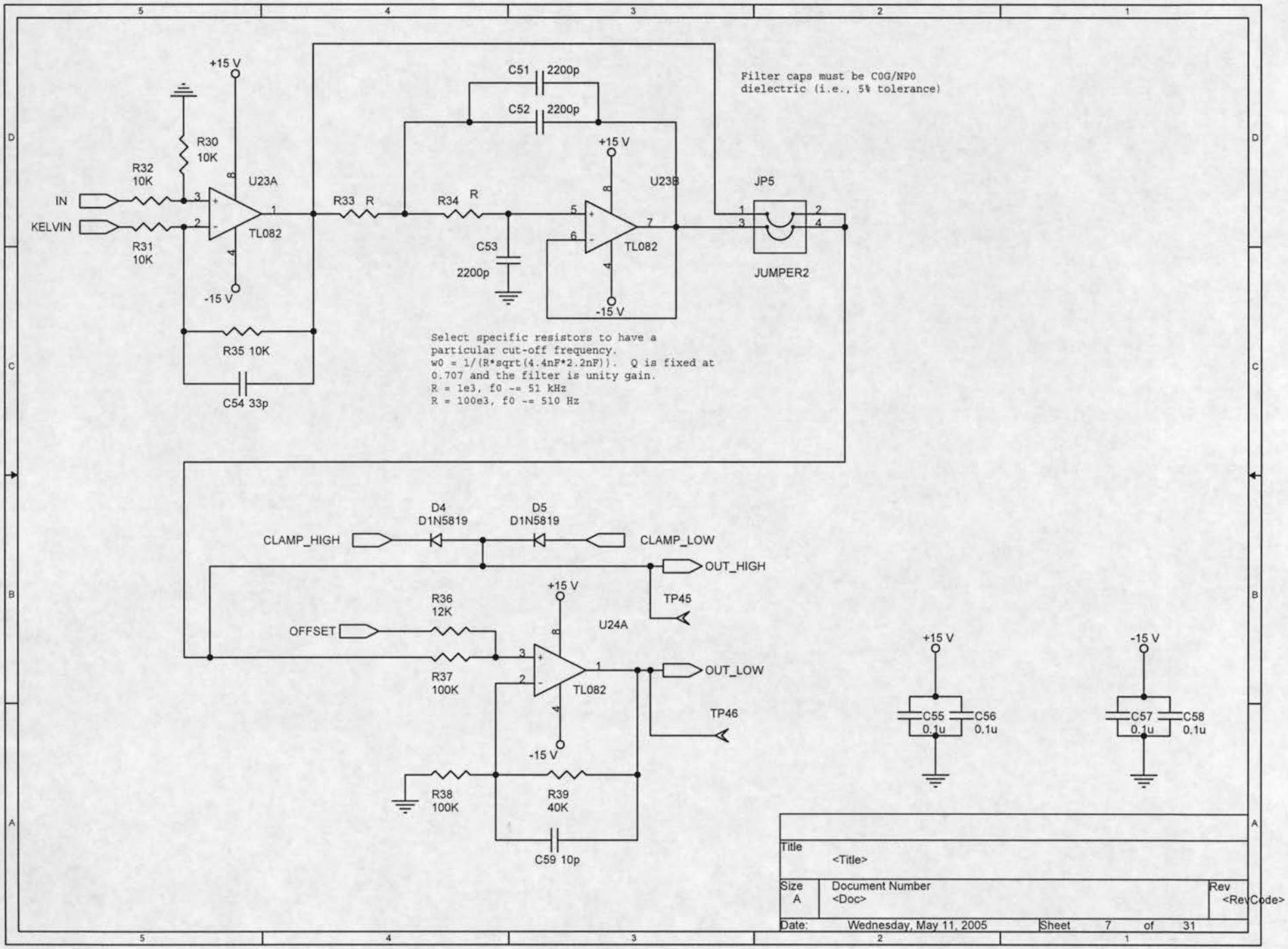

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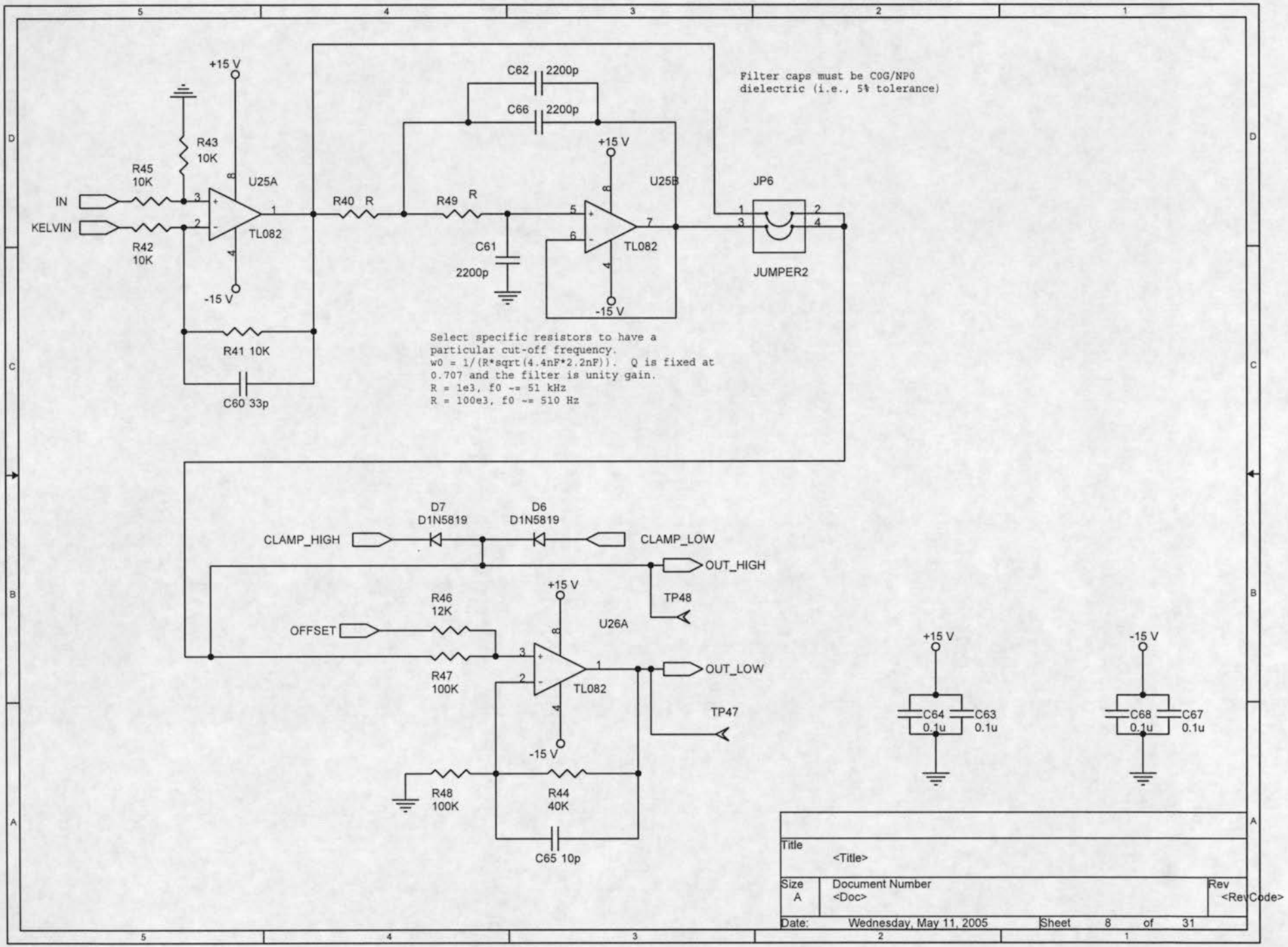

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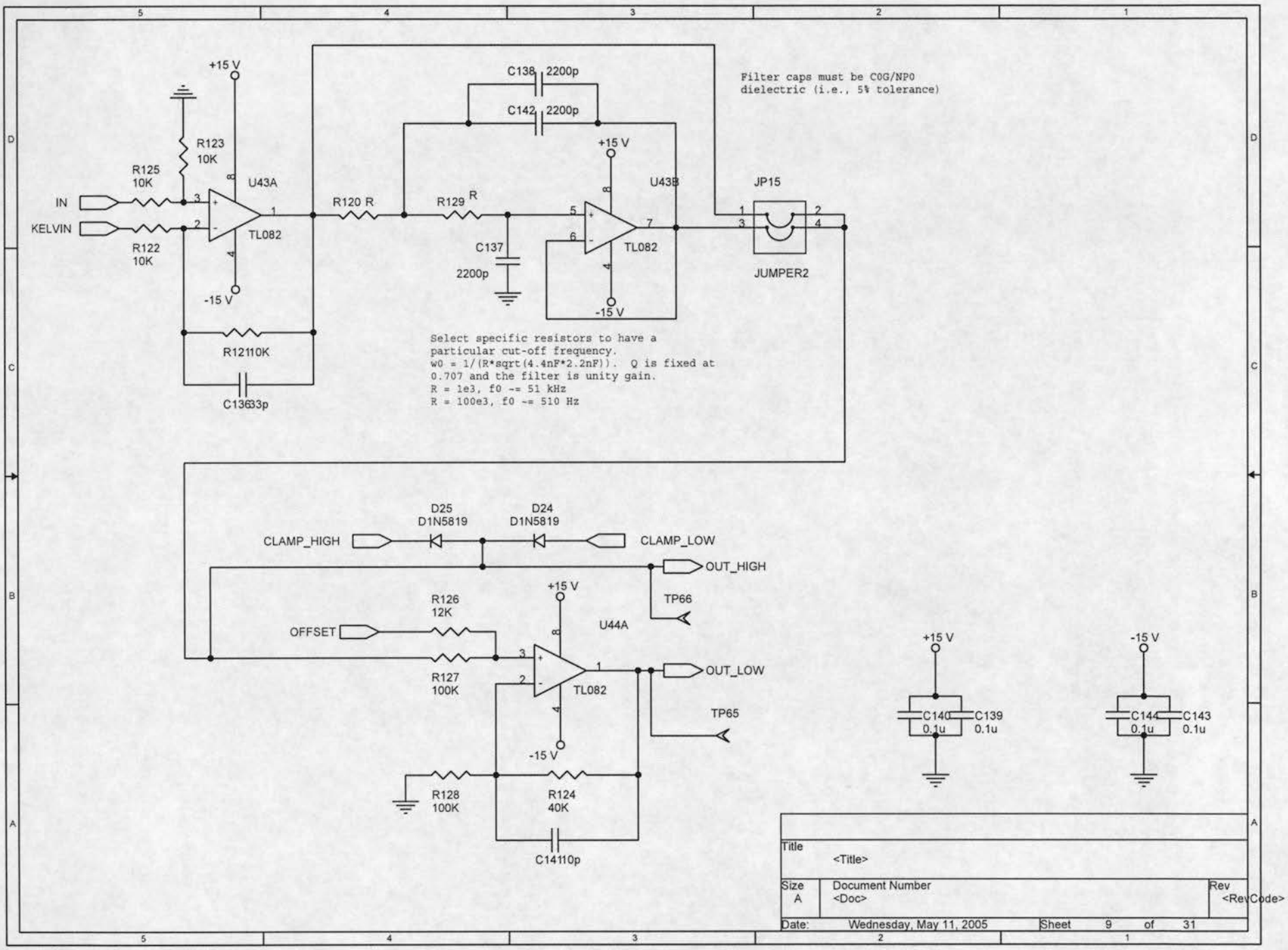
+15 V
C138 2200p
C142 2200p
Filter caps must be C0G/NP0
dielectric (i.e., 5% tolerance)
R123
10K
R125
10K
U43A
U43B
JP15
IN
KELVIN
R120 R
R129 R
R122
10K
TL082
C137
2200p
JUMPER2
-15 V
R12110K
C13633p
Select specific resistors to have a
particular cut-off frequency.
w0 = 1/(R*sqrt(4.4nF*2.2nF)). Q is fixed at
0.707 and the filter is unity gain.
R = 1e3, f0 ~= 51 kHz
R = 100e3, f0 ~= 510 Hz
D25
D1N5819
D24
D1N5819
CLAMP_HIGH
CLAMP_LOW
OUT_HIGH
TP66
R126
12K
U44A
OFFSET
R127
100K
OUT_LOW
TP65
R128
100K
R124
40K
C14110p
C140
0.1u
C139
0.1u
C144
0.1u
C143
0.1u
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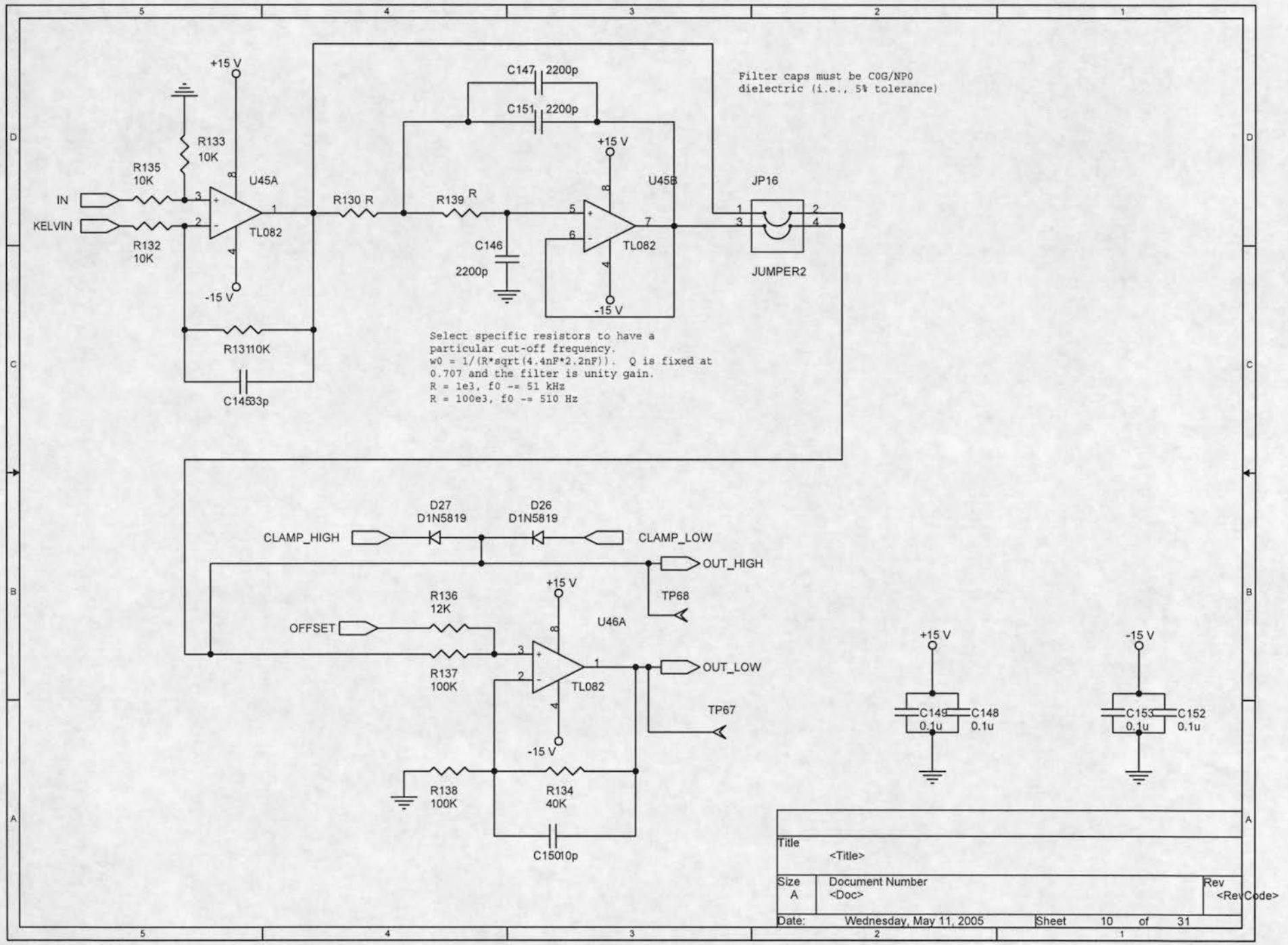
+15 V
C147 2200p
C151 2200p
Filter caps must be C0G/NP0
dielectric (i.e., 5% tolerance)
R133
10K
R135
10K
U45A
U45B
JP16
IN
KELVIN
R132
10K
TL082
R130 R
R139 R
C146
2200p
JUMPER2
-15 V
R13110K
C14533p
Select specific resistors to have a
particular cut-off frequency.
w0 = 1/(R*sqrt(4.4nF*2.2nF)). Q is fixed at
0.707 and the filter is unity gain.
R = 1e3, f0 -= 51 kHz
R = 100e3, f0 -= 510 Hz
D27
D1N5819
D26
D1N5819
CLAMP_HIGH
CLAMP_LOW
OUT_HIGH
TP68
R136
12K
U46A
OFFSET
OUT_LOW
R137
100K
TP67
R138
100K
R134
40K
C15010p
C149
0.1u
C148
0.1u
C153
0.1u
C152
0.1u
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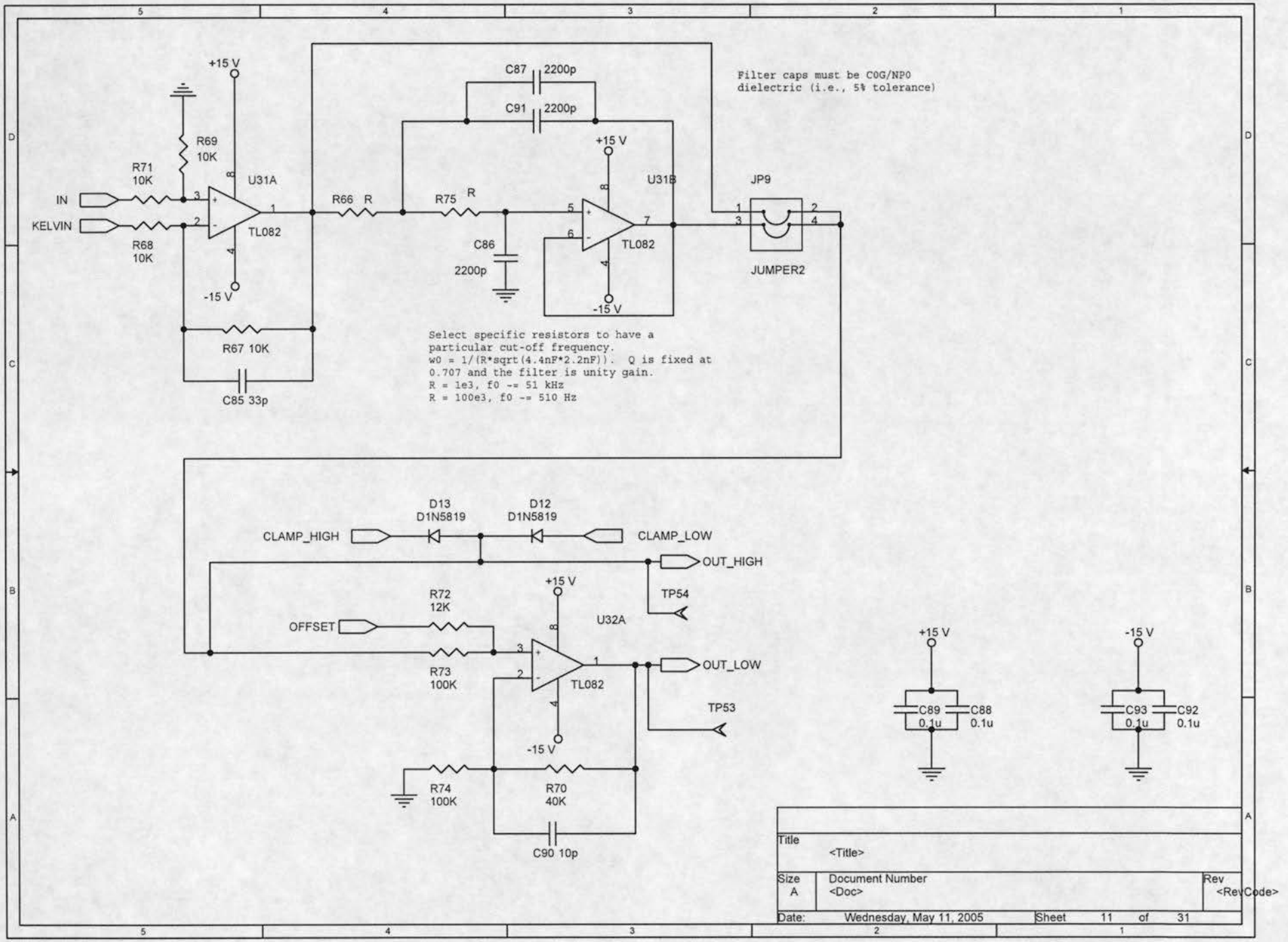
+15 V
C87 2200p
C91 2200p
Filter caps must be C0G/NP0
dielectric (i.e., 5% tolerance)
R69
10K
R71
10K
U31A
U31B
JP9
IN
KELVIN
R68
10K
TL082
R66 R
R75 R
C86
2200p
JUMPER2
-15 V
R67 10K
C85 33p
Select specific resistors to have a
particular cut-off frequency.
w0 = 1/(R*sqrt(4.4nF*2.2nF)). Q is fixed at
0.707 and the filter is unity gain.
R = 1e3, f0 -= 51 kHz
R = 100e3, f0 -= 510 Hz
D13
D1N5819
D12
D1N5819
CLAMP_HIGH
CLAMP_LOW
OUT_HIGH
TP54
R72
12K
OFFSET
U32A
R73
100K
OUT_LOW
TP53
R74
100K
R70
40K
C90 10p
C89
0.1u
C88
0.1u
C93
0.1u
C92
0.1u
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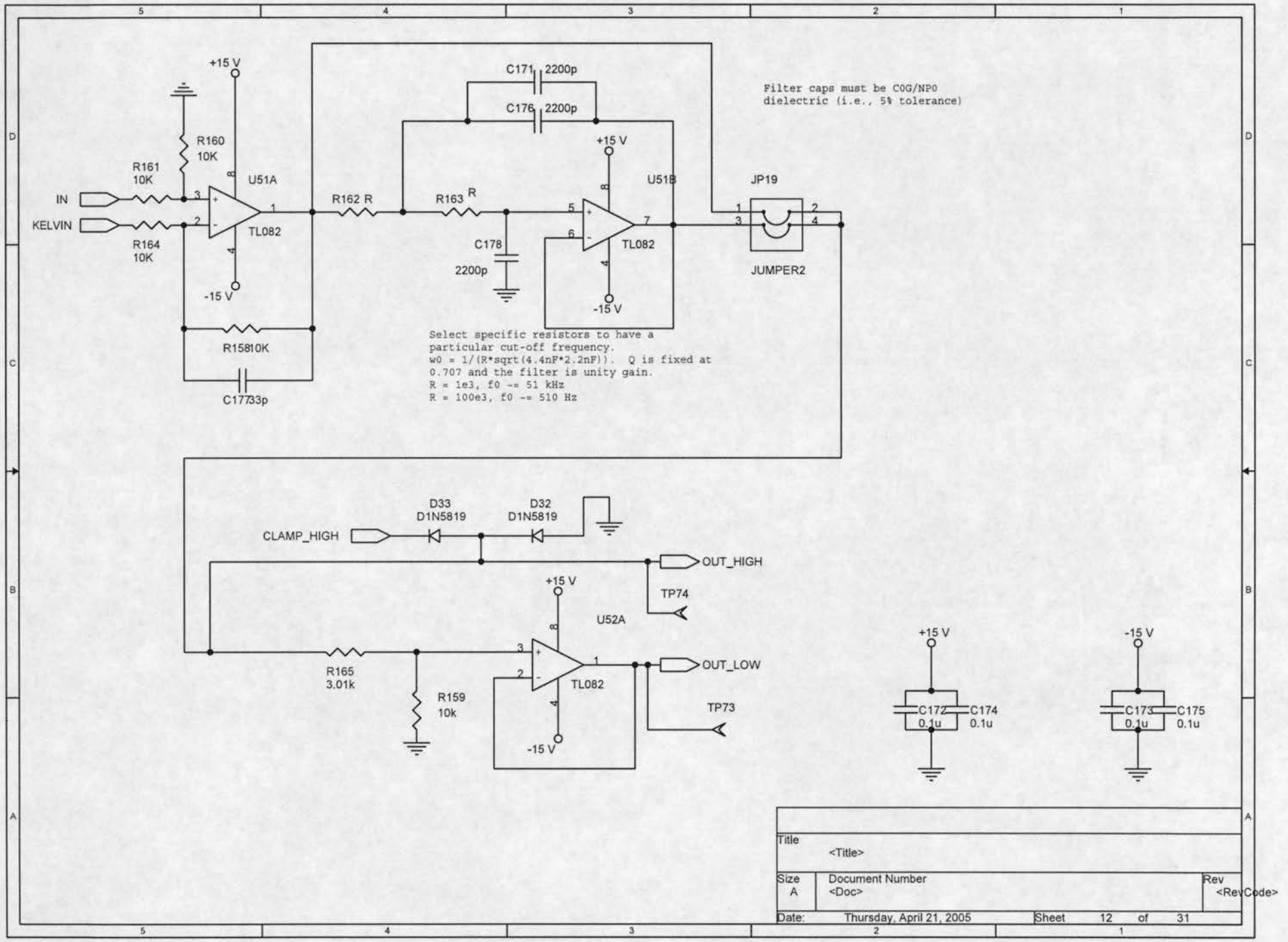
+15 V
C171 2200p
C176 2200p
Filter caps must be C0G/NP0
dielectric (i.e., 5% tolerance)
R160
10K
R161
10K
U51A
U51B
JP19
IN
KELVIN
R164
10K
TL082
R162 R
R163 R
C178
2200p
JUMPER2
-15 V
R15810K
C17733p
Select specific resistors to have a
particular cut-off frequency.
w0 = 1/(R*sqrt(4.4nF*2.2nF)). Q is fixed at
0.707 and the filter is unity gain.
R = 1e3, f0 -= 51 kHz
R = 100e3, f0 -= 510 Hz
D33
D1N5819
D32
D1N5819
CLAMP_HIGH
OUT_HIGH
TP74
U52A
R165
3.01k
R159
10k
OUT_LOW
TP73
C172
0.1u
C174
0.1u
C173
0.1u
C175
0.1u
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<Title>
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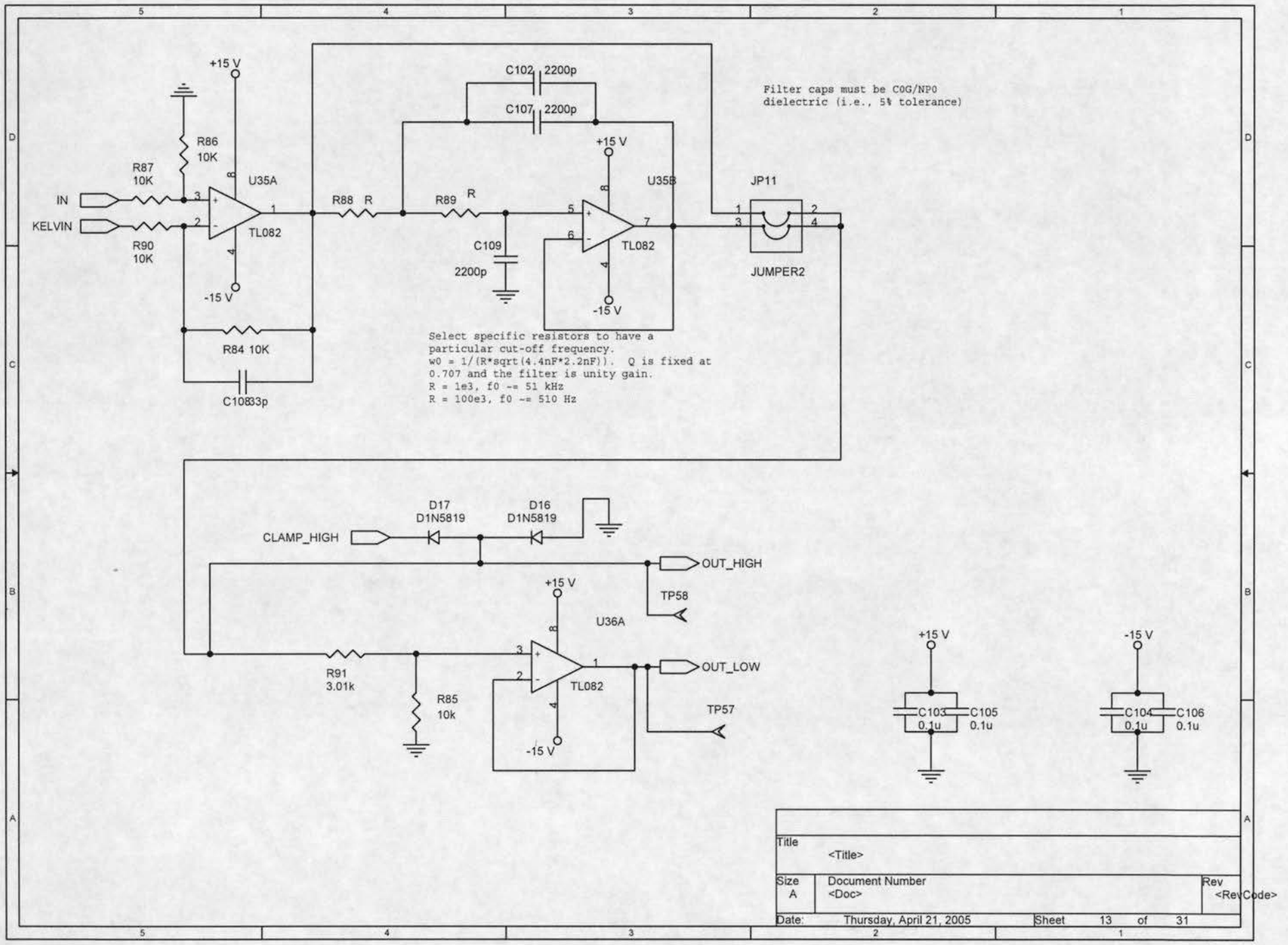

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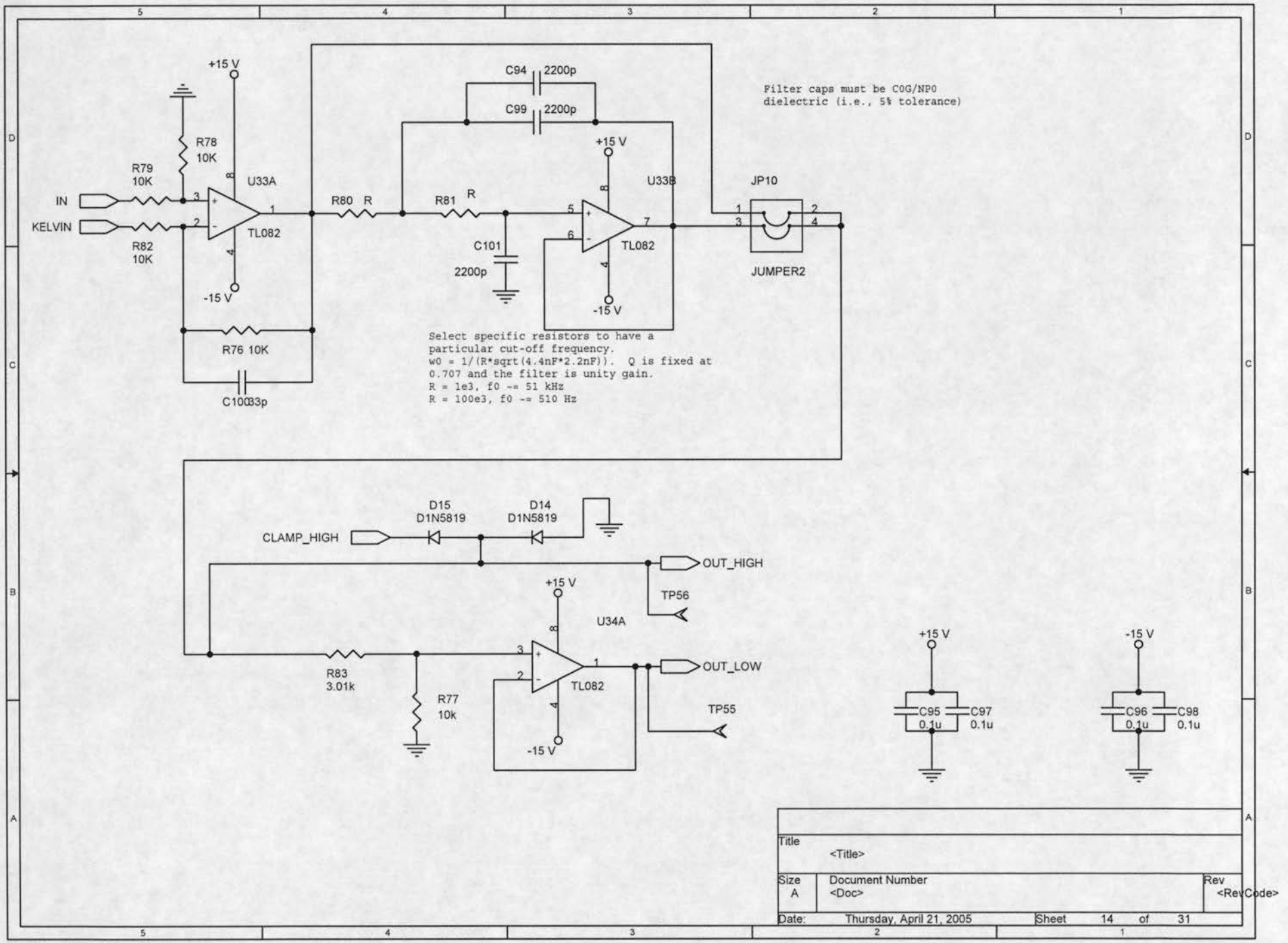

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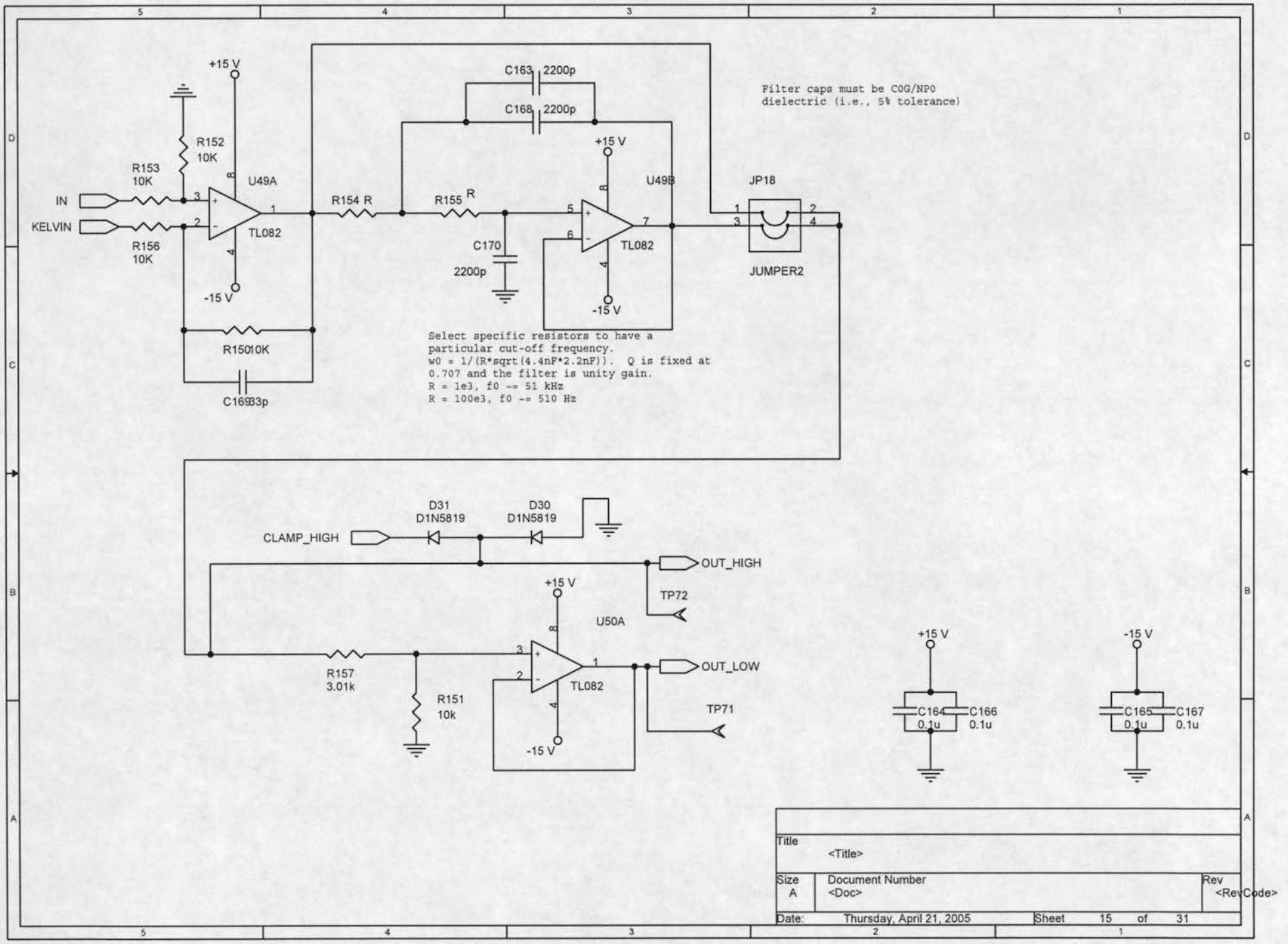

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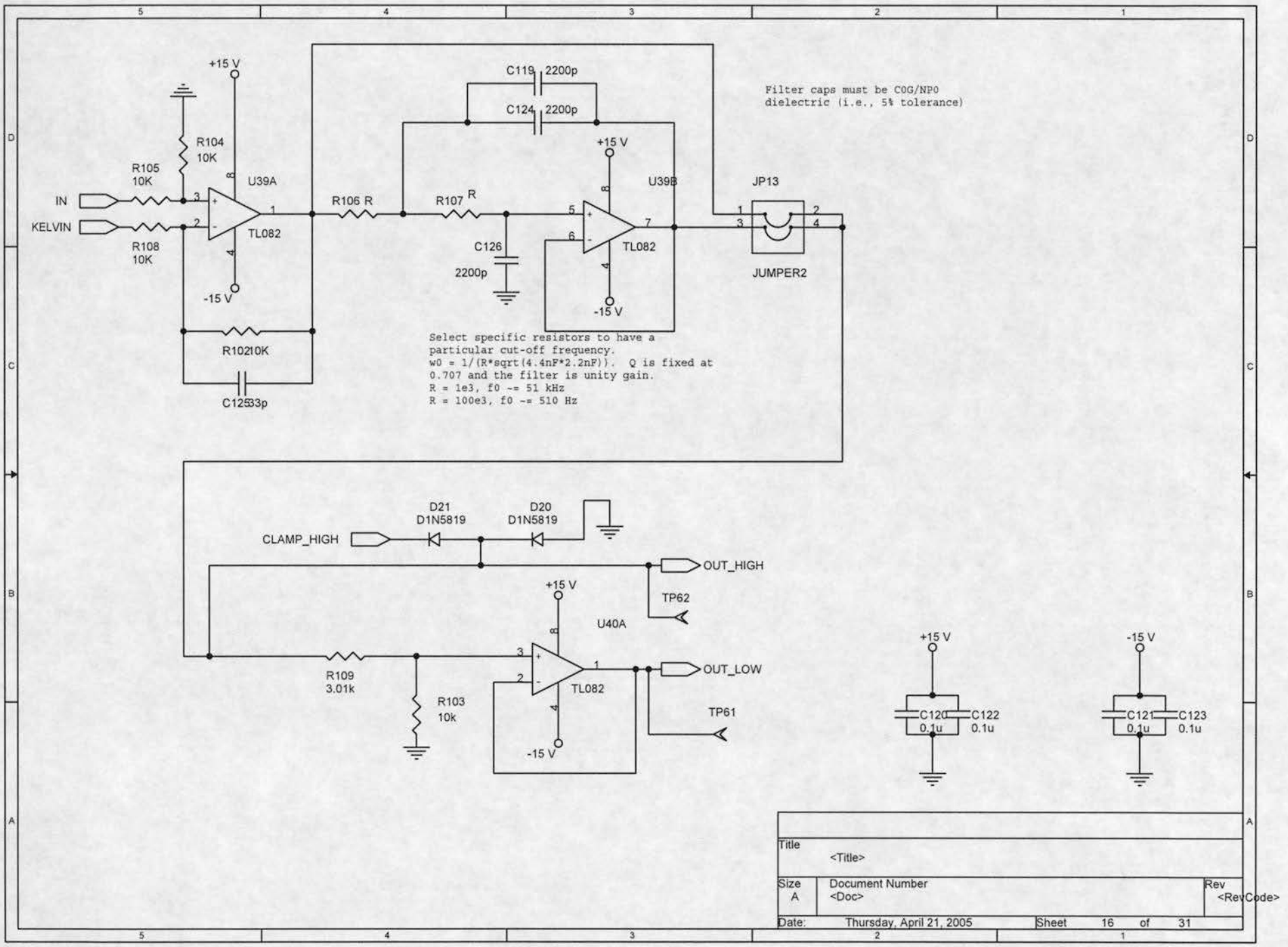

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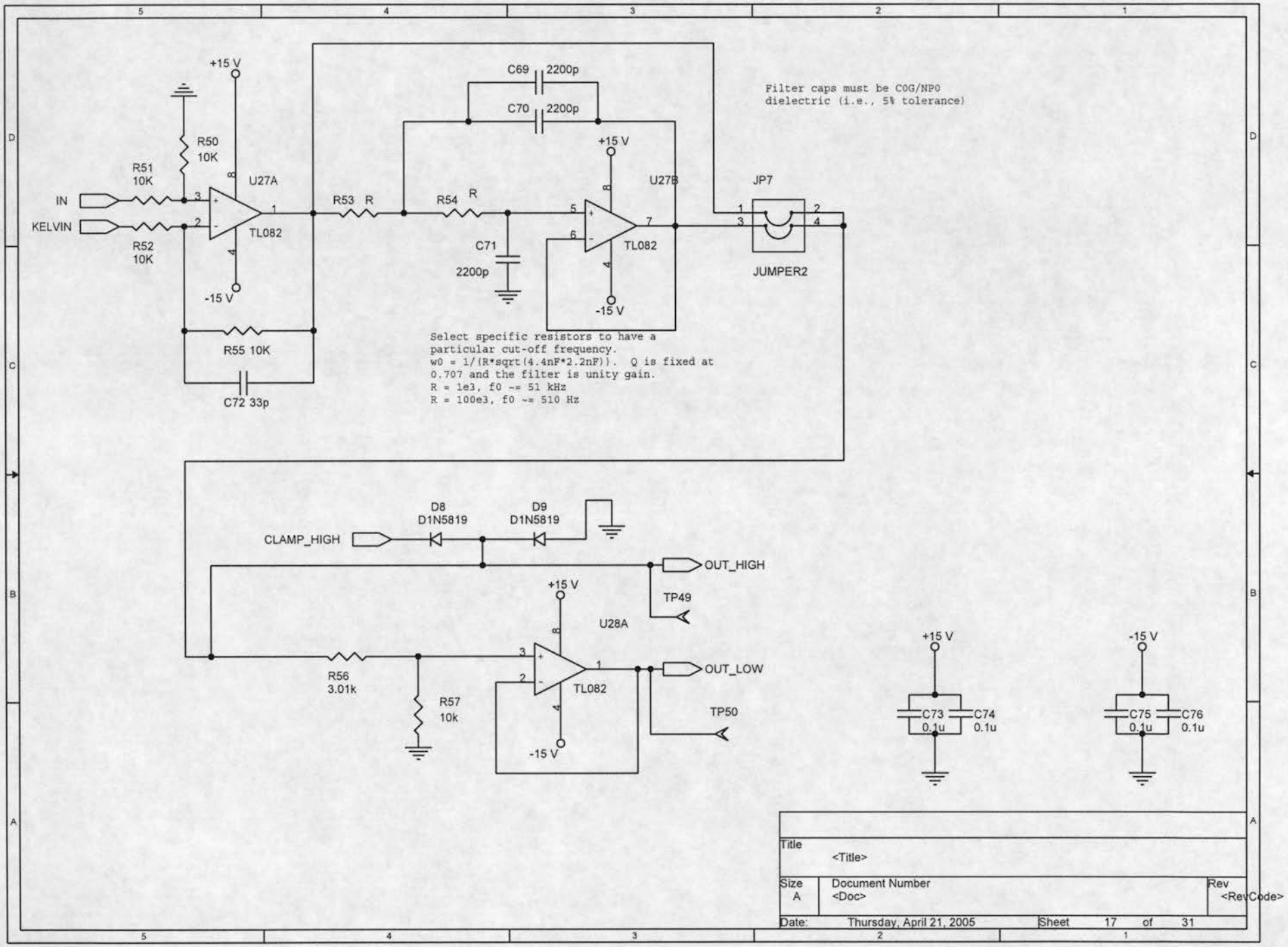

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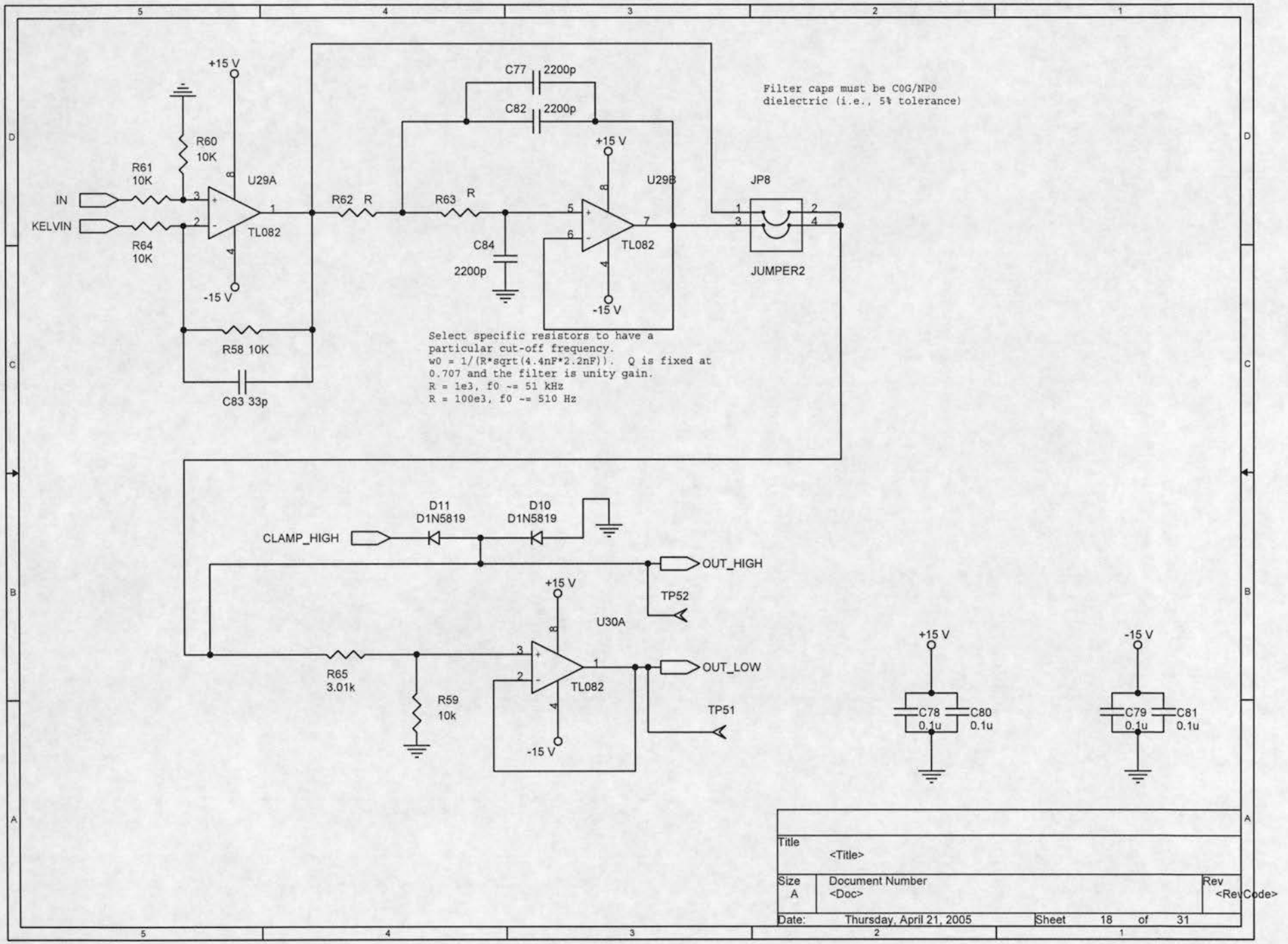

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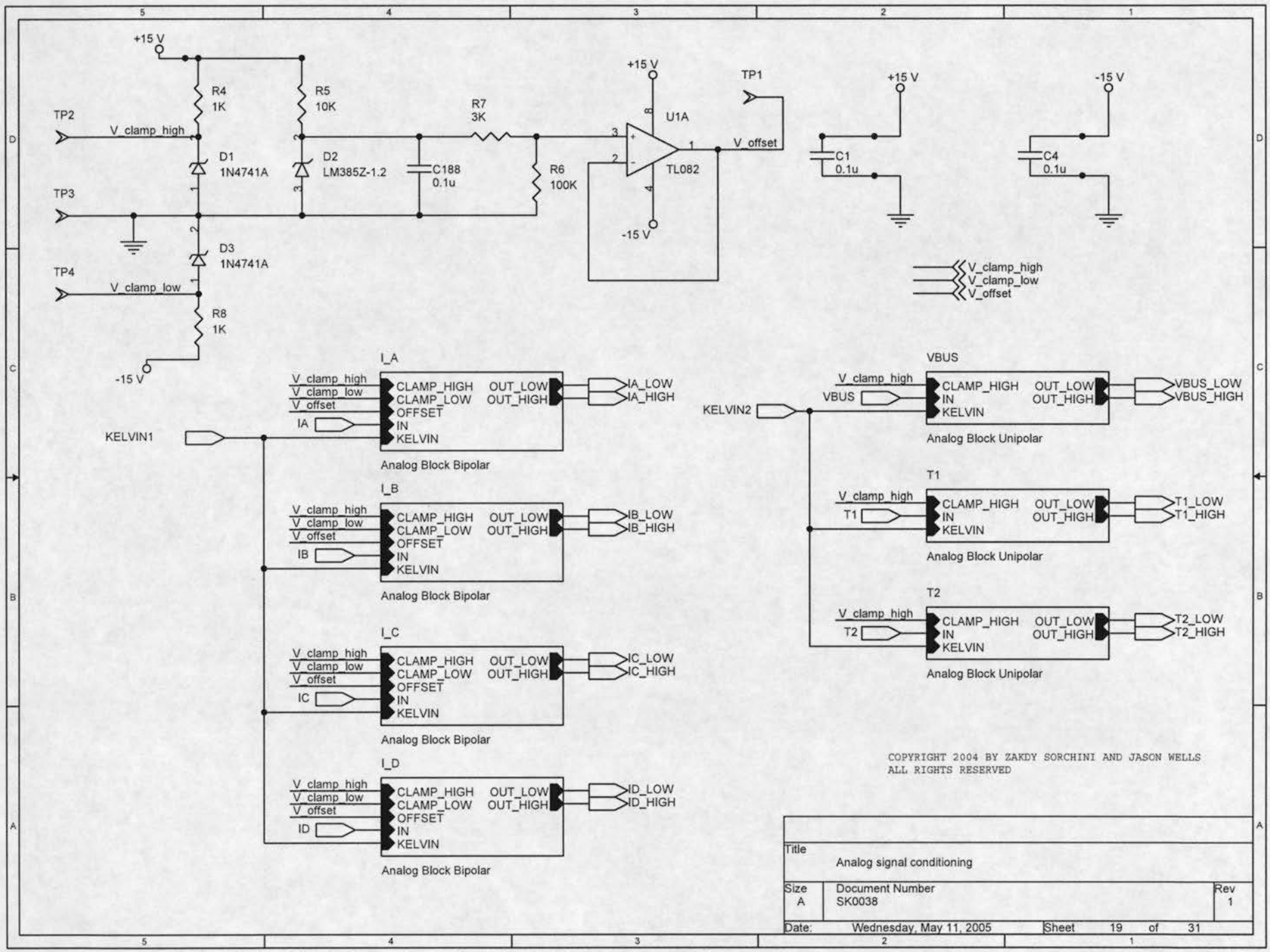

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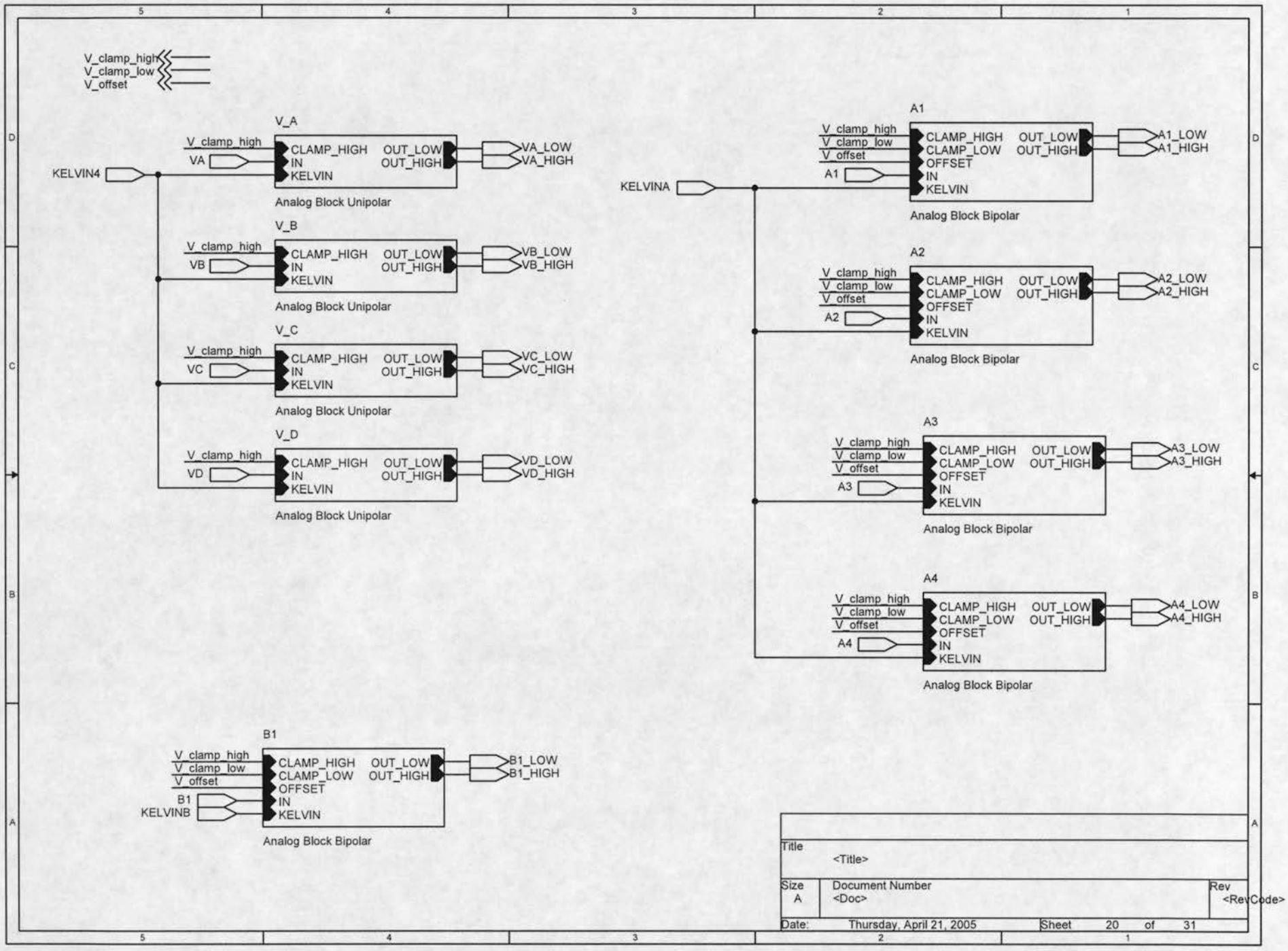
V_clamp_high
V_clamp_low
V_offset
V_A
V_clamp_high
VA
KELVIN4
CLAMP_HIGH
IN
KELVIN
OUT_LOW
OUT_HIGH
VA_LOW
VA_HIGH
Analog Block Unipolar
V_B
V_clamp_high
VB
CLAMP_HIGH
IN
KELVIN
OUT_LOW
OUT_HIGH
VB_LOW
VB_HIGH
Analog Block Unipolar
V_C
V_clamp_high
VC
CLAMP_HIGH
IN
KELVIN
OUT_LOW
OUT_HIGH
VC_LOW
VC_HIGH
Analog Block Unipolar
V_D
V_clamp_high
VD
CLAMP_HIGH
IN
KELVIN
OUT_LOW
OUT_HIGH
VD_LOW
VD_HIGH
Analog Block Unipolar
A1
V_clamp_high
V_clamp_low
V_offset
A1
KELVINA
CLAMP_HIGH
CLAMP_LOW
OFFSET
IN
KELVIN
OUT_LOW
OUT_HIGH
A1_LOW
A1_HIGH
Analog Block Bipolar
A2
V_clamp_high
V_clamp_low
V_offset
A2
CLAMP_HIGH
CLAMP_LOW
OFFSET
IN
KELVIN
OUT_LOW
OUT_HIGH
A2_LOW
A2_HIGH
Analog Block Bipolar
A3
V_clamp_high
V_clamp_low
V_offset
A3
CLAMP_HIGH
CLAMP_LOW
OFFSET
IN
KELVIN
OUT_LOW
OUT_HIGH
A3_LOW
A3_HIGH
Analog Block Bipolar
A4
V_clamp_high
V_clamp_low
V_offset
A4
CLAMP_HIGH
CLAMP_LOW
OFFSET
IN
KELVIN
OUT_LOW
OUT_HIGH
A4_LOW
A4_HIGH
Analog Block Bipolar
B1
V_clamp_high
V_clamp_low
V_offset
B1
KELVINB
CLAMP_HIGH
CLAMP_LOW
OFFSET
IN
KELVIN
OUT_LOW
OUT_HIGH
B1_LOW
B1_HIGH
Analog Block Bipolar
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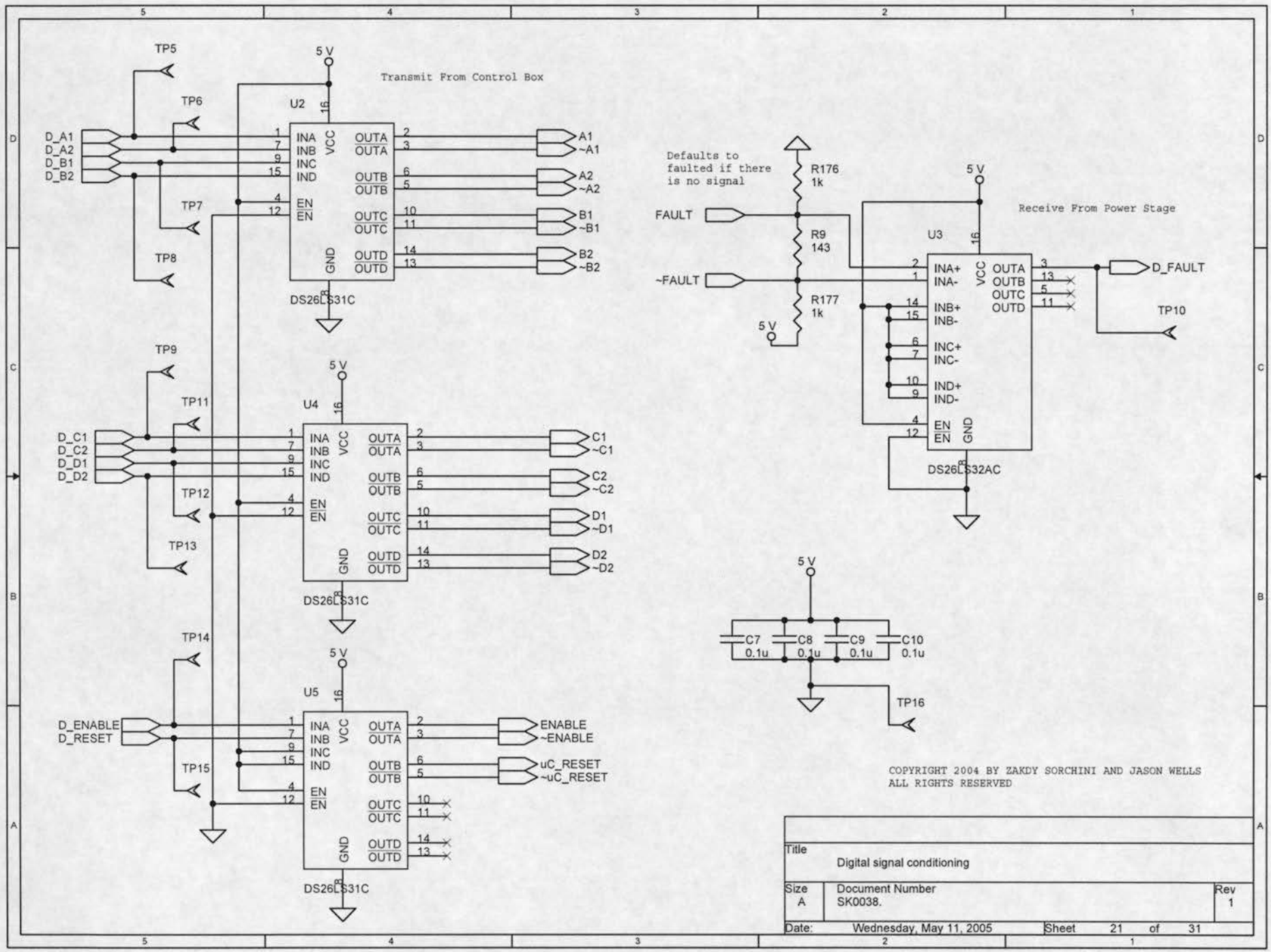
Transmit From Control Box
TP5
TP6
TP7
TP8
5 V
U2
D_A1
D_A2
D_B1
D_B2
INA
INB
INC
IND
EN
EN
VCC
GND
OUTA
OUTA
OUTB
OUTB
OUTC
OUTC
OUTD
OUTD
A1
~A1
A2
~A2
B1
~B1
B2
~B2
DS26LS31C
Defaults to faulted if there is no signal
R176 1k
R9 143
R177 1k
FAULT
~FAULT
Receive From Power Stage
U3
INA+
INA-
INB+
INB-
INC+
INC-
IND+
IND-
D_FAULT
TP10
DS26LS32AC
TP9
TP11
TP12
TP13
U4
D_C1
D_C2
D_D1
D_D2
C1
~C1
C2
~C2
D1
~D1
D2
~D2
TP14
TP15
U5
D_ENABLE
D_RESET
ENABLE
~ENABLE
uC_RESET
~uC_RESET
C7 0.1u
C8 0.1u
C9 0.1u
C10 0.1u
TP16
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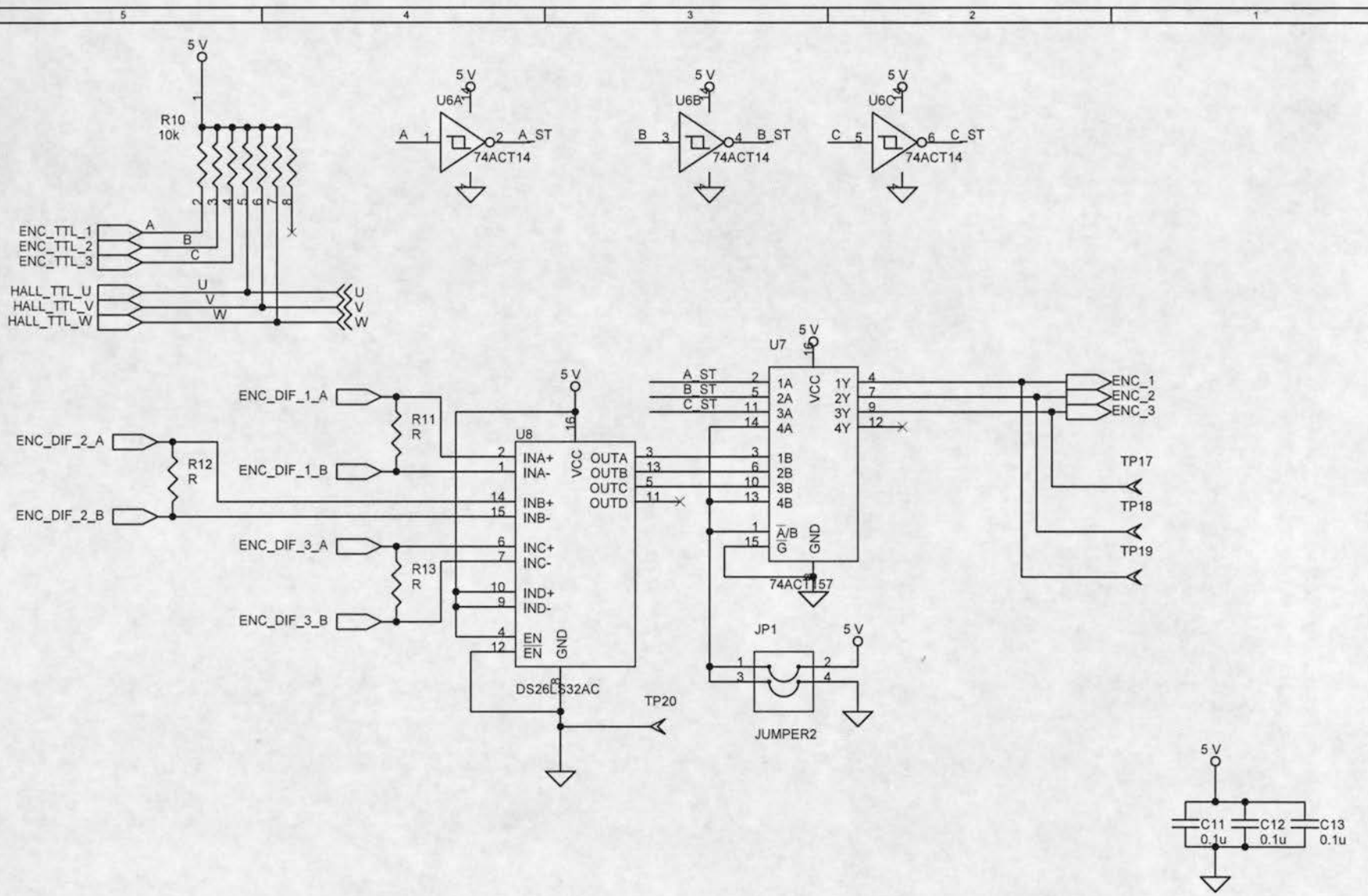

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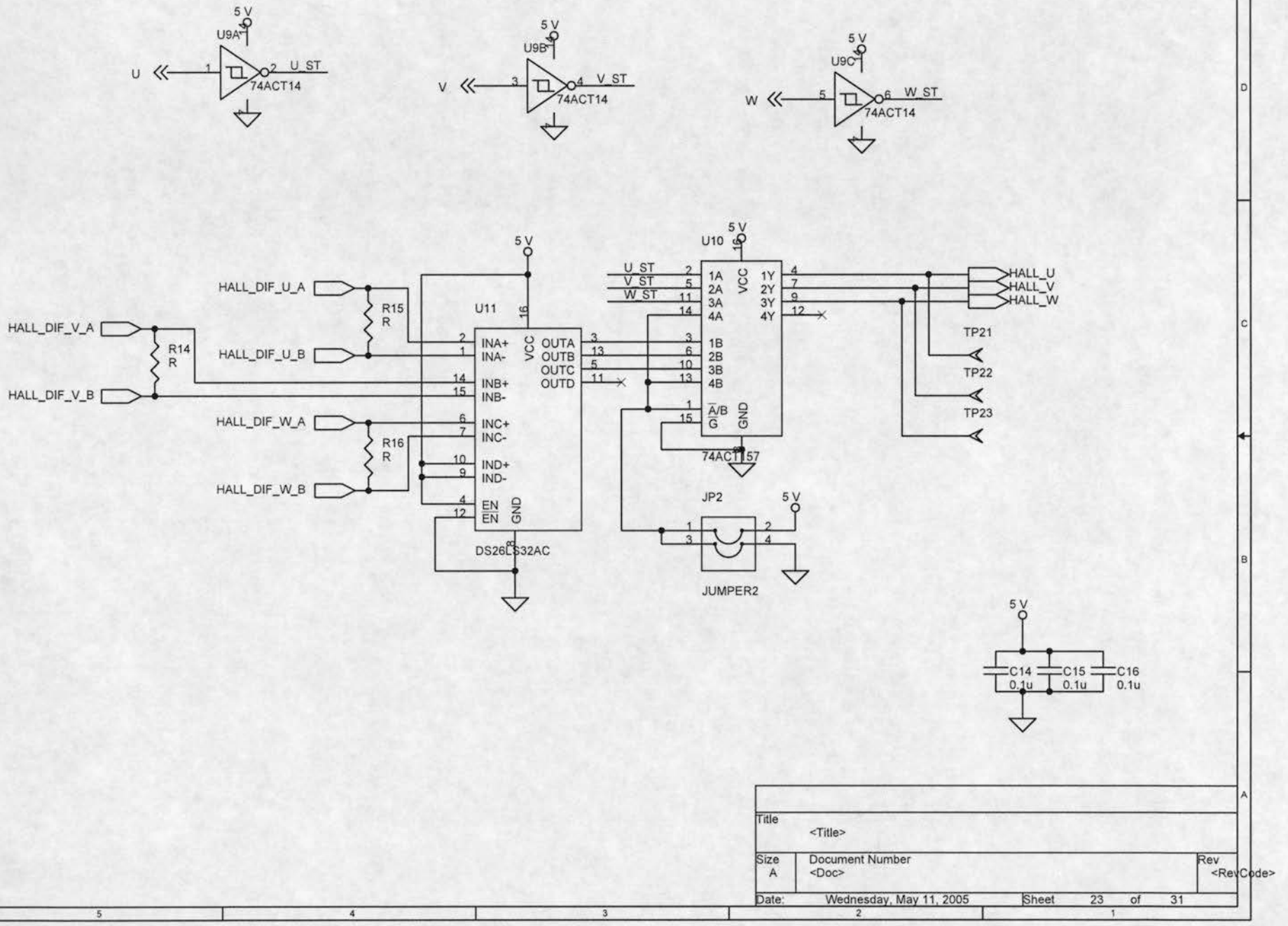

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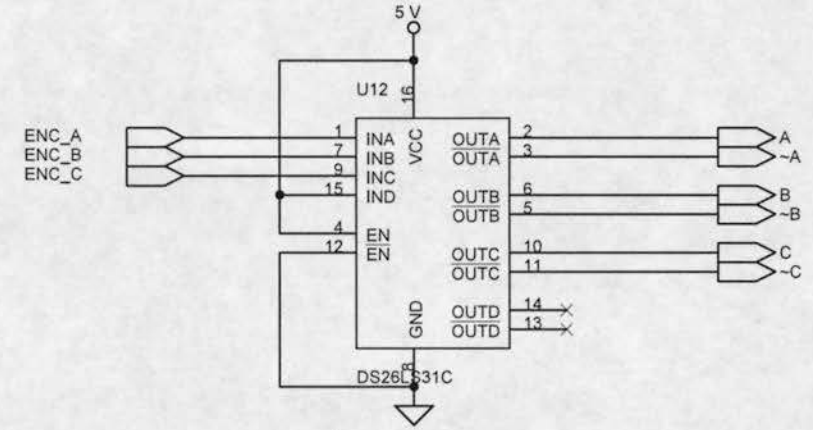

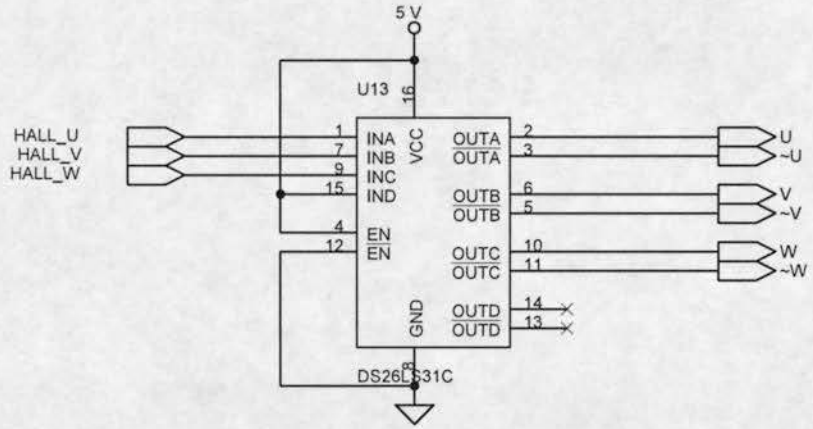

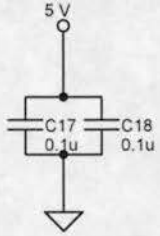

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Title: Encoder and Hall Retransmit		
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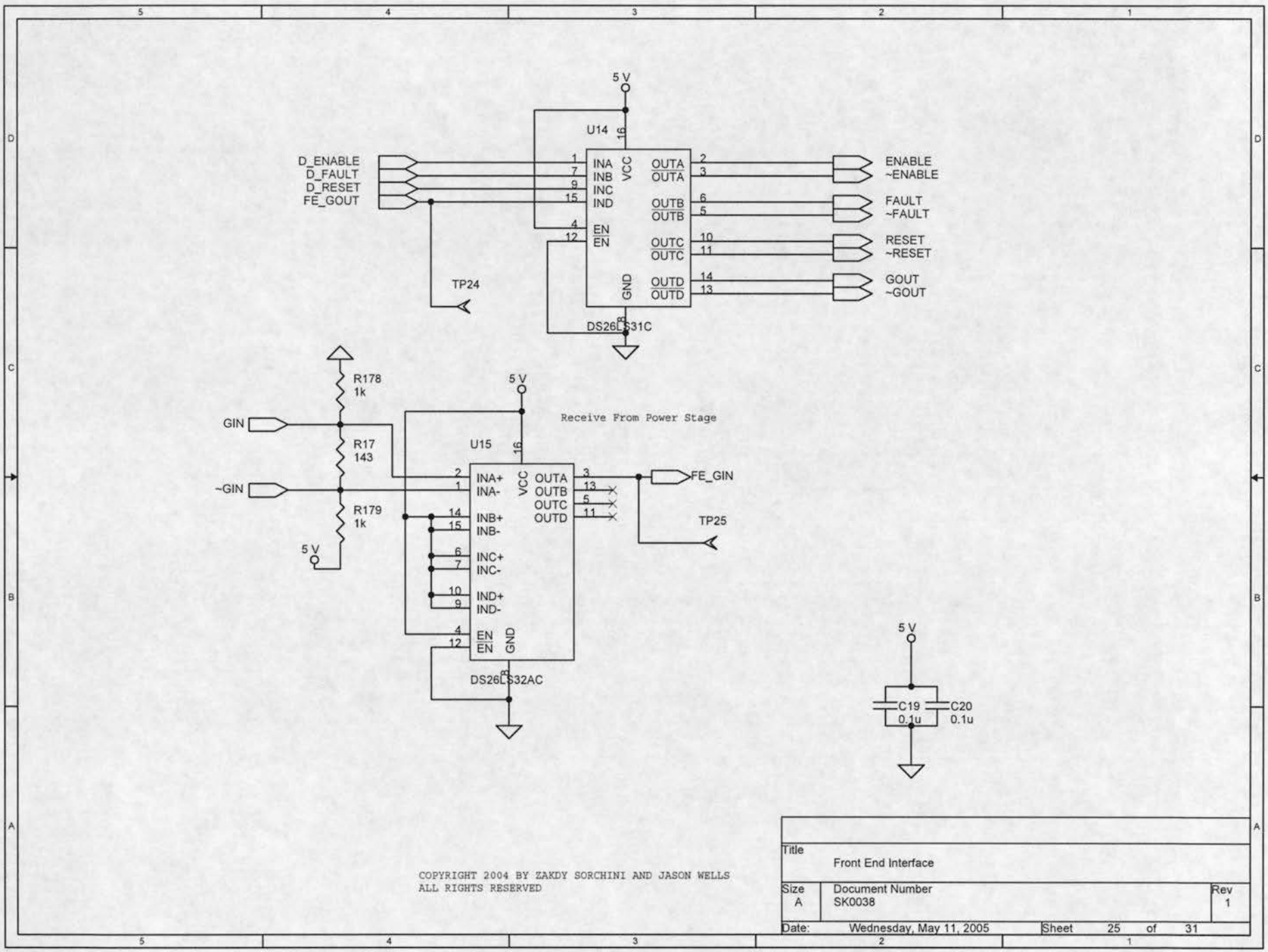

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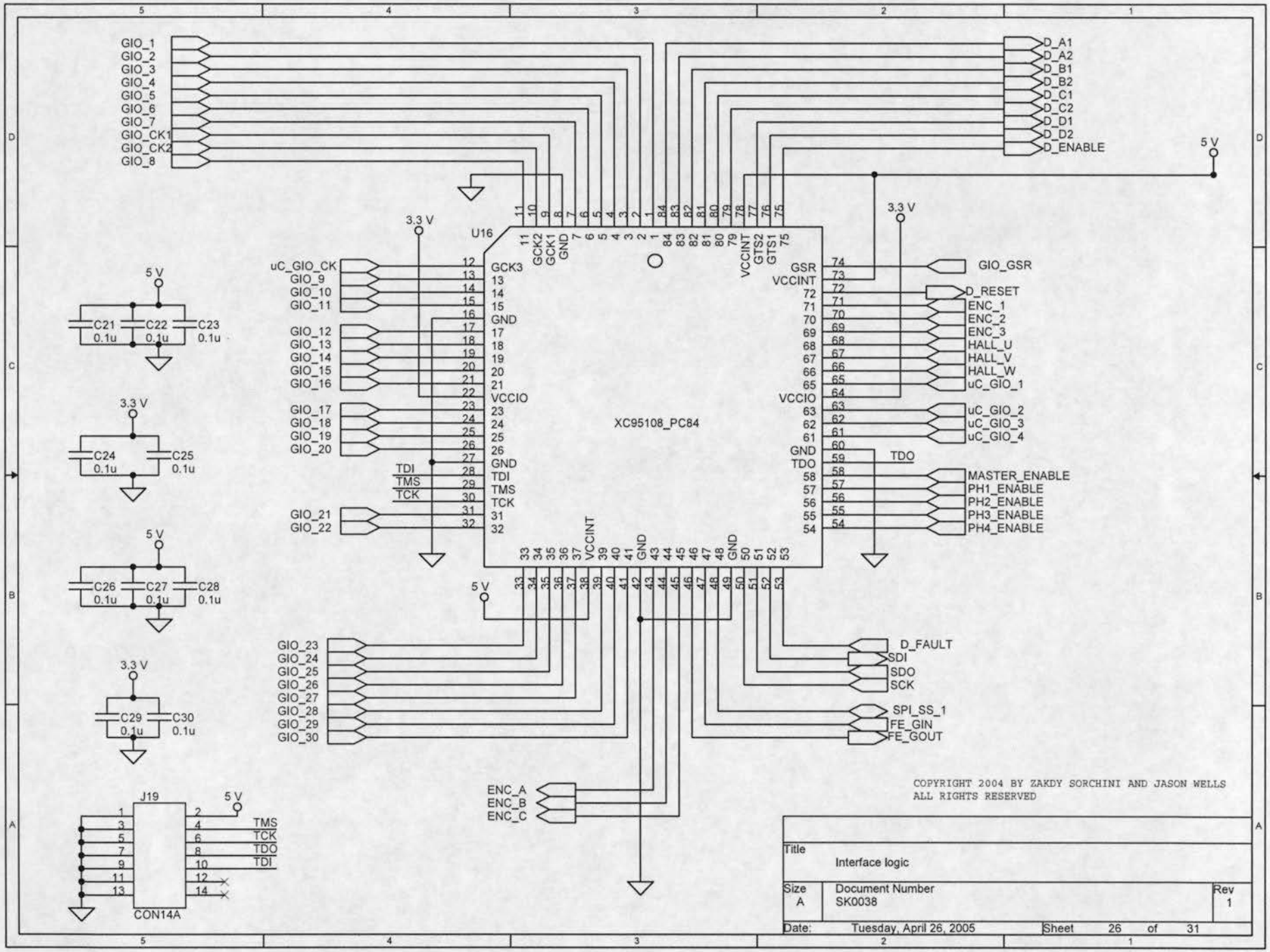

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Title: Interface logic		
Size: A	Document Number: SK0038	Rev: 1
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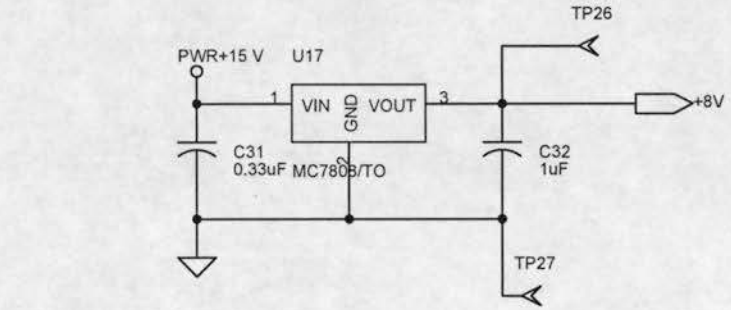

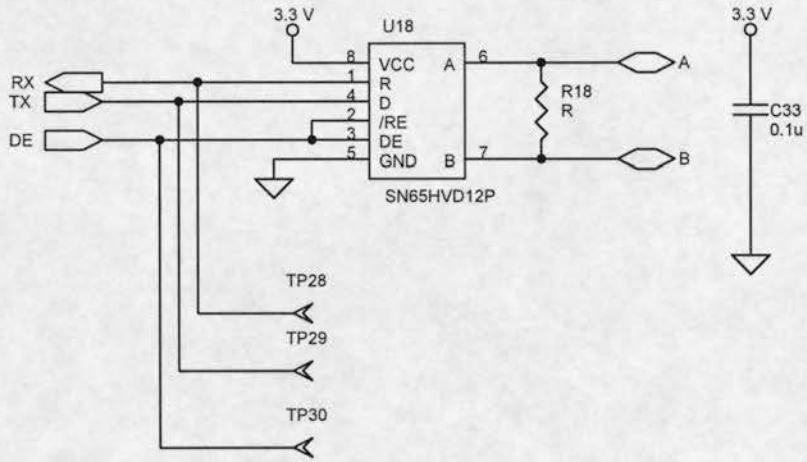

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Title	Keypad interface for Baldor Smart Motor keypad	
Size A	Document Number SK0038	Rev 1
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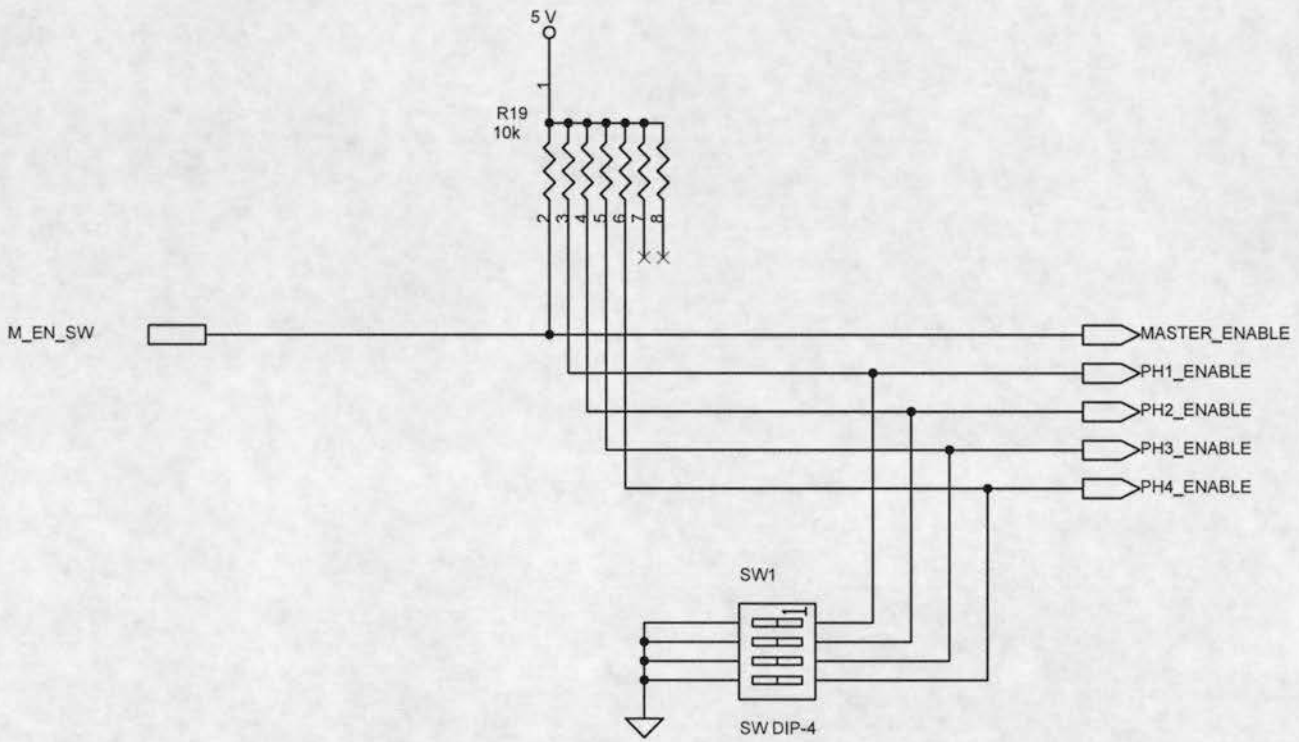

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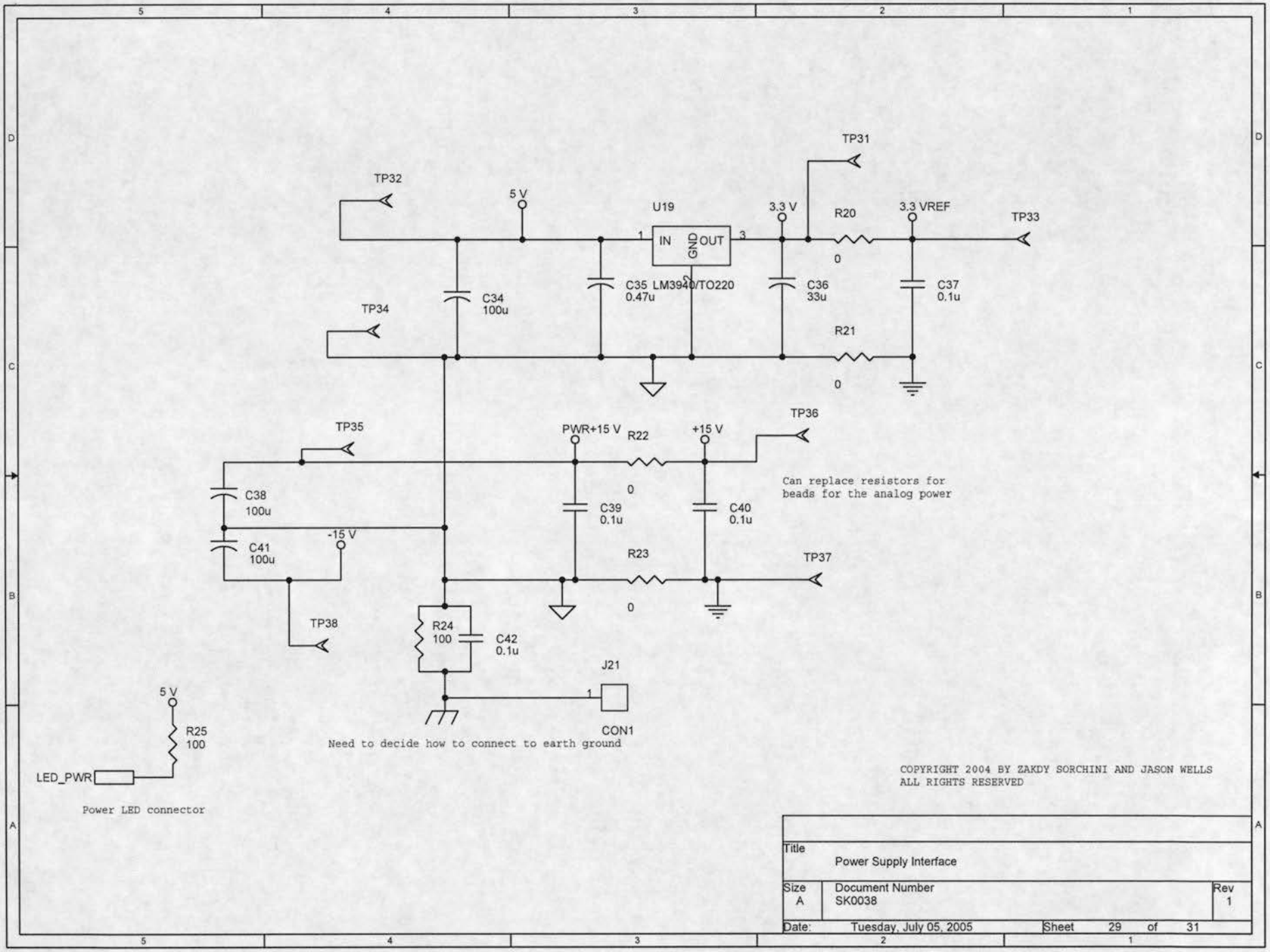
Size A	Document Number <Doc>	Rev <RevCode>
Date: Wednesday, May 11, 2005	Sheet 28 of 31	



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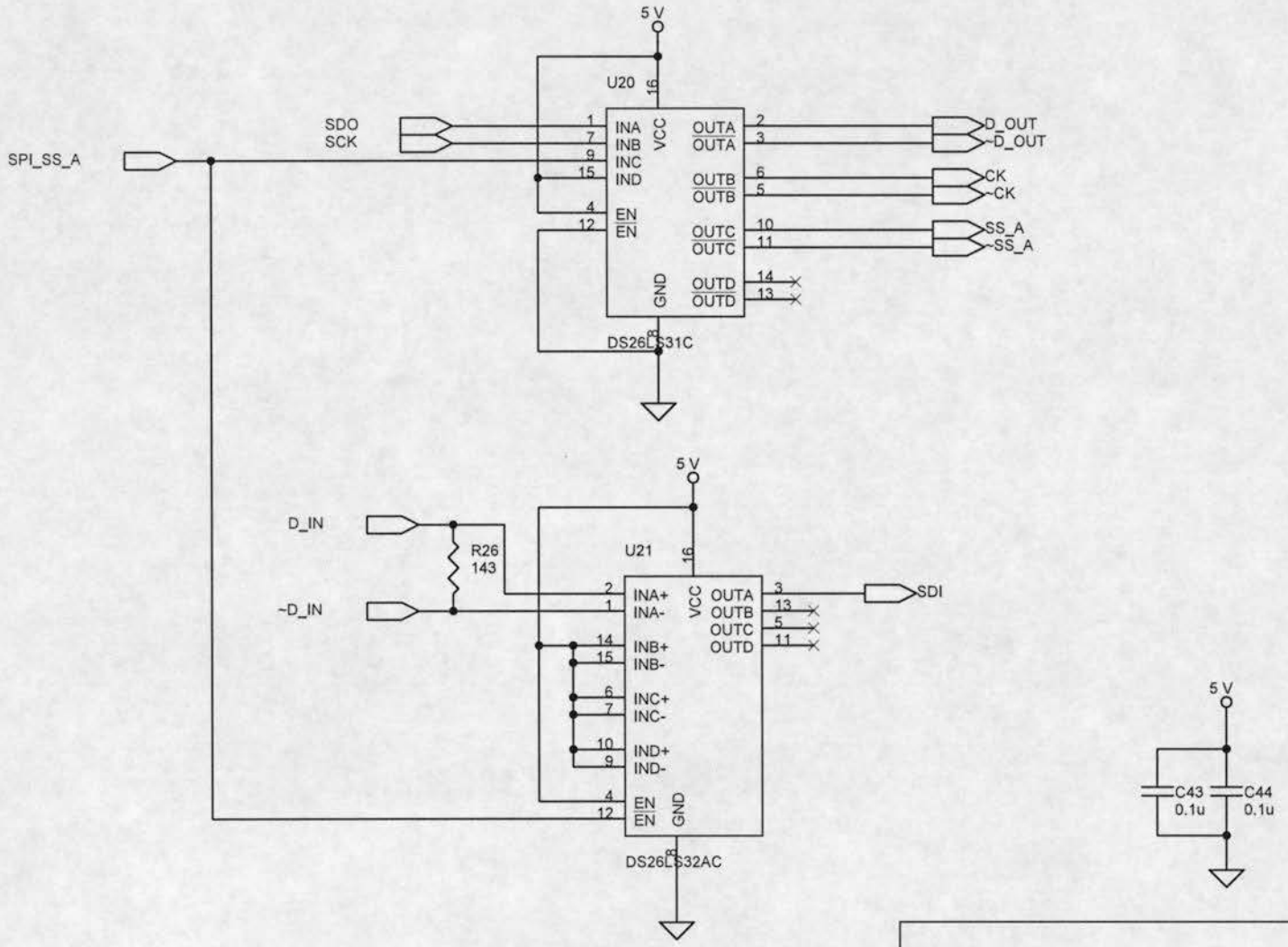
Title	Power Supply Interface	
Size A	Document Number SK0038	Rev 1
Date: Tuesday, July 05, 2005	Sheet 29 of 31	



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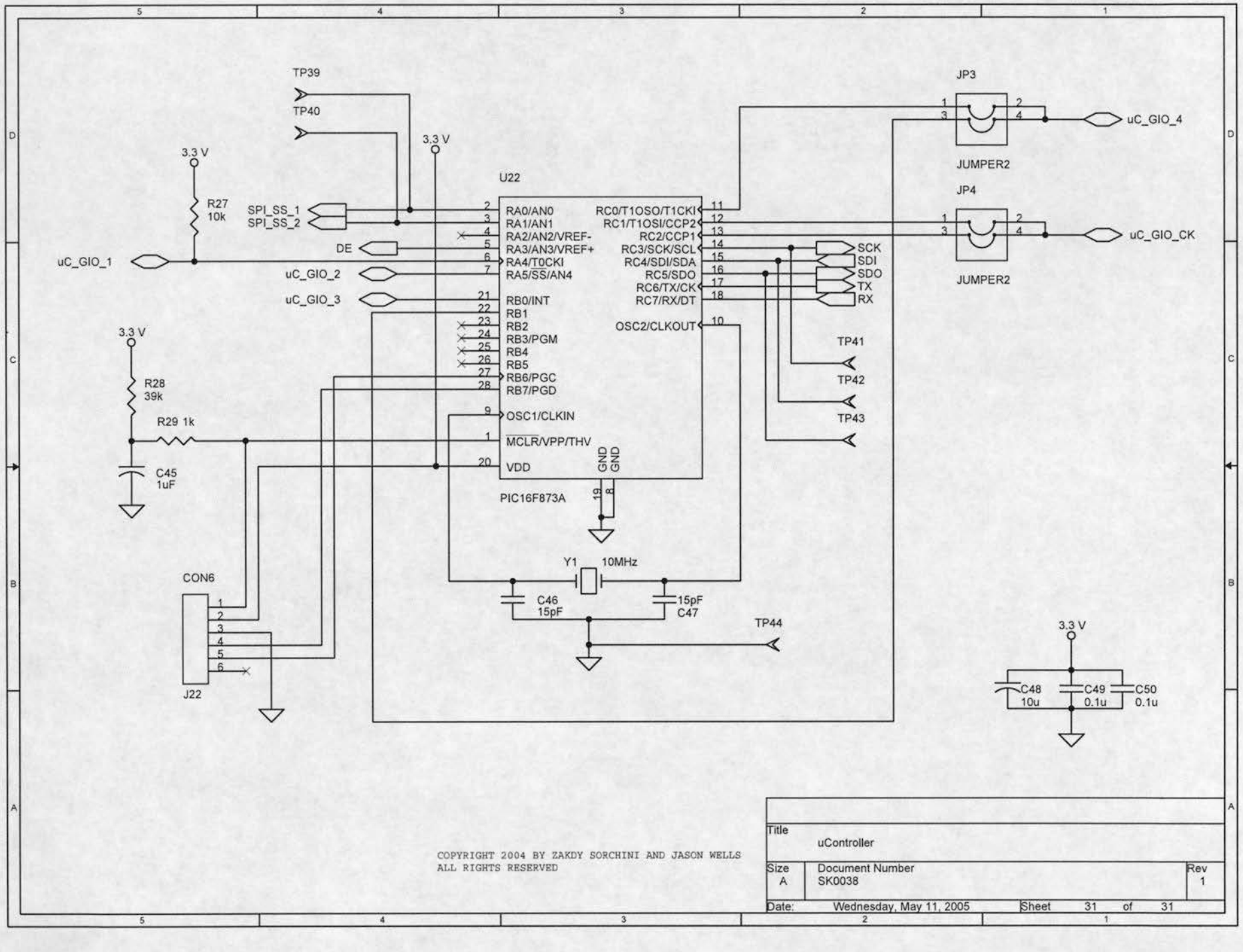
Title	SPI Bus Interface	
Size A	Document Number SK0038	Rev 1
Date: Thursday, April 21, 2005	Sheet 30 of 31	



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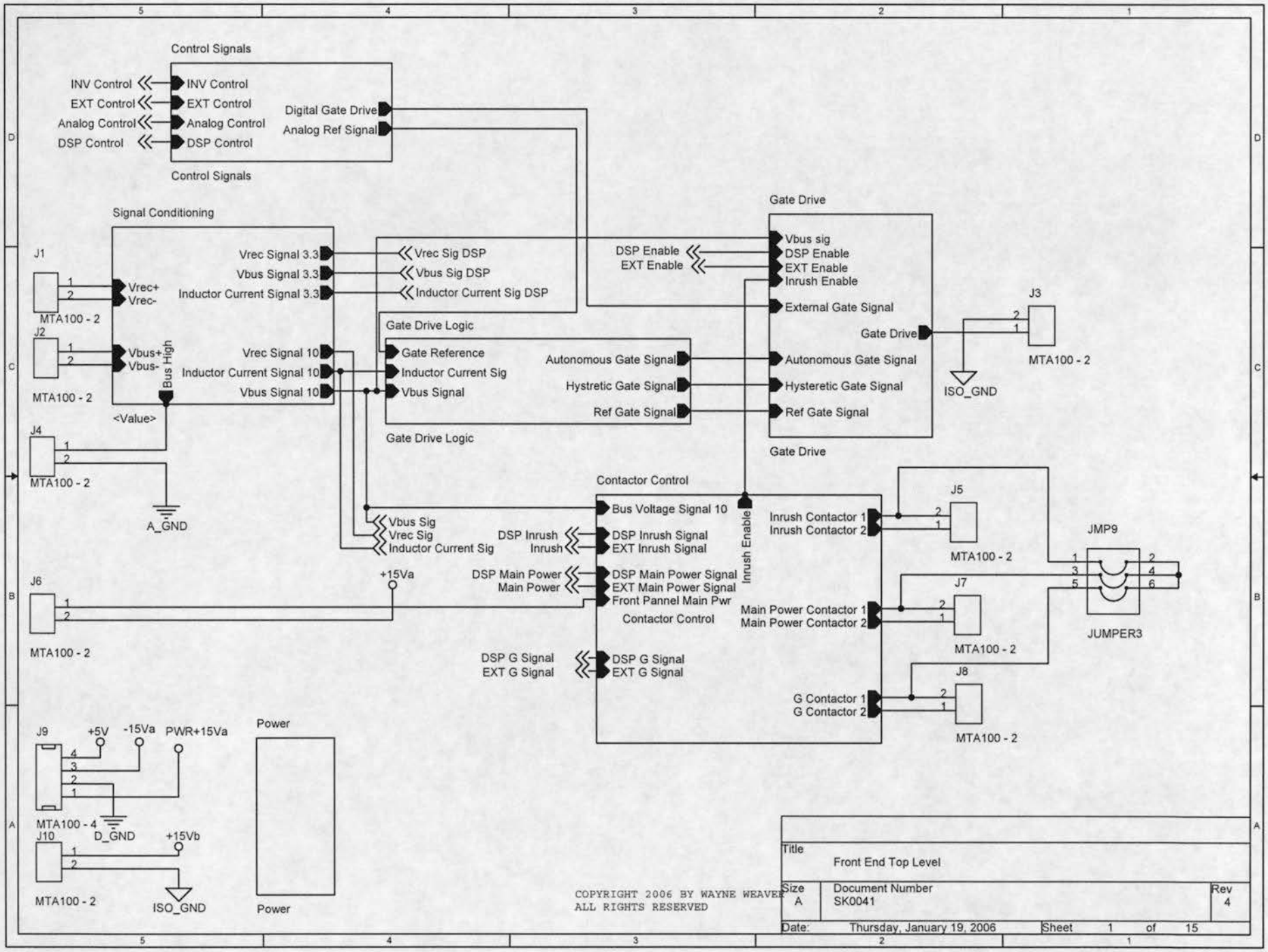
Title	uController	
Size A	Document Number SK0038	Rev 1
Date: Wednesday, May 11, 2005	Sheet 31 of 31	


Control Signals
INV Control
EXT Control
Analog Control
DSP Control
Digital Gate Drive
Analog Ref Signal
Control Signals
Signal Conditioning
J1
Vrec+
Vrec-
MTA100 - 2
J2
Vbus+
Vbus-
Bus High
MTA100 - 2
<Value>
J4
MTA100 - 2
A_GND
Vrec Signal 3.3
Vbus Signal 3.3
Inductor Current Signal 3.3
Vrec Signal 10
Inductor Current Signal 10
Vbus Signal 10
Vrec Sig DSP
Vbus Sig DSP
Inductor Current Sig DSP
Gate Drive Logic
Gate Reference
Inductor Current Sig
Vbus Signal
Autonomous Gate Signal
Hystretic Gate Signal
Ref Gate Signal
Gate Drive Logic
Gate Drive
DSP Enable
EXT Enable
Vbus sig
DSP Enable
EXT Enable
Inrush Enable
External Gate Signal
Gate Drive
Autonomous Gate Signal
Hysteretic Gate Signal
Ref Gate Signal
Gate Drive
J3
MTA100 - 2
ISO_GND
Contactor Control
Bus Voltage Signal 10
Vbus Sig
Vrec Sig
Inductor Current Sig
DSP Inrush
Inrush
DSP Inrush Signal
EXT Inrush Signal
DSP Main Power
Main Power
DSP Main Power Signal
EXT Main Power Signal
Front Pannel Main Pwr
Contactor Control
Inrush Enable
+15Va
J6
MTA100 - 2
DSP G Signal
EXT G Signal
DSP G Signal
EXT G Signal
Inrush Contactor 1
Inrush Contactor 2
J5
MTA100 - 2
JMP9
Main Power Contactor 1
Main Power Contactor 2
J7
MTA100 - 2
JUMPER3
G Contactor 1
G Contactor 2
J8
MTA100 - 2
J9
+5V
-15Va
PWR+15Va
MTA100 - 4
D_GND
J10
+15Vb
MTA100 - 2
ISO_GND
Power
Power
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Title
Front End Top Level
Size
A
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SK0041
Rev
4
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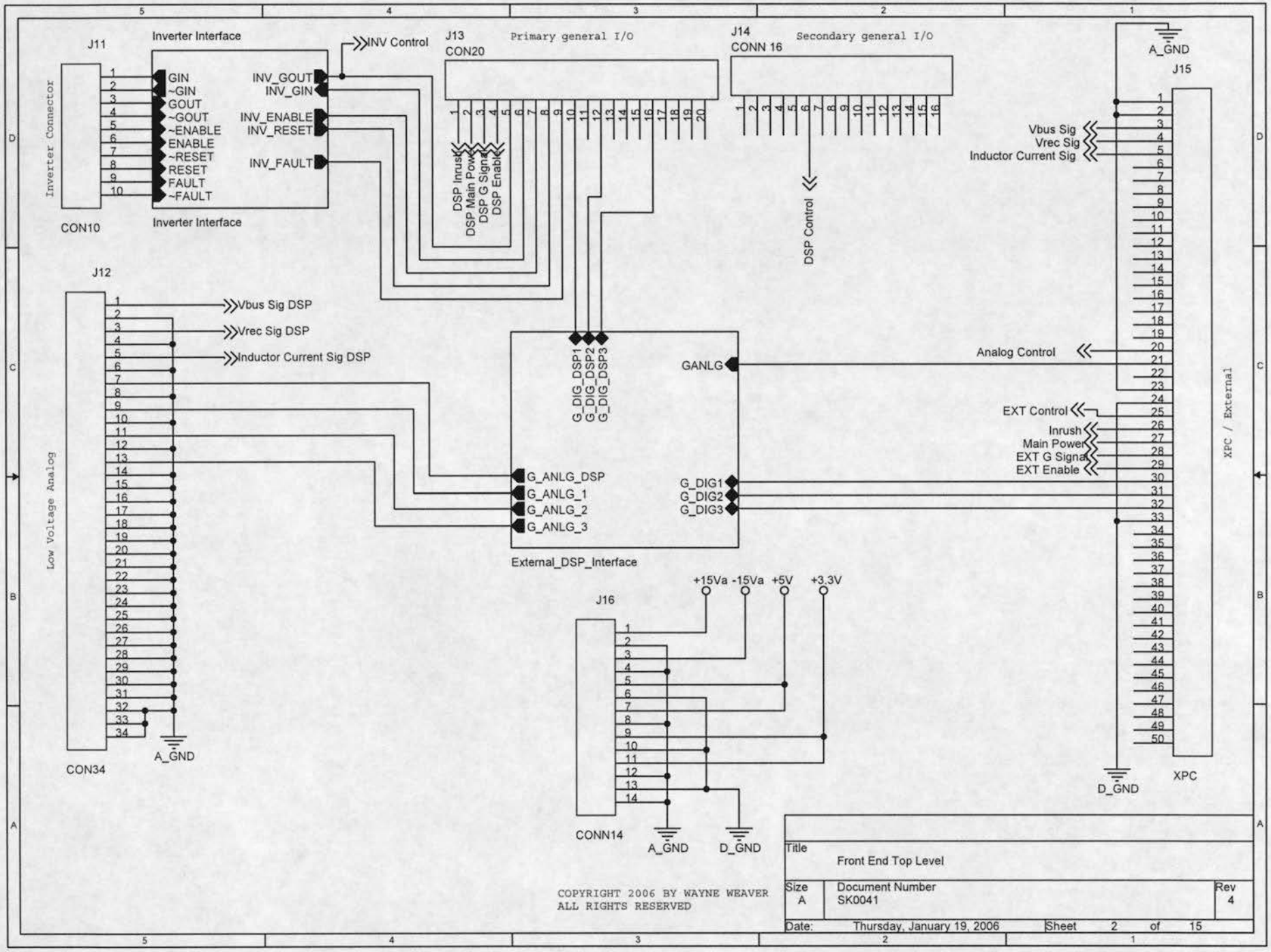
J11
Inverter Interface
Inverter Connector
GIN
~GIN
GOUT
~GOUT
~ENABLE
ENABLE
~RESET
RESET
FAULT
~FAULT
INV_GOUT
INV_GIN
INV_ENABLE
INV_RESET
INV_FAULT
CON10
Inverter Interface
INV Control
J13
CON20
Primary general I/O
DSP Inrush
DSP Main Power
DSP G Signal
DSP Enable
J14
CONN 16
Secondary general I/O
DSP Control
A_GND
J15
Vbus Sig
Vrec Sig
Inductor Current Sig
Analog Control
EXT Control
Inrush
Main Power
EXT G Signal
EXT Enable
XPC / External
XPC
D_GND
J12
Low Voltage Analog
Vbus Sig DSP
Vrec Sig DSP
Inductor Current Sig DSP
CON34
A_GND
G_DIG_DSP1
G_DIG_DSP2
G_DIG_DSP3
GANLG
G_ANLG_DSP
G_ANLG_1
G_ANLG_2
G_ANLG_3
G_DIG1
G_DIG2
G_DIG3
External_DSP_Interface
+15Va
-15Va
+5V
+3.3V
J16
CONN14
A_GND
D_GND
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Title
Front End Top Level
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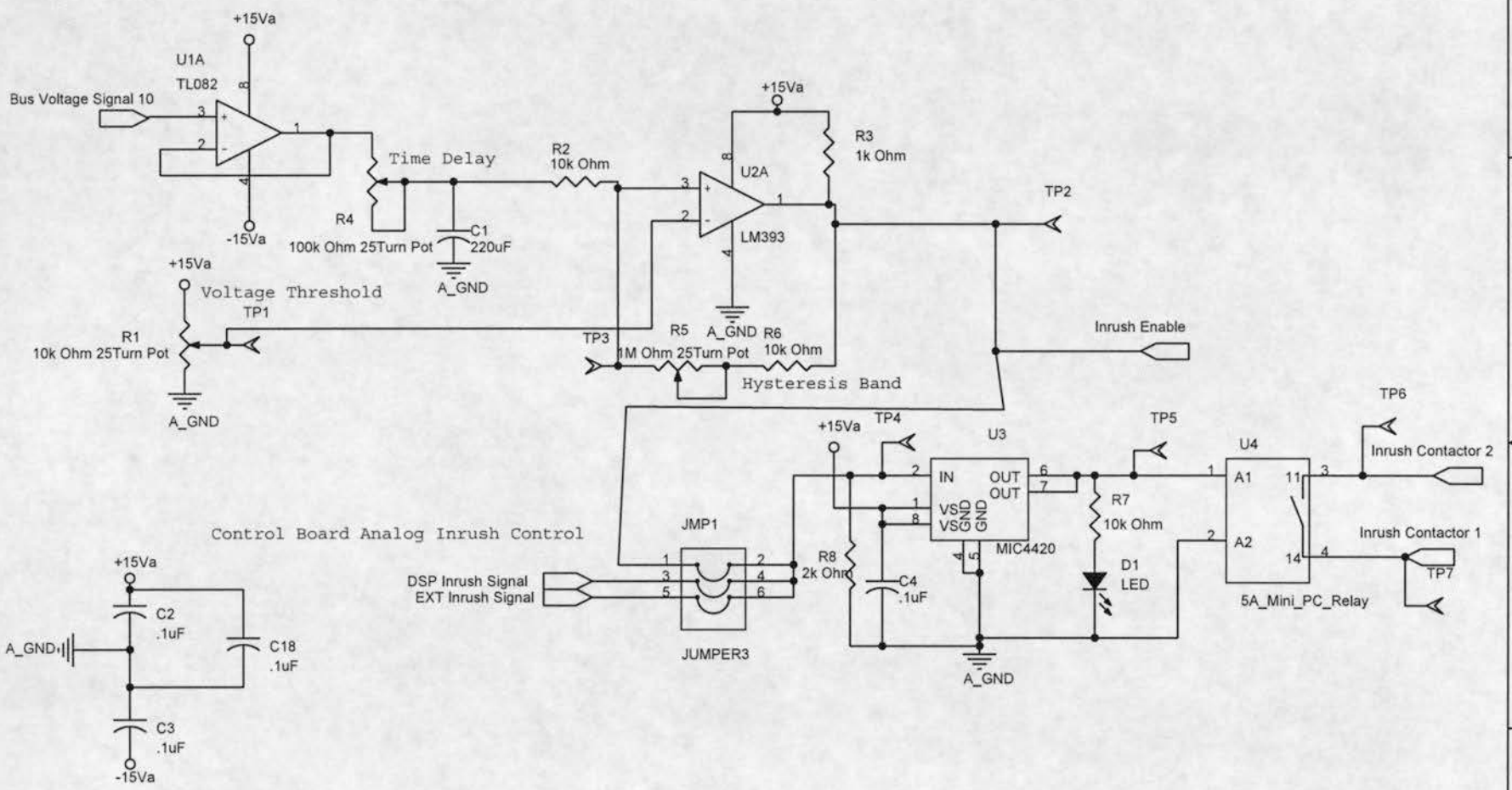

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Title	Inrush Contactor Control	
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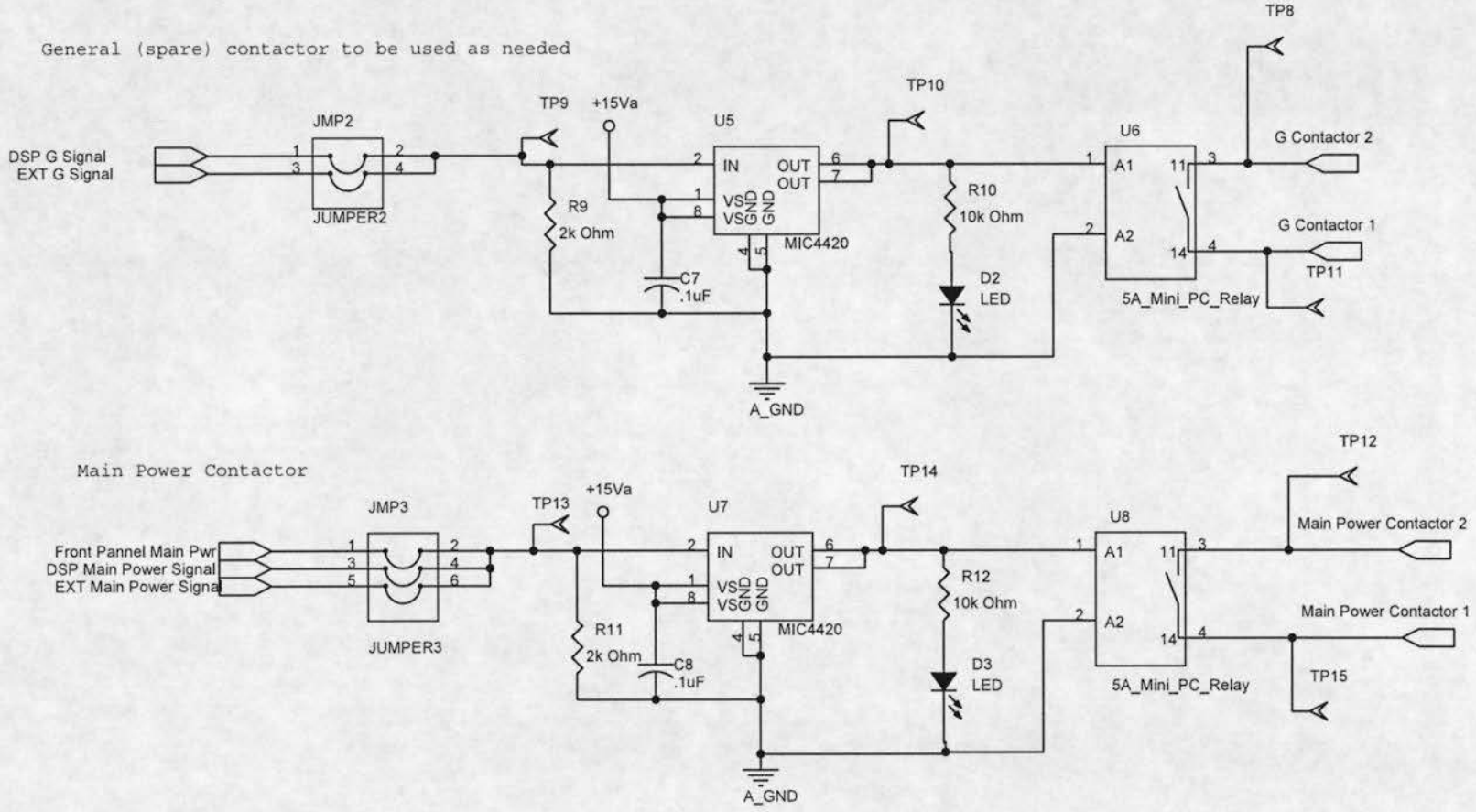

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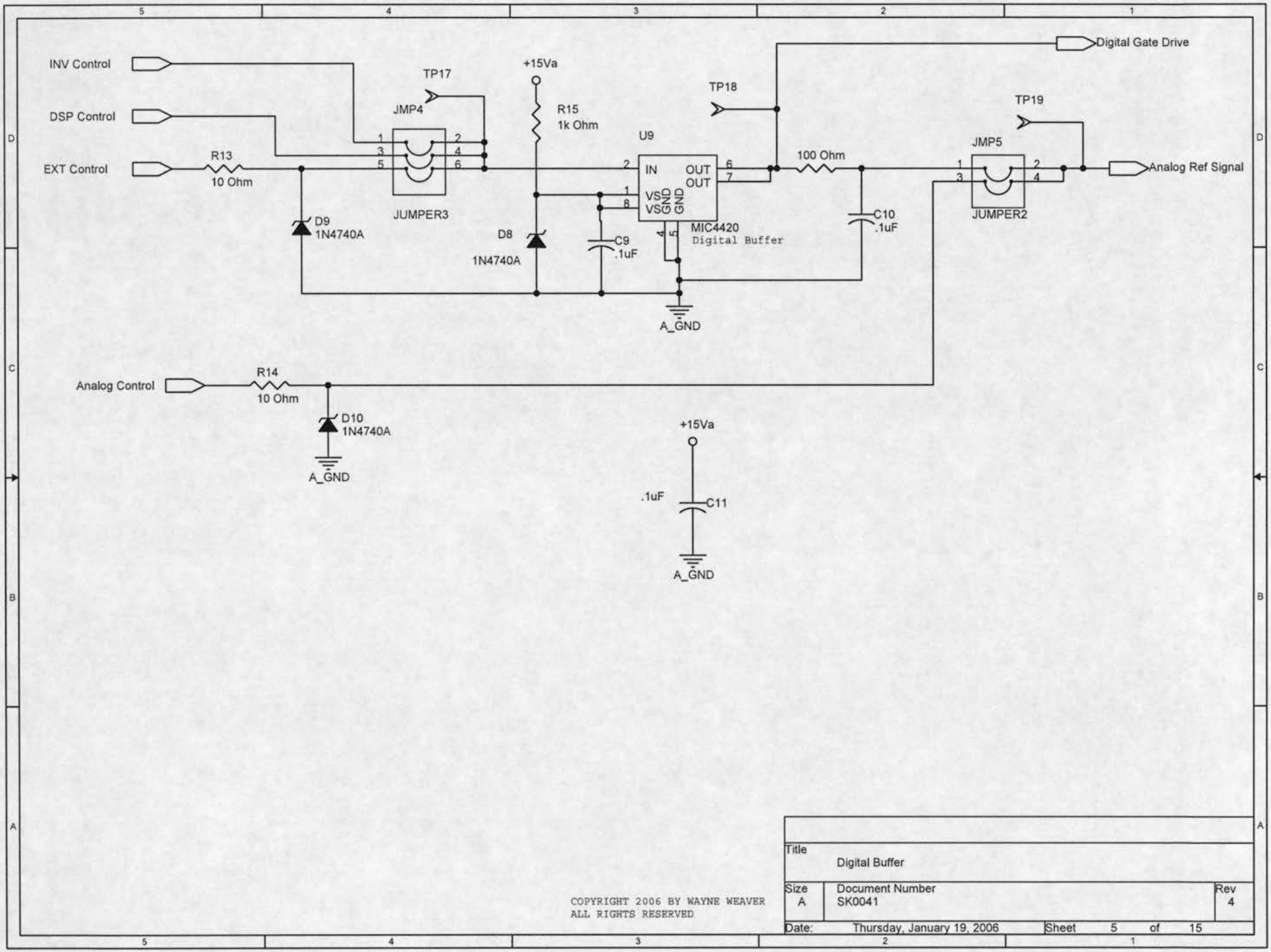
Title: Main Power and General Contactor Control		
Size: A	Document Number: SK0041	Rev: 4
Date: Thursday, January 19, 2006	Sheet 4 of 15	



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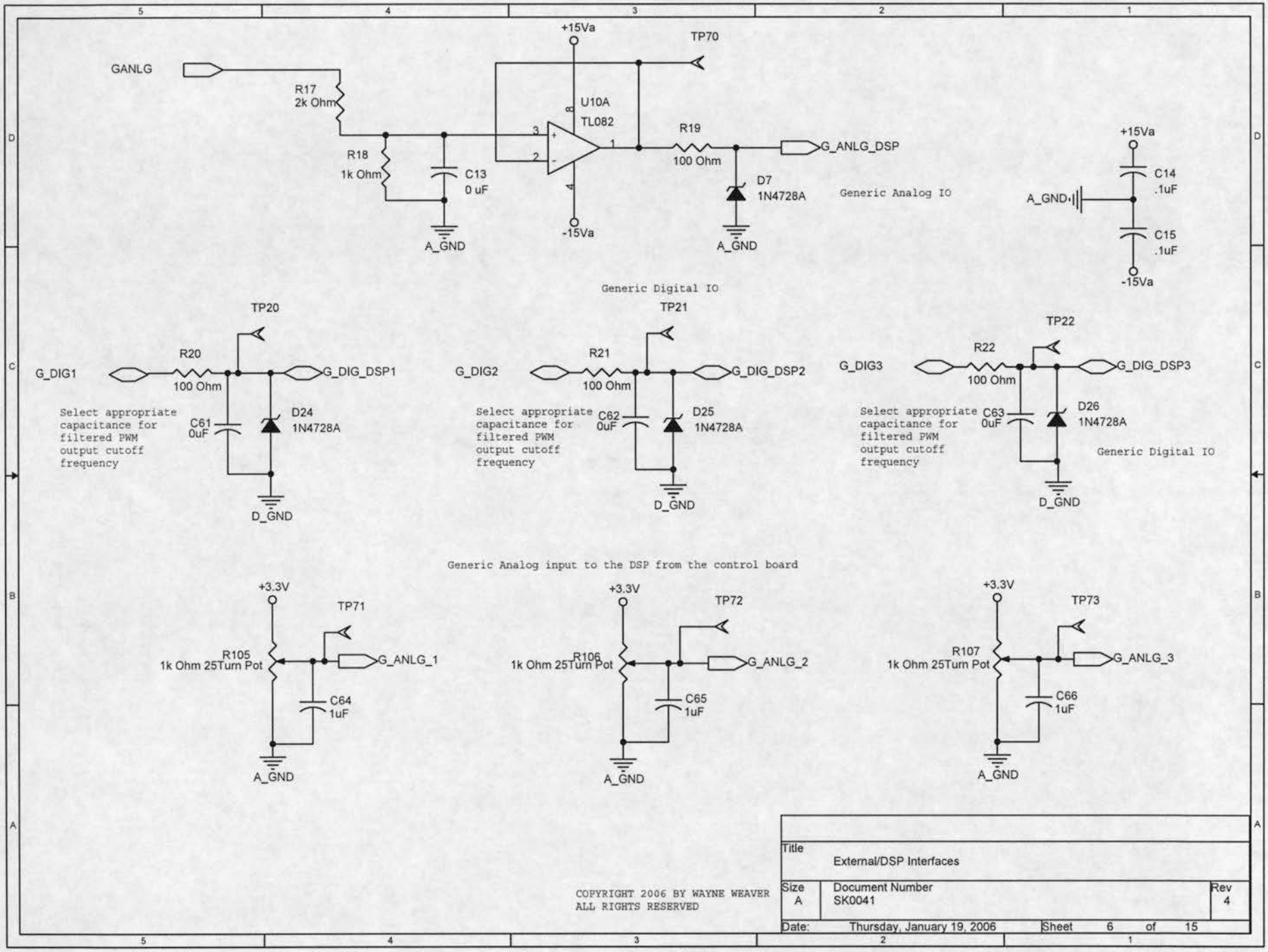
Title: Digital Buffer		
Size: A	Document Number: SK0041	Rev: 4
Date: Thursday, January 19, 2006	Sheet 5 of 15	


GANLG
R17
2k Ohm
R18
1k Ohm
C13
0 uF
A_GND
+15Va
-15Va
U10A
TL082
TP70
R19
100 Ohm
G_ANLG_DSP
D7
1N4728A
A_GND
Generic Analog IO
+15Va
C14
.1uF
A_GND
C15
.1uF
-15Va
Generic Digital IO
TP20
G_DIG1
R20
100 Ohm
G_DIG_DSP1
Select appropriate capacitance for filtered PWM output cutoff frequency
C61
0uF
D24
1N4728A
D_GND
TP21
G_DIG2
R21
100 Ohm
G_DIG_DSP2
Select appropriate capacitance for filtered PWM output cutoff frequency
C62
0uF
D25
1N4728A
D_GND
TP22
G_DIG3
R22
100 Ohm
G_DIG_DSP3
Select appropriate capacitance for filtered PWM output cutoff frequency
C63
0uF
D26
1N4728A
D_GND
Generic Digital IO
Generic Analog input to the DSP from the control board
+3.3V
TP71
R105
1k Ohm 25Turn Pot
G_ANLG_1
C64
1uF
A_GND
+3.3V
TP72
R106
1k Ohm 25Turn Pot
G_ANLG_2
C65
1uF
A_GND
+3.3V
TP73
R107
1k Ohm 25Turn Pot
G_ANLG_3
C66
1uF
A_GND
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Title
External/DSP Interfaces
Size
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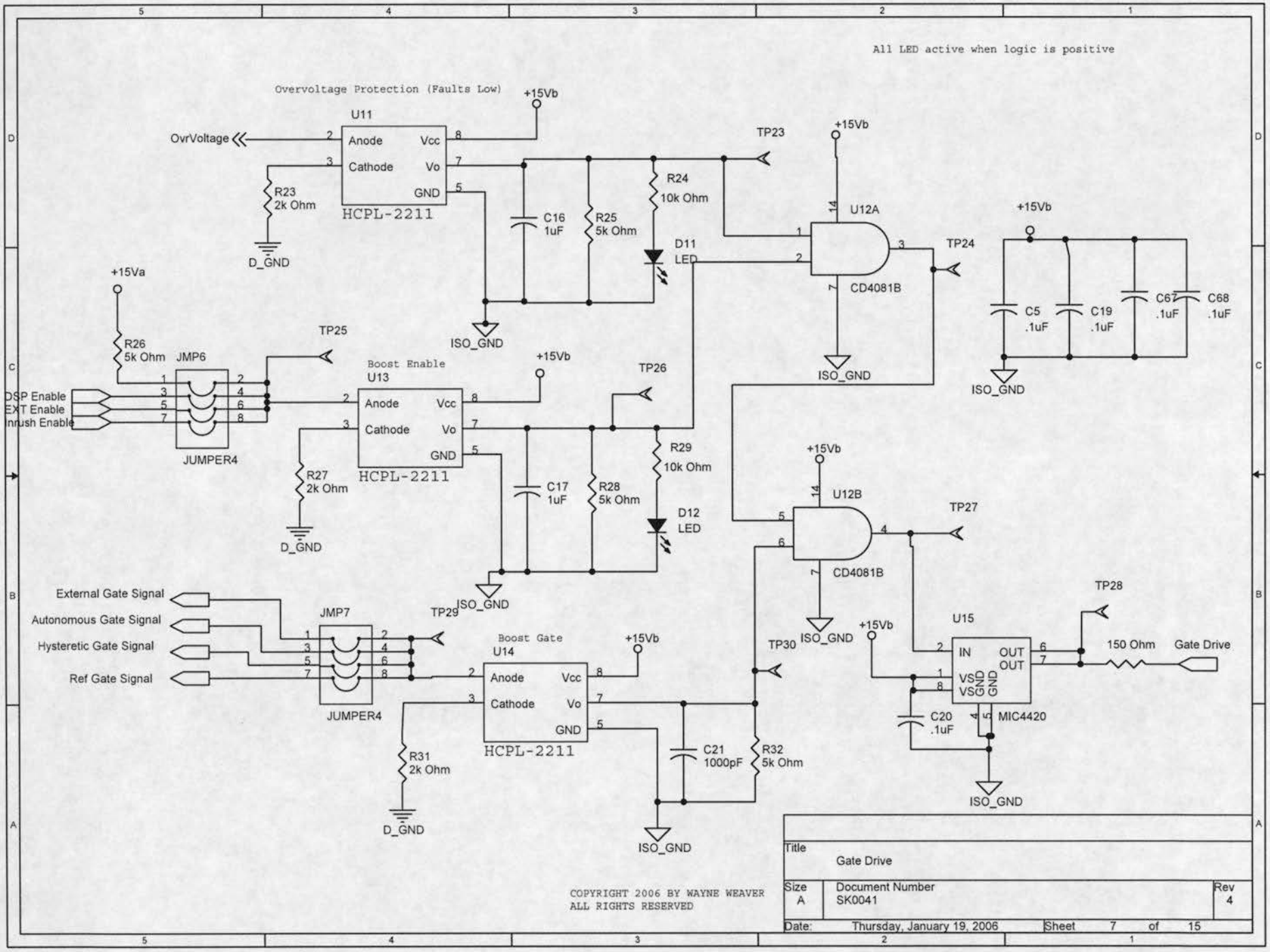
All LED active when logic is positive
Overvoltage Protection (Faults Low)
+15Vb
U11
OvrVoltage
Anode
Cathode
Vcc
Vo
GND
HCPL-2211
R23
2k Ohm
D_GND
C16
1uF
R25
5k Ohm
R24
10k Ohm
TP23
+15Vb
U12A
D11
LED
TP24
CD4081B
ISO_GND
+15Va
R26
5k Ohm
JMP6
TP25
Boost Enable
U13
TP26
DSP Enable
EXT Enable
Inrush Enable
JUMPER4
R27
2k Ohm
C17
1uF
R28
5k Ohm
R29
10k Ohm
D12
LED
TP29
U12B
TP27
External Gate Signal
Autonomous Gate Signal
Hysteretic Gate Signal
Ref Gate Signal
JMP7
Boost Gate
U14
TP30
U15
TP28
IN
OUT
VSS
GND
150 Ohm
Gate Drive
C20
.1uF
MIC4420
R31
2k Ohm
C21
1000pF
R32
5k Ohm
C5
.1uF
C19
.1uF
C67
.1uF
C68
.1uF
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Title
Gate Drive
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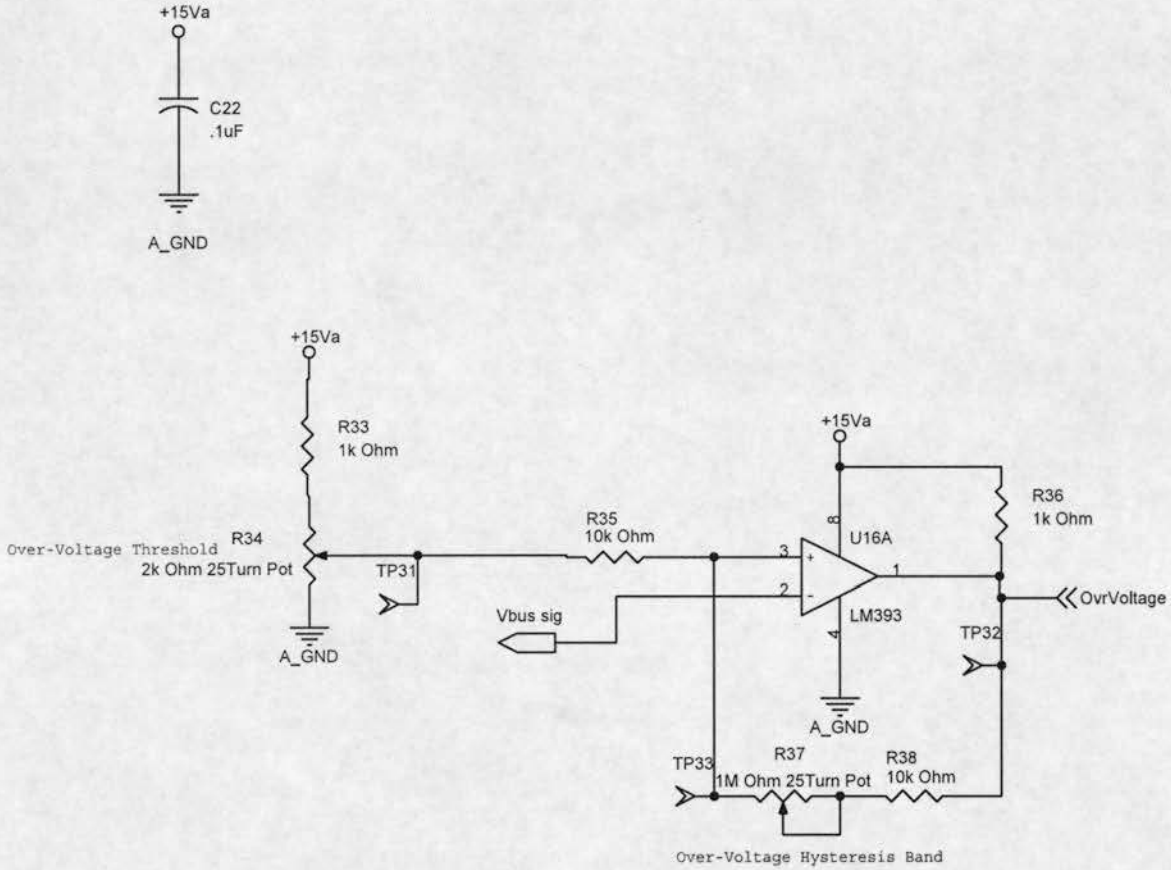

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Title: Gate Drive Overvoltage Enable		
Size: A	Document Number: SK0041	Rev: 4
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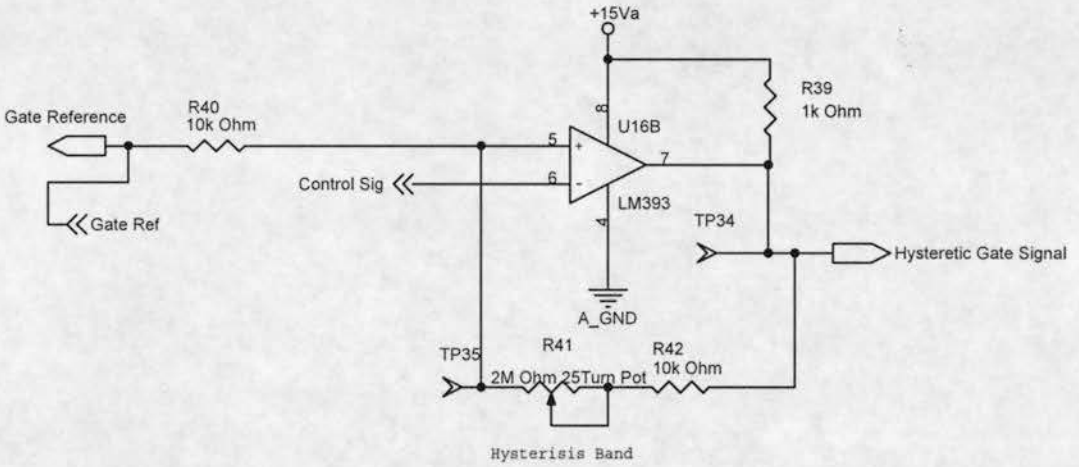

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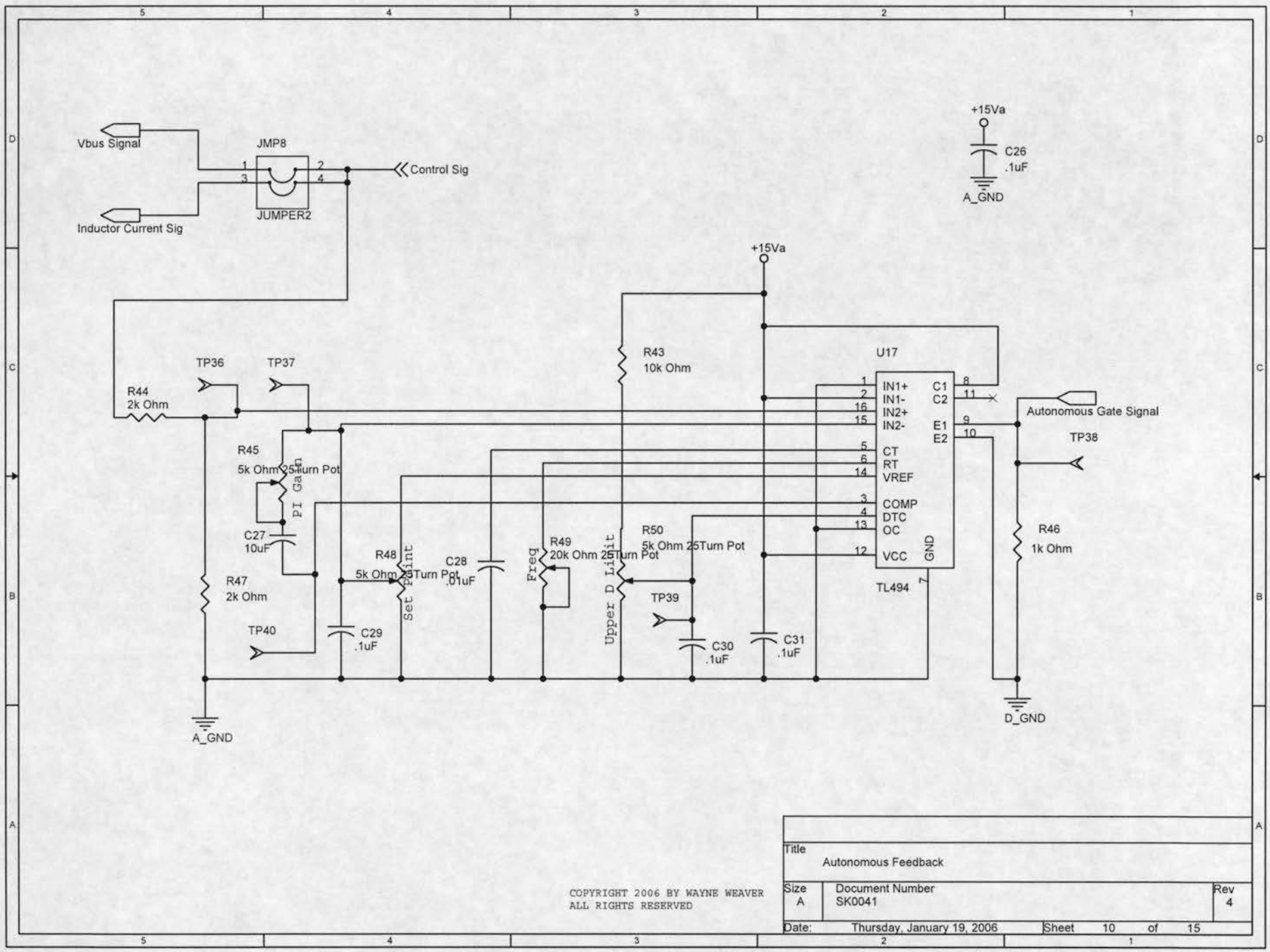
Title: Boost Hysteretic Control		
Size: A	Document Number: SK0041	Rev: C
Date: Thursday, January 19, 2006	Sheet 9 of 15	



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Title: Autonomous Feedback		
Size: A	Document Number: SK0041	Rev: 4
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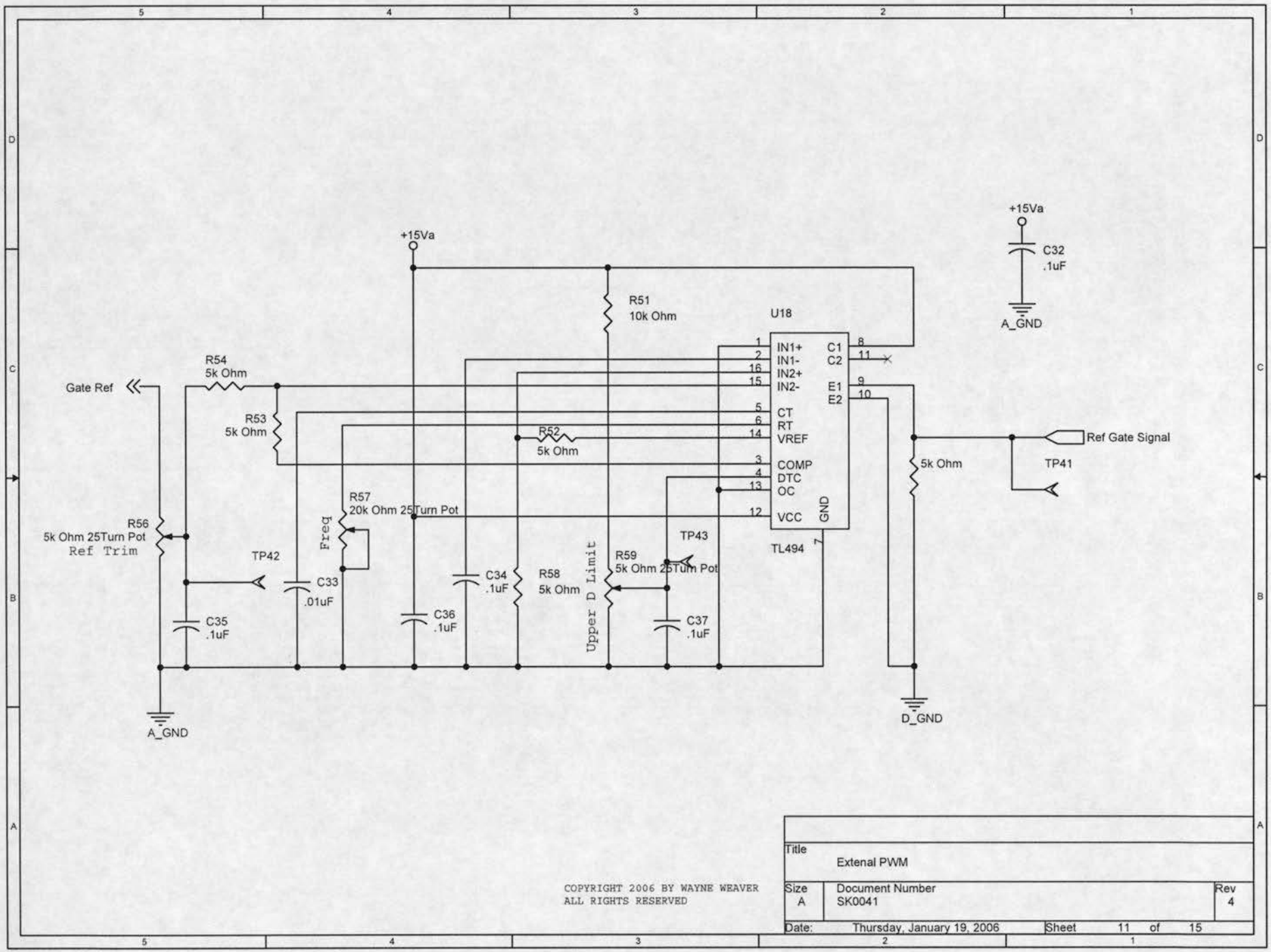

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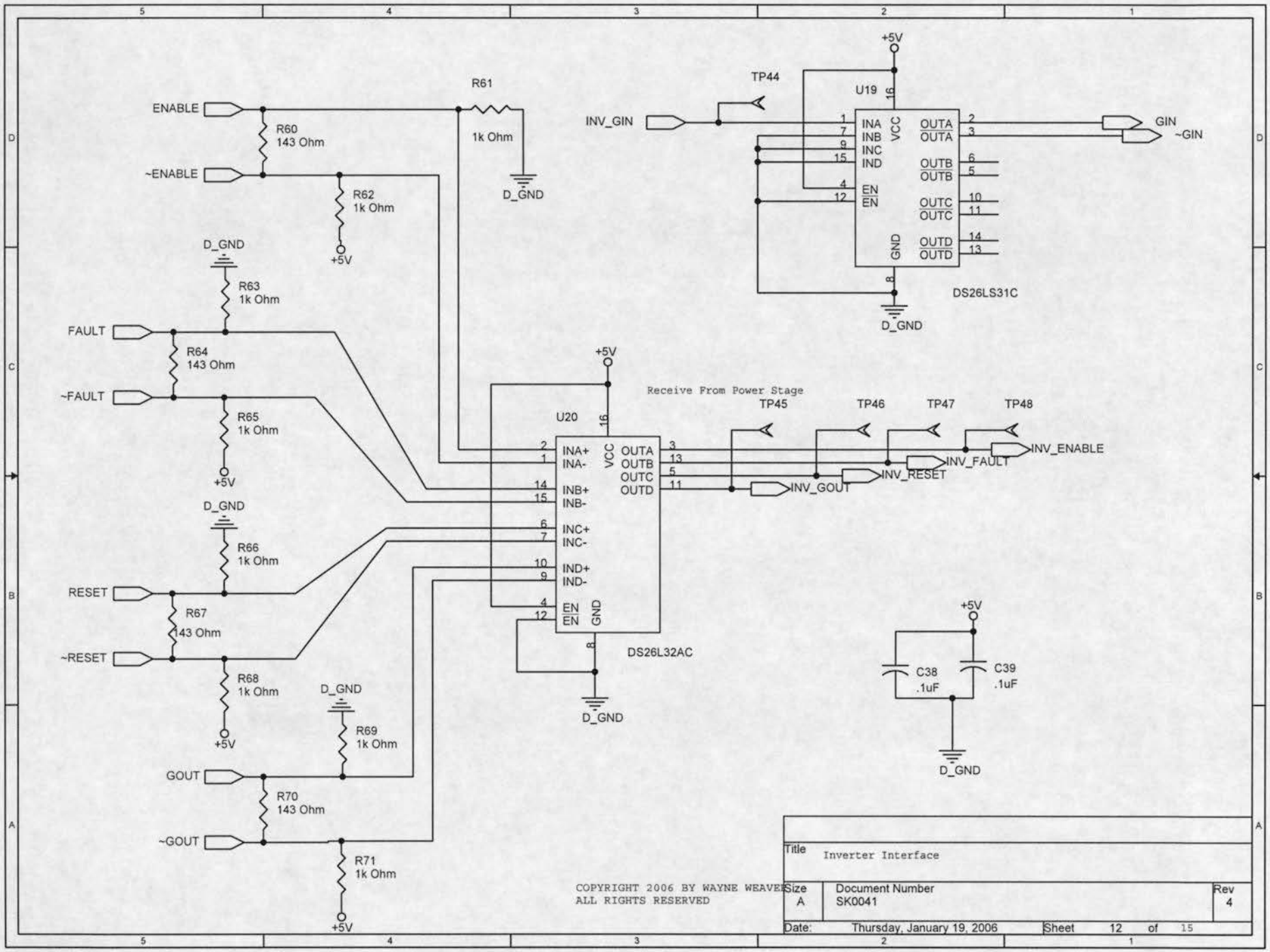
Title: Extenal PWM		
Size: A	Document Number: SK0041	Rev: 4
Date: Thursday, January 19, 2006	Sheet 11 of 15	


ENABLE
~ENABLE
R60
143 Ohm
R61
1k Ohm
R62
1k Ohm
D_GND
+5V
FAULT
~FAULT
R63
1k Ohm
R64
143 Ohm
R65
1k Ohm
RESET
~RESET
R66
1k Ohm
R67
143 Ohm
R68
1k Ohm
GOUT
~GOUT
R69
1k Ohm
R70
143 Ohm
R71
1k Ohm
INV_GIN
TP44
U19
DS26LS31C
GIN
~GIN
Receive From Power Stage
U20
DS26L32AC
TP45
TP46
TP47
TP48
INV_ENABLE
INV_FAULT
INV_RESET
INV_GOUT
C38
.1uF
C39
.1uF
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Inverter Interface
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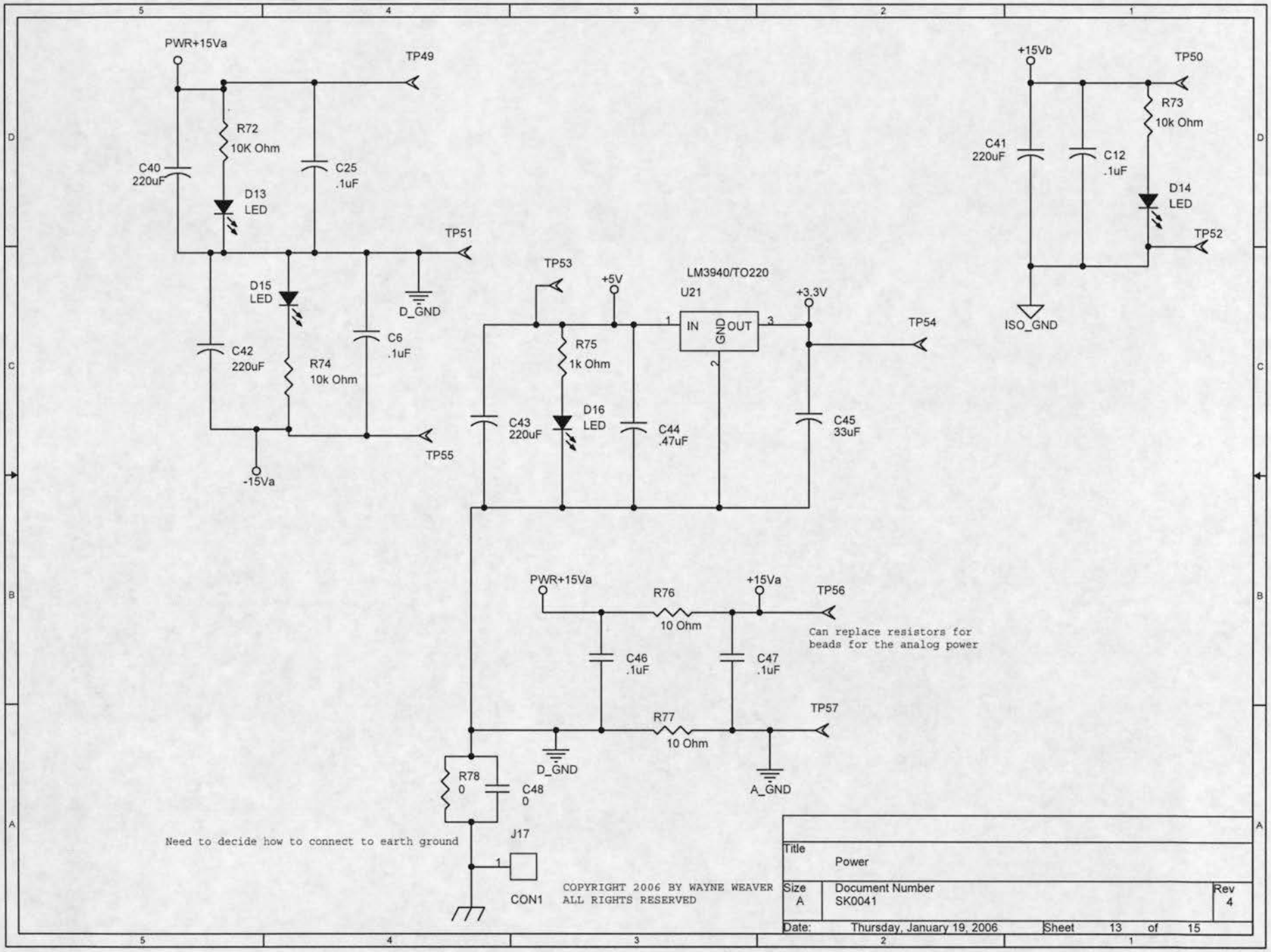
PWR+15Va
TP49
R72
10K Ohm
C40
220uF
C25
.1uF
D13
LED
TP51
D15
LED
D_GND
C42
220uF
R74
10k Ohm
C6
.1uF
TP55
-15Va
TP53
+5V
LM3940/TO220
U21
+3.3V
IN
GND
OUT
TP54
R75
1k Ohm
C43
220uF
D16
LED
C44
.47uF
C45
33uF
+15Vb
TP50
R73
10k Ohm
C41
220uF
C12
.1uF
D14
LED
TP52
ISO_GND
PWR+15Va
R76
10 Ohm
+15Va
TP56
Can replace resistors for
beads for the analog power
C46
.1uF
C47
.1uF
R77
10 Ohm
TP57
D_GND
A_GND
R78
0
C48
0
Need to decide how to connect to earth ground
J17
CON1
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Power
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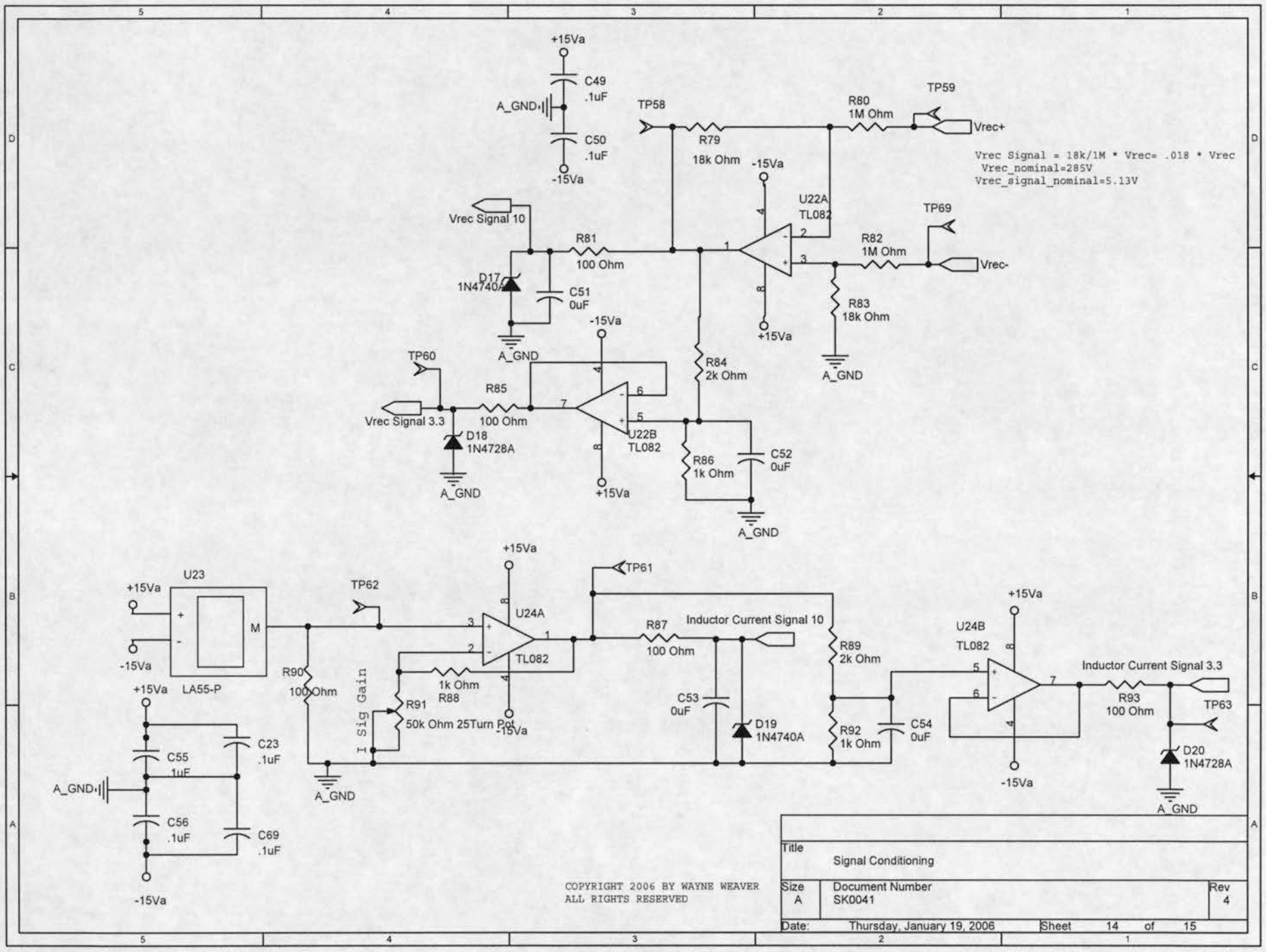

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Title	Signal Conditioning	
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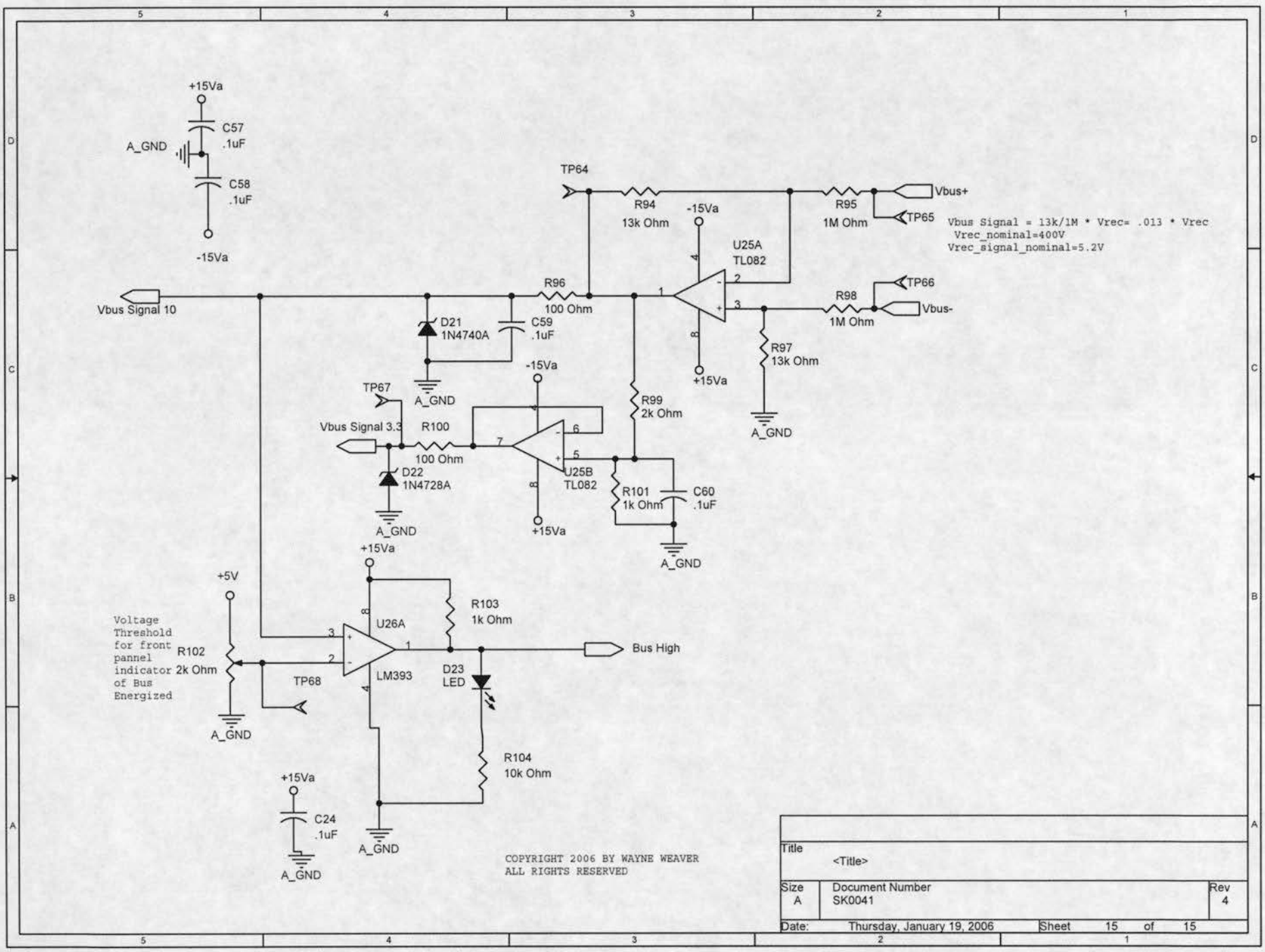
Date: Thursday, January 19, 2006	Sheet 14 of 15	


+15Va
C57
.1uF
A_GND
C58
.1uF
-15Va
TP64
R94
13k Ohm
-15Va
R95
1M Ohm
Vbus+
TP65
Vbus Signal = 13k/1M * Vrec= .013 * Vrec
Vrec_nominal=400V
Vrec_signal_nominal=5.2V
U25A
TL082
R96
100 Ohm
TP66
R98
1M Ohm
Vbus-
Vbus Signal 10
D21
1N4740A
C59
.1uF
R97
13k Ohm
+15Va
A_GND
-15Va
TP67
R99
2k Ohm
Vbus Signal 3.3
R100
100 Ohm
D22
1N4728A
U25B
TL082
R101
1k Ohm
C60
.1uF
A_GND
+15Va
A_GND
+15Va
+5V
R103
1k Ohm
U26A
Voltage
Threshold
for front
pannel
indicator
of Bus
Energized
R102
2k Ohm
TP68
LM393
D23
LED
Bus High
A_GND
R104
10k Ohm
+15Va
C24
.1uF
A_GND
A_GND
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Title
<Title>
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A
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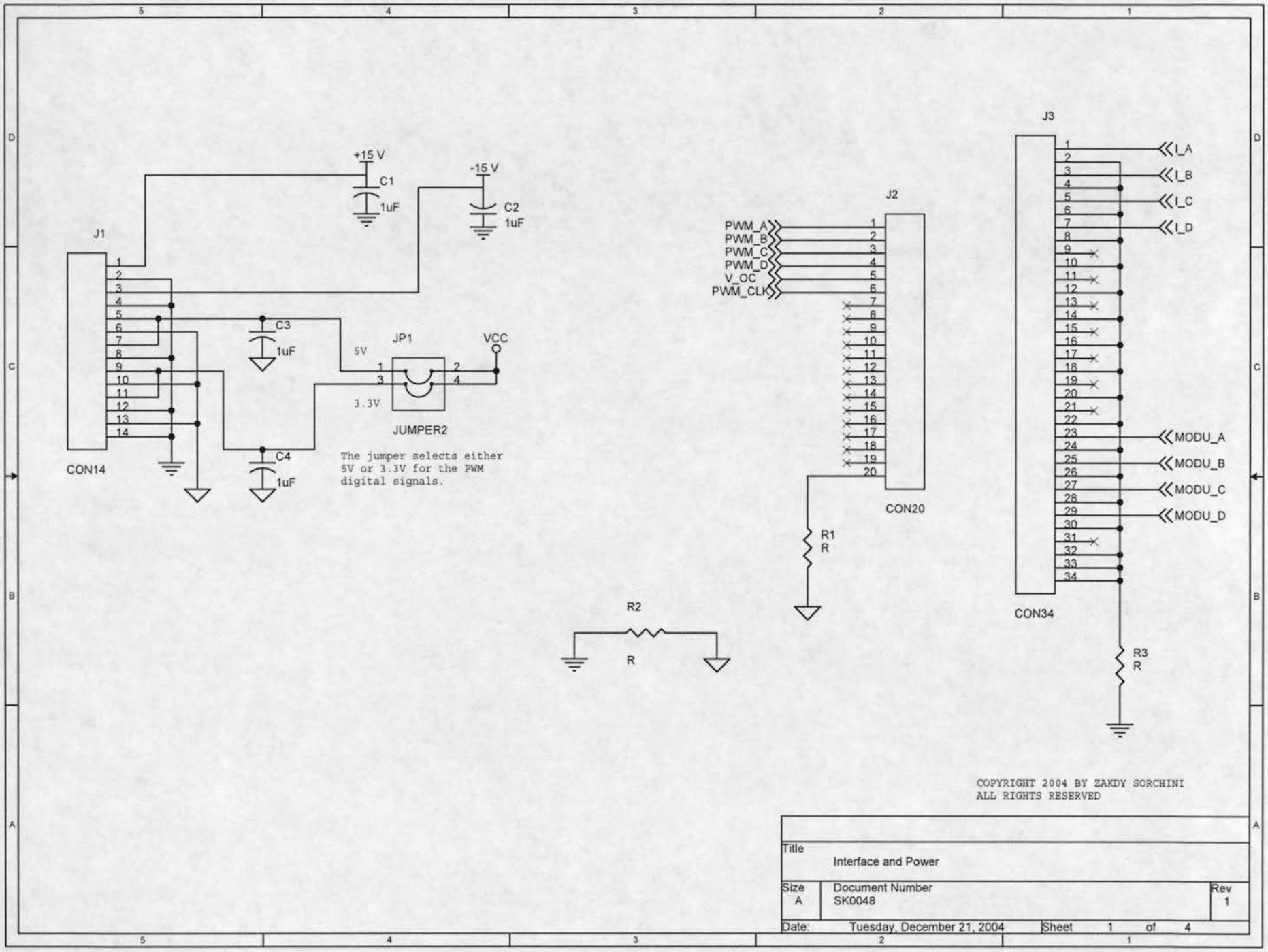
+15 V
C1
1uF
-15 V
C2
1uF
J1
C3
1uF
JP1
5V
VCC
3.3V
JUMPER2
C4
1uF
CON14
The jumper selects either 5V or 3.3V for the PWM digital signals.
J2
PWM_A
PWM_B
PWM_C
PWM_D
V_OC
PWM_CLK
CON20
R1
R
R2
R
J3
I_A
I_B
I_C
I_D
MODU_A
MODU_B
MODU_C
MODU_D
CON34
R3
R
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Interface and Power
Size
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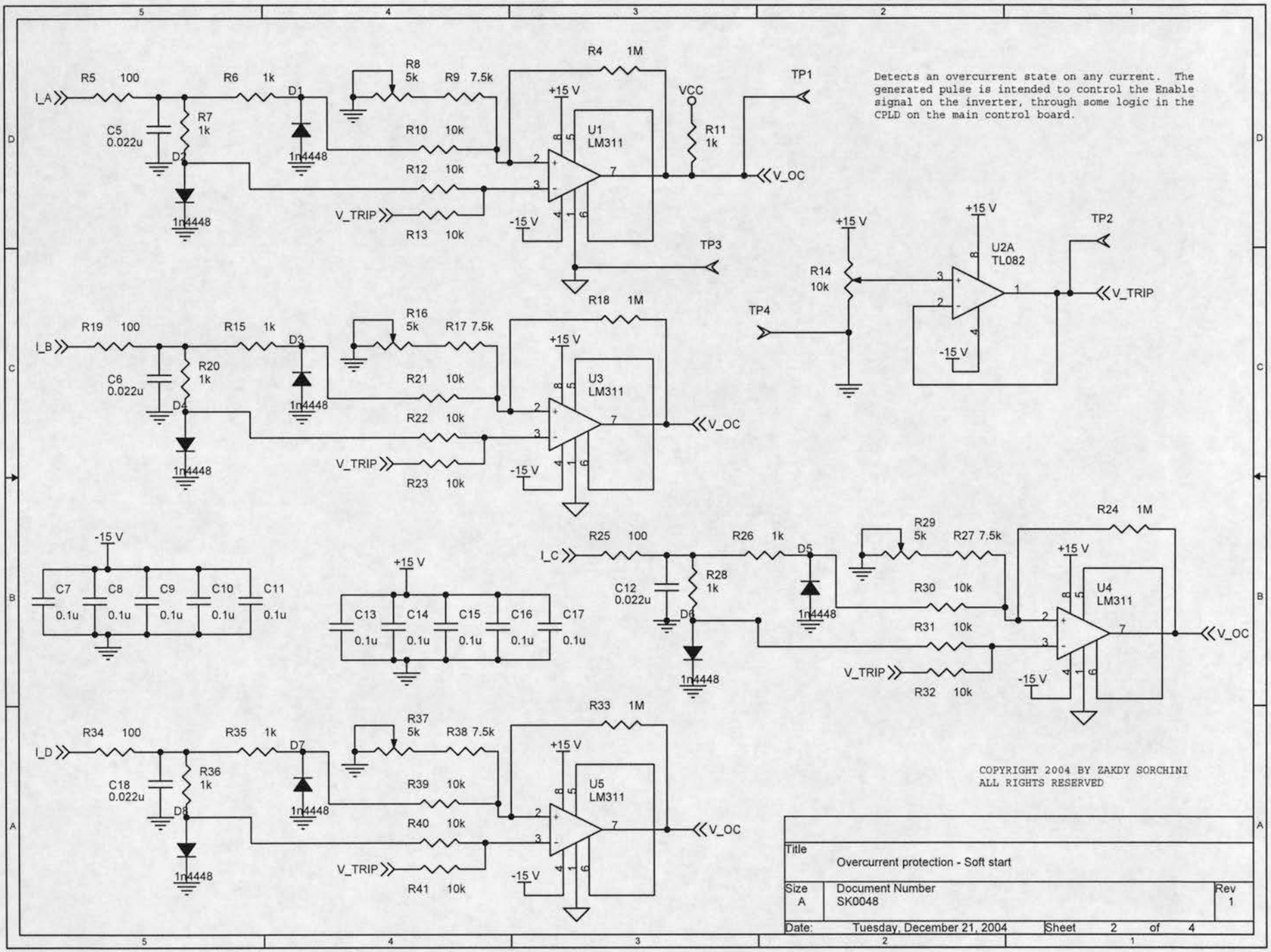
Detects an overcurrent state on any current. The generated pulse is intended to control the Enable signal on the inverter, through some logic in the CPLD on the main control board.
I_A
R5 100
R6 1k
D1
R7 1k
C5 0.022u
D2
1n4448
R8 5k
R9 7.5k
R10 10k
R12 10k
V_TRIP
R13 10k
R4 1M
+15 V
-15 V
U1 LM311
VCC
R11 1k
TP1
V_OC
TP3
I_B
R19 100
R15 1k
D3
R20 1k
C6 0.022u
D4
1n4448
R16 5k
R17 7.5k
R21 10k
R22 10k
V_TRIP
R23 10k
R18 1M
+15 V
-15 V
U3 LM311
V_OC
+15 V
R14 10k
TP4
+15 V
U2A TL082
TP2
V_TRIP
-15 V
-15 V
C7 0.1u
C8 0.1u
C9 0.1u
C10 0.1u
C11 0.1u
+15 V
C13 0.1u
C14 0.1u
C15 0.1u
C16 0.1u
C17 0.1u
I_C
R25 100
R26 1k
D5
R28 1k
C12 0.022u
D6
1n4448
R29 5k
R27 7.5k
R30 10k
R31 10k
V_TRIP
R32 10k
R24 1M
+15 V
-15 V
U4 LM311
V_OC
I_D
R34 100
R35 1k
D7
R36 1k
C18 0.022u
D8
1n4448
R37 5k
R38 7.5k
R39 10k
R40 10k
V_TRIP
R41 10k
R33 1M
+15 V
-15 V
U5 LM311
V_OC
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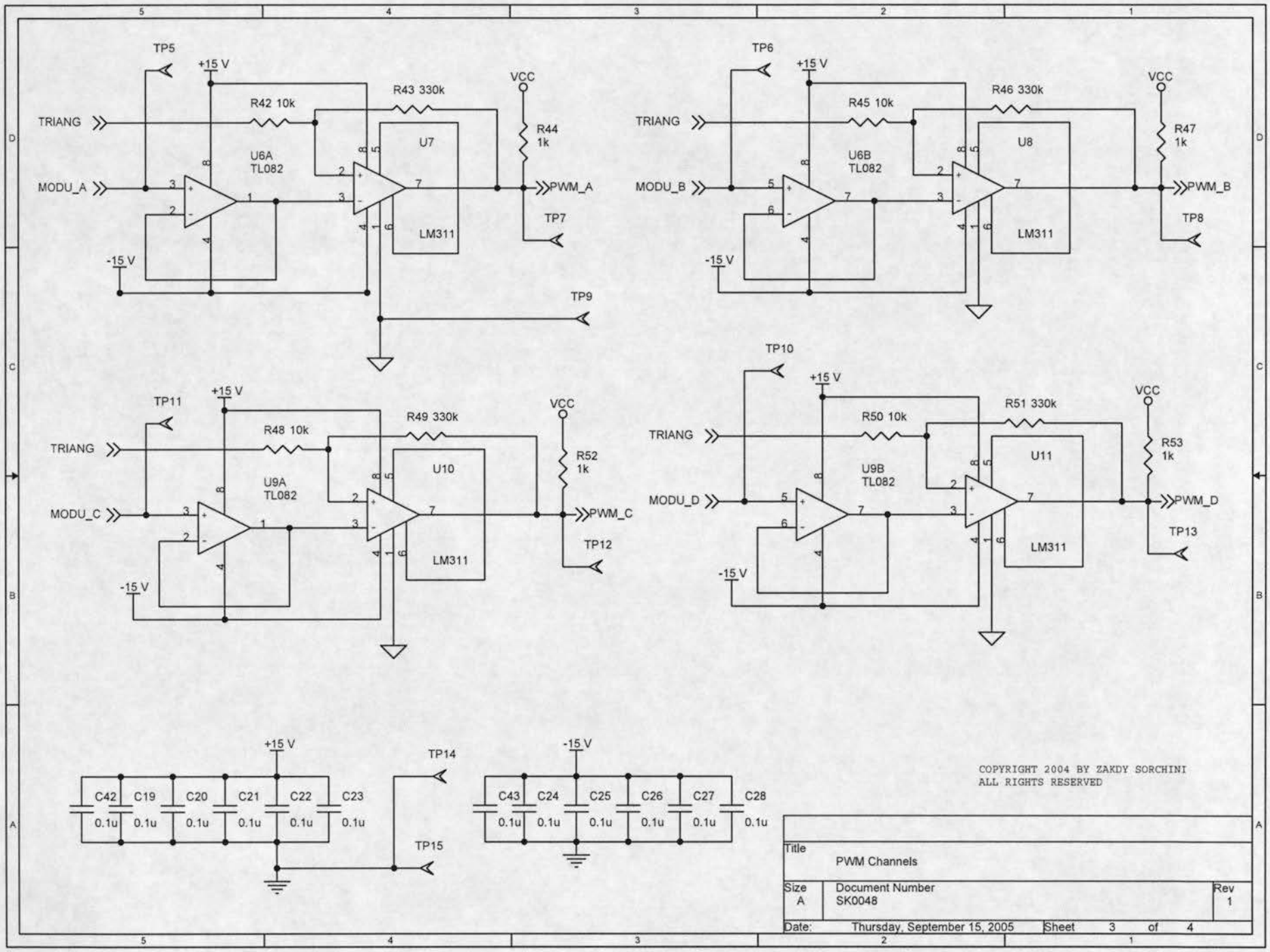
Title
Overcurrent protection - Soft start
Size A
Document Number SK0048
Rev 1
Date: Tuesday, December 21, 2004
Sheet 2 of 4



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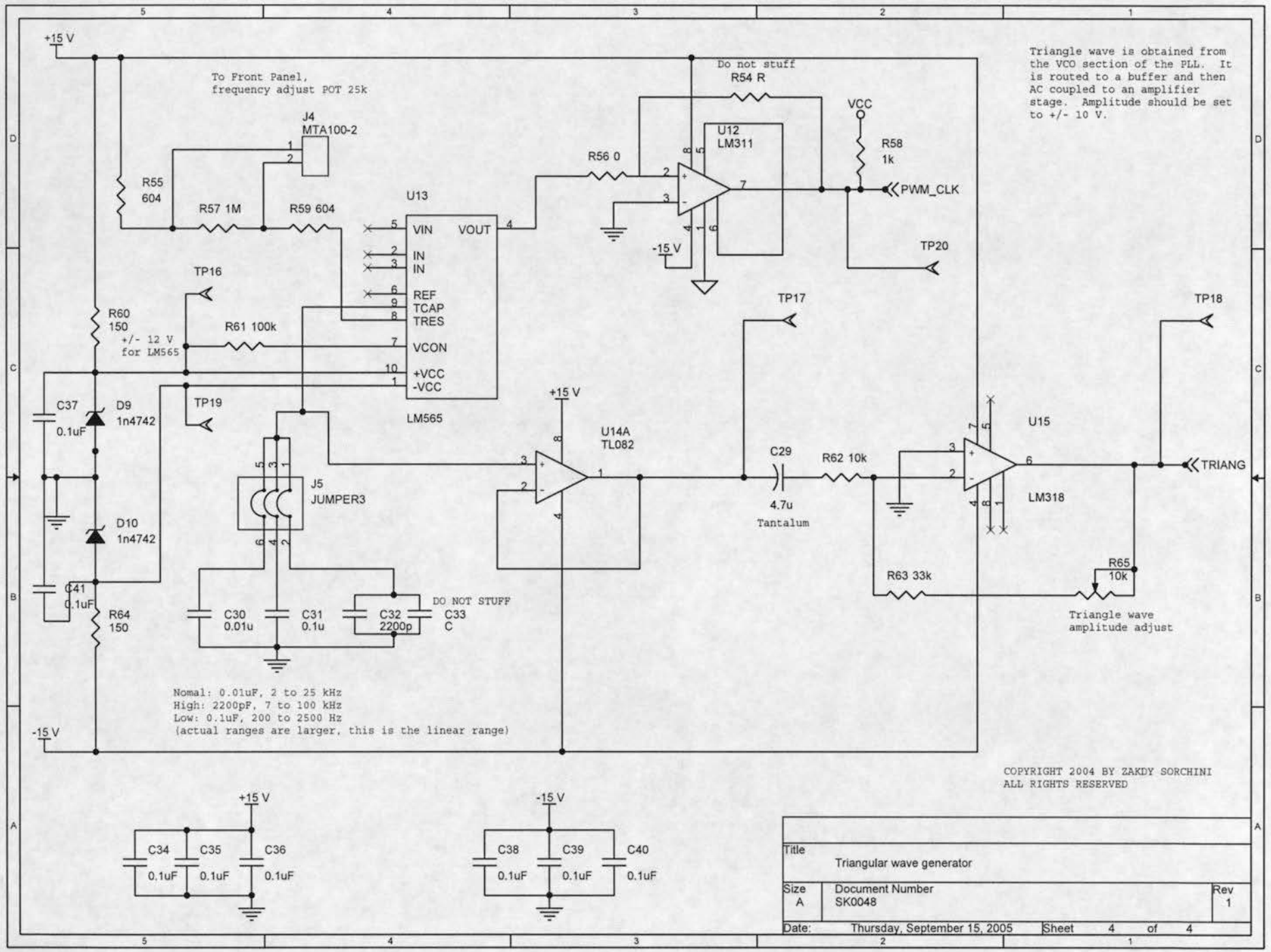
Title: PWM Channels		
Size: A	Document Number: SK0048	Rev: 1
Date: Thursday, September 15, 2005	Sheet 3 of 4	


+15 V
To Front Panel,
frequency adjust POT 25k
J4
MTA100-2
R55
604
R57 1M
R59 604
U13
VIN
VOUT
IN
IN
REF
TCAP
TRES
VCON
+VCC
-VCC
LM565
R56 0
Do not stuff
R54 R
U12
LM311
VCC
R58
1k
PWM_CLK
TP20
-15 V
TP16
R60
150
+/- 12 V
for LM565
R61 100k
TP19
C37
0.1uF
D9
1n4742
D10
1n4742
C41
0.1uF
R64
150
J5
JUMPER3
C30
0.01u
C31
0.1u
C32
2200p
C33
C
DO NOT STUFF
Nomal: 0.01uF, 2 to 25 kHz
High: 2200pF, 7 to 100 kHz
Low: 0.1uF, 200 to 2500 Hz
(actual ranges are larger, this is the linear range)
U14A
TL082
TP17
C29
4.7u
Tantalum
R62 10k
U15
LM318
TP18
TRIANG
R63 33k
R65
10k
Triangle wave
amplitude adjust
Triangle wave is obtained from
the VCO section of the PLL. It
is routed to a buffer and then
AC coupled to an amplifier
stage. Amplitude should be set
to +/- 10 V.
C34
C35
C36
0.1uF
C38
C39
C40
COPYRIGHT 2004 BY ZAKDY SORCHINI
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Title
Triangular wave generator
Size
A
Document Number
SK0048
Rev
1
Date:
Thursday, September 15, 2005
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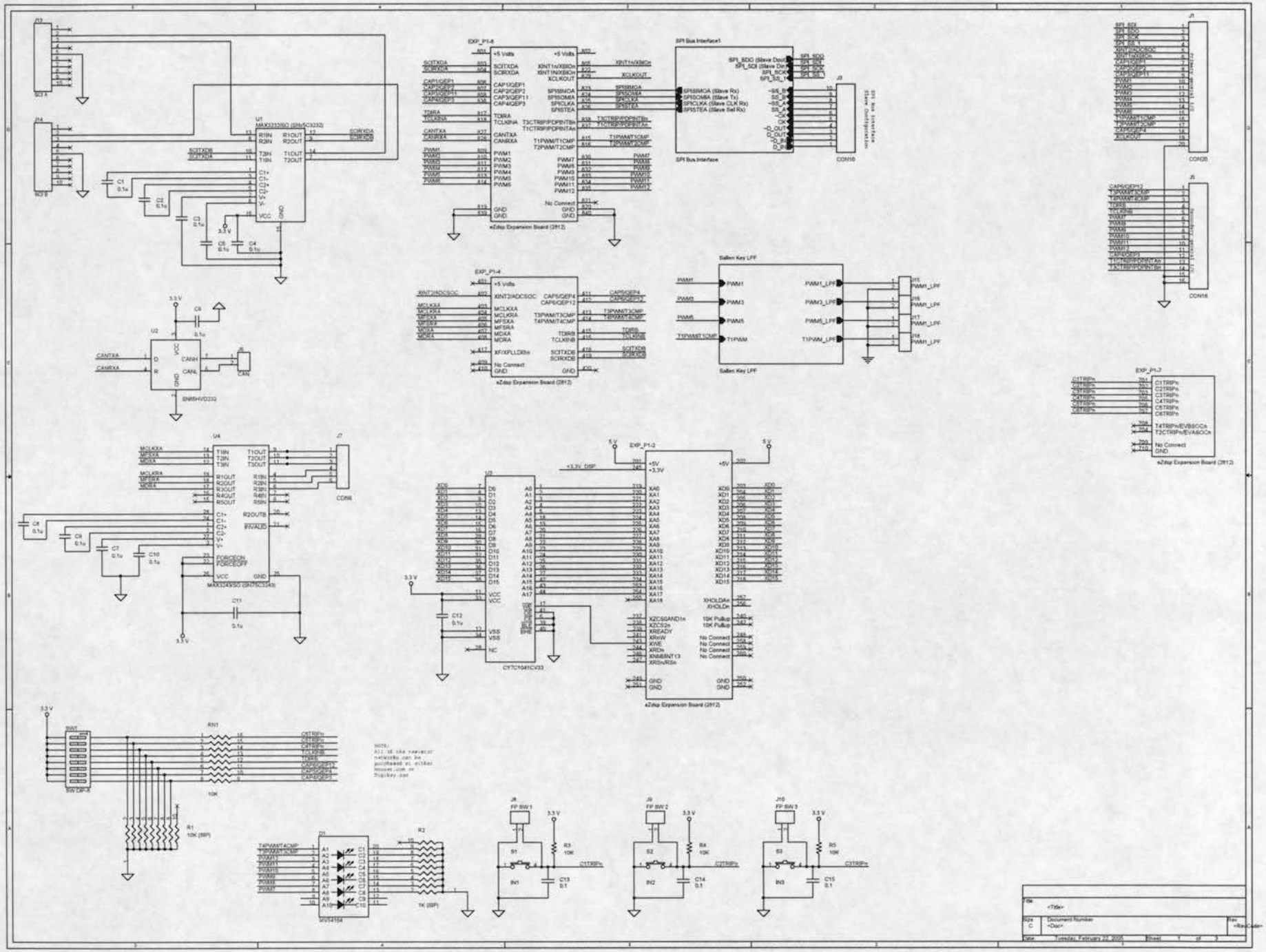

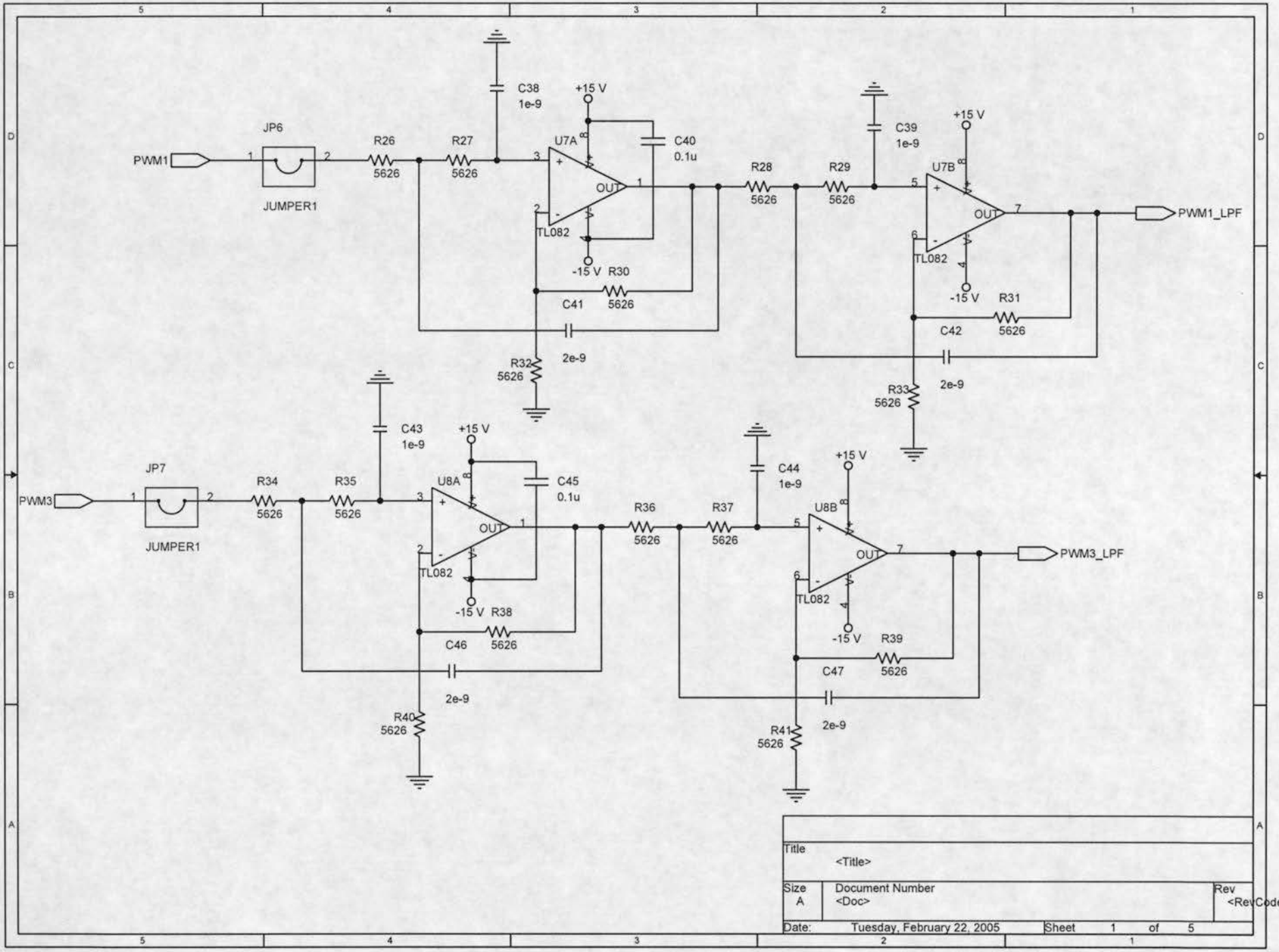
PWM1
JP6
JUMPER1
R26
5626
R27
5626
C38
1e-9
U7A
+15 V
C40
0.1u
TL082
OUT
-15 V
R30
5626
C41
2e-9
R32
5626
R28
5626
R29
5626
C39
1e-9
U7B
R31
5626
C42
2e-9
R33
5626
PWM1_LPF
PWM3
JP7
JUMPER1
R34
5626
R35
5626
C43
1e-9
U8A
C45
0.1u
R38
5626
C46
2e-9
R40
5626
R36
5626
R37
5626
C44
1e-9
U8B
R39
5626
C47
2e-9
R41
5626
PWM3_LPF
Title
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<RevCode>
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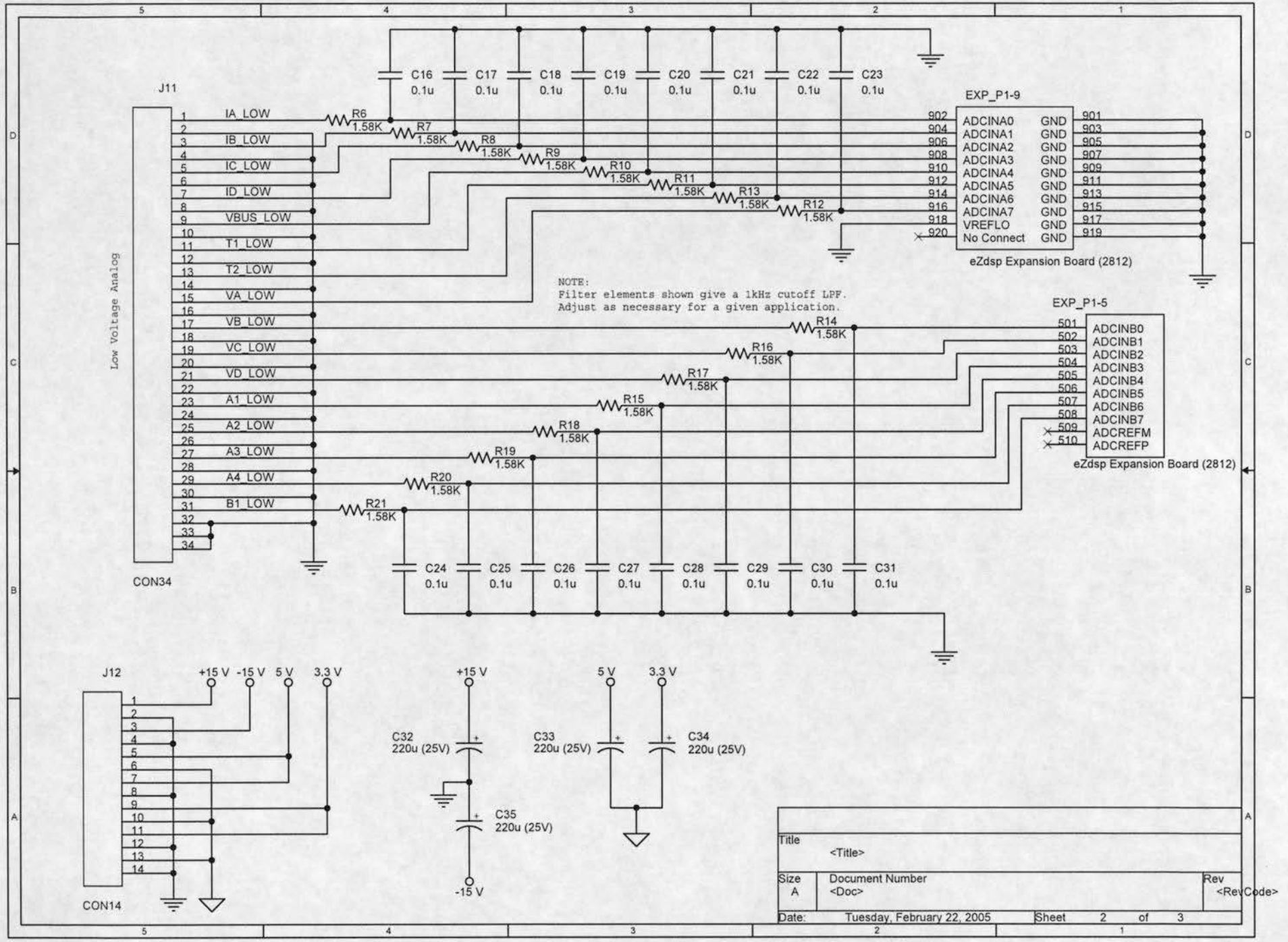
J11
CON34
Low Voltage Analog
IA_LOW
IB_LOW
IC_LOW
ID_LOW
VBUS_LOW
T1_LOW
T2_LOW
VA_LOW
VB_LOW
VC_LOW
VD_LOW
A1_LOW
A2_LOW
A3_LOW
A4_LOW
B1_LOW
R6 1.58K
R7 1.58K
R8 1.58K
R9 1.58K
R10 1.58K
R11 1.58K
R12 1.58K
R13 1.58K
R14 1.58K
R15 1.58K
R16 1.58K
R17 1.58K
R18 1.58K
R19 1.58K
R20 1.58K
R21 1.58K
C16 0.1u
C17 0.1u
C18 0.1u
C19 0.1u
C20 0.1u
C21 0.1u
C22 0.1u
C23 0.1u
C24 0.1u
C25 0.1u
C26 0.1u
C27 0.1u
C28 0.1u
C29 0.1u
C30 0.1u
C31 0.1u
EXP_P1-9
ADCINA0
ADCINA1
ADCINA2
ADCINA3
ADCINA4
ADCINA5
ADCINA6
ADCINA7
VREFLO
No Connect
GND
eZdsp Expansion Board (2812)
EXP_P1-5
ADCINB0
ADCINB1
ADCINB2
ADCINB3
ADCINB4
ADCINB5
ADCINB6
ADCINB7
ADCREFM
ADCREFP
eZdsp Expansion Board (2812)
NOTE:
Filter elements shown give a 1kHz cutoff LPF.
Adjust as necessary for a given application.
J12
CON14
+15 V
-15 V
5 V
3.3 V
C32 220u (25V)
C33 220u (25V)
C34 220u (25V)
C35 220u (25V)
Title
<Title>
Size A
Document Number
<Doc>
Rev
<RevCode>
Date: Tuesday, February 22, 2005
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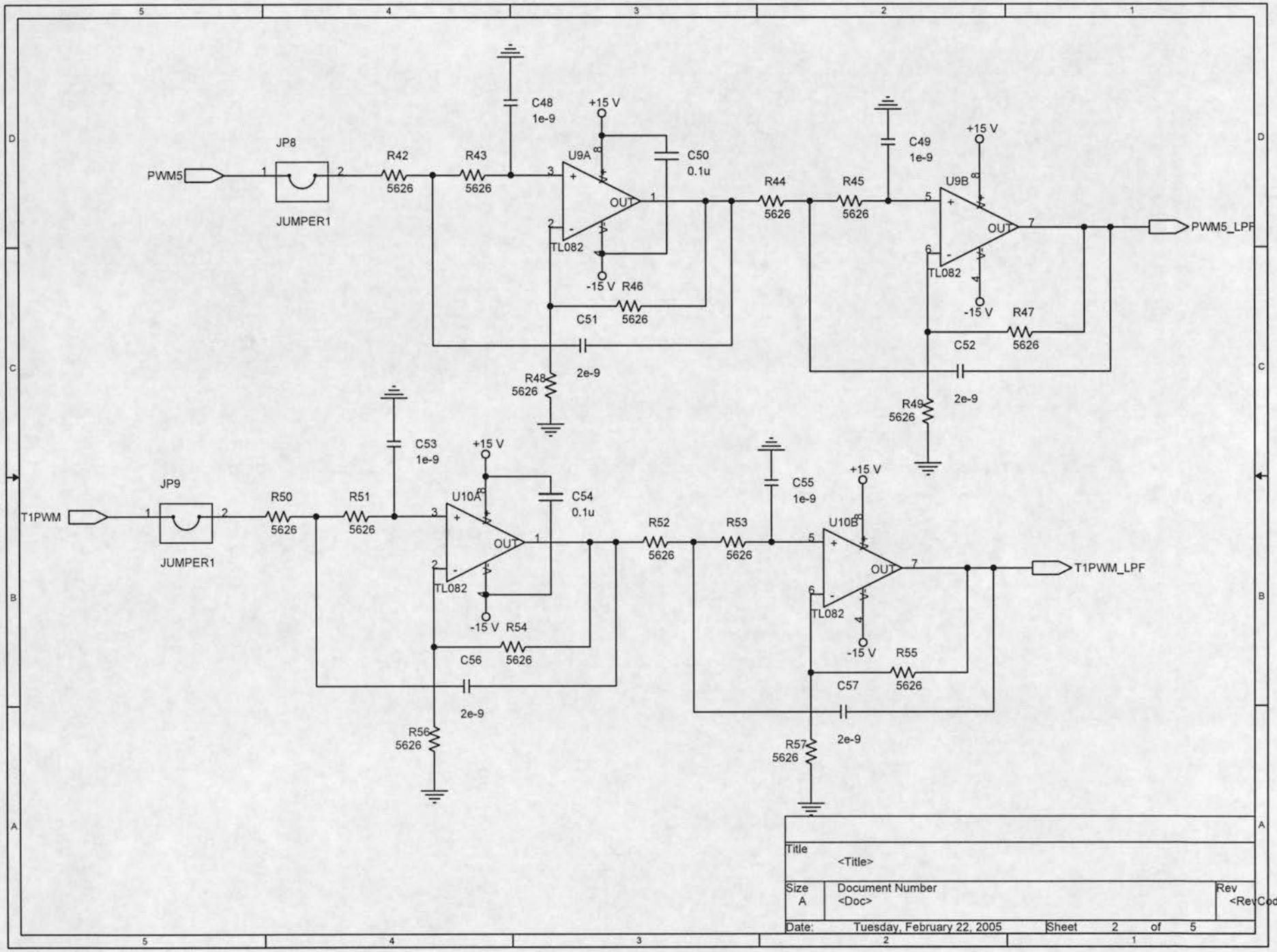
PWM5
JP8
JUMPER1
R42
5626
R43
5626
C48
1e-9
+15 V
U9A
C50
0.1u
TL082
-15 V
R46
5626
C51
2e-9
R48
5626
R44
5626
R45
5626
C49
1e-9
U9B
OUT
PWM5_LPF
R47
5626
C52
2e-9
R49
5626
T1PWM
JP9
JUMPER1
R50
5626
R51
5626
C53
1e-9
U10A
C54
0.1u
TL082
-15 V
R54
5626
C56
2e-9
R56
5626
R52
5626
R53
5626
C55
1e-9
U10B
T1PWM_LPF
R55
5626
C57
2e-9
R57
5626
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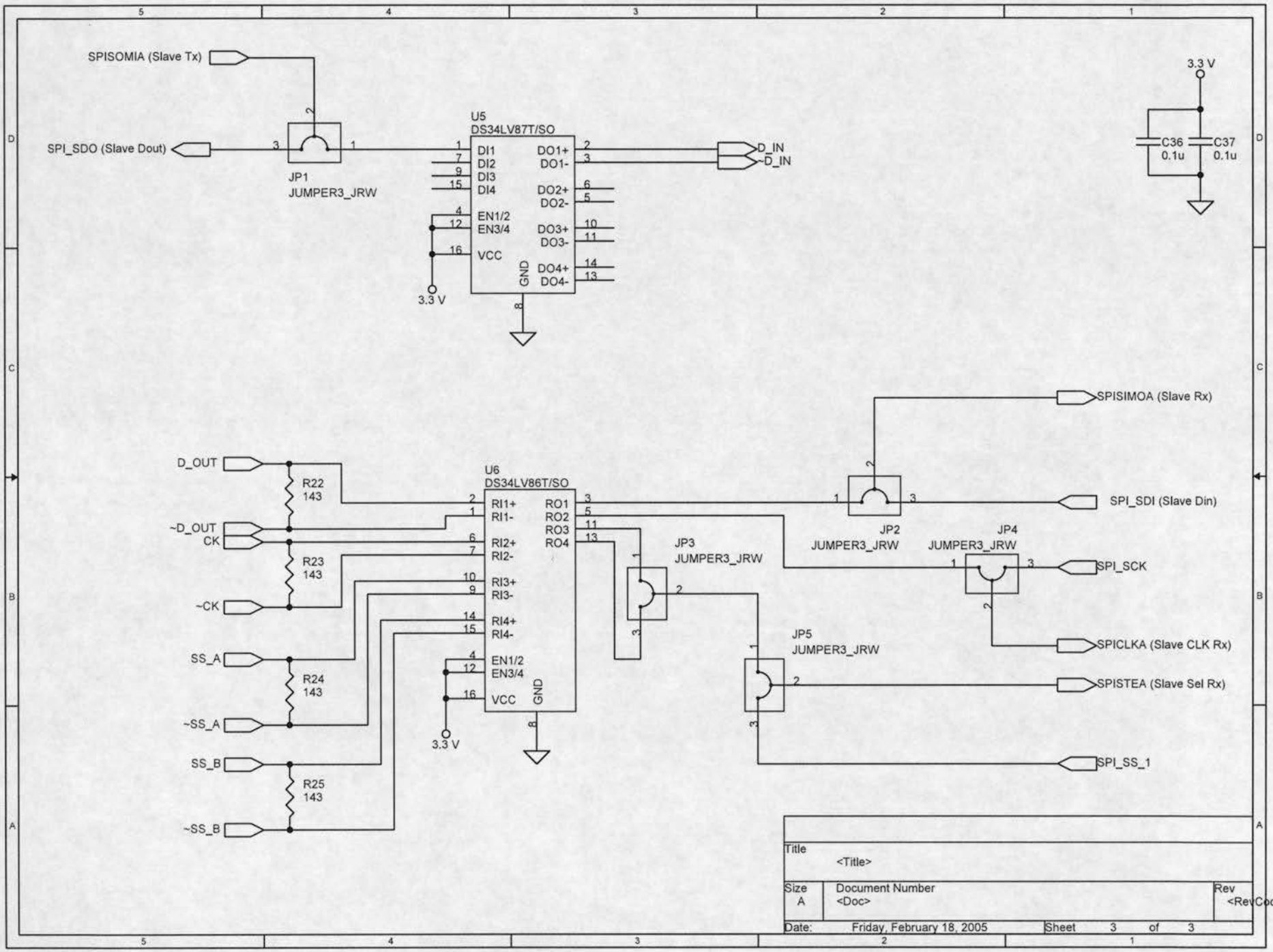
SPISOMIA (Slave Tx)
SPI_SDO (Slave Dout)
JP1
JUMPER3_JRW
U5
DS34LV87T/SO
DI1
DI2
DI3
DI4
EN1/2
EN3/4
VCC
GND
DO1+
DO1-
DO2+
DO2-
DO3+
DO3-
DO4+
DO4-
3.3 V
D_IN
~D_IN
C36
0.1u
C37
0.1u
D_OUT
~D_OUT
CK
~CK
SS_A
~SS_A
SS_B
~SS_B
R22
143
R23
143
R24
143
R25
143
U6
DS34LV86T/SO
RI1+
RI1-
RI2+
RI2-
RI3+
RI3-
RI4+
RI4-
RO1
RO2
RO3
RO4
JP2
JUMPER3_JRW
JP3
JUMPER3_JRW
JP4
JUMPER3_JRW
JP5
JUMPER3_JRW
SPISIMOA (Slave Rx)
SPI_SDI (Slave Din)
SPI_SCK
SPICLKA (Slave CLK Rx)
SPISTEA (Slave Sel Rx)
SPI_SS_1
Title
<Title>
Size
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Document Number
<Doc>
Rev
<RevCode>
Date:
Friday, February 18, 2005
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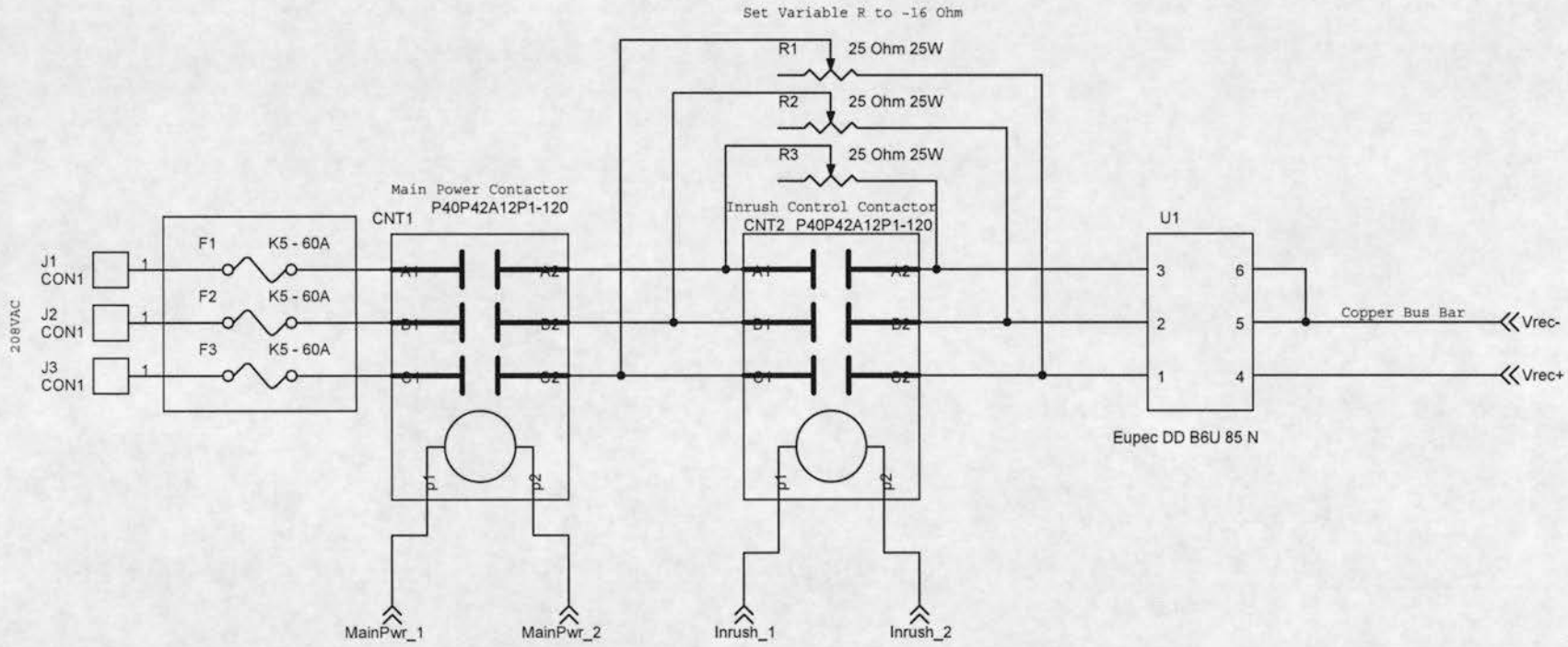
of
3



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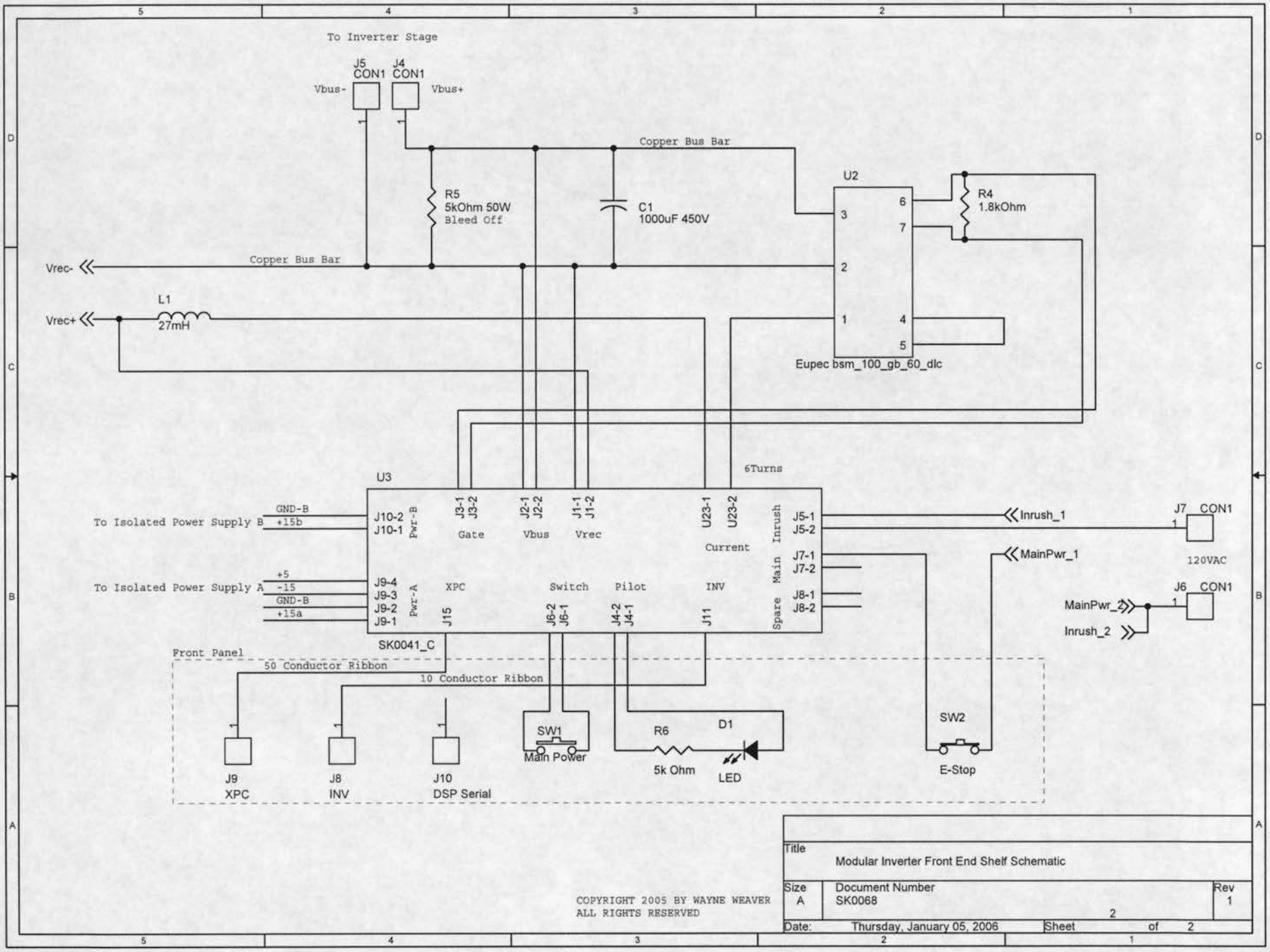
Title	Modular Inverter Front End Shelf Schematic	
Size A	Document Number SK0068	Rev 1
Date: Thursday, January 05, 2006	Sheet 1 of 2	



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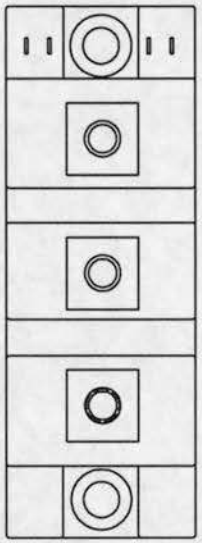
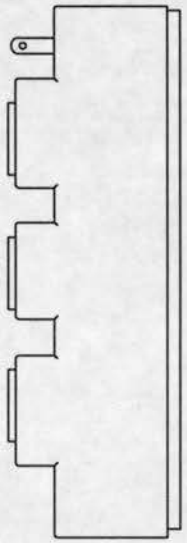
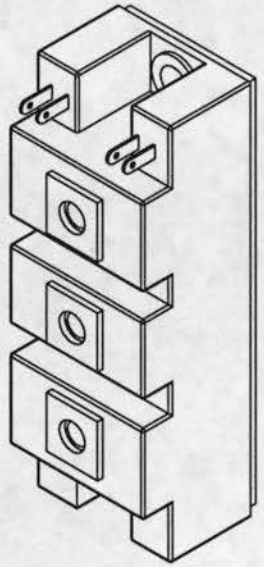
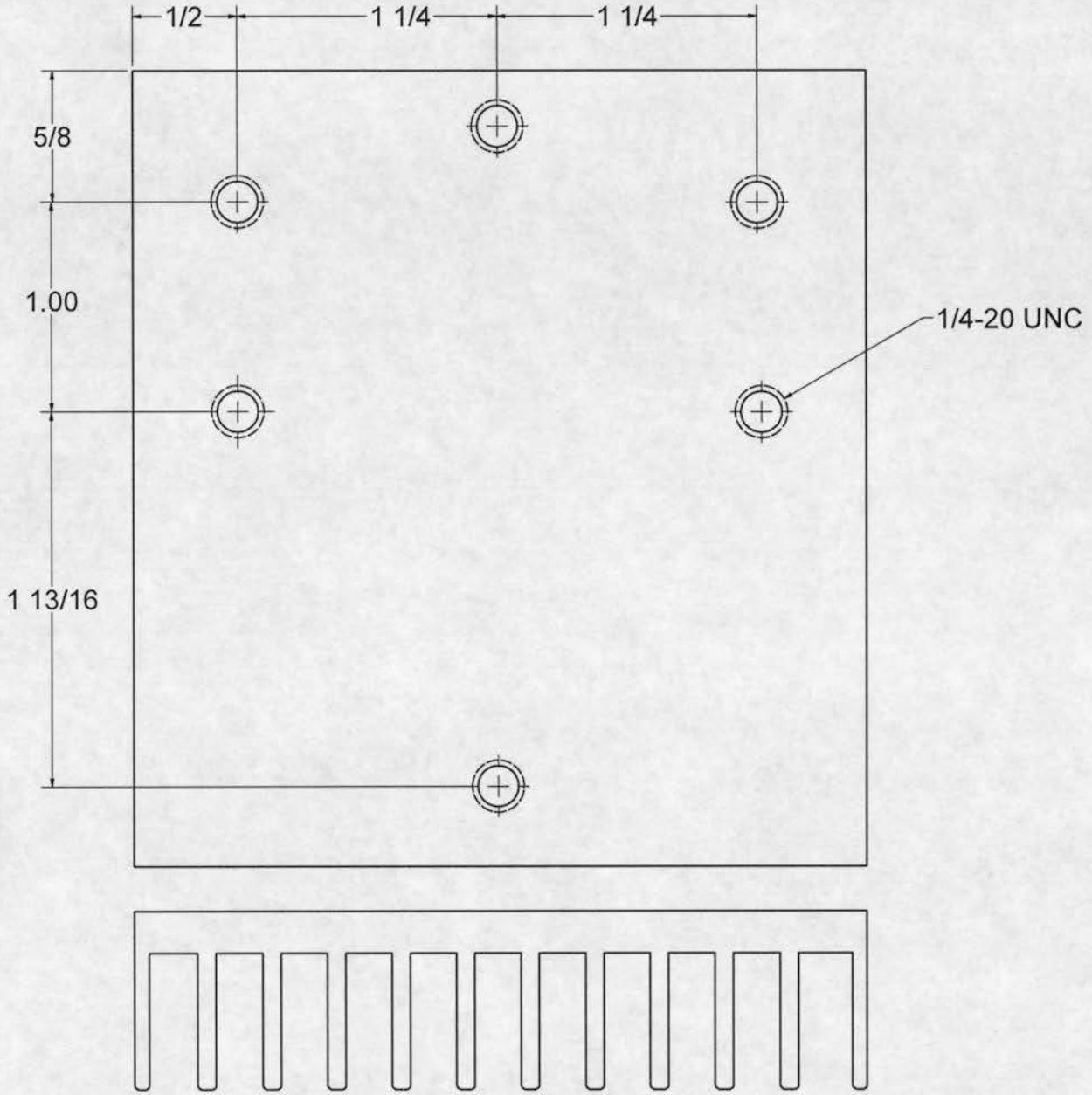
Title: Modular Inverter Front End Shelf Schematic		
Size: A	Document Number: SK0068	Rev: 1
Date: Thursday, January 05, 2006	Sheet 2 of 2	



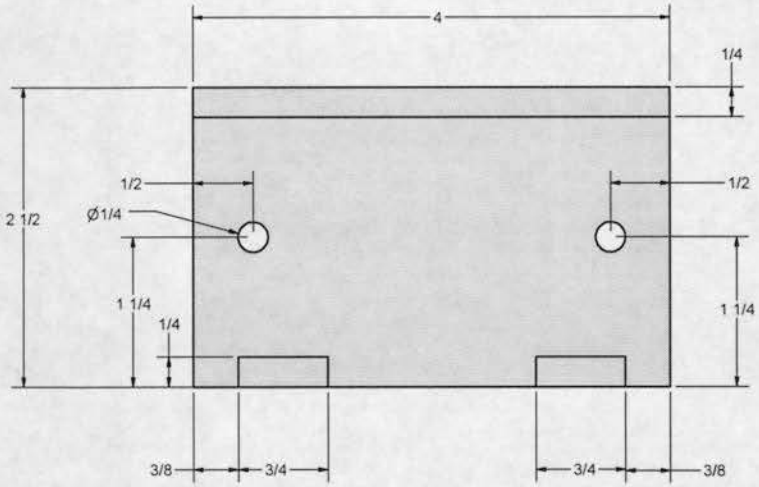


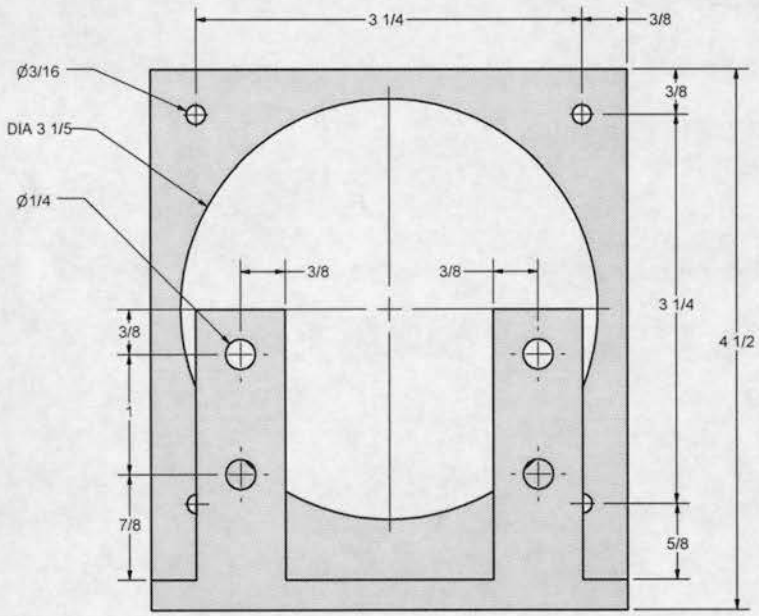


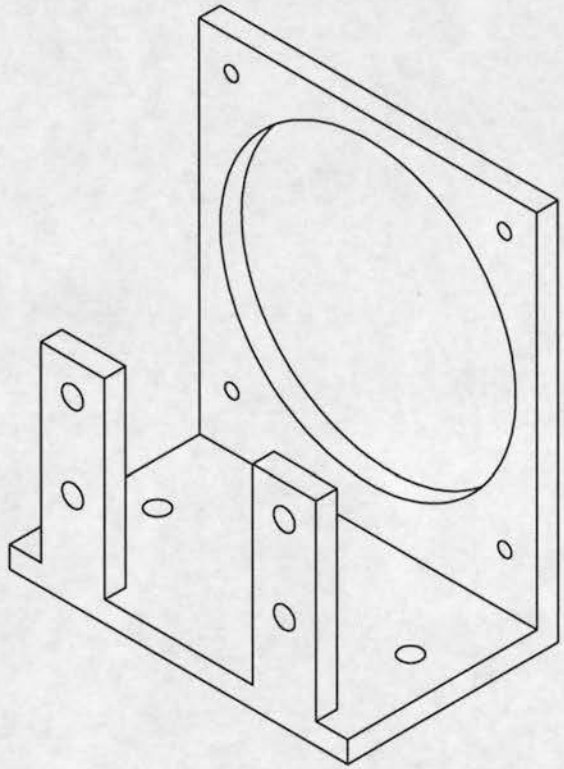
DRAWN W. Weaver	9/2/2004	UIUC	
CHECKED J. Kimball		TITLE	
QA		Eupec BSM 100GB 60 DCL IGBT	
MFG			
APPROVED		SIZE C	DWG NO DR0002_PJ0011_A REV
		SCALE	SHEET 1 OF 1



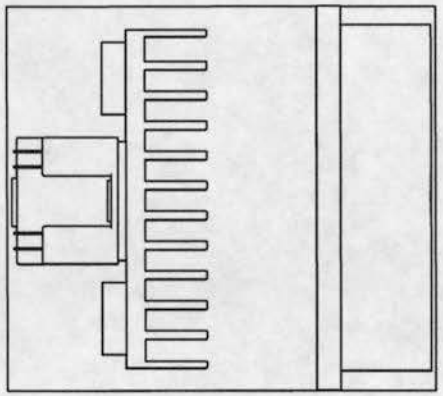
DRAWN W. Weaver	8/30/2004	UIUC
CHECKED J. Kimball		TITLE: Heat Sink Mounting Threaded Hole Layout
QA		
MFG		
APPROVED		
SIZE C	DWG NO DR0019_PJ0011_A	REV
SCALE	SHEET 1 OF 1	

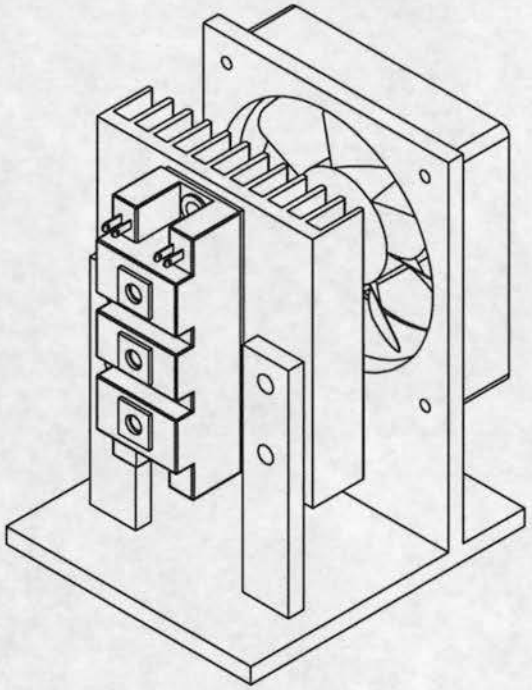


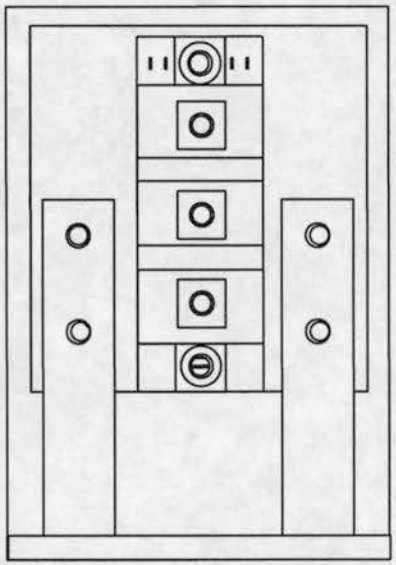


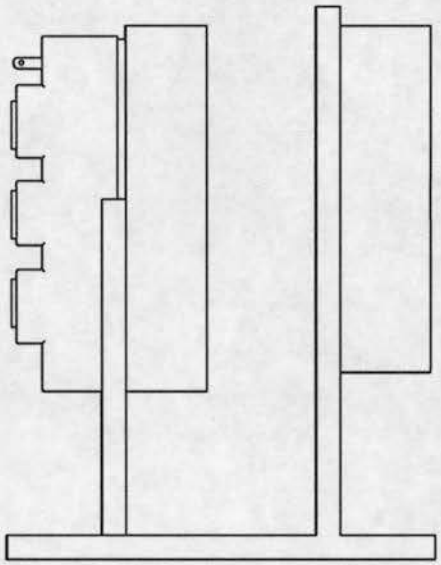


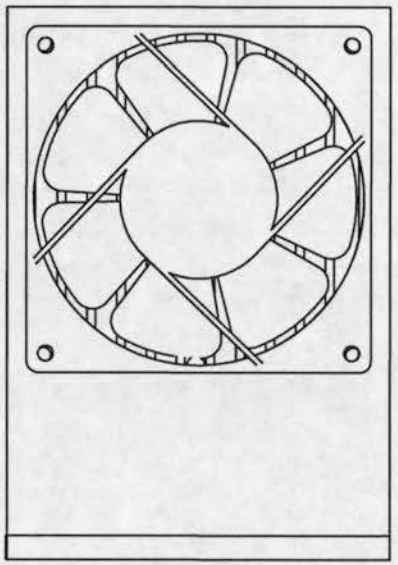
DRAWN W. Weaver	1/10/2005	UIUC	
CHECKED		TITLE	
QA		Heat Sink and Fan Mounting Stand	
MFG			
APPROVED		SIZE C	DWG NO DR0020_PJ0011_B REV
		SCALE	SHEET 1 OF 1



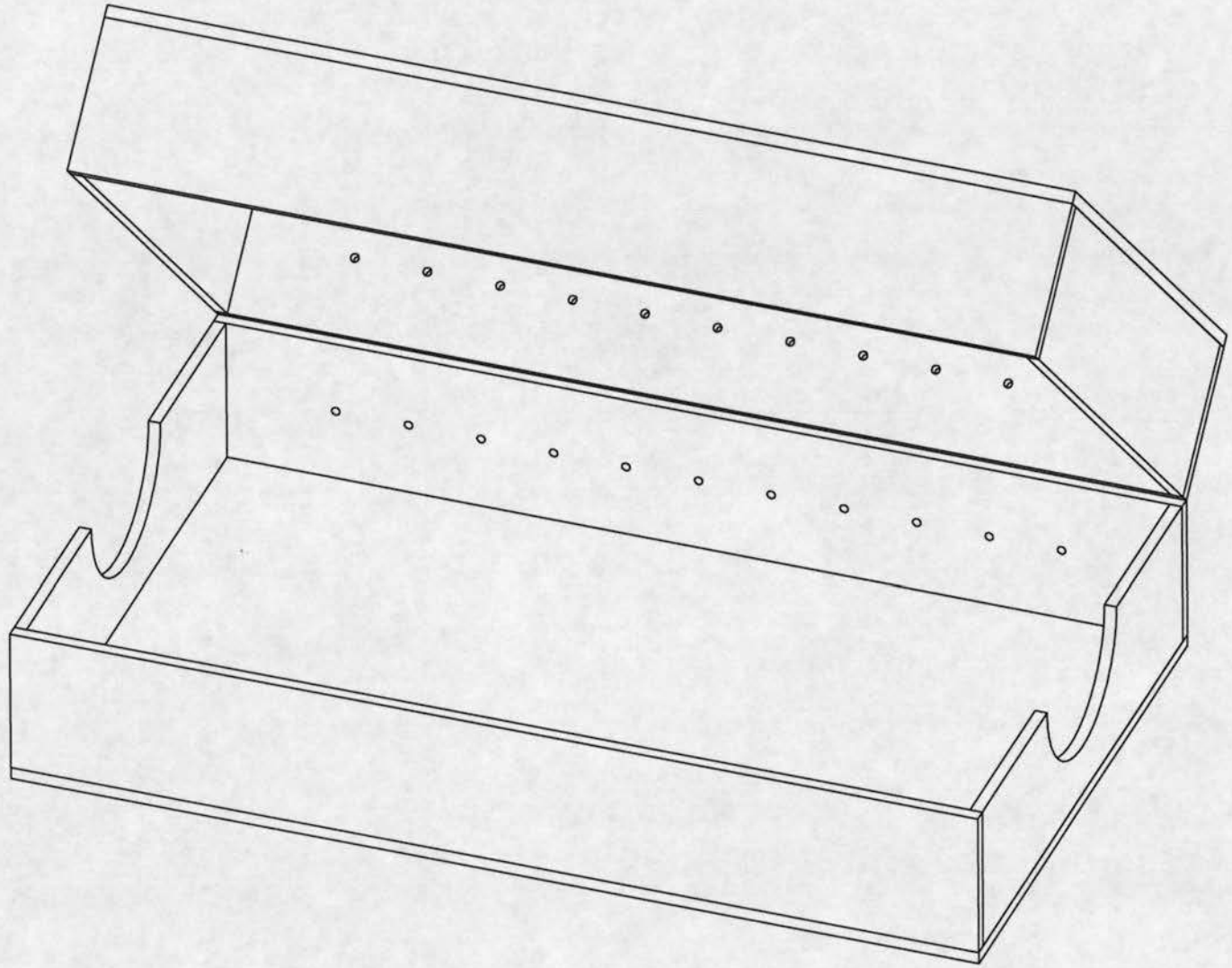




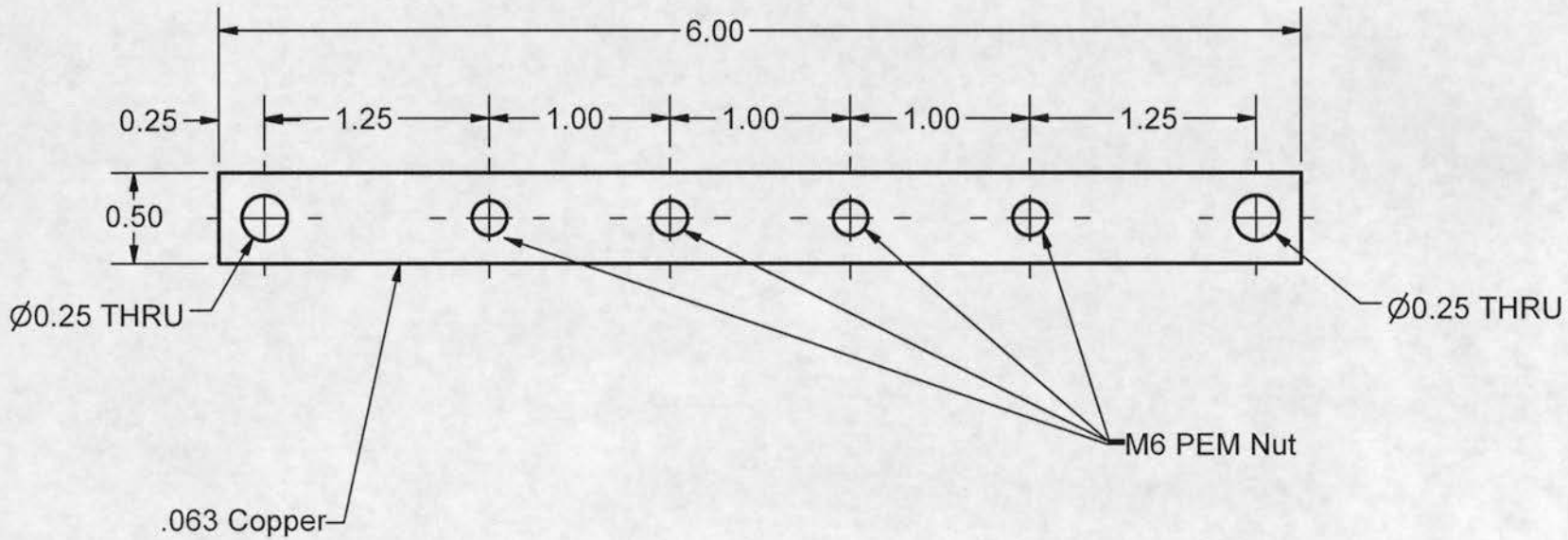




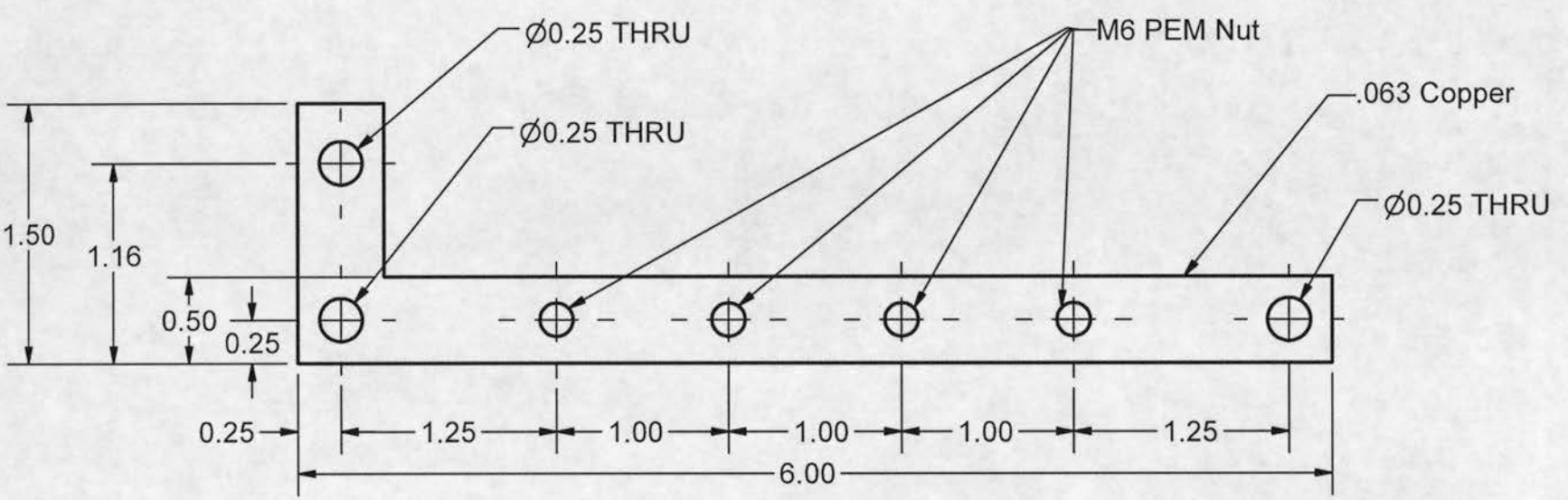
DRAWN W. Weaver	8/31/2004	UIUC	
CHECKED J. Kimball		TITLE	
QA		Heatsink Fan Assembly	
MFG			
APPROVED		SIZE C	DWG NO DR0021_PJ0011_A REV
		SCALE	SHEET 1 OF 1



DRAWN W. Weaver	8/30/2004	UIUC
CHECKED J. Kimball		TITLE
QA		Blast Box Drawing
MFG		
APPROVED		
		SIZE C / DWG NO DR0022_PJ0011_A / REV
		SCALE / SHEET 1 OF 1



DRAWN W. Weaver	8/31/2004	UIUC
CHECKED J. Kimball		TITLE: Straight Bus Bar
QA		
MFG		
APPROVED		
		SIZE A / DWG NO DR0023_PJ0011_A / REV
		SCALE / SHEET 1 OF 1



DRAWN	W. Weaver	8/31/2004
CHECKED	J. Kimball	
QA		
MFG		
APPROVED		

UIUC

TITLE

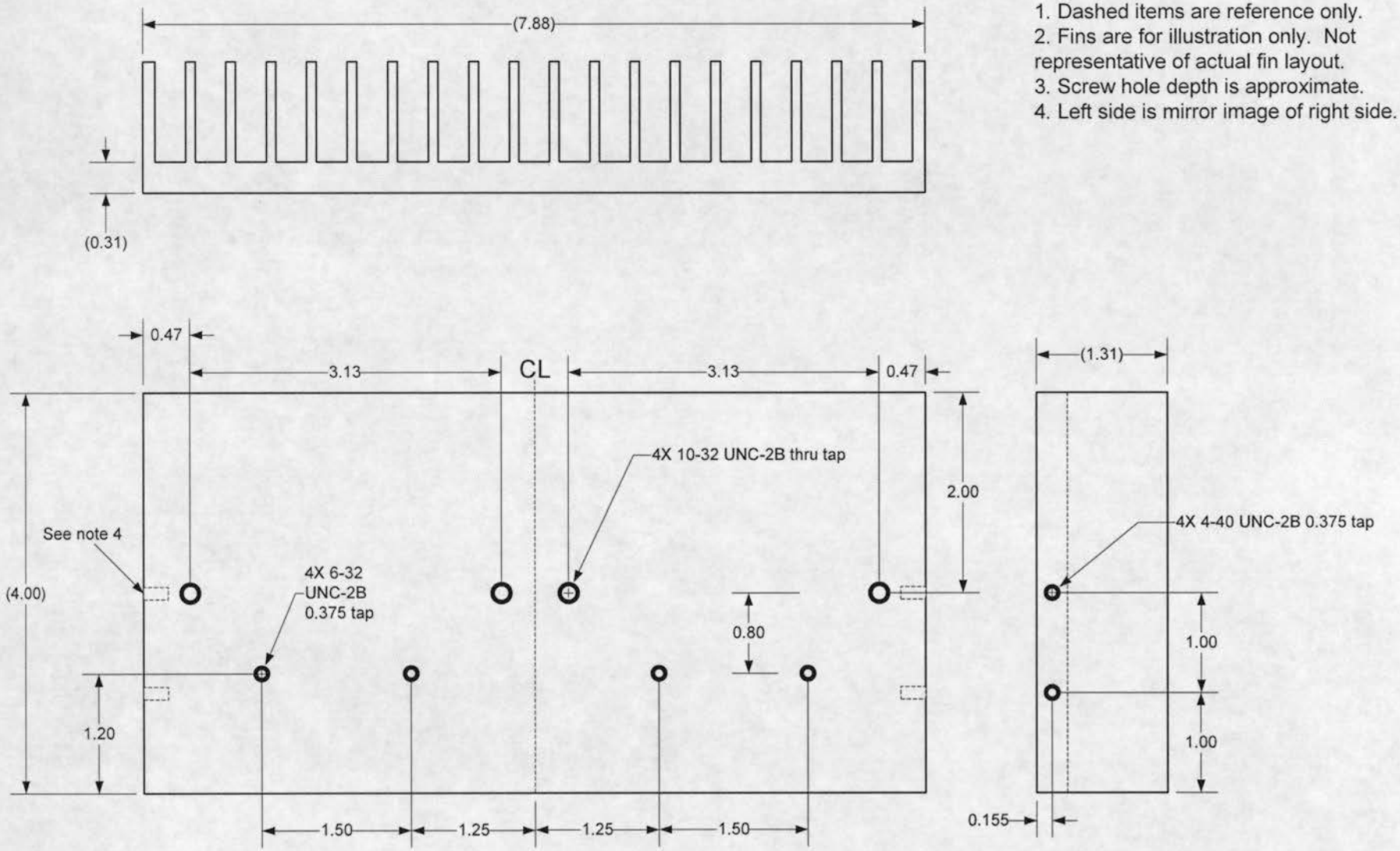
L Bus Bar

SIZE	DWG NO	REV
A	DR0024_PJ0011_A	

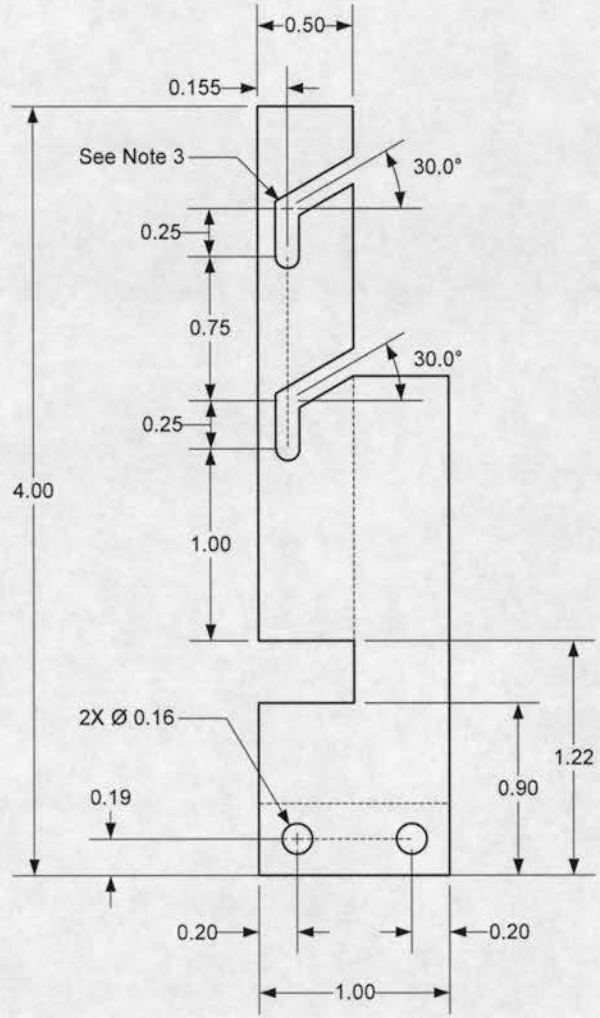
SCALE

SHEET 1 OF 1

Notes
1. Dashed items are reference only.
2. Fins are for illustration only. Not representative of actual fin layout.
3. Screw hole depth is approximate.
4. Left side is mirror image of right side.



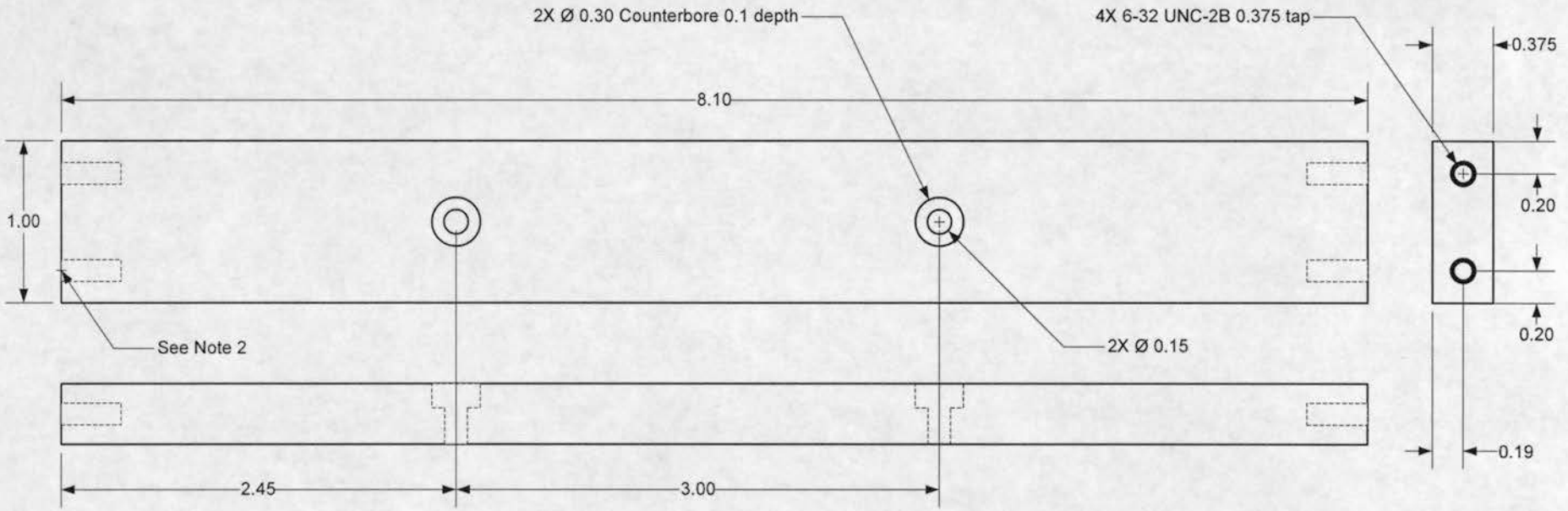
	TITLE: Heatsink for inverter, ThermaFlo E3107Bx4.00"	
DRAWN BY: Z. SORCHINI	SCALE: 1: 1.5	DWG NO: DR0001
CHECKED BY: NONE		REV: A



NOTES
1. Dashed items are reference only.
2. Machine from 3/16" aluminum sheet.
3. The slots should have enough clearance to slide 4-40 screws. Slot bend radii not critical.

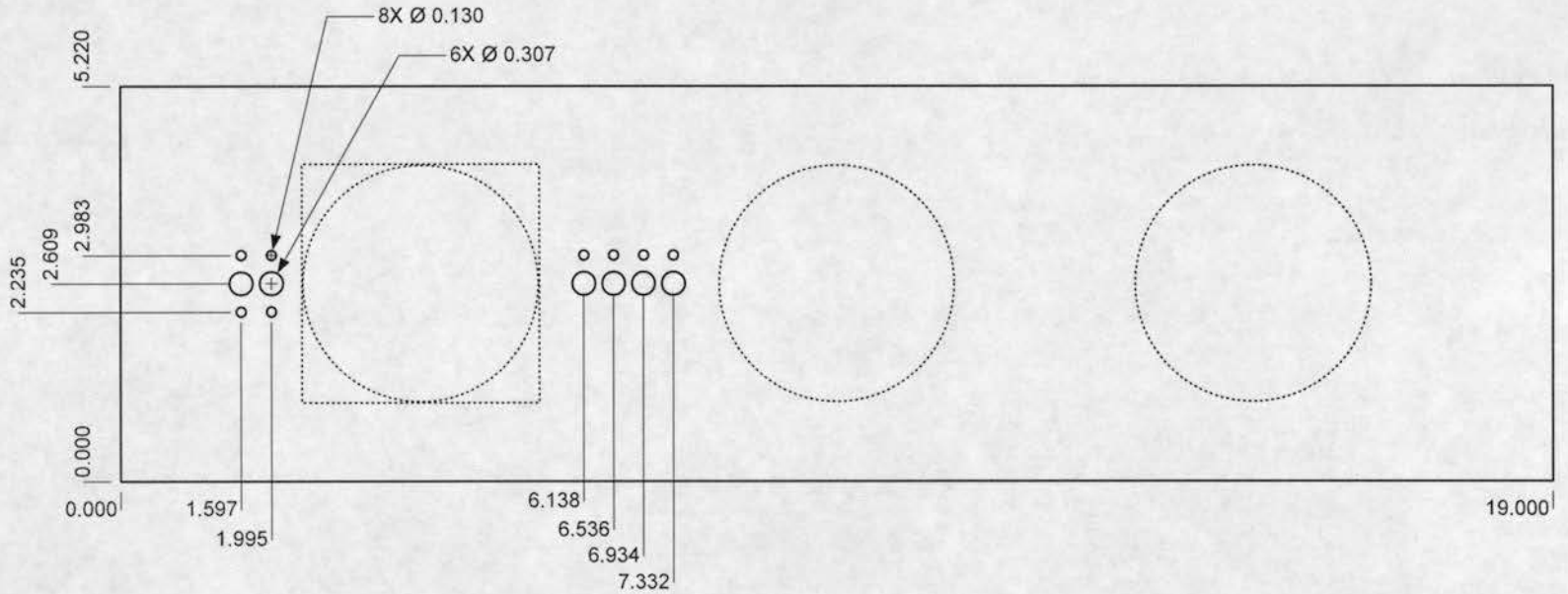
	TITLE: Inverter heatsink mounting post		
DRAWN BY: Z. SORCHINI	SCALE: 1: 1	DWG NO: DR0002	REV: A
CHECKED BY: NONE			

NOTES
1. Dashed items are reference only.
2. Left side is mirror image of right side.
3. Material is aluminum.



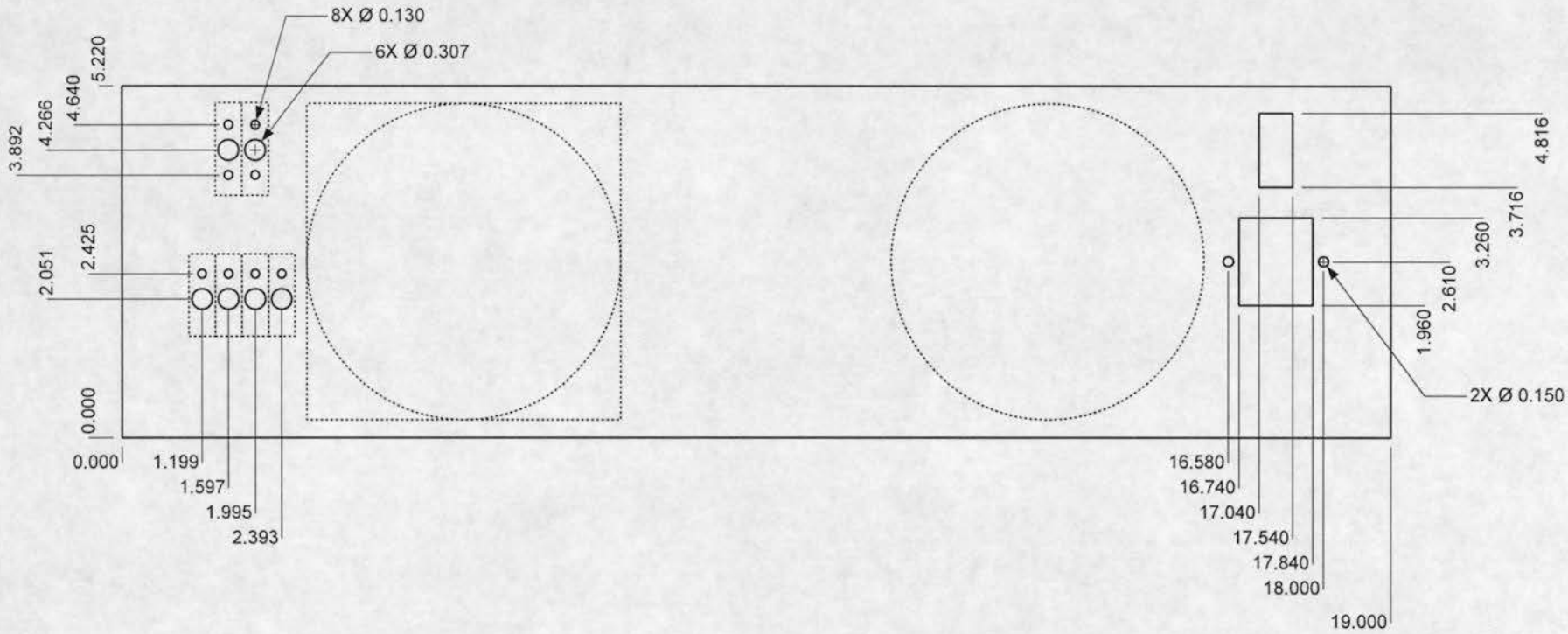
	TITLE: Inverter heatsink mounting post link		
DRAWN BY: Z. SORCHINI	SCALE: 1: 1	DWG NO: DR0003	REV: A
CHECKED BY: NONE			

NOTES
1. Dashed items are reference only
2. Front view



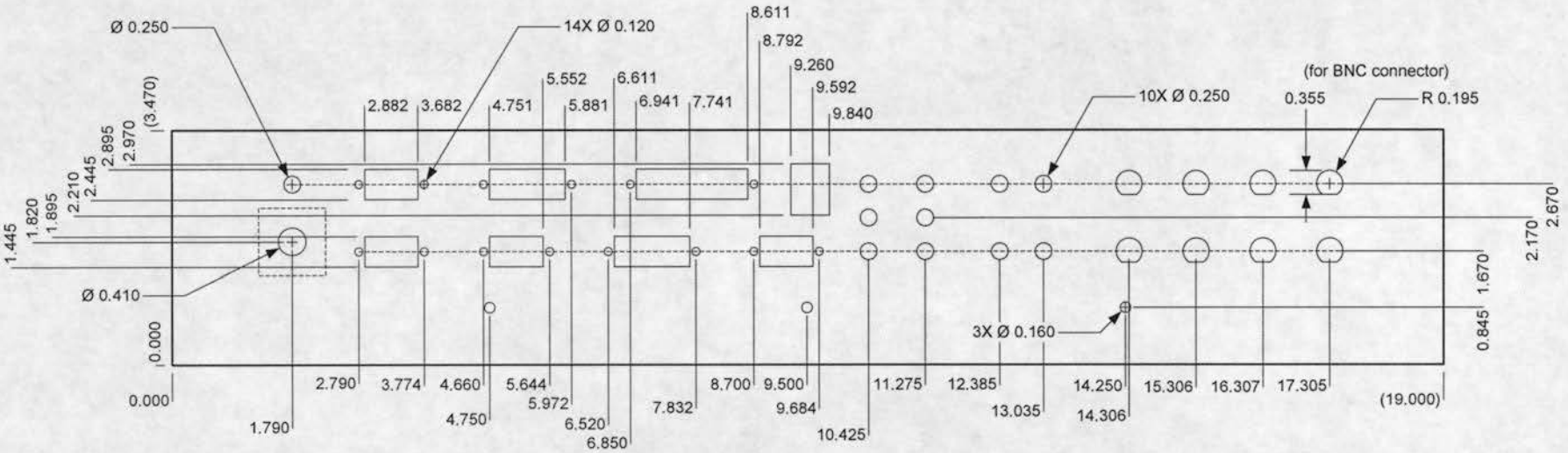
	TITLE: Middle-back panel, Hammond PPFP190803BK1		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2.5	DWG NO: DR0004	REV: A
CHECKED BY: NONE			

NOTES
1. Dashed items are reference only
2. Front view



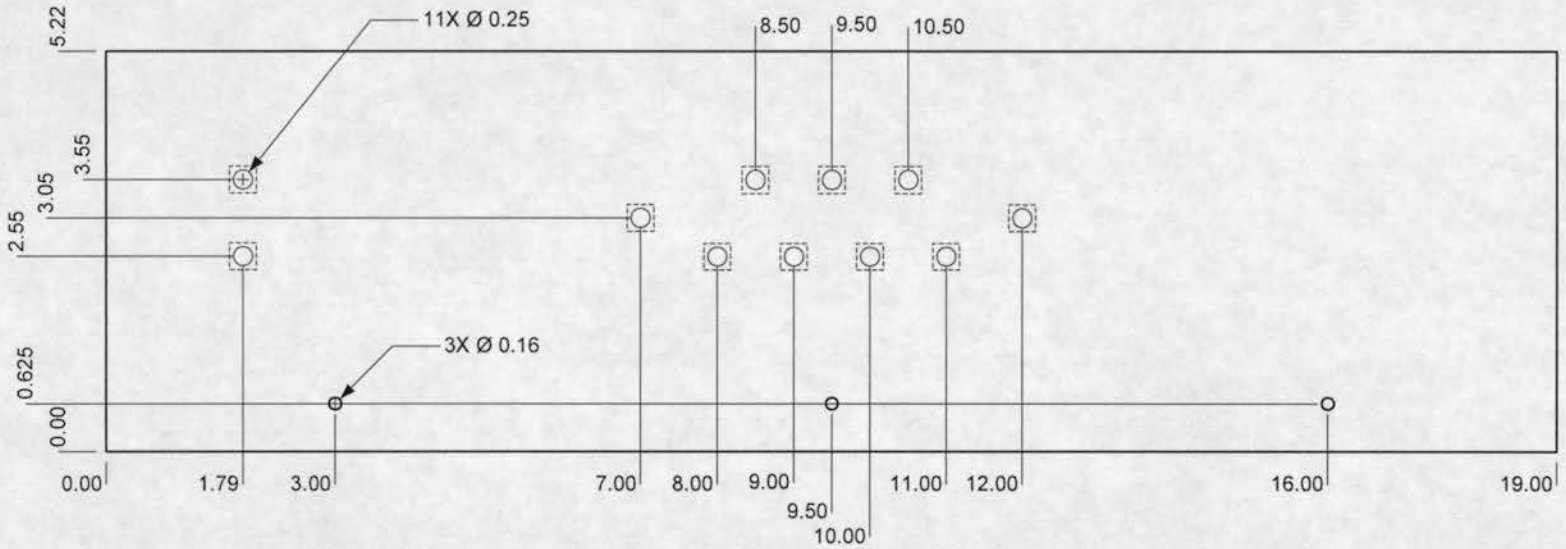
	TITLE: Bottom-back panel, Hammond PPGP191202BK1		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2.5	DWG NO: DR0005	REV: A
CHECKED BY: NONE			

NOTES
1. Dashed items are reference only



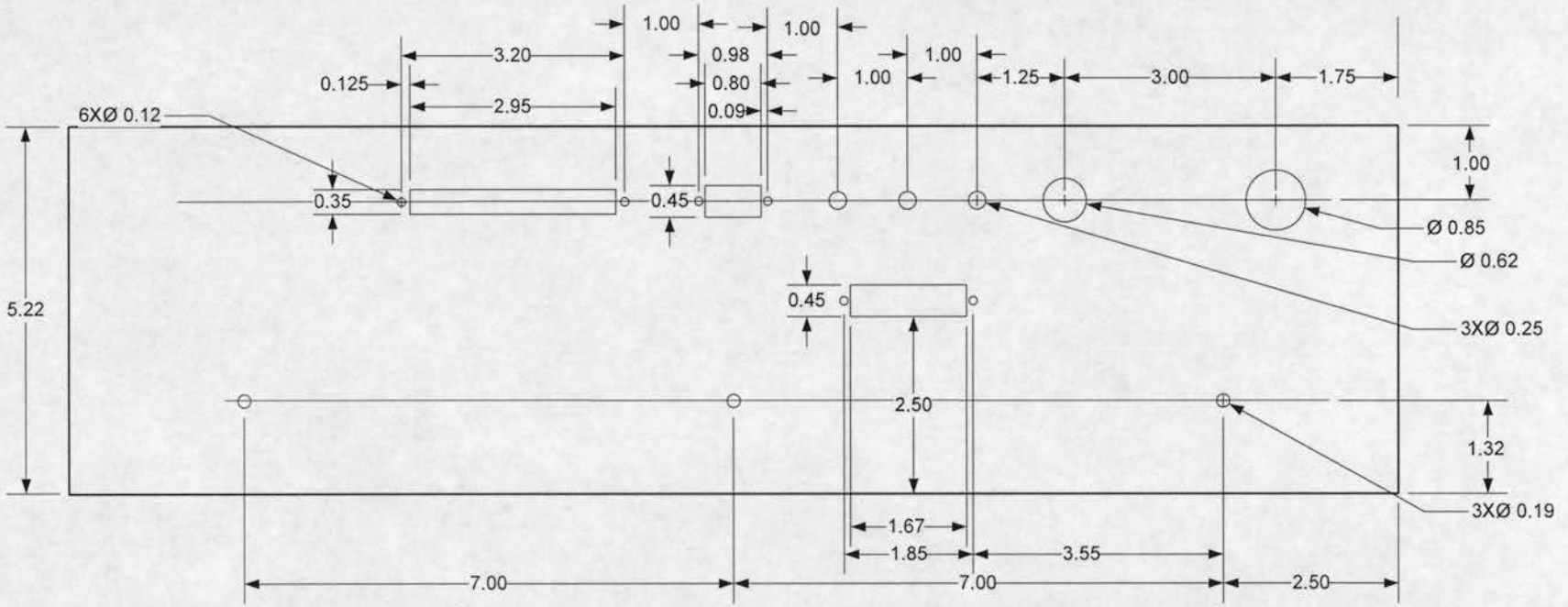
	TITLE: Top-front panel, Hammond PBPS19003BK2		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2.5	DWG NO: DR0006	REV: A
CHECKED BY: NONE			

NOTES
1. Dashed items are reference only

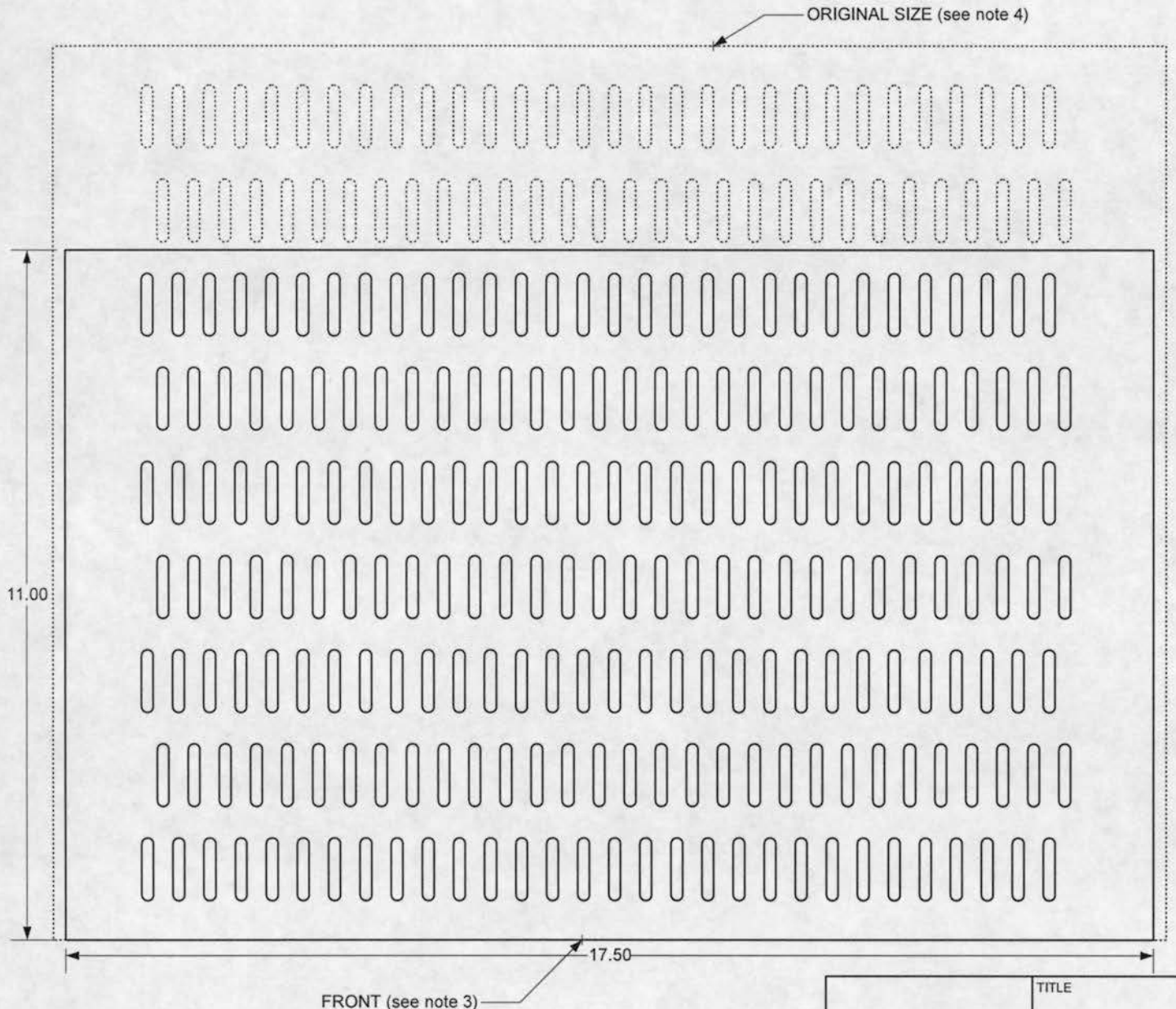


	TITLE		
	Middle-front panel, Hammond PBPS19005BK2		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2.5	DWG NO: DR0007	REV: A
CHECKED BY: NONE			

NOTES
1. Dashed items are reference only

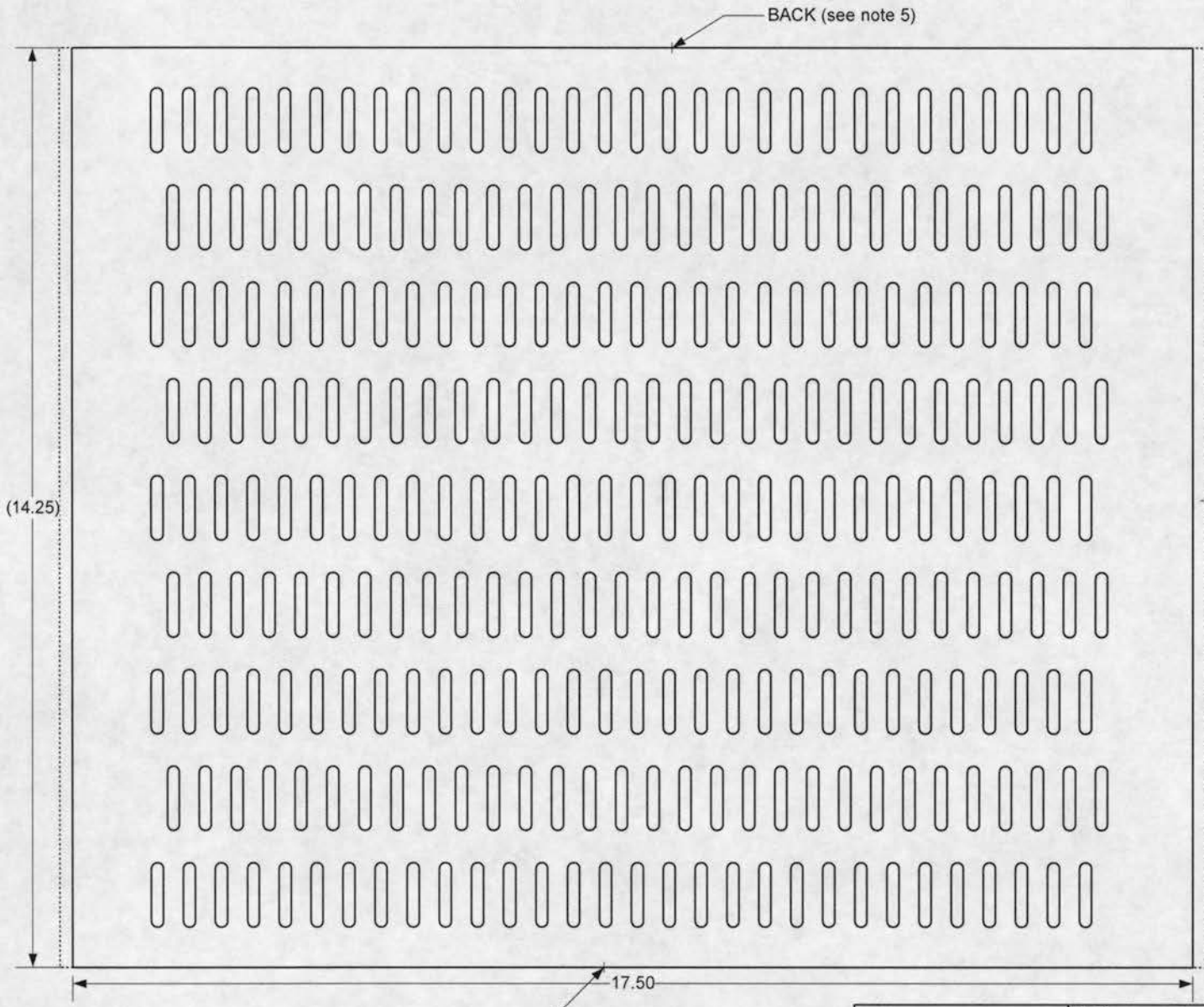


	TITLE: Bottom-front panel, Hammond PBPS19005BK2		
DRAWN BY: Wayne Weaver	SCALE: 1: 2.5	DWG NO: DR0008	REV: A
CHECKED BY: NONE			



Notes
1. Top view. Front and back lip bend downwards.
2. Trim shelf to specified size.
3. Part is not symmetric due to hole distribution.
4. Dashed lines show the unmodified shelf.

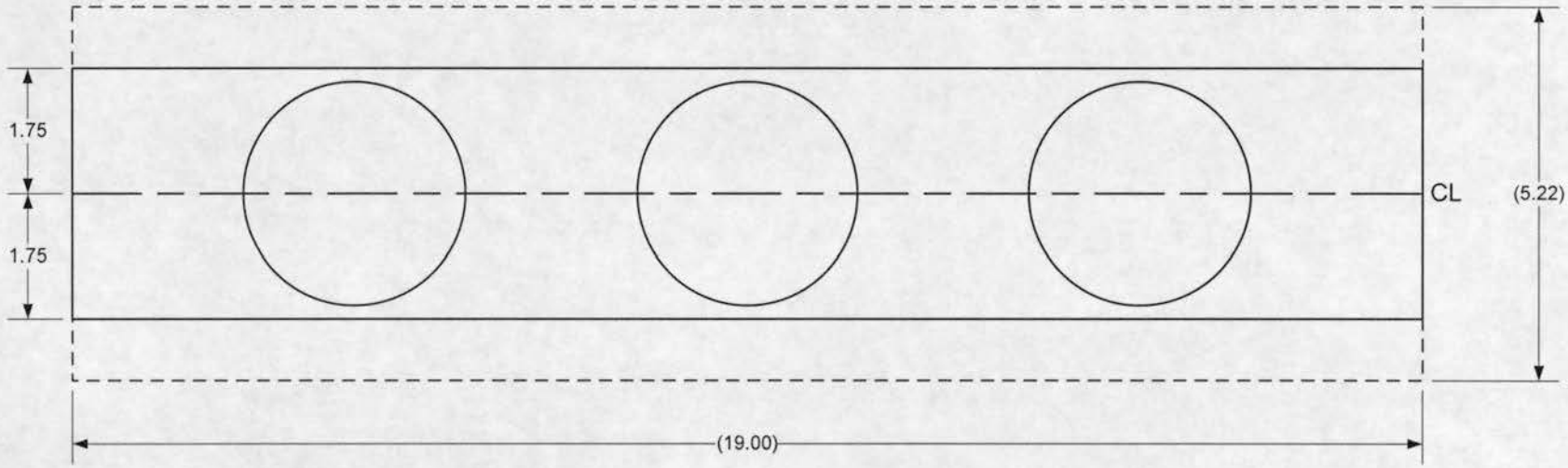
	TITLE: Top shelf, Bud SH-2383		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2.5	DWG NO: DR0009	REV: A
CHECKED BY: NONE			



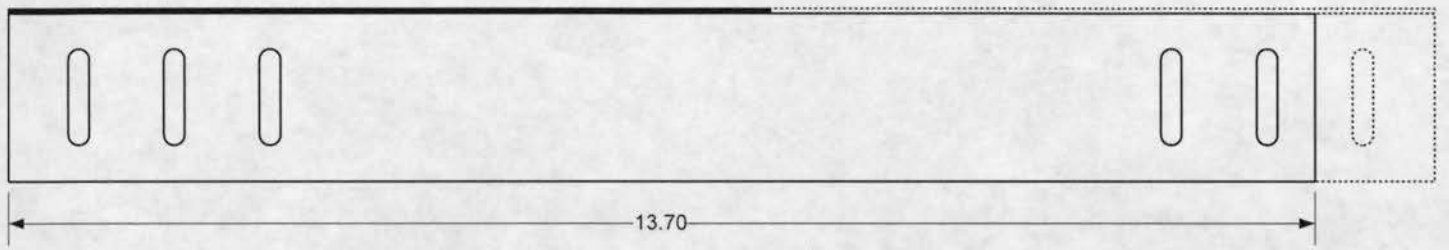
Notes
1. Top view. Front and back lip bend downwards.
2. Trim shelf to specified size.
3. Part is not symmetric due to hole distribution.
4. Dashed lines show the unmodified shelf.
5. Remove back lip.

	TITLE: Middle and bottom shelves, Bud SH-2383		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2.5	DWG NO: DR0010	REV: A
CHECKED BY: NONE			

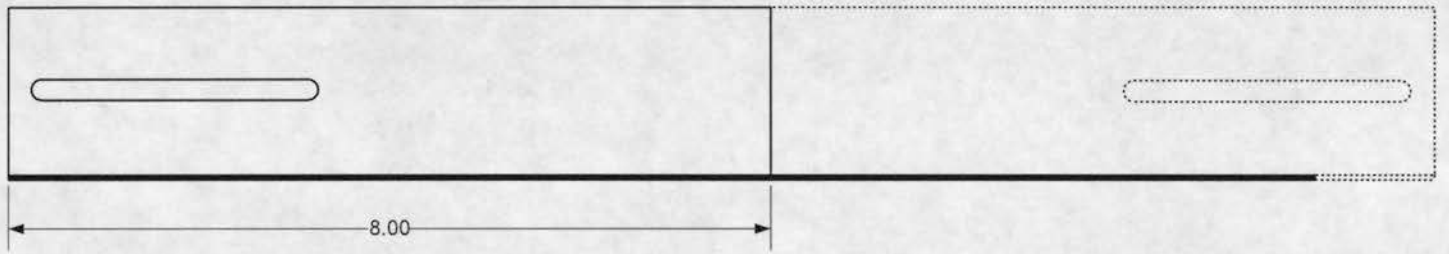
NOTES
1. Trim panel to specified size
2. Dashed lines show unmodified panel

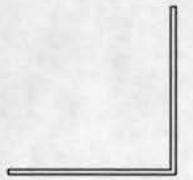


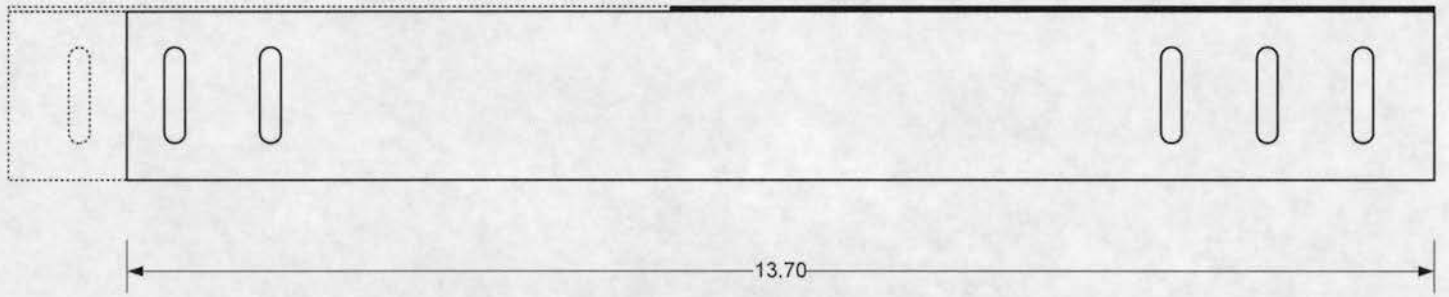
	TITLE: Top-back panel, Hammond PPFP190803BK1		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2.5	DWG NO: DR0011	REV: A
CHECKED BY: NONE			



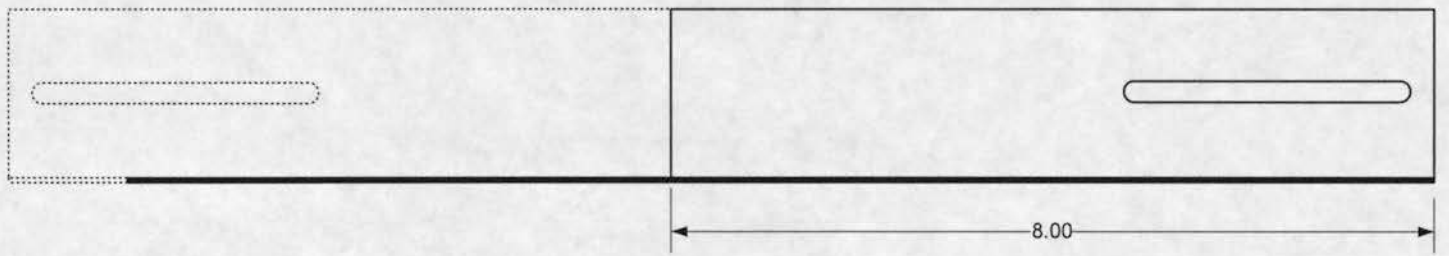
RIGHT BRACKET

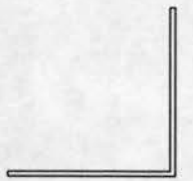






LEFT BRACKET

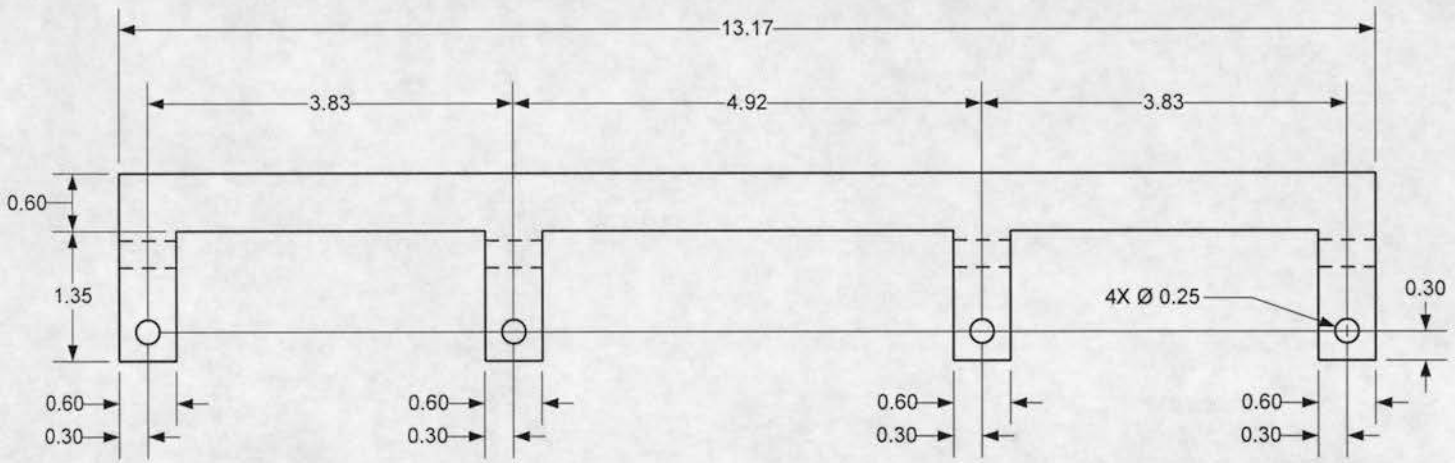


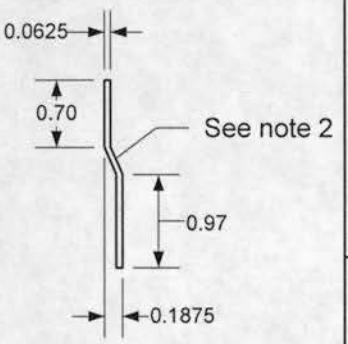


Notes
1. Trim brackets to specified size.
2. Dashed lines show the unmodified bracket.
3. Left bracket is mirror of right bracket.

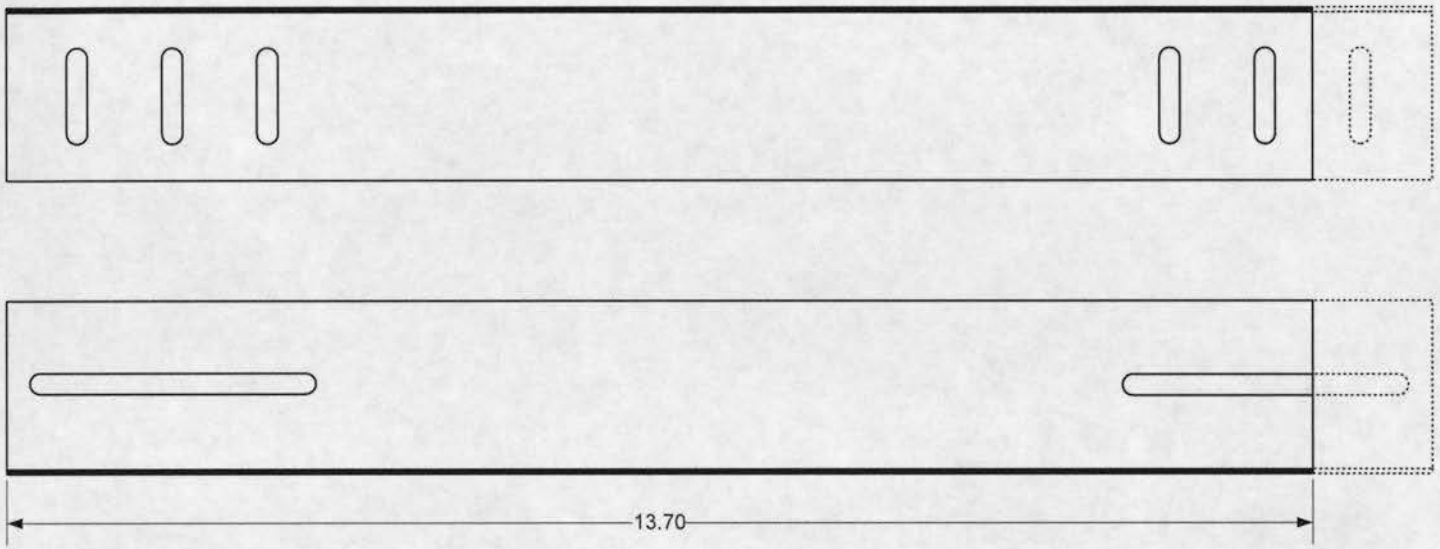
	TITLE: L-brackets for top shelf, Hammond RASA16BK3		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2	DWG NO: DR0012	REV: A
CHECKED BY: NONE			

Notes
1. Material is copper.
2. Bend radii not critical.

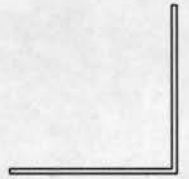


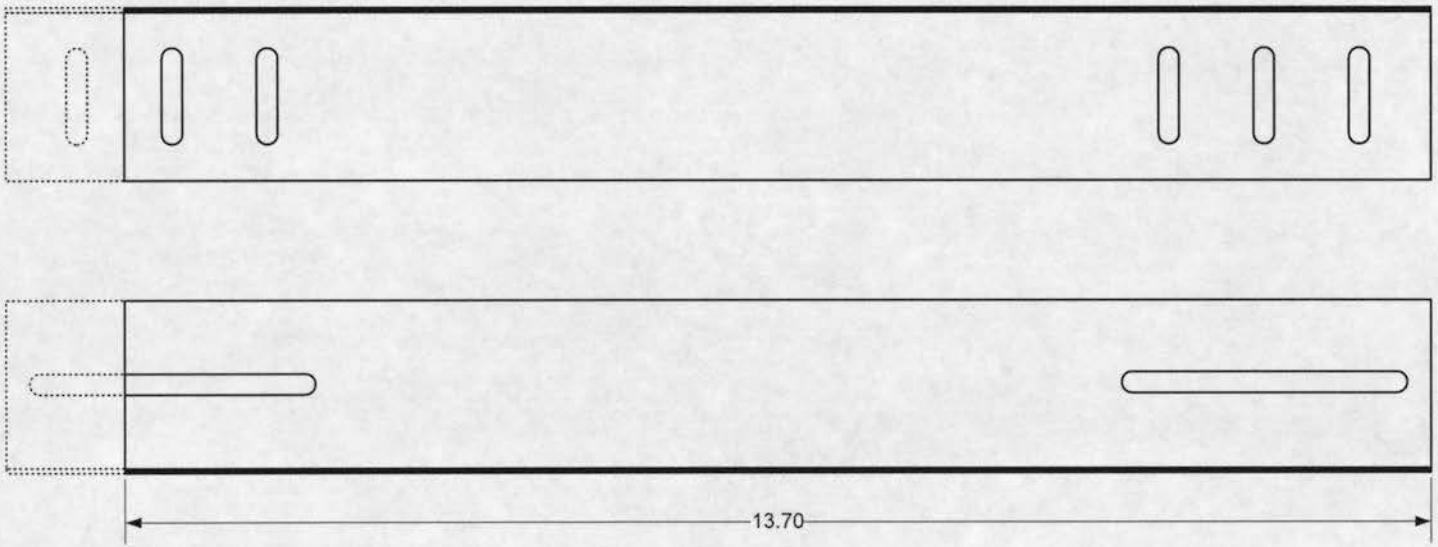


	TITLE: Bus bar for IGBT modules		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2	DWG NO: DR0013	REV: A
CHECKED BY: NONE			

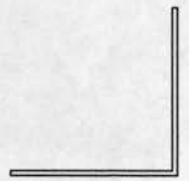


RIGHT BRACKET



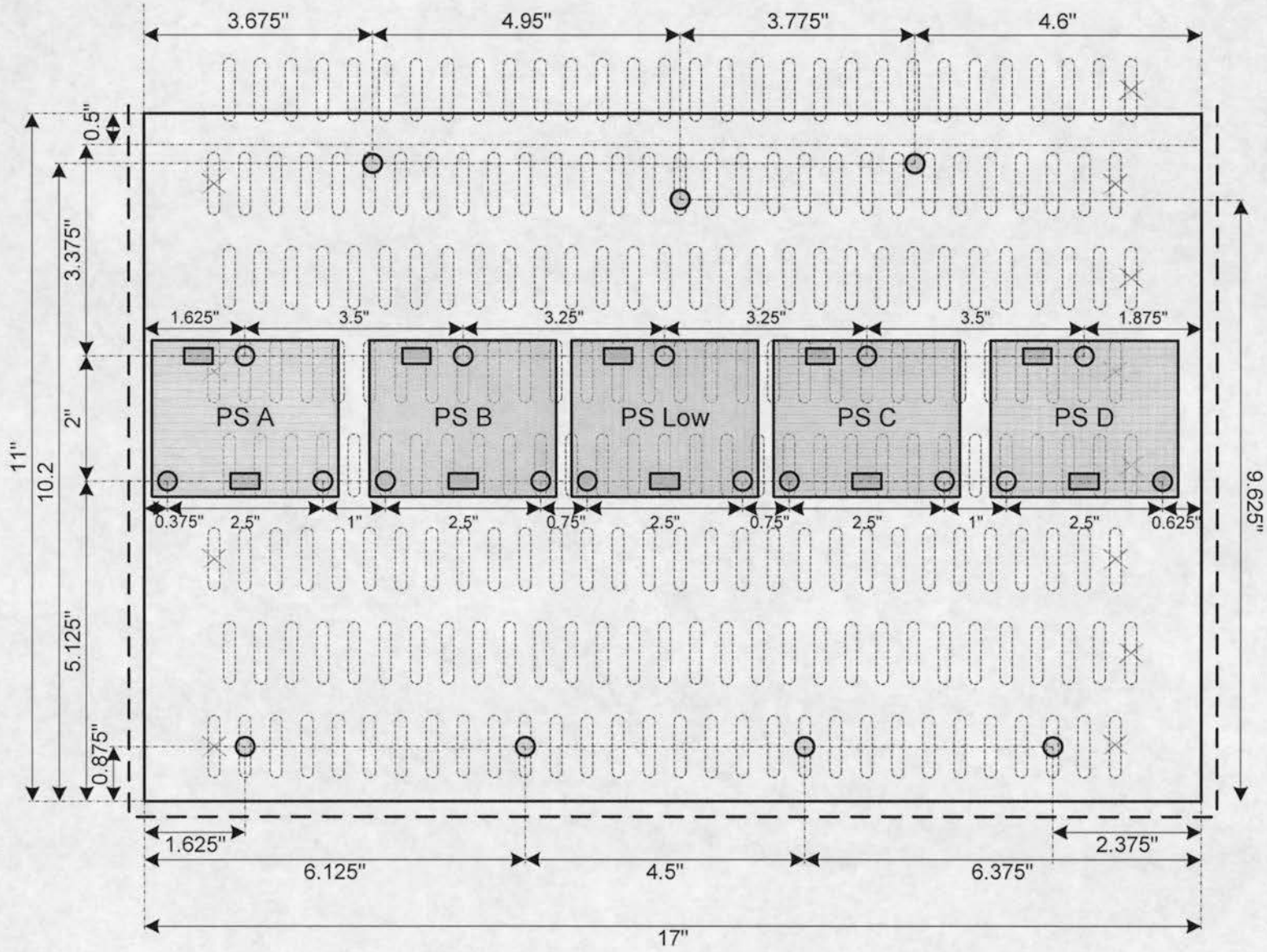


LEFT BRACKET

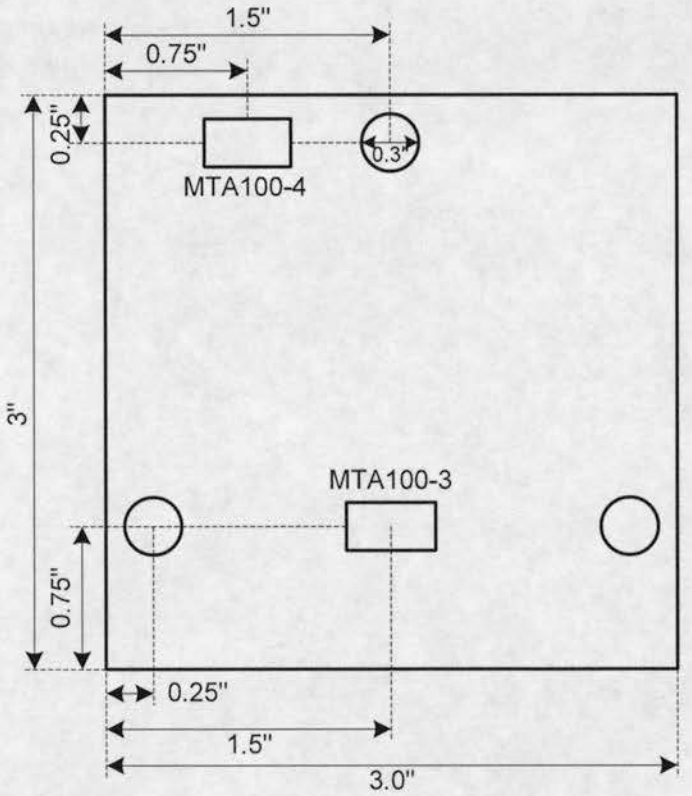


Notes
1. Trim brackets to specified size.
2. Dashed lines show the unmodified bracket.
3. Left bracket is mirror of right bracket.

	TITLE: L-brackets for middle and bottom shelves, Hammond RASA16BK3		
DRAWN BY: Z. SORCHINI	SCALE: 1: 2	DWG NO: DR0014	REV: A
CHECKED BY: NONE			



	TITLE: Mounting holes, Power Stage PCB		
DRAWN BY: M. AMRHEIN	SCALE: 1: 2.5	DWG NO: DR0015	REV: A
CHECKED BY: NONE			



	TITLE: PCB Design of Power Supplies for Power Stage		
DRAWN BY: M. AMRHEIN	SCALE: 1: 1	DWG NO: DR0016	REV: A
CHECKED BY: NONE			